NEW MEXICO OIL CONSERVATION COMMSSION

# MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

| | | | | | |
|---|---|---|---|---|---|
| Type Test: [XX] Initial [ ] Annual [ ] Special | | | | Test Date: 1-6-74 | |
| Company: Northwest Pipeline Corp. | | Connection: New Completion | | | |
| Pool: Blanco | | Formation: Pictured Cliffs | | | Unit: Cox Canyon |
| Completion Date: 12-19-74 | Total Depth: 3689 | Plug Back TD: 3677 | Elevation: 6881 | | Farm or Lease Name: Cox Canyon Unit |
| Csg. Size: 2-7/8 | Wt.: 6.4 | d: 2.441 | Set At: 3686 | Perforations: From 3576 To 3616 | Well No.: 17 |
| Tbg. Size: T-C | Wt.: | d: | Set At: | Perforations: From To | Unit: M Sec.: 16 Twp.: 32 Rge.: 11 |
| Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Gas - Single tubingless completion | | | Packer Set At: none | | County: San Juan |
| Producing Thru: casing | Reservoir Temp. °F: @ | Mean Annual Temp. °F: | Baro. Press. – $P_a$: 12.0 | | State: New Mexico |

| L | H | Gg | % $CO_2$ | % $N_2$ | % $H_2S$ | Prover | Meter Run | Taps |
|---|---|---|---|---|---|---|---|---|
| | | .635 | | – | – | 3/4" THC | – | – |

| FLOW DATA | | | | | TUBING DATA | | CASING DATA | | Duration of Flow |
|---|---|---|---|---|---|---|---|---|---|
| NO. | Prover Line Size x Orifice Size | Press. p.s.i.g. | Diff. $h_w$ | Temp. °F | Press. p.s.i.g. | Temp. °F | Press. p.s.i.g. | Temp. °F | |
| SI | | | | | | | 860 | | 7 day SI |
| 1. | 2 x .750 | | | | | | 81 | 51° | 3 hours |
| 2. | | | | | | | | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

## RATE OF FLOW CALCULATIONS

| NO. | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ | Pressure $P_m$ | Flow Temp. Factor Ft. | Gravity Factor Fg | Super Compress. Factor, Fpv | Rate of Flow Q, Mcfd |
|---|---|---|---|---|---|---|---|
| 1 | 12.365 | | 93 | 1.0088 | .9721 | 1.008 | 1,137 |
| 2. | | | | | | | |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

| NO. | $P_t$ | Temp. °R | $T_r$ | Z |
|---|---|---|---|---|
| 1. | | | | |
| 2. | | | | |
| 3. | | | | |
| 4. | | | | |
| 5. | | | | |

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

$P_c$ 872 $P_c^2$ _____

| NO | $P_t^2$ | $P_w$ | $P_w^2$ | $P_c^2 - P_w^2$ |
|---|---|---|---|---|
| 1 | | | | |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{760,384}{745,743}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0166$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1156$

Absolute Open Flow 1156 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .85

Remarks: Calculated $P_W$ 121 psia
Blew dry gas throughout

RECEIVED JAN 14 1975 OIL CON. COM. DIST. 3

| Approved By Commission: | Conducted By: | Calculated By: | Checked By: |
|---|---|---|---|
| | Ross Lankford | Ross Lankford | |