NEW MEXICO OIL CONSERVATION COMMSSION

# MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

| | | | | |
|---|---|---|---|---|
| Type Test: [X] Initial [ ] Annual [ ] Special | | | Test Date: 10-11-77 | |
| Company: Northwest Pipeline Corp. | Connection: New Completion | | | |
| Pool: Blanco | Formation: Pictured Cliffs | | | Unit: Cox Canyon |
| Completion Date: 9-23-77 | Total Depth: 3408 | Plug Back TD: 3398 | Elevation: 6654 GR | Farm or Lease Name: Cox Canyon Unit |
| Csg. Size: 2.875 / Wt.: 6.4 / d: 2.441 / Set At: 3402 | | Perforations: From 3298 To 3322 | | Well No.: Com. #23 |
| Tbg. Size: None / Wt. / d / Set At | | Perforations: From To | | Unit: C / Sec.: 17 / Twp.: 32 / Rge.: 11 |
| Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Gas - Tubingless Completion | | Packer Set At: None | | County: San Juan |
| Producing Thru: Casing | Reservoir Temp. °F: @ | Mean Annual Temp. °F | Baro. Press. – $P_a$: 12.0 | State: New Mexico |

| L | H | Gg | % $CO_2$ | % $N_2$ | % $H_2S$ | Prover | Meter Run | Taps |
|---|---|---|---|---|---|---|---|---|
| | | .665 | | | | Positive Choke | | |

| | FLOW DATA | | | | TUBING DATA | | CASING DATA | | |
|---|---|---|---|---|---|---|---|---|---|
| NO. | Prover Line Size X Orifice Size | Press. p.s.i.g. | Diff. $h_w$ | Temp. °F | Press. p.s.i.g. | Temp. °F | Press. p.s.i.g. | Temp. °F | Duration of Flow |
| SI | 11 day SIP | | | | | | 1014 | | SIP |
| 1. | 2 X .750 | 192 | | 59° | | | 192 | | 3 hrs. |
| 2. | | | | | | | | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

## RATE OF FLOW CALCULATIONS

| NO. | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ | Pressure $P_m$ | Flow Temp. Factor Ft. | Gravity Factor Fg | Super Compress. Factor, Fpv | Rate of Flow Q, Mcfd |
|---|---|---|---|---|---|---|---|
| 1 | 9.402 | | 204 | 1.001 | 1.226 | 1.020 | 2401 |
| 2. | | | | | | | |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

| NO. | $P_t$ | Temp. °R | $T_r$ | Z |
|---|---|---|---|---|
| 1. | | | | |
| 2. | | | | |
| 3. | | | | |
| 4. | | | | |
| 5. | | | | |

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

$P_c$ 1026 $P_c^2$ 1052676

| NO | $P_t^2$ | $P_w$ | $P_w^2$ | $P_c^2 - P_w^2$ |
|---|---|---|---|---|
| 1 | | 260 | 67600 | 985076 |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0686$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0580$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2540$

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Absolute Open Flow 2540 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .85

Remarks: Well produced very light mist of water with a trace of condensate.

| Gl | 1-e-s | $Fc0^2$ | $R^2$ | $Pt^2$ | $Pt^2 + R^2$ | Calc. PW |
|---|---|---|---|---|---|---|
| 2193 | 147 | 177634 | 26112 | 41616 | 67728 | 260 |

| Approved By Commission: | Conducted By: | Calculated By: | Checked By: |
|---|---|---|---|
| | Wilfred Charley | B.J. Broughton | |