

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-28-80			
Company Southland Royalty Company				Connection Northwest Pipeline Corporation					
Pool South Los Pinos Fruitland				Formation Pictured Cliffs				Unit	
Completion Date 10-28-80		Total Depth 6158'		Plug Back TD 6010'		Elevation 6548' GR		Farm or Lease Name Burnt Mesa	
Gas Str. 7.000 4.500	Wt. 20# 10.5#	d 6.456 4.052	Set At 3715' 3545'-6158'	Perforations: From To		Well No. #1A			
Tub. Size 1.900	Wt. 2.90#	d 1.610	Set At 3543'	Perforations: From 3370' To 3568'		Unit Sec. Twp. Rge. J 25 32N 7W			
Type Well - Single - Bradenhead - G.C. or G.O. Multiple GG-Multiple						Packer Set At 3629'		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F p		Mean Annual Temp. °F		Baro. Press. - P _a 12.2		State New Mexico	
L	H	Gg .700	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1158		1168		
1.	2" X 3/4"						101		659		1 Hour
2.							45		560		2 Hours
3.							36		539		3 Hours
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		48.2	1.0000	.9258	1.0000	552
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.										
2.										
3.										
4.										
5.										

$P_c = 1180.2$ $P_c^2 = 1392872.0$					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.2790$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2326$	
NO	P _t ²	P _w	P _w ²	P _c ² - P _w ²				
1		551.2	303821.4	1089050.6				
2								
3								
4								
5								

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 680$					
Absolute Open Flow 680		Mcfd @ 15.025		Angle of Slope θ	Slope, n .85

Remarks:			
Approved By Division		Conducted By: Don Thompson	Calculated By: James Smith
		Checked By: L. O. Van Ryan	