

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special						Test Date 4/17/78			
Company Robert C. Anderson				Connection New Well					
Pool Straight Canyon				Formation Dakota				Unit	
Completion Date 12/7/77		Total Depth 2325		Plug Back TD		Elevation 5676		Farm or Lease Name Ute Mountain Ute	
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 2325	Perforations: From 2258 To 2268				Well No. #4	
Tbg. Size	Wt.	d	Set At	Perforations: From To				Unit Sec. Twp. Rye. J 14 31 16	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Gas - Single						Packer Set At None		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12.0		State New Mexico	
L	H	Gg .60	% CO ₂	% N ₂	% H ₂ S	Prover 2"	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							781		781		SIP
1.	2"	x	1/8"	759		52°	762		764		2 hr.
2.	2"	x	3/16"	735		60°	737		738		2 hr.
3.	2"	x	5/16"	469		65°	480		659		2 hr.
4.	2"	x	3/8"	384		65°	400		626		2 hr.
5.	2"	x	3/8"	327		72°	344		578		12 hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	0.2648		771	1.008	1.291	1.083	288
2	0.6082		747	1.000	1.291	1.073	629
3	1.672		481	.995	1.291	1.043	1078
4	2.378		396	.995	1.291	1.034	1251
5	2.378		339	.989	1.291	1.028	1058

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
2.					Specific Gravity Separator Gas _____ X X X X X X X X			
3.					Specific Gravity Flowing Fluid _____ X X X X X			
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.			
5.					Critical Temperature _____ R _____ R			

P _c 793	P _c ² 628849		
NO.	P _t ²	P _w	P _w ²
1		776	602176
2		750	562500
3		671	450241
4		638	407044
5		590	348100

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____	
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____			

Absolute Open Flow 1800	Mcf/d @ 15.025	Angle of Slope @ 34°	Slope, n .67
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Remarks:			
Approved By Commission:	Conducted By: Fred S. Hamrick	Calculated By: Fred S. Hamrick	Checked By: B.J. Broughton