STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 11-10-80	
Company: Southland Royalty Company		Connection: Northwest Pipeline Corporation			
Pool: Basin		Formation: Dakota		Unit	
Completion Date: 9-28-80	Total Depth: 8700'	Plug Back TD: 8696'	Elevation: 6999' GR	Farm or Lease Name: Reese Mesa	
Csg. Size: 7.000 / 4.500	Wt.: 20 & 23# / 10.5 & 11.6	d: 6.366 / 4.052	Set At: 6652' / 8698'	Perforations: From ____ To ____	Well No.: #6
Tbg. Size: 2.375	Wt.: 4.7#	d: 1.995	Set At: 8670'	Perforations: From 8512' To 8678'	Unit: J; Sec.: 10; Twp.: 32N; Rge.: 8W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: GG-Multiple			Packer Set At: 6575'		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. – P_a: 12.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
		.700						

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					2725				
1.	2" X 3/4"				134				1 Hour
2.					94				2 Hours
3.					73				3 Hours
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		85.2	1.0000	.9258	1.000	975
2.							
3.							
4.							
5.							

NO.	P_r	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/Bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid _____ XXXXXXXXXX
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 2737.2 P_c^2 7492263.8

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		85.2	7259.0	7485004.8
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0010$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0007$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 976$

RECEIVED
DEC 8 1980
OIL CON. COM.
DIST. 3

Absolute Open Flow _____ Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Don Thompson	James Smith	L. O. Van Ryan