NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 11-06-79	
Company: Southland Royalty Company		Connection: Southern Union Gathering			
Pool: Undesignated Gallup		Formation: Gallup		Unit	
Completion Date: 10-30-79	Total Depth: 7704'	Plug Back TD: 7626'	Elevation: 6375' GR	Farm or Lease Name: Dusenberry	
Csg. Size: 7.625 / 5.500 — Wt.: 26.40# / 15.5&17# — d: 6.969 / 4.950 — Set At: 5134' / 4910-7658 — Perforations: From 6818' To 6871'				Well No.: 3-E	
Tbg. Size: 1.900 — Wt.: 2.76# — d: 1.610 — Set At: 6699' — Perforations: From --- To ---				Unit: H — Sec.: 1 — Twp.: 31N — Rge.: 12W	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: G. G. Multiple			Packer Set At: 6968'	County: San Juan	
Producing Thru: Tbg	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. – P_a: 12.2	State: New Mexico	
L	H	Gg: .700	% CO_2	% N_2	% H_2S — Prover — Meter Run — Taps

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							1107		1178		
1.	2"	X	3/4"				0		1158		3hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		12.2	1.0000	.9258	1.0000	140
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1190.2 P_c^2 1,416,576

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1170.2	1,369,368	47,208
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 30.0071$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 12.8209$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1795$

NOV 19 '79
OIL CON. COM.

Absolute Open Flow 1795 Mcfd @ 15.025 — Angle of Slope θ _____ — Slope, n .75

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Dick Irvin	James Smith	