

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 7-80																																																																																														
Company Southland Royalty Company				Connection Southern Union																																																																																															
Pool Basin				Formation Dakota																																																																																															
Completion Date 12-31-79		Total Depth 7340'		Plug Back TD 7295'																																																																																															
		Elevation 6087'		Farm or Lease Name Grenier																																																																																															
Csg. Size 7.625 5.500	Wt. 26# 15.5#	d 6.969 4.892	Set At 4819' 4663'-7304'	Perforations: From 7075' To 7264'																																																																																															
Thg. Size 2.875	Wt. 4.7#	d 2.441	Set At 7242'	Perforations: From To																																																																																															
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At 4700'																																																																																															
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F 12.2																																																																																															
L		H	Gg .700	% CO ₂	% N ₂																																																																																														
				% H ₂ S	Prover																																																																																														
					Meter Run																																																																																														
					Taps																																																																																														
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="6">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th colspan="2">CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>SI</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1609</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>1.</td> <td>2" X 3/4"</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>188</td> <td></td> <td></td> <td></td> <td>1 Hour</td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>169</td> <td></td> <td></td> <td></td> <td>2 Hours</td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>154</td> <td></td> <td></td> <td></td> <td>3 Hours</td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>						FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	SI							1609					1.	2" X 3/4"						188				1 Hour	2.							169				2 Hours	3.							154				3 Hours	4.												5.											
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RATE OF FLOW CALCULATIONS																																																																																																			
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd																																																																																												
1	12.365		166.2	1.0000	.9258	1.0000	1903																																																																																												
2.																																																																																																			
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NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R																																																																																														
1.																																																																																																			
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5.																																																																																																			
P _c 1621.2 P _c ² 2628289.4					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0106$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0080$																																																																																														
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²																																																																																															
1		155.2	27622.4	2600667																																																																																															
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5																																																																																																			
Absolute Open Flow 1918 Mcfd @ 15.025					Angle of Slope @ _____																																																																																														
Remarks: H ₂ O																																																																																																			
Approved By Commission:				Conducted By: Mick Ferrari				Calculated By: James Smith																																																																																											
								Checked By: 																																																																																											

