

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-172
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-14-80	
Company Southland Royalty Company				Connection Southern Union Gathering			
Pool Undesignated				Formation Fruitland			
Completion Date 12-31-79		Total Depth 7340'		Plug Back TD 7295'		Elevation 6087'	
Farm or Lease Name Grenier				Well No. 11E			
Casing Size 5.625	Wt. 26#	ID 6.969	Set At 4819'	Perforations: From 2345' To 2358'		Unit Sec. Twp. Rge. N 13 31N 12W	
Tubg. Size 1.900	Wt. 2.76#	ID 1.610	Set At 2636'	Perforations: From To		County San Juan	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple				Packer Set At 4700'		State New Mexico	
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12.2	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run
		.700					Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							758		758		
1.							64		280		1 Hour
2.							45		210		2 Hours
3.							32		185		3 Hours
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	12.365		44.2	1.0000	.9258	1.0000	506
2.							
3.							
4.							
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 770.2 P _c ² 593208.0	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0702$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0593$																														
<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>NO.</th> <th>P_f²</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> </thead> <tbody> <tr> <td>1</td> <td></td> <td>197.2</td> <td>38887.8</td> <td>554320.2</td> </tr> <tr> <td>2</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>3</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>4</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>	NO.	P _f ²	P _w	P _w ²	P _c ² - P _w ²	1		197.2	38887.8	554320.2	2					3					4					5					AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 536$	
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1		197.2	38887.8	554320.2																												
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3																																
4																																
5																																

Absolute Open Flow _____ Mcfd @ 15.025	Angle of Slope @ _____
Remarks: _____	
Approved By Commission: _____	Conducted By: Mick Ferrari
Calculated By: James Smith	Checked By:

