STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 9-6-80	
Company: Southland Royalty Company		Connection: Southern Union Gathering		
Pool: Basin		Formation: Dakota		Unit
Completion Date: 9-13-80	Total Depth: 7450'	Plug Back TD: 7405'	Elevation: 6231' GR	Farm or Lease Name: Richardson
Csg. Size: 7.000 / 4.500 — Wt.: 23# / 10.5# — d: 6.366 / 4.052 — Set At: 4988' / 4707'-7450' — Perforations: From / To				Well No.: #10E
Tbg. Size: 2.375 — Wt.: 4.7# — d: 1.995 — Set At: 7332' — Perforations: From 7268' To 7388'				Unit: L — Sec.: 10 — Twp.: 31N — Rge.: 12W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: GG-Multiple		Packer Set At: 2682'		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F: 8	Mean Annual Temp. °F:	Baro. Press. – P_a: 12.2	State: NM

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
		.700						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					311				
1.	2" X 3/4"				0				1 Hour
2.					0				2 Hours
3.					0				3 Hours
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		12.2	1.0000	.9258	1.0000	140
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 323.2 P_c^2 104458.2

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		12.2	148.8	104309.4
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0014$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0010$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 140$

RECEIVED
NOV 25 1980
OIL CON. COM.
DIST. 3

Absolute Open Flow 140 Mcfd @ 15.025 — Angle of Slope θ _____ — Slope, n .75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Tom Wagner	James Smith	L. O. Van Ryan