

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 5-31-84	
Company Consolidated Oil & Gas, Inc.		Connection	
Pool Basin Dakota <u>FLORA VISTA</u>		Formation Gallup	
Completion Date 5/18/84		Total Depth 6570	Plug Back TD 6527
Elevation 5595		Farm or Lease Name Nance	
Csg. Size 5 1/2	Wt. 15.5#	d 4.950	Set At 6569
Perforations: From 5410 To 5582		Well No. 1-E	
Trg. Size 2 1/16	Wt. 3.25#	d 1.751	Set At 5648
Perforations: From To		Unit Sec. Twp. Rge. N 27 31N 13W	
Type Well - Single - Bradenhead - G.G. or C.O. Multiple Dual		Packer Set At 5780	County San Juan
Producing Thru Tubing	Reservoir Temp. °F θ	Mean Annual Temp. °F	Baro. Press. - P _a State New Mexico
L	H	G _g	% CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							857		857		3 hours
1.	2" X 3/4"						2		237		
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	OWT Coef.						102.8
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 869		P _c ² 755161		
NO	P _t	P _w	P _w ²	P _c ² - P _w ²
1		249	62001	693160
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.0894}{}$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{109.6}{}$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.0663}{}$$

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0894 \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0663$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 109.6$$

Absolute Open Flow 109.6 Mcfd @ 15.025 Angle of Slope 53.13° Slope, n 0.75

Remarks:

Approved By Division Conducted By: Calculated By: