

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 9/18/84		OCT 13 1984		
Company Union Texas Petroleum Corp.				Connection Southern Union Gathering Co.				OIL CO. NO.	
Pool Cedar Hill				Formation Fruitland Basal Coal				Unit DST-2	
Completion Date 7/7/84		Total Depth 7810		Plug Back TD 4200		Elevation 6276		Farm or Lease Name Payne	
Chg. Size 7.625	Wt. 26.40	d 6.969	Set At 4551	Perforations: From 2810 To 3064		Well No. 8			
Thg. Size 2.875	Wt. 6.50	d 2.441	Set At 3117	Perforations: From 3087 To 3093		Unit Sec. Twp. Rge. K 21 32N 10W			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single - Gas					Packer Set At -----		County San Juan		
Producing Thru Casing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12		State New Mexico	
L 2800	H	G _g 0.650	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"						1362		19 days
1.									70	68°	3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		82	0.9924	0.9608	1.000	967
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1374 P _c ² 1,887,876				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1			6765	1,881,111
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0036$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0030$$

$$AOI = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 970$$

Absolute Open Flow 970		Mcf @ 15.025	Angle of Slope θ	Slope, n 0.85
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Remarks:

Approved By Commission:	Conducted By: Connie Clevenger	Calculated By: Ken Roddy	Checked By:
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