

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 6-1-78	
Company Amoco Production Company				Connection Gas Company Of New Mexico		
Pool Ute Dome				Formation Dakota		Unit
Completion Date 5-25-78		Total Depth 2800		Plug Back TD 2740		Elevation 6277
Farm or Lease Name Ute Indians "A"						Well No. 12
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 2800	Perforations: From 2550 To 2642		Unit Sec. Twp. Rge. G 36 32N 14W
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 2646	Perforations: From Open To Ended		County San Juan
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None		State New Mexico
Producing Thru Tubing		Reservoir Temp. °F #		Mean Annual Temp. °F		Baro. Press. - P _a
L	H	Gg .65	% CO ₂	% N ₂	% H ₂ S	Prover
						Meter Run
						Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	7 days						513		523		
1.	2.375	0.750					120	60	340		
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		132	1.000	.9608	1.012	1587
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 535	P _c ² 286225				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	
1		352	123904	162321	
2					
3					
4					
5					

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.7633$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5302$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2428$$

Absolute Open Flow	2428	Mcfd @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks:

Approved By Commission:	Conducted By:	Calculated By: T. M. Oliver	Checked By:
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