

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 12-29-83							
Company Robert L. Bayless				Connection Northwest Pipeline Corp.							
Pool Ballard Pic. Cliffs				Formation Pictured Cliffs							
Completion Date 12-21-83		Total Depth 2685		Plug Back TD 2625							
Elevation 7082 GL		Farm or Lease Name Jicarilla 390 B									
Csg. Size 2-7/8"	Wt. 7.9	d 2.323"	Set At 2669	Perforations: From 2524 To 2583							
Trg. Size None	Wt.	d	Set At	Perforations: From To							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None							
Producing Thru Casing				Baro. Press. - P _a 12 psia est.							
Reservoir Temp. °F #				Mean Annual Temp. °F							
L H Gg % CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps											
.65 est.											
FLOW DATA				TUBING DATA							
Casing Data				Duration of Flow							
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	8 days								640		
1.	2" X 3/4"			50					50	60	3 hrs.
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow O, Mcfd				
1	12.3650		62	1.0000	.9608	1.007	742				
2.											
3.											
4.											
5.											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
P _c 652 P _c ² 425,104											
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0151$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0128$						
1		79.4	6304	418,800							
2											
3			calculated		AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 751$						
4											
5											
Absolute Open Flow 751 Mcfd @ 15.025 Angle of Slope θ Slope, n .85											
Remarks:											
Approved By Division Conducted By: Walsh Engineering Calculated By: Kevin McCord Checked By: Robert L. Bayless											