NEW ME CO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 4-16-68	
Company: TOM L. INGRAM			Connection: NONE		Unit: 320 ACRES
Pool: UNDESIGNATED			Formation: ATOKA PENN		
Completion Date: 4-16-68	Total Depth: 11710'		Plug Back TD: 11348'	Elevation: 4019' DF-11'	Farm or Lease Name: DICKINSON
Csg. Size: 5 1/2 / Wt.: 17 / 20 / d: 4.892 / 4.778 / Set At: 11710'			Perforations: From 11263' To 11268'		Well No.: 1
Tbg. Size: 2 3/8 / Wt.: 4.7 / d: 1.995 / Set At: 11197'			Perforations: From OPEN ENDED To 11197'		Unit: M / Sec.: 33 / Twp.: 10 / Rge.: 36
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE			Packer Set At: 11132'		County: LEA
Producing Thru: TUBING	Reservoir Temp. °F: 178° @ 11065'	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11263	–	0.751	0.62	3.75	0.00	–	4.026	FLANGE

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						1774	62	PKR		94.0
1.	4	19/64 1.25	930	78	70	1305	79	–		5.00
2.	4	17/64 1.25	930	55	75	1360	76	–		1.25
3.	4	14/64 1.25	930	35	80	1390	76	–		1.00
4.	4	10/64 1.25	930	14	84	1453	70	–		1.00
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.469	271.24	943.2	0.9905	1.154	1.127	2609.8
2.	7.469	227.75	943.2	0.9859	1.154	1.123	2173.4
3.	7.469	181.69	943.2	0.9813	1.154	1.114	171 .9
4.	7.469	114.92	943.2	0.9777	1.154	1.110	1075.0
5							

NO.	P_t	Temp. °R	T_r	Z
1.	1.42	530	1.33	.787
2.	1.42	535	1.34	.793
3.	1.42	540	1.36	.806
4.	1.42	544	1.37	.811
5.				

Gas Liquid Hydrocarbon Ratio 13297 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 52.0 @ 60 Deg.
Specific Gravity Separator Gas 0.751 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX –
Critical Pressure 666 P.S.I.A. – P.S.I.A.
Critical Temperature 398 R – R

P_c 3126.2 P_c^2 9773.1

NO	P_t^2	P_w *	P_w^2	$P_c^2 - P_w^2$
		1936.2	3748.9	6024.2
2		2139.2	4576.2	5196.9
3		2415.2	5833.2	3939.9
4		2701.2	7296.5	2476.6
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.622$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.602$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 4181$

Absolute Open Flow 4180 Mcfd @ 15.025 Angle of Slope θ 45.5° Slope, n 0.973

Remarks: BHP @ (-7247) 11266' USED FOR PRESSURE CALCULATIONS

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	COLEMAN PET. ENG. CO	JOE A. COLEMAN	JOE A. COLEMAN