## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool	Sawyer			_Formatio	n S <b>an</b>	Andres		_County_	Lea		
Init	ial	<u> </u>	_Annual	<u> </u>	Spec	cial		Date of	Test_1-	-14-65	
Comp	any Bogle	& Kemper	011 Co.		_Lease_ <b>U</b> r	nion Fede	ral	Wel	1 No. <u>3</u>		
Unit	Н	Sec31	Twp	<b>9</b> S R	ge	BE Purc	haser	5.0.& G.		····	
Casi	ng 5 }	Wt. 15.	5_I.D.	<b>4892</b> S	et at 49	<b>11</b> Pe	rf	<b>4896</b>	To49	906	
Tubi	ng 2 3/8	Wt. 4.7	I.D	<b>1.995</b> S	et at 49	<b>56</b> Pe	rf	open	To		
Gas	Pay: From	L896	То <b>4977</b>	L_ <b>49</b>	<u>56</u> x	G_812		4024	Bar.Pre	ss. <u>13.2</u>	
Prod	ucing Thru	: Casi	.ng	Tı	ubing	X	Type We	:11	single		
Date	of Comple	tion:		Packe	er <u> 488</u> 0	Sin	gle-Brade Reserve	enhead-G. oir Temp.	G. or G	.0. Dual	
					OBSERV	ED DATA					
Test	ed Through	(albumanara	<u>r) afeliusia</u>	(Meter	Σ			Type Tap	s flan	<b>30</b>	
			ow Data			Tubing		Casing D			
No.	(Line)	(Orifi	.ce)	ss. Diff	1		ł		,	Duration of Flow	
	Size	Siz	e ps	ig h <sub>w</sub>	· · ·		°F.	psig	Tr.		
SI						596	ļ			72 SI	
1. 2.	3	875	463	3.92	58	451	ļ			24	
<del>2.</del> 1					<b></b>	<del> </del>	<del> </del>		<del> </del>		
4.		<del></del>			<del> </del>	<del> </del>	<del> </del>		<del> </del>		
5. 1					<del>                                     </del>		† · · · · · · · · · · · · · · · · · · ·			<del></del>	
······											
	FLOW CALCULATIONS  Coefficient   Pressure   Flow Temp.   Gravity   Compress.   Rate of F										
No.	Coefficient										
140.1	(24-Hour) √ h <sub>w</sub> i		/h na	nsia		LOP	ractor F	Factor		@ 15.025 nsia	
<del>,</del> -											
1. 2.	4.713		O:88	476.2	1.0019	<del></del>	8607	1.089		180,9	
3.	<del></del>					<del></del>				<del></del>	
3 c 4 .			<del></del>								
5.							<del></del>	<del></del>			
	iquid Hydro ty of Liqui <b>9.936</b>	id Hydro		neg.	cf/bbldeg.		Speci Speci			rator Gas <b>g12</b> ing Fluid 5	
No.	P <sub>w</sub> Pt (psia)	Pt <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F (1	cQ) <sup>2</sup> -e <sup>-s</sup> )	P <sub>w</sub> 2	$P_c^2 - P_w^2$	Ca P	I	
	464.2		negligi	ble			215.5	129.5	464.2	2	
1. 2. 3.		<del> </del>	+	<del> </del>					<del> </del>	<del></del>	
-		<del> </del>	+	<del></del>		<del></del>		<del></del>	+	- ;	
<del>Š.</del> 1	·	<del> </del>	<del> </del>	+					<del>                                     </del>		
	Lute Potent		460.4 11 & Gas	Co.	MCFPD;	n	L.000				
ADDRE	ESS Box	308: 1	Catum. N.			111					
	and TITLE			Inst. Tec	h.	Faul	wife				
VII'NE COMPA	ESSED										
JOPIPA	714.T				REM	ARKS			<del></del>		

used pravious n slope A. F. calculated

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- Pc= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw- Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- $F_g \subseteq Gravity$  correction factor.
- $F_{t}$  Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .