

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 8/10/83	
Company HNG Oil Company		Connection Transwestern Pipeline	
Pool Pitchfork Ranch		Formation Morrow	
Completion Date		Total Depth 15290'	Plug Back TD 15075'
		Elevation 3500' GL	
Coq. Size 4 1/2" Liner	Wt. 13.5	Set At 15290'	Perforations: From 14894 To 14944
Req. Size 2 7/8"	Wt.	Set At 12967'	Perforations: From Open To Ended
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		Packer Set At 12967'	Unit J
Producing Thru Tbg.	Reservoir Temp. °F 223	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2
L 14919	H 14919	C _g .5782	% CO ₂ .677
		% N ₂ .180	% H ₂ S
		Prover	Meter Run 4.026
			Taps Flg.

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							6293				36.0 hrs
1.	4	X	1.625	730	5.0	84	5909	63			1.0 hr
2.	4	X	1.625	730	11.0	86	5704	63			1.0 hr
3.	4	X	1.625	740	22.0	86	5400	63			1.0 hr
4.	4	X	1.625	750	40.0	86	4975	63			1.0 hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.79	60.96	743.2	.9777	1.315	1.052	1055
2	12.79	90.42	743.2	.9759	1.315	1.051	1560
3	12.79	128.73	753.2	.9759	1.315	1.051	2221
4	12.79	174.72	763.2	.9759	1.315	1.052	3017
5							

NO.	R ₁	Temp. °R	T ₁	Z	Gas Liquid Hydrocarbon Ratio	Dry	Mcf/bbl.
1	1.11	544	1.55	.904	A.P.I. Gravity of Liquid Hydrocarbons		Deg.
2	1.11	546	1.56	.906	Specific Gravity Separator Gas	.5782	X X X X X X X X
3	1.12	546	1.56	.905	Specific Gravity Flowing Fluid	X X X X X	
4	1.14	546	1.56	.904	Critical Pressure	672	P.S.I.A.
5					Critical Temperature	350	R

P _c *6423.7		P _c ² 41264.0	
NO.	P ₁ ²	P _w	P _w ²
1	7608.2	6032.1	36385.8
2	7396.2	5842.3	34132.3
3	7055.2	5537.1	30659.4
4	6547.2	5090.3	25911.1
5	8051.2	S.I.P.	

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.688$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.375$

AOF = O $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 7166$

Absolute Open Flow 7166 Mcfd @ 15.025 Angle of Slope @ 48.75 Slope, n .875

Remarks: CALCULATED FROM BOTTOM HOLE BOMBS SET @ 14919'

Approved By Division	Conducted By: JARREL WELL TESTING INC.	Calculated By: Rick Pagan	Checked By: Rick Pagan
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