## U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Sundry Print Report

Well Name: BIG STAG FED COM Well Location: T21S / R32E / SEC 1 / County or Parish/State: LEA /

SWSE / 32.500766 / -103.6272207 NM

Well Number: 504H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMNM127892. Unit or CA Name: Unit or CA Number:

NMNM92187

US Well Number: 3002547066 Well Status: Approved Application for Operator: ASCENT ENERGY

Permit to Drill L

#### **Notice of Intent**

Type of Submission: Notice of Intent

Type of Action Other

Date Sundry Submitted: 05/28/2021 Time Sundry Submitted: 01:09

Date proposed operation will begin: 05/31/2021

**Procedure Description:** Ascent Energy respectfully requests approval for the following revisions to the Big Stagg Fed Com 603H. -Change the well name from the Big Stagg Fed Com 603H to Big Stag Fed Com 504H -Revise the BHL from 1270' FNL, 2310' FEL to 1271' FNL, 2178' FWL -Revise target formation from 3rd Bone Spring Sand to 2nd Bone Spring Sand. -Request approval to increase casing diameter on shallow casing strings to improve drilling efficiencies - Propose BOP substitution to fit on the larger casing sizes of the shallow casing strings. Attached documents include: Updated Big Stag Fed Com 504H C102, Proposed Directional Survey plan and drawing, Anti-Collision plan, Well Pad plat, and Proposed casing and BOP substitution document.

#### **Surface Disturbance**

Is any additional surface disturbance proposed?: No

#### **NOI Attachments**

#### **Procedure Description**

Big\_Stag\_504H\_Sundry\_24May\_v3\_20210528130400.pdf

AC\_REPORT\_2\_BIG\_STAG\_FED\_COM\_504H\_20210527152230.pdf

PROPOSAL\_2\_BIG\_STAG\_FED\_COM\_504H\_20210527152226.pdf

 $2020010110\_ASCENT\_BIG\_STAG\_504H\_WELL\_SITE\_REVISED\_05\_07\_2021\_20210525163408.pdf$ 

2020010110\_ASCENT\_BIG\_STAG\_FED\_COM\_LEA\_504H\_C\_102\_REVISED\_05\_07\_2021\_FINAL\_2021052 5163407.pdf

DWG2\_\_\_24X36\_20210525163343.pdf

Page 1 of 2

leceived by OCD: 6/1/2021 1:46:04 PM
Well Name: BIG STAG FED COM
Well Location: T21

**Well Location:** T21S / R32E / SEC 1 / SWSE / 32.500766 / -103.6272207

Well Number: 504H

Type of Well: OIL WELL

Allottee or Tribe Name:

County or Parish/State: LEA/

Lease Number: NMNM127892,

NMNM92187

**Unit or CA Name:** 

Unit or CA Number:

**US Well Number:** 3002547066

Well Status: Approved Application for

Permit to Drill

**Operator:** ASCENT ENERGY

LLC

#### **Conditions of Approval**

#### **Additional Reviews**

Big\_Stagg\_Fed\_Com\_603H\_Sundry\_COA\_20210601105012.pdf

1\_21S\_32E\_O\_ATS\_19\_3155\_Big\_Stagg\_Fed\_Com\_603H\_Sundry\_Lea\_NMNM127892\_Ascent\_Energy\_LLC\_13\_22\_06\_01\_2021\_Yolanda\_Jimenez\_20210601105001.pdf

#### **Operator Certification**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a submission of Form 3160-5 or a Sundry Notice.

Operator Electronic Signature: BEN METZ Signed on: MAY 28, 2021 01:08 PM

Name: ASCENT ENERGY LLC

Title: Vice President Exploration

Street Address: PO BOX 270983

City: LITTLETON State: CO

Phone: (303) 513-8590

Email address: BMETZ@ASCENTENERGY.US

#### **Field Representative**

**Representative Name:** 

**Street Address:** 

City: State:

Zip:

Phone:

**Email address:** 

#### **BLM Point of Contact**

BLM POC Name: CHRISTOPHER WALLS

BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752342234 BLM POC Email Address: cwalls@blm.gov

**Disposition:** Approved **Disposition Date:** 06/01/2021

Signature: Chris Walls

Page 2 of 2

District I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 <u>District III</u> 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170

<u>District IV</u> 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462 State of New Mexico
Energy, Minerals & Natural Resources Department
OIL CONSERVATION DIVISION
1220 South St. Francis Dr.
Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

<sup>1</sup> API Number 30-025-47066	E SPRING
<sup>4</sup> Property Code	<sup>6</sup> Well Number
327306	504H
<sup>7</sup> OGRID No.	<sup>9</sup> Elevation
325830	3,795'

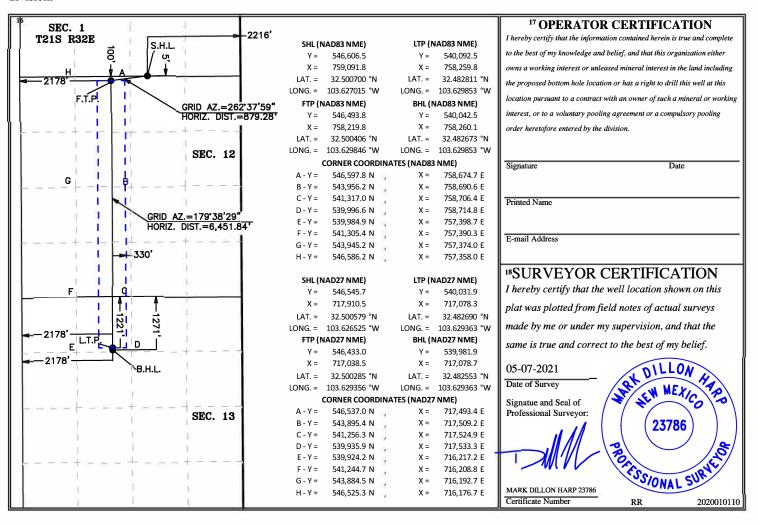
<sup>10</sup> Surface Location

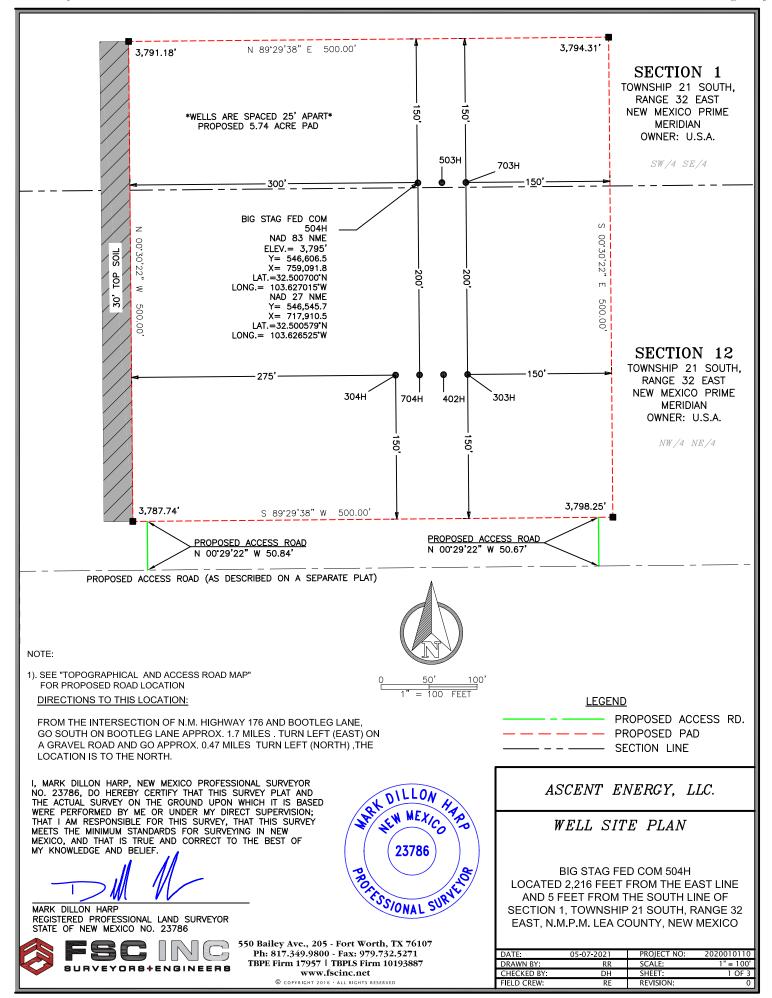
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
0	1	21 S	32 E		5	SOUTH	2,216	EAST	LEA

11 Bottom Hole Location If Different From Surface

42	G. G	No.		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			50		A
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
В	13	21 S	32 E		1,271	NORTH	2,178	WEST	LEA
12 Dedicated Acres	Joint of	r Infill 14 C	onsolidation	Code 15 Or	der No.	311	12		

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



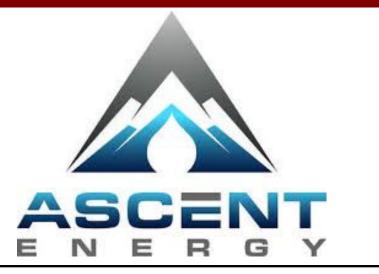


### **ASCENT ENERGY**

LEA COUNTY, NEW MEXICO (NAD 83) (GRID) SEC. 1 T21S R32E N.M.P.M. (GRID) BIG STAG FED COM 504H

ORIGINAL WELLBORE 10 May, 2021

Plan: PROPOSAL #2



START NUDGE (2°/100ft BUR)

END OF TANGENT

- EOT TO 269.99° AZ-

**END OF TANGENT** 

**EOD TO VERTICAL** 

KOP (10°/100ft BUR)

Vertical Section at 280.78° (700 usft/in)

**EOB TO 12° INC** 

4000-

usft/in)

(700

Depth -0009

Vertical 2000-

7500-

8000-

8500-

9000-

9500-

10000-

Project: LEA COUNTY, NEW MEXICO (NAD 83) (GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well: BIG STAG FED COM 504H Wellbore: ORIGINAL WELLBORE

Design: PROPOSAL #2

	ANNOTATIONS											
MD	Inc	Azi	TVD	+N/-S	+E/-W	VSect	Dep	Annotation				
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	SHL: 5ft FSL & 2216ft FEL of Sec 1				
2000.00	0.00	0.00	2000.00	0.00	0.00	0.00	0.00	START NUDGE (2°/100ft BUR)				
2600.00	12.00	292.00	2595.62	23.45	-58.04	-23.82	62.60	EOB TO 12° INC				
4322.75	12.00	292.00	4280.73	157.63	-390.14	-160.08	420.78	END OF TANGENT				
4550.23	12.00	269.99	4503.35	166.49	-435.74	-169.22	467.59	EOT TO 269.99° AZ				
6356.68	12.00	269.99	6270.35	166.39	-811.25	-171.49	843.11	END OF TANGENT				
6956.57	0.00	0.00	6865.86	166.38	-873.83	-171.87	905.69	EOD TO VERTICAL				
10288.26	0.00	0.00	10197.55	166.38	-873.83	-171.87	905.69	KOP (10°/100ft BUR)				
10880.86	59.26	179.64	10690.00	-113.71	-872.07	108.23	1186.05	FTP: 100ft FNL & 2178ft FWL of Sec 12				
11185.97	89.77	179.64	10770.50	-404.28	-870.24	398.80	1476.35	HZ LP: 390.57ft FNL & 2178ft FWL of Sec 12				
17295.93	89.77	179.64	10794.80	-6514.07	-832.05	6508.71	7586.27	LTP: 1221ft FNL & 2178ft FWL of Sec 13				
17345.93	89.77	179.63	10795.00	-6564.07	-831.73	6558.71	7636.27	BHL: 1271ft FNL & 2178ft FWL of Sec 13				
						WEL	LBORE 1	TARGET DETAILS (LAT/LONG)				

PROPOSED LOCAL COORDINATES:

FTP: 100ft FNL & 2178ft FWL of Sec 12

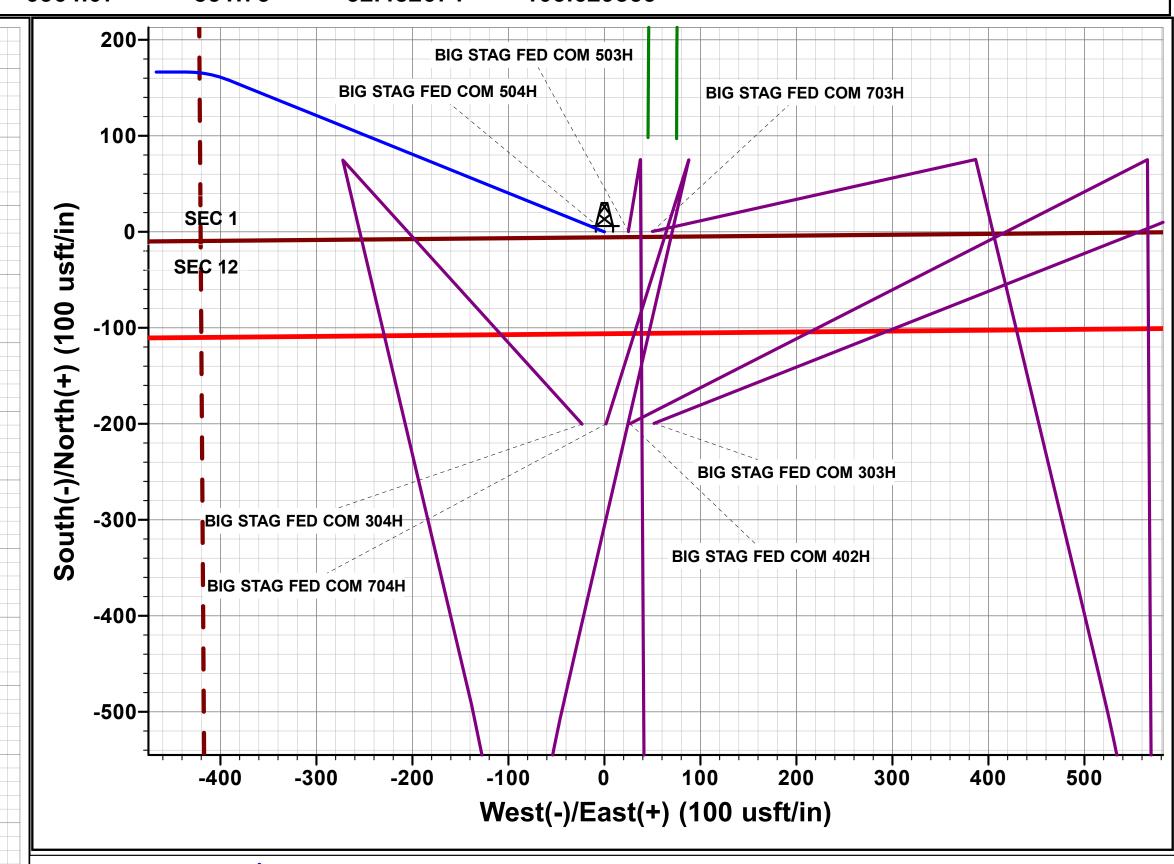
SHL: 5ft FSL & 2216ft FeL Sec 1

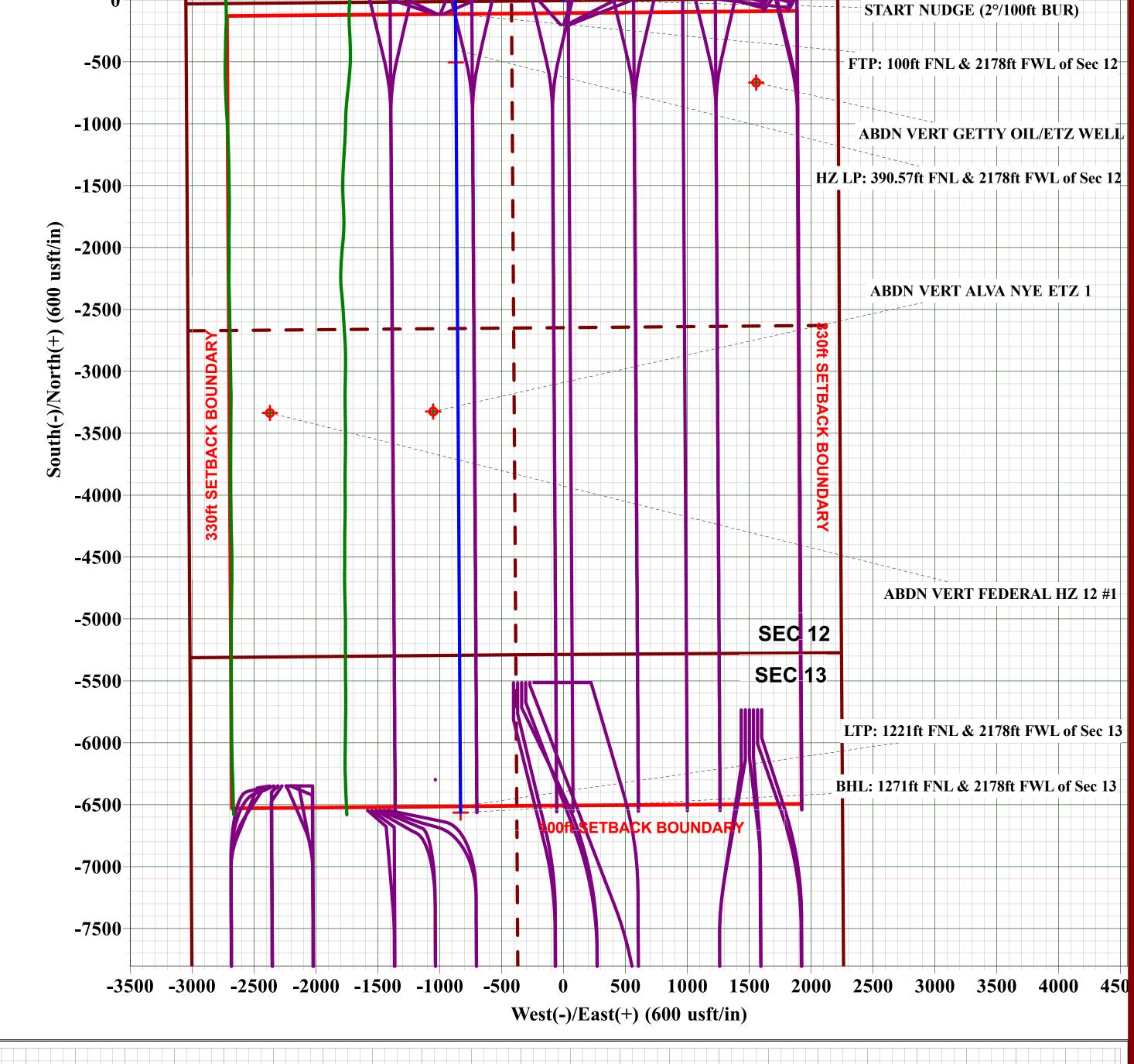
HZ LP: 390.57ft FNL & 2178ft FWL Sec 12

LTP: 1221ft FNL & 2178ft FWL of Sec 13

BHL: 1271ft FNL & 2178ft FWL of Sec 13

Name	TVD	+N/-S	+E/-W	Latitude	Longitude
KOP - BIG STAG FED COM 504H	10197.55	166.38	-873.83	32.501173	-103.629846
FTP - BIG STAG FED COM 504H	10690.00	-113.71	-872.01	32.500403	-103.629846
HZ LP - BIG STAG FED COM 504H	10770.50	-504.26	-869.62	32.499330	-103.629847
LTP - BIG STAG FED COM 504H	10794.80	-6514.07	-832.05	32.482811	-103.629853
BHL - BIG STAG FED COM 504H	10795.00	-6564.07	-831.73	32.482674	-103.629853





SEC 1

KOP (10°/100ft BUR)

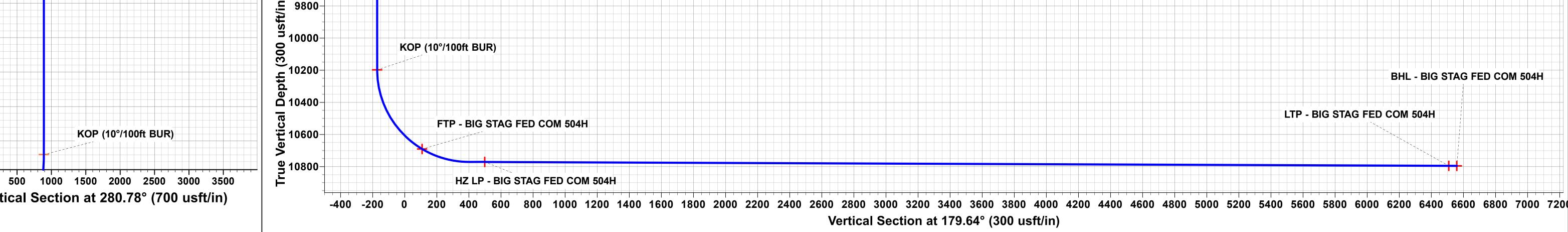
EOD TO VERTICAL

END OF TANGENT

**EOT TO 269.99° AZ** 

END OF TANGENT

EOB TO 12° INC



1500

\_ ABDN VERT | EDERAL ONE #1

ABDN VERT SHEPHARD B FED

Database: Database 1

Company: ASCENT ENERGY

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well:

Wellbore:

Design:

BIG STAG FED COM 504H

ORIGINAL WELLBORE

PROPOSAL #2

Local Co-ordinate Reference:

TVD Reference:
MD Reference:

North Reference:

**Survey Calculation Method:** 

Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

Minimum Curvature

Project LEA COUNTY, NEW MEXICO (NAD 83) (GRID)

Map System:US State Plane 1983Geo Datum:North American Datum 1983

North American Datum 1983

New Mexico Eastern Zone

System Datum:

Mean Sea Level

Using geodetic scale factor

Site SEC. 1 T21S R32E N.M.P.M. (GRID)

Site Position: Northing: 546,692.70 usft Latitude: 32.500955 Easting: 758,094.60 usft Longitude: -103.630248 From: Map **Position Uncertainty:** 0.00 usft Slot Radius: 1.10ft **Grid Convergence:** 0.38°

Well BIG STAG FED COM 504H

 Well Position
 +N/-S
 -86.20 usft
 Northing:
 546,606.50 usft
 Latitude:
 32.500700

 +E/-W
 997.24 usft
 Easting:
 759,091.80 usft
 Longitude:
 -103.627015

Position Uncertainty0.00 usftWellhead Elevation:usflGround Level:3,795.00 usft

Wellbore ORIGINAL WELLBORE

 Magnetics
 Model Name
 Sample Date (°)
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2020
 2021-05-10
 6.60
 60.15
 47,659.41276401

Design PROPOSAL #2

Audit Notes:

Map Zone:

Version:Phase:PROTOTYPETie On Depth:0.00

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S (usft)
 +E/-W (usft)
 Direction (°)

 0.00
 0.00
 0.00
 179.64

Plan Sectio	ns										
MD (usft)	Inc (°)	Azi (°)	Vertical Depth	SS (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usf	Build Rate (°/100usf	Turn Rate (°/100usf	TFO (°)	Target
0.00	0.00	0.00	0.00	-3,820.00	0.00	0.00	0.00	0.00	0.00	0.00	
2,000.00	0.00	0.00	2,000.00	-1,820.00	0.00	0.00	0.00	0.00	0.00	0.00	
2,600.00	12.00	292.00	2,595.62	-1,224.38	23.45	-58.04	2.00	2.00	0.00	292.00	
4,322.75	12.00	292.00	4,280.73	460.73	157.63	-390.14	0.00	0.00	0.00	0.00	
4,550.23	12.00	269.99	4,503.36	683.36	166.49	-435.74	2.00	0.00	-9.68	-100.80	
6,356.68	12.00	269.99	6,270.35	2,450.35	166.39	-811.25	0.00	0.00	0.00	0.00	
6,956.57	0.00	0.00	6,865.86	3,045.86	166.38	-873.83	2.00	-2.00	15.01	180.00	
10,288.26	0.00	0.00	10,197.55	6,377.55	166.38	-873.83	0.00	0.00	0.00	0.00	KOP - BIG STAG F
11,185.97	89.77	179.64	10,770.50	6,950.50	-404.28	-870.24	10.00	10.00	0.00	179.64	
17,295.93	89.77	179.64	10,794.80	6,974.80	-6,514.07	-832.05	0.00	0.00	0.00	0.00	LTP - BIG STAG FE
17,345.93	89.77	179.63	10,795.00	6,975.00	-6,564.07	-831.73	0.02	0.00	-0.02	-92.35	BHL - BIG STAG FE

Database: Database 1

Company: ASCENT ENERGY

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well:
Wellbore:
Design:
BIG STAG FED COM 504H
ORIGINAL WELLBORE
PROPOSAL #2

Local Co-ordinate Reference:

TVD Reference:
MD Reference:

North Reference:

**Survey Calculation Method:** 

Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

Planned Surve	<b>Э</b> у									
							Mantla al	D. alea	D. U.I	<b>T</b>
MD	lma	A =:	TVD	SS	+N/-S	+E/-W	Vertical Section	Dogleg Rate	Build Rate	Turn Rate
(usft)	Inc (°)	Azi (°)	(usft)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
SHI · E		216ft FEL of S	Soc 1		()	()				
0.00	0.00	0.00	0.00	3,820.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	3,720.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	3,620.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00 400.00	0.00 0.00	0.00 0.00	300.00 400.00	3,520.00 3,420.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
500.00	0.00	0.00	500.00	3,320.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	3,220.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	3,120.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	3,020.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	2,920.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	2,820.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00 1,200.00	0.00 0.00	0.00 0.00	1,100.00 1,200.00	2,720.00 2,620.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
1,300.00	0.00	0.00	1,300.00	2,520.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.00	1,400.00	2,420.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	2,320.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.00	1,600.00	2,220.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00 1,800.00	0.00 0.00	0.00 0.00	1,700.00 1,800.00	2,120.00 2,020.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
1,900.00	0.00	0.00	1,900.00	1,920.00	0.00	0.00	0.00	0.00	0.00	0.00
		2°/100ft BUR)	·	,						
2,000.00	0.00 (2	0.00	2.000.00	1,820.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	2.00	292.00	2,099.98	1,720.02	0.65	-1.62	-0.66	2.00	2.00	0.00
2,200.00	4.00	292.00	2,199.84	1,620.16	2.61	-6.47	-2.65	2.00	2.00	0.00
2,300.00 2,400.00	6.00 8.00	292.00 292.00	2,299.45 2,398.70	1,520.55 1,421.30	5.88 10.44	-14.55 -25.85	-5.97 -10.61	2.00 2.00	2.00 2.00	0.00 0.00
		292.00	2,497.47	1,322.53	16.30	-40.35	-16.56	2.00	2.00	0.00
2,500.00	10.00 <b>TO 12° INC</b>	292.00	2,497.47	1,322.53	10.30	-40.35	-10.30	2.00	2.00	0.00
2,600.00	12.00	292.00	2,595.62	1,224.38	23.45	-58.04	-23.82	2.00	2.00	0.00
2,700.00	12.00	292.00	2,693.44	1,126.56	31.24	-77.32	-31.73	0.00	0.00	0.00
2,800.00	12.00	292.00	2,791.25	1,028.75	39.03	-96.60	-39.63	0.00	0.00 0.00	0.00
2,900.00	12.00	292.00	2,889.07	930.93	46.82	-115.88	-47.54	0.00		0.00
3,000.00 3,100.00	12.00 12.00	292.00 292.00	2,986.88 3,084.70	833.12 735.30	54.61 62.39	-135.15 -154.43	-55.45 -63.36	0.00 0.00	0.00 0.00	0.00 0.00
3,200.00	12.00	292.00	3,182.51	637.49	70.18	-173.71	-03.30 -71.27	0.00	0.00	0.00
3,300.00	12.00	292.00	3,280.33	539.67	77.97	-192.98	-79.18	0.00	0.00	0.00
3,400.00	12.00	292.00	3,378.14	441.86	85.76	-212.26	-87.09	0.00	0.00	0.00
3,500.00	12.00	292.00	3,475.96	344.04	93.55	-231.54	-95.00	0.00	0.00	0.00
3,600.00 3,700.00	12.00 12.00	292.00 292.00	3,573.77 3,671.59	246.23 148.41	101.34 109.12	-250.82 -270.09	-102.91 -110.82	0.00 0.00	0.00 0.00	0.00 0.00
3,700.00	12.00	292.00 292.00	3,671.59 3,769.40	50.60	116.91	-270.09 -289.37	-110.82 -118.73	0.00	0.00	0.00
3,900.00	12.00	292.00	3,867.22	-47.22	124.70	-308.65	-126.64	0.00	0.00	0.00
4,000.00	12.00	292.00	3,965.03	-145.03	132.49	-327.93	-134.55	0.00	0.00	0.00
4,100.00	12.00	292.00	4,062.84	-242.84	140.28	-347.20	-142.46	0.00	0.00	0.00
4,200.00	12.00	292.00	4,160.66	-340.66	148.07	-366.48	-150.37	0.00	0.00	0.00
4,300.00	12.00 <b>DF TANGEN</b>	292.00	4,258.47	-438.47	155.86	-385.76	-158.28	0.00	0.00	0.00
4,322.75	12.00	292.00	4,280.73	-460.73	157.63	-390.14	-160.08	0.00	0.00	0.00
4,400.00	11.81	284.56	4,356.32	-536.32	162.62	-405.24	-165.17	2.00	-0.25	-9.63
4,500.00	11.85	274.80	4,454.21	-634.21	166.06	-425.38	-168.72	2.00	0.04	-9.77
EOT T	O 269.99° A	λZ								
4,550.23	12.00	269.99	4,503.35	-683.35	166.49	-435.74	-169.22	2.00	0.29	-9.58

Database: Database 1

Company: ASCENT ENERGY

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well: BIG STAG FED COM 504H
Wellbore: ORIGINAL WELLBORE

Design: PROPOSAL #2

**Local Co-ordinate Reference:** 

TVD Reference:
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North Reference:

**Survey Calculation Method:** 

Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

Planned Surve	Эy									
MD (usft)	Inc (°)	Azi (°)	TVD (usft)	SS (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
4,600.00 4,700.00	12.00 12.00	269.99 269.99	4,552.04 4,649.85	-732.04 -829.85	166.48 166.48	-446.08 -466.87	-169.28 -169.41	0.00 0.00	0.00 0.00	0.00 0.00
4,800.00 4,900.00 5,000.00 5,100.00 5,200.00	12.00 12.00 12.00 12.00 12.00	269.99 269.99 269.99 269.99 269.99	4,747.67 4,845.48 4,943.30 5,041.11 5,138.93	-927.67 -1,025.48 -1,123.30 -1,221.11 -1,318.93	166.47 166.47 166.46 166.46 166.45	-487.66 -508.44 -529.23 -550.02 -570.81	-169.53 -169.66 -169.78 -169.91 -170.04	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
5,300.00 5,400.00 5,500.00 5,600.00 5,700.00	12.00 12.00 12.00 12.00 12.00	269.99 269.99 269.99 269.99 269.99	5,236.75 5,334.56 5,432.38 5,530.19 5,628.01	-1,416.75 -1,514.56 -1,612.38 -1,710.19 -1,808.01	166.45 166.44 166.43 166.43	-591.59 -612.38 -633.17 -653.96 -674.74	-170.16 -170.29 -170.41 -170.54 -170.66	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
5,800.00 5,900.00 6,000.00 6,100.00 6,200.00	12.00 12.00 12.00 12.00 12.00	269.99 269.99 269.99 269.99 269.99	5,725.82 5,823.64 5,921.45 6,019.27 6,117.09	-1,905.82 -2,003.64 -2,101.45 -2,199.27 -2,297.09	166.42 166.42 166.41 166.41 166.40	-695.53 -716.32 -737.10 -757.89 -778.68	-170.79 -170.91 -171.04 -171.17 -171.29	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
6,300.00	12.00	269.99	6,214.90	-2,394.90	166.40	-799.47	-171.42	0.00	0.00	0.00
6,356.68	OF TANGEN 12.00	IT 269.99	6,270.35	-2,450.35	166.39	-811.25	-171.49	0.00	0.00	0.00
6,400.00 6,500.00 6,600.00	11.13 9.13 7.13	269.99 269.99 269.99	6,312.78 6,411.22 6,510.21	-2,492.78 -2,591.22 -2,690.21	166.39 166.39 166.38	-819.93 -837.52 -851.67	-171.54 -171.65 -171.73	2.00 2.00 2.00	-2.00 -2.00 -2.00	0.00 0.00 0.00 0.00
6,700.00 6,800.00 6,900.00	5.13 3.13 1.13 TO VERTICA	269.99 269.99 269.99	6,609.63 6,709.37 6,809.29	-2,789.63 -2,889.37 -2,989.29	166.38 166.38 166.38	-862.35 -869.55 -873.27	-171.80 -171.84 -171.86	2.00 2.00 2.00	-2.00 -2.00 -2.00	0.00 0.00 0.00
6,956.57	0.00	0.00	6,865.86	-3,045.86	166.38	-873.83	-171.87	2.00	-2.00	159.12
7,000.00	0.00	0.00	6,909.29	-3,089.29	166.38	-873.83	-171.87	0.00	0.00	0.00
7,100.00 7,200.00 7,300.00 7,400.00 7,500.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	7,009.29 7,109.29 7,209.29 7,309.29 7,409.29	-3,189.29 -3,289.29 -3,389.29 -3,489.29 -3,589.29	166.38 166.38 166.38 166.38	-873.83 -873.83 -873.83 -873.83 -873.83	-171.87 -171.87 -171.87 -171.87 -171.87	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
7,600.00 7,700.00 7,800.00 7,900.00 8,000.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	7,509.29 7,609.29 7,709.29 7,809.29 7,909.29	-3,689.29 -3,789.29 -3,889.29 -3,989.29 -4,089.29	166.38 166.38 166.38 166.38	-873.83 -873.83 -873.83 -873.83 -873.83	-171.87 -171.87 -171.87 -171.87 -171.87	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
8,100.00 8,200.00 8,300.00 8,400.00 8,500.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	8,009.29 8,109.29 8,209.29 8,309.29 8,409.29	-4,189.29 -4,289.29 -4,389.29 -4,489.29 -4,589.29	166.38 166.38 166.38 166.38	-873.83 -873.83 -873.83 -873.83 -873.83	-171.87 -171.87 -171.87 -171.87 -171.87	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
8,600.00 8,700.00 8,800.00 8,900.00 9,000.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	8,509.29 8,609.29 8,709.29 8,809.29 8,909.29	-4,689.29 -4,789.29 -4,889.29 -4,989.29 -5,089.29	166.38 166.38 166.38 166.38 166.38	-873.83 -873.83 -873.83 -873.83 -873.83	-171.87 -171.87 -171.87 -171.87 -171.87	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
9,100.00 9,200.00 9,300.00 9,400.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	9,009.29 9,109.29 9,209.29 9,309.29	-5,189.29 -5,289.29 -5,389.29 -5,489.29	166.38 166.38 166.38 166.38	-873.83 -873.83 -873.83 -873.83	-171.87 -171.87 -171.87 -171.87	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00

Database: Database 1

Company: ASCENT ENERGY

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well:
Wellbore:
Design:
BIG STAG FED COM 504H
ORIGINAL WELLBORE
PROPOSAL #2

Local Co-ordinate Reference:

TVD Reference:
MD Reference:

North Reference: Survey Calculation Method: Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

Planned Survey	y									
MD (usft)	Inc (°)	Azi (°)	TVD (usft)	SS (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,500.00	0.00	0.00	9,409.29	-5,589.29	166.38	-873.83	-171.87	0.00	0.00	0.00
9,600.00	0.00	0.00	9,509.29	-5,689.29	166.38	-873.83	-171.87	0.00	0.00	0.00
9,700.00	0.00	0.00	9,609.29	-5,789.29	166.38	-873.83	-171.87	0.00	0.00	0.00
9,800.00	0.00	0.00	9,709.29	-5,889.29	166.38	-873.83	-171.87	0.00	0.00	0.00
9,900.00	0.00	0.00	9,809.29	-5,989.29	166.38	-873.83	-171.87	0.00	0.00	0.00
10,000.00	0.00	0.00	9,909.29	-6,089.29	166.38	-873.83	-171.87	0.00	0.00	0.00
10,100.00	0.00	0.00	10,009.29	-6,189.29	166.38	-873.83	-171.87	0.00	0.00	0.00
10,200.00	0.00	0.00	10,109.29	-6,289.29	166.38	-873.83	-171.87	0.00	0.00	0.00
	0°/100ft B	•								
<b>10,288.26</b>	<b>0.00</b>	<b>0.00</b>	<b>10,197.55</b> 10,209.29 10,308.58	<b>-6,377.55</b>	<b>166.38</b>	<b>-873.83</b>	<b>-171.87</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>
10,300.00	1.17	179.64		-6,389.29	166.26	-873.83	-171.75	10.00	10.00	1,530.31
10,400.00	11.17	179.64		-6,488.58	155.52	-873.76	-161.00	10.00	10.00	0.00
10,500.00	21.17	179.64	10,404.50	-6,584.50	127.70	-873.59	-133.18	10.00	10.00	0.00
10,600.00	31.17	179.64	10,494.13	-6,674.13	83.65	-873.31	-89.13	10.00	10.00	0.00
10,700.00	41.17	179.64	10,574.75	-6,754.75	24.70	-872.94	-30.18	10.00	10.00	0.00
10,800.00	51.17	179.64	10,643.91	-6,823.91	-47.35	-872.49	41.87	10.00	10.00	0.00
FTP: 10	00ft FNL &	2178ft FWL	of Sec 12							
10,880.86	59.26	179.64	10,690.00	-6,870.00	-113.71	-872.07	108.23	10.00	10.00	0.00
10,900.00	61.17	179.64	10,699.51	-6,879.51	-130.32	-871.96	124.84	10.00	10.00	0.00
11,000.00	71.17	179.64	10,739.86	-6,919.86	-221.68	-871.39	216.20	10.00	10.00	0.00
11,100.00	81.17	179.64	10,763.72	-6,943.72	-318.66	-870.78	313.18	10.00	10.00	0.00
			FWL of Sec 12							
<b>11,185.97</b> 11,200.00	<b>89.77</b>	<b>179.64</b>	<b>10,770.50</b>	<b>-6,950.50</b>	<b>-404.28</b>	<b>-870.24</b>	<b>398.80</b>	<b>10.00</b>	<b>10.00</b>	<b>0.00</b>
	89.77	179.64	10,770.56	-6,950.56	-418.31	-870.15	412.83	0.00	0.00	0.00
11,300.00	89.77	179.64	10,770.96	-6,950.96	-518.30	-869.53	512.83	0.00	0.00	0.00
11,400.00	89.77	179.64	10,771.36	-6,951.36	-618.30	-868.90	612.83	0.00	0.00	0.00
11,500.00	89.77	179.64	10,771.76	-6,951.76	-718.30	-868.27	712.83	0.00	0.00	0.00
11,600.00	89.77	179.64	10,772.16	-6,952.16	-818.30	-867.64	812.83	0.00	0.00	0.00
11,700.00	89.77	179.64	10,772.56	-6,952.56	-918.29	-867.01	912.83	0.00	0.00	0.00
11,800.00	89.77	179.64	10,772.96	-6,952.96	-1,018.29	-866.38	1,012.83	0.00	0.00	0.00
11,900.00	89.77	179.64	10,773.36	-6,953.36	-1,118.29	-865.76	1,112.83	0.00	0.00	0.00
12,000.00	89.77	179.64	10,773.76	-6,953.76	-1,218.28	-865.13	1,212.82	0.00	0.00	0.00
12,100.00	89.77	179.64	10,774.16	-6,954.16	-1,318.28	-864.50	1,312.82	0.00	0.00	0.00
12,200.00	89.77	179.64	10,774.56	-6,954.56	-1,418.28	-863.87	1,412.82	0.00	0.00	0.00
12,300.00	89.77	179.64	10,774.96	-6,954.96	-1,518.28	-863.24	1,512.82	0.00	0.00	0.00
12,400.00	89.77	179.64	10,775.36	-6,955.36	-1,618.27	-862.61	1,612.82	0.00	0.00	0.00
12,500.00	89.77	179.64	10,775.76	-6,955.76	-1,718.27	-861.99	1,712.82	0.00	0.00	0.00
12,600.00	89.77	179.64	10,776.15	-6,956.15	-1,818.27	-861.36	1,812.82	0.00	0.00	0.00
12,700.00	89.77	179.64	10,776.55	-6,956.55	-1,918.26	-860.73	1,912.82	0.00	0.00	0.00
12,800.00	89.77	179.64	10,776.95	-6,956.95	-2,018.26	-860.10	2,012.82	0.00	0.00	0.00
12,900.00	89.77	179.64	10,777.35	-6,957.35	-2,118.26	-859.47	2,112.82	0.00	0.00	0.00
13,000.00	89.77	179.64	10,777.75	-6,957.75	-2,218.26	-858.85	2,212.82	0.00	0.00	0.00
13,100.00	89.77	179.64	10,778.15	-6,958.15	-2,318.25	-858.22	2,312.82	0.00	0.00	0.00
13,200.00	89.77	179.64	10,778.55	-6,958.55	-2,418.25	-857.59	2,412.81	0.00	0.00	0.00
13,300.00	89.77	179.64	10,778.95	-6,958.95	-2,518.25	-856.96	2,512.81	0.00	0.00	0.00
13,400.00	89.77	179.64	10,779.35	-6,959.35	-2,618.25	-856.33	2,612.81	0.00	0.00	0.00
13,500.00	89.77	179.64	10,779.75	-6,959.75	-2,718.24	-855.70	2,712.81	0.00	0.00	0.00
13,600.00	89.77	179.64	10,780.15	-6,960.15	-2,818.24	-855.08	2,812.81	0.00	0.00	0.00
13,700.00	89.77	179.64	10,780.55	-6,960.55	-2,918.24	-854.45	2,912.81	0.00	0.00	0.00
13,800.00	89.77	179.64	10,780.95	-6,960.95	-3,018.23	-853.82	3,012.81	0.00	0.00	0.00
13,900.00	89.77	179.64	10,781.35	-6,961.35	-3,118.23	-853.19	3,112.81	0.00	0.00	0.00
14,000.00	89.77	179.64	10,781.75	-6,961.75	-3,218.23	-852.56	3,212.81	0.00	0.00	0.00
14,100.00	89.77	179.64	10,782.15	-6,962.15	-3,318.23	-851.93	3,312.81	0.00	0.00	0.00

Database: Database 1

ASCENT ENERGY Company:

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well: BIG STAG FED COM 504H Wellbore: ORIGINAL WELLBORE Design:

PROPOSAL #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference:

**Survey Calculation Method:** 

Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

MD										
(usft)	Inc (°)	Azi (°)	TVD (usft)	SS (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,200.00	89.77	179.64	10,782.55	-6,962.55	-3,418.22	-851.31	3,412.81	0.00	0.00	0.00
14,300.00 14,400.00 14,500.00 14,600.00 14,700.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,782.95 10,783.35 10,783.75 10,784.15 10,784.55	-6,962.95 -6,963.35 -6,963.75 -6,964.15 -6,964.55	-3,518.22 -3,618.22 -3,718.21 -3,818.21 -3,918.21	-850.68 -850.05 -849.42 -848.79 -848.16	3,512.81 3,612.81 3,712.80 3,812.80 3,912.80	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
14,800.00 14,900.00 15,000.00 15,100.00 15,200.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,784.95 10,785.35 10,785.75 10,786.15 10,786.55	-6,964.95 -6,965.35 -6,965.75 -6,966.15 -6,966.55	-4,018.21 -4,118.20 -4,218.20 -4,318.20 -4,418.20	-847.54 -846.91 -846.28 -845.65 -845.02	4,012.80 4,112.80 4,212.80 4,312.80 4,412.80	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
15,300.00 15,400.00 15,500.00 15,600.00 15,700.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,786.95 10,787.35 10,787.75 10,788.15 10,788.54	-6,966.95 -6,967.35 -6,967.75 -6,968.15 -6,968.54	-4,518.19 -4,618.19 -4,718.19 -4,818.18 -4,918.18	-844.39 -843.77 -843.14 -842.51 -841.88	4,512.80 4,612.80 4,712.80 4,812.80 4,912.79	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
15,800.00 15,900.00 16,000.00 16,100.00 16,200.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,788.94 10,789.34 10,789.74 10,790.14 10,790.54	-6,968.94 -6,969.34 -6,969.74 -6,970.14 -6,970.54	-5,018.18 -5,118.18 -5,218.17 -5,318.17 -5,418.17	-841.25 -840.62 -840.00 -839.37 -838.74	5,012.79 5,112.79 5,212.79 5,312.79 5,412.79	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
16,300.00 16,400.00 16,500.00 16,600.00 16,700.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,790.94 10,791.34 10,791.74 10,792.14 10,792.54	-6,970.94 -6,971.34 -6,971.74 -6,972.14 -6,972.54	-5,518.17 -5,618.16 -5,718.16 -5,818.16 -5,918.15	-838.11 -837.48 -836.85 -836.23 -835.60	5,512.79 5,612.79 5,712.79 5,812.79 5,912.79	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
16,800.00 16,900.00 17,000.00 17,100.00 17,200.00	89.77 89.77 89.77 89.77 89.77	179.64 179.64 179.64 179.64 179.64	10,792.94 10,793.34 10,793.74 10,794.14 10,794.54	-6,972.94 -6,973.34 -6,973.74 -6,974.14 -6,974.54	-6,018.15 -6,118.15 -6,218.15 -6,318.14 -6,418.14	-834.97 -834.34 -833.71 -833.08 -832.46	6,012.79 6,112.79 6,212.78 6,312.78 6,412.78	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
		% 2178ft FWL								
17,295.93	89.77	179.64	10,794.80	-6,974.80	-6,514.07	-832.05	6,508.71	0.00	0.00	0.00
17,300.00	89.77	179.64	10,794.82	-6,974.82	-6,518.14	-832.02	6,512.78	0.02	0.00	-0.02
17,345.93	71ft FNL 89.77	& 2178ft FWL 179.63	_ of Sec 13 10,795.00	-6,975.00	-6,564.07	-831.73	6,558.71	0.02	0.00	-0.02

Database: Database 1

ASCENT ENERGY Company:

Project: LEA COUNTY, NEW MEXICO (NAD 83)

(GRID)

Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well: BIG STAG FED COM 504H Wellbore: ORIGINAL WELLBORE Design:

PROPOSAL #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference:

**Survey Calculation Method:** 

Well BIG STAG FED COM 504H

KB 25ft @ 3820.00usft KB 25ft @ 3820.00usft

Grid

Plan Annotations				
MD (usft)	TVD (usft)	Local Co +N/-S (usft)	ordinates +E/-W (usft)	Comment
0.00	0.00	0.00	0.00	SHL: 5ft FSL & 2216ft FEL of Sec 1
2,000.00	2,000.00	0.00	0.00	START NUDGE (2°/100ft BUR)
2,600.00	2,595.62	23.45	-58.04	EOB TO 12° INC
4,322.75	4,280.73	157.63	-390.14	END OF TANGENT
4,550.23	4,503.35	166.49	-435.74	EOT TO 269.99° AZ
6,356.68	6,270.35	166.39	-811.25	END OF TANGENT
6,956.57	6,865.86	166.38	-873.83	EOD TO VERTICAL
10,288.26	10,197.55	166.38	-873.83	KOP (10°/100ft BUR)
10,880.86	10,690.00	-113.71	-872.07	FTP: 100ft FNL & 2178ft FWL of Sec 12
11,185.97	10,770.50	-404.28	-870.24	HZ LP: 390.57ft FNL & 2178ft FWL of Sec 12
17,295.93	10,794.80	-6,514.07	-832.05	LTP: 1221ft FNL & 2178ft FWL of Sec 13
17,345.93	10,795.00	-6,564.07	-831.73	BHL: 1271ft FNL & 2178ft FWL of Sec 13

Name

**KOP - BIG STAG FED COM 504H** 

FTP - BIG STAG FED COM 504H

LTP - BIG STAG FED COM 504H

**BHL - BIG STAG FED COM 504H** 

4000-

usft/in)

(700

Depth -0009

Vertical 2000-

7500-

8000-

8500-

9000-

9500-

10000-

START NUDGE (2°/100ft BUR)

**END OF TANGENT** 

- EOT TO 269.99° AZ-

**END OF TANGENT** 

**EOD TO VERTICAL** 

KOP (10°/100ft BUR)

Vertical Section at 280.78° (700 usft/in)

**EOB TO 12° INC** 

**HZ LP - BIG STAG FED COM 504H** 

Project: LEA COUNTY, NEW MEXICO (NAD 83) (GRID) Site: SEC. 1 T21S R32E N.M.P.M. (GRID)

Well: BIG STAG FED COM 504H Wellbore: ORIGINAL WELLBORE

Design: PROPOSAL #2

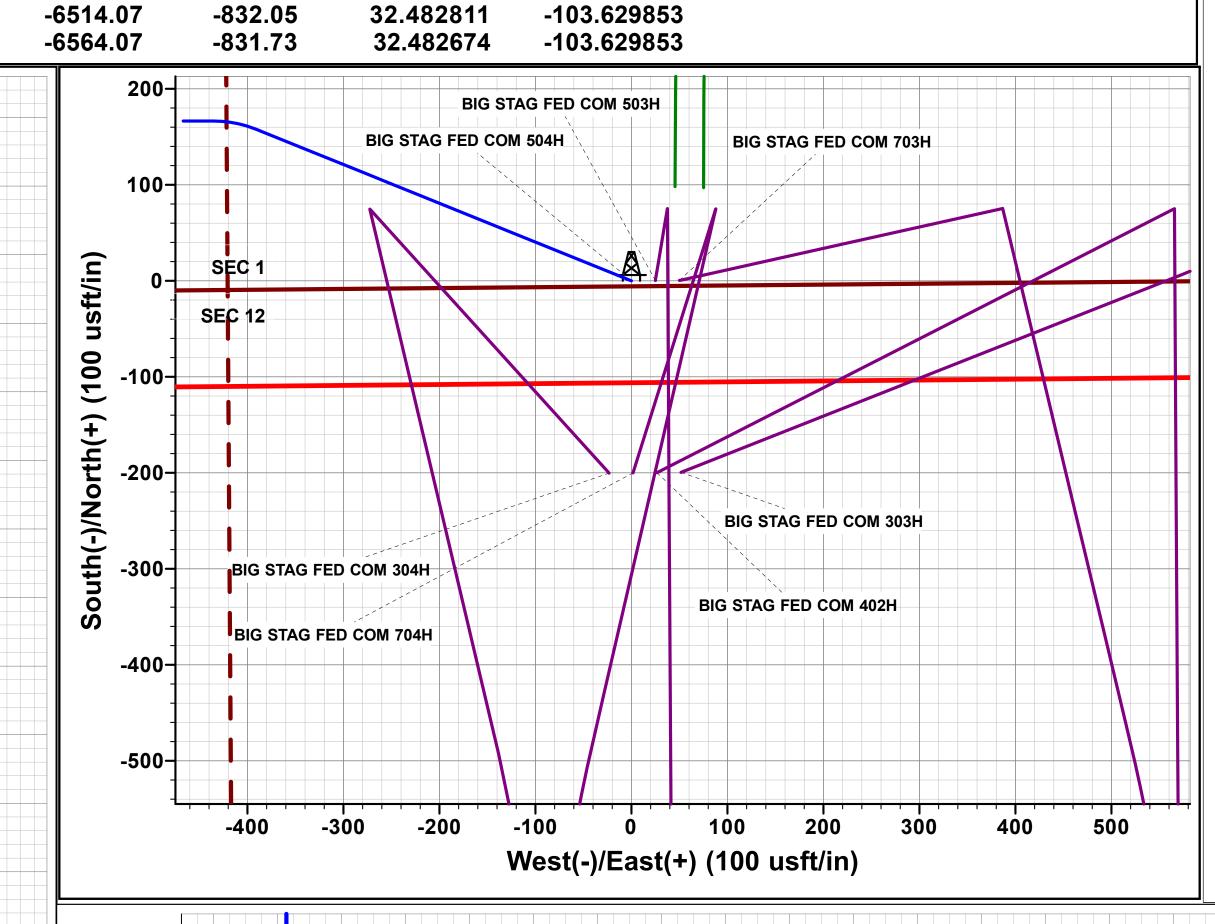
	ANNOTATIONS											
MD	Inc	Azi	TVD	+N/-S	+E/-W	VSect	Dep	Annotation				
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	SHL: 5ft FSL & 2216ft FEL of Sec 1				
2000.00	0.00	0.00	2000.00	0.00	0.00	0.00	0.00	START NUDGE (2°/100ft BUR)				
2600.00	12.00	292.00	2595.62	23.45	-58.04	-23.82	62.60	EOB TO 12° INC				
4322.75	12.00	292.00	4280.73	157.63	-390.14	-160.08	420.78	END OF TANGENT				
4550.23	12.00	269.99	4503.35	166.49	-435.74	-169.22	467.59	EOT TO 269.99° AZ				
6356.68	12.00	269.99	6270.35	166.39	-811.25	-171.49	843.11	END OF TANGENT				
6956.57	0.00	0.00	6865.86	166.38	-873.83	-171.87	905.69	EOD TO VERTICAL				
10288.26	0.00	0.00	10197.55	166.38	-873.83	-171.87	905.69	KOP (10°/100ft BUR)				
10880.86	59.26	179.64	10690.00	-113.71	-872.07	108.23	1186.05	FTP: 100ft FNL & 2178ft FWL of Sec 12				
11185.97	89.77	179.64	10770.50	-404.28	-870.24	398.80	1476.35	HZ LP: 390.57ft FNL & 2178ft FWL of Sec 12				
17295.93	89.77	179.64	10794.80	-6514.07	-832.05	6508.71	7586.27	LTP: 1221ft FNL & 2178ft FWL of Sec 13				
17345.93	89.77	179.63	10795.00	-6564.07	-831.73	6558.71	7636.27	BHL: 1271ft FNL & 2178ft FWL of Sec 13				
						WEL	LBORE 1	TARGET DETAILS (LAT/LONG)				

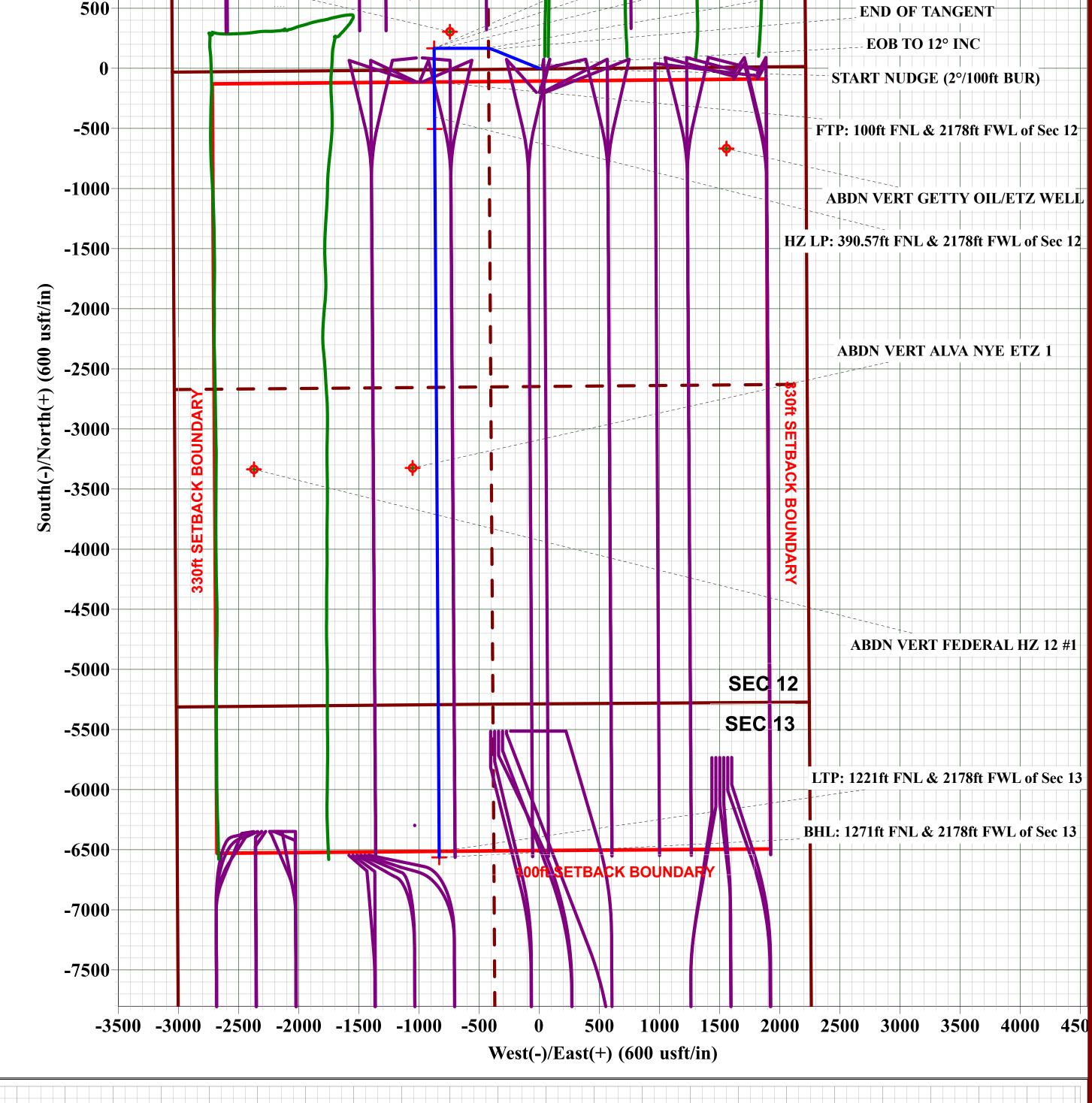
10795.00

PROPOSED LOCAL COORDINATES: SHL: 5ft FSL & 2216ft FeL Sec 1 FTP: 100ft FNL & 2178ft FWL of Sec 12

HZ LP: 390.57ft FNL & 2178ft FWL Sec 12 LTP: 1221ft FNL & 2178ft FWL of Sec 13 BHL: 1271ft FNL & 2178ft FWL of Sec 13

TVD +N/-S +E/-W Latitude Longitude -103.629846 10197.55 166.38 -873.83 32.501173 10690.00 -113.71 -872.01 32.500403 -103.629846 -504.26 -103.629847 10770.50 -869.62 32.499330 10794.80





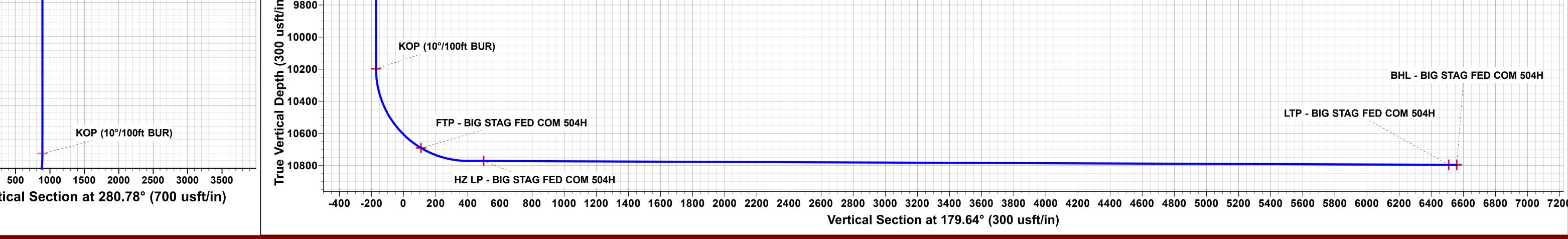
SEC 1

**KOP (10°/100ft BUR)** 

EOD TO VERTICAL

END OF TANGENT

**EOT TO 269.99° AZ** 



1500

\_ ABDN VERT | EDERAL ONE #1

ABDN VERT SHEPHARD B FED

Ascent Energy respectfully requests approval on the Big Stagg Fed Com 603H (proposed name change to: Big Stag Fed Com 504H) for an option to:

- Addition of an External Casing Packer on the 9-5/8" Casing
- Increase the casing size of our vertical casing strings
- Revise proposed BOP beneath the base of the 20" surface shoe to setting the 1st Intermediate casing string only (13 3/8").

The reason for the request is based on improved drilling efficiencies and improved cementing in-place for each casing string. We believe the larger casing diameters in the vertical section will increase the likelihood of getting cement to surface for each string.

There will be no change in Geology formations, and mud specifications.

#### **External Casing Packer:**

The pending hole conditions the addition of an External Casing Packer to the Intermediate #2 9-5/8" casing string is requested. A DV Tool is already approved, and the cement volumes will not change with the addition of an External Casing Packer.

#### New/Optional proposed design:

#### Casing:

			INTERVAL (ft)					FORMATION	MW @	SAFETY FACTORS			
DESCRIPTION	Hole Size (in)	CSG Size	TOP MD	B1 TVD	Γ <b>M</b> MD	WEIGHT (ppf)	GRADE	COUPLING	PRESS @ CSG DEPTH (PPG)	CSG DEPTH (PPG)	BURST (psi)	COLLAPSE (psi)	TENSION (1000 lbs)
CONDUCTOR	36	30	0	120	120			WELD					
CONDUCTOR	30	30	U	120	120			WELD					
SURFACE	26	20	0	1.600	1.600	94	J-55	BTC	8.3	9.0	2,110	520	1480
SURFACE	20	20	U	1,600	1,600	94	J-55	ыс	0.3	9.0	2.8	2.7	9.8
INT. #1	17.5	13.375	0	3.600	3.627	54.5	J-55	BTC	8.3	10.0	2,730	1,130	853
IIN1.#1	17.5	13.375	U	3,600	3,627	54.5	J-55	BIC	8.3	10.0	1.5	1.6	4.3
INT. #2	12.25	9.625	0	5.600	5,671	40	J-55	BTC	8.3	9.2	3,950	2,570	630
IIN1.#Z	12.25	9.025	U	5,600	5,671	40	J-55	ыс	0.3	9.2	1.1	3.2	2.8
PRODUCTION	8.75	5.5	0	10.795	17.345	20	P-110	BTC	8.7	9.6	12,630	11,100	641
PRODUCTION	0.75	5.5	U	10,795	17,345	20	P-110	ыс	0.7	9.0	3.5	2.7	1.8

#### Cement:

DESCRIPTION	HOLE	CSG	ТОР	втм	LENGTH	SLURRY DESCRIPTION	FT <sup>3</sup>	EXCESS	WEIGHT	YIELD
DESCRIPTION	(IN)	(IN)	101	DIW	(FT)	SLUKKT DESCRIPTION	SACKS	EXCESS	(ppg)	(FT <sup>3</sup> /SK)
CONDUCTOR	36	30	0	120	120	Class G	518	100%	15.8	1.17
CONDUCTOR	30	30	0	120	120	Class G	443	10076	13.0	1.17
SURFACE - LEAD	26	20	0	1,100	1,100	Class C	3203	100%	13.5	1.72
SONI ACE - LEAD	20	20	0	1,100	1,100	Ciass C	1862	10076	10.0	1.72
SURFACE - TAIL	26	20	1,100	1,600	500	Class C	1506	100%	14.8	1.33
OUTH AGE TAIL	20	20	1,100	1,000	300	0.000 0	1132	10070	14.0	1.55
INT #1 - LEAD	17.5	13.375	0	3,127	3,127	Class C	3488	75%	12.7	2.32
INT #1 LEAD	17.0	10.070	0	5,127	0,127	Ciass C	1503	7570	12.1	2.02
INT #1 - TAIL	17.5	13.375	3,127	3,627	500	Class C	608	75%	14.8	1.33
117. 77. 17.02	17.0	10.070	0,121	0,021	000	0.000 0	457	1070	1 1.0	1.00
INT #2 - LEAD	12.25	9.625	0	5,171	5,171	50/50Poz Class C	2283	100%	11.5	2.2
1111 //2 EE/18	12.20	0.020		0,171	0,171		1038	10070	11.0	
INT #2 - TAIL	12.25	9.625	5,171	5,671	500	Class C	313	100%	14.8	1.33
		0.020	0,	0,0	000		236	10070		
INT #2 - DV LEAD	12.25	9.625	0	3,177	3,177	50/50Poz Class C	1104	50%	11.5	2.2
				-,	-,		502			
INT # 2 - DV TAIL	12.25	9.625	3,177	3,677	500	Class C	235	50%	14.8	1.33
		0.000	-,	-,			177			
PRODUCTION - LEAD	8.75	5.5	0	9,000	9,000	Nine Lite	2488	20%	11.0	2.48
				-,,,,,	-,,,,,,	**	1003			
PRODUCTION - TAIL	8.75	5.5	9,000	17,345	8,345	35/65 Poz Class H	2530	20%	13.2	1.47
	2.70	5.0	2,300	,0.10	2,3.0		1721	=370		

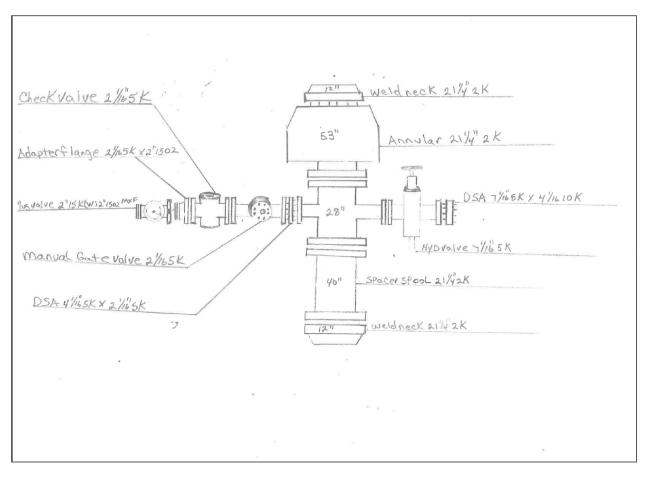
Note: Int 2 is two stage cement job. DVT and External Casing packer to be placed @ approximately 3,677' MD. 50ft from previous casing shoe and will be adjusted real time

#### **New Proposed BOP:**

From the Base of the 20" Surface pipe, the well will be equipped with a 2M Annular system. Before drilling out the 20" surface pipe, the 2M system will be tested to 250psi low and 1000psi high by an 3<sup>rd</sup> party service company. The 2M BOPE and related equipment will meet or exceed the requirements of a 2M psi system as set forth in On Shore Order No. 2 while drilling below the 20" surface shoe and to TD of Intermediate #1 (13-3/8" Casing). Once the Intermediate #1 13-3/8" Casing is cemented the 20" 2M BOPE and 21-1/4" wellhead will be removed and a 13-5/8" Multi-bowl wellhead and previously permitted 13-5/8" 5M BOPE will be installed. From the base of the Intermediate #1 13-3/8" casing string through running of the 5-1/2" production string the 5M BOPE will be equipped.

The previously permitted 5M choke will be utilized in conjunction with the 2M Annular System.

# ASCENT ENERGY 2M ANNULAR BOPE & DIAGRAM



1-21S-32E-O ATS-19-3155 Big Stagg Fed Com 603H Sundry Lea NMNM127892 Ascent Energy LLC 13-22 06-01-2021 Yolanda Jimenez

Big Stagg Fed Com 603H

20	surface o	-	26	inch hole.		<u>Design</u>				Surface		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	94.00	J	55	BTC	9.32	0.7	1.12	1,600	3	1.94	1.31	150,40
"B"				BTC				0				0
	g mud, 30min Sf			Tail Cmt	does not	circ to sfc.	Totals:	1,600				150,40
	f Proposed to											
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
26	1.5053	2994	4708	2409	95	9.00	1086	2M				2.50
13 3/8	casing ins	side the	20			<u>Design l</u>	Factors			Int 1		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	54.50	J	55	втс	4.35	0.6	1.01	3,600	1	1.87	1.05	196,20
"B"								0				Ó
w/8.4#/	g mud, 30min Sf	c Csg Test psig:					Totals:	3,600	_			196,20
1	The cement vo	olume(s) are	intended to ac	chieve a top of	0	ft from su	rface or a	1600				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
			CEt Ct	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
Size	Volume	Cmt Sx	CuFt Cmt	ouit	70 EX0000	WIGG VVC	1117 101	BOLL				
<b>Size 17 1/2</b> lass 'H' tail cm	0.6946	1960	4095	3020	36	10.00	1463	2M			,	1.56
17 1/2 lass 'H' tail cm	0.6946 at yld > 1.20	1960		3020	36	10.00  Design Fa	1463			Int 2	,	
17 1/2 lass 'H' tail cm 9 5/8 Segment	0.6946 at yld > 1.20  casing ins #/ft	1960 Side the Grade	4095	3020  Coupling	36 Body	10.00  Design Fa Collapse	1463  ctors  Burst	2M	B@s	а-В	<b>a-C</b>	Weigh
17 1/2 lass 'H' tail cm 9 5/8 Segment "A"	0.6946 at yld > 1.20	1960 Side the Grade	4095	3020	36	10.00  Design Fa	1463	2M Length 5,600	<b>B@s</b>		<b>a-C</b> 1.78	Weigh 224,00
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B"	0.6946 at yld > 1.20 casing ins #/ft 40.00	1960 side the Grade	4095 <b>13 3/8</b> 55	3020  Coupling	36 Body	10.00  Design Fa Collapse	ctors Burst 0.73	2M Length 5,600 0	_	а-В		Weigh 224,00
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B" w/8.4#/	0.6946 at yld > 1.20  casing ins #/ft 40.00	1960  Side the Grade  Grade  C Csg Test psig:	4095 13 3/8 55 321	3020  Coupling BTC	36 Body 2.81	Design Fa Collapse 0.96	1463  Cotors  Burst 0.73  Totals:	2M Length 5,600 0 5,600	_	а-В	1.78	Weigh 224,00 0 224,00
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B" w/8.4#/	0.6946 at yld > 1.20  casing ins #/ft 40.00  /g mud, 30min Sfi The cement vo	1960  Side the Grade J c Csg Test psig: blume(s) are	4095  13 3/8  55  321 intended to ac	3020  Coupling BTC  Chieve a top of	36  Body 2.81	Design Fa Collapse 0.96	1463  Cotors  Burst 0.73  Totals: rface or a	2M Length 5,600 0 5,600 3600	_	а-В	1.78	Weigh 224,00 0 224,00 overlap.
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B" w/8.4#/ Hole	0.6946 at yld > 1.20  casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo	1960  Side the Grade J c Csg Test psig: olume(s) are 1 Stage	4095  13 3/8  55  321 intended to ac 1 Stage	3020  Coupling BTC  Chieve a top of Min	36  Body 2.81  0 1 Stage	Design Fa Collapse 0.96  ft from su Drilling	1463  Cotors  Burst 0.73  Totals:  rface or a Calc	2M Length 5,600 0 5,600 3600 Req'd	_	а-В	1.78	Weigh 224,00 0 224,00 overlap. Min Dis
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B" w/8.4#/	0.6946 at yld > 1.20  casing ins #/ft 40.00  /g mud, 30min Sfi The cement vo	1960  Side the Grade J c Csg Test psig: blume(s) are	4095  13 3/8  55  321 intended to ac	3020  Coupling BTC  Chieve a top of	36  Body 2.81	Design Fa Collapse 0.96	1463  Cotors  Burst 0.73  Totals: rface or a Calc MASP	2M Length 5,600 0 5,600 3600	_	а-В	1.78	Weigh 224,00 0 224,00 overlap. Min Dis
17 1/2 lass 'H' tail cm 9 5/8 Segment "A" "B" w/8.4#/ Hole Size 12 1/4	casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo Annular Volume	1960 Side the Grade J c Csg Test psig: blume(s) are 1 Stage Cmt Sx 1274	13 3/8 55 321 intended to ac 1 Stage CuFt Cmt 2597	3020  Coupling BTC  Chieve a top of Min Cu Ft	Body 2.81  0 1 Stage % Excess	Design Fa Collapse 0.96  ft from su Drilling Mud Wt	1463  Cotors  Burst 0.73  Totals:  rface or a Calc	2M Length 5,600 0 5,600 3600 Req'd BOPE	_	а-В	1.78	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cp
17 1/2 lass 'H' tail cm  9 5/8  Segment "A" "B"  w/8.4#/ Hole Size 12 1/4  urst Frac Grad	casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo Annular Volume 0.3132 dient(s) for Segi	side the Grade J c Csg Test psig: olume(s) are 1 Stage Cmt Sx 1274 ment(s): A, B,	4095  13 3/8  55  321 intended to ac     1 Stage     CuFt Cmt     2597  . C, D = 0.71,	3020  Coupling BTC  Chieve a top of Min Cu Ft	Body 2.81  0 1 Stage % Excess	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20	ctors Burst 0.73  Totals: rface or a Calc MASP 3009	2M Length 5,600 0 5,600 3600 Req'd BOPE	_	<b>a-B</b> 1.31	1.78	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cp
9 5/8  9 5/8  Segment "A" "B"  w/8.4#/ Hole Size 12 1/4  urst Frac Grad	casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo Annular Volume 0.3132 dient(s) for Segi	side the Grade  J c Csg Test psig: blume(s) are 1 Stage Cmt Sx 1274 ment(s): A, B,	13 3/8 55 321 intended to ac 1 Stage CuFt Cmt 2597	Coupling BTC  Chieve a top of Min Cu Ft 1932	Body 2.81 0 1 Stage % Excess 34	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20	ctors Burst 0.73  Totals: rface or a Calc MASP 3009	2M Length 5,600 0 5,600 3600 Req'd BOPE 5M	Ĭ	a-B 1.31	1.78	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cp 0.81
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B" w/8.4#/ Hole Size 12 1/4 urst Frac Grad  5 1/2 Segment	casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo Annular Volume 0.3132 dient(s) for Seg	side the Grade J c Csg Test psig: blume(s) are 1 Stage Cmt Sx 1274 ment(s): A, B,	4095  13 3/8  55  321 intended to ac 1 Stage CuFt Cmt 2597  . C, D = 0.71, 9 5/8	Coupling BTC  Chieve a top of Min Cu Ft 1932  Coupling	Body 2.81  0 1 Stage % Excess 34	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20  Design Collapse	ctors Burst 0.73  Totals: rface or a Calc MASP 3009  Factors Burst	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M	1 B@s	a-B 1.31 Prod 1 a-B	1.78	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cr 0.81
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B"  w/8.4#/ Hole Size 12 1/4 urst Frac Grad	casing ins #/ft 40.00 /g mud, 30min Sfi The cement vo Annular Volume 0.3132 dient(s) for Segi	side the Grade J c Csg Test psig: blume(s) are 1 Stage Cmt Sx 1274 ment(s): A, B,	4095  13 3/8  55  321 intended to ac     1 Stage     CuFt Cmt     2597  . C, D = 0.71,	Coupling BTC  Chieve a top of Min Cu Ft 1932	Body 2.81 0 1 Stage % Excess 34	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20	ctors Burst 0.73  Totals: rface or a Calc MASP 3009	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M  Length 17,345	Ĭ	a-B 1.31	1.78	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cr 0.81
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B"  w/8.4#/ Hole Size 12 1/4 urst Frac Grad  5 1/2 Segment "A" "B"	casing ins #/ft 40.00  /g mud, 30min Sfr The cement vo Annular Volume 0.3132  dient(s) for Seg  casing ins #/ft 20.00	1960  side the Grade  J c csg Test psig: olume(s) are 1 Stage Cmt Sx 1274  ment(s): A, B, side the Grade P	4095  13 3/8  55  321 intended to ac 1 Stage CuFt Cmt 2597  .C, D = 0.71, 9 5/8  110	Coupling BTC  Chieve a top of Min Cu Ft 1932  Coupling	Body 2.81  0 1 Stage % Excess 34	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20  Design Collapse	ctors Burst 0.73  Totals: urface or a Calc MASP 3009  Factors Burst 2.35	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M  Length 17,345 0	1 B@s	a-B 1.31 Prod 1 a-B	1.78	Weigl 224,00 0 224,00 overlap. Min Dis Hole-Cţ 0.81
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B" w/8.4#/ Hole Size 12 1/4 urst Frac Grad  5 1/2 Segment "A" "B" w/8.4#/	casing ins #/ft 40.00  g mud, 30min Sfo The cement vo Annular Volume 0.3132  dient(s) for Seg casing ins #/ft 20.00	at 1960  Side the Grade  J  C Csg Test psig: plume(s) are 1 Stage Cmt Sx 1274  ment(s): A, B, side the Grade P  C Csg Test psig:	4095  13 3/8  55  321 intended to ac 1 Stage CuFt Cmt 2597  .C, D = 0.71, 9 5/8  110  2,375	Coupling BTC  Chieve a top of Min Cu Ft 1932  Coupling	Body 2.81  0 1 Stage % Excess 34	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20  Design Collapse	ctors Burst 0.73  Totals: urface or a Calc MASP 3009  Factors Burst 2.35  Totals:	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M  Length 17,345	1 B@s	a-B 1.31 Prod 1 a-B	1.78 a-C 3.68	Weigl 224,00 0 224,00 overlap. Min Dis Hole-Cr 0.81 Weigl 346,90
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B" w/8.4#/ Hole Size 12 1/4 urst Frac Grad  5 1/2 Segment "A" "B" w/8.4#/	casing ins #/ft 40.00  g mud, 30min Sfo The cement vo Annular Volume 0.3132  dient(s) for Seg casing ins #/ft 20.00	at 1960  Side the Grade  J  C Csg Test psig: plume(s) are 1 Stage Cmt Sx 1274  ment(s): A, B, side the Grade P  C Csg Test psig:	4095  13 3/8  55  321 intended to ac 1 Stage CuFt Cmt 2597  .C, D = 0.71, 9 5/8  110  2,375	Coupling BTC  Chieve a top of Min Cu Ft 1932  Coupling BTC	Body 2.81 0 1 Stage % Excess 34 Body 2.97	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20  Design Collapse 2.06	ctors Burst 0.73  Totals: urface or a Calc MASP 3009  Factors Burst 2.35  Totals:	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M  Length 17,345 0 17,345 5600	1 B@s	a-B 1.31 Prod 1 a-B	1.78 a-C 3.68	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cp 0.81 Weigh 346,90 0
17 1/2 lass 'H' tail cm  9 5/8 Segment "A" "B" w/8.4#/ Hole Size 12 1/4 urst Frac Grad  5 1/2 Segment "A" "B" w/8.4#/	casing ins #/ft 40.00  /g mud, 30min Sfr The cement vo Annular Volume 0.3132  dient(s) for Seg casing ins #/ft 20.00  /g mud, 30min Sfr	side the Grade J c Csg Test psig: blume(s) are 1 Stage Cmt Sx 1274 ment(s): A, B, side the Grade P c Csg Test psig: blume(s) are	4095  13 3/8  55  321 intended to ac 1 Stage CuFt Cmt 2597  .C, D = 0.71, 9 5/8  110  2,375 intended to ac	Coupling BTC  Chieve a top of Min Cu Ft 1932  Coupling BTC	Body 2.81 0 1 Stage % Excess 34 Body 2.97	Design Fa Collapse 0.96  ft from su Drilling Mud Wt 9.20  Design Collapse 2.06	ctors Burst 0.73  Totals: rface or a Calc MASP 3009  Factors Burst 2.35  Totals: rface or a	2M  Length 5,600 0 5,600 3600 Req'd BOPE 5M  Length 17,345 0 17,345	1 B@s	a-B 1.31 Prod 1 a-B	1.78 a-C 3.68	Weigh 224,00 0 224,00 overlap. Min Dis Hole-Cr 0.81 Weigh 346,90 0 346,90 overlap.

Carlsbad Field Office 6/1/2021

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL Sundry

OPERATOR'S NAME: | Ascent Energy LLC

**LEASE NO.:** | NMNM127892

WELL NAME & NO.: Big Stagg Federal Com 603H

**SURFACE HOLE FOOTAGE:** 5'/S & 2216'/E **BOTTOM HOLE FOOTAGE** 1271'/N & 2178'/W

**LOCATION:** | Section 1, T.21 S., R.32 E., NMPM

**COUNTY:** Lea County, New Mexico

#### COA

H2S	• Yes	○ No	
Potash	None	© Secretary	© R-111-P
Cave/Karst Potential	• Low	© Medium	○ High
Cave/Karst Potential	Critical		
Variance	© None	Flex Hose	Other
Wellhead	Conventional	Multibowl	○ Both
Other	☐ 4 String Area	☑ Capitan Reef	□WIPP
Other	Fluid Filled	☐ Cement Squeeze	☐ Pilot Hole
Special Requirements	☐ Water Disposal	<b>☑</b> COM	□ Unit

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Bone Spring** formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

#### **B. CASING**

Surface, Intermediate 1, and Intermediate 2 casing must be kept fluid filled to meet BLM minimum collapse requirement.

1. The **20 inch** surface casing shall be set at approximately **1600 feet** (a minimum of **25 feet** (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface.

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- a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 13-3/8 inch Intermediate 1 casing shall be set at approximately 3600 feet and the minimum required fill of cement behind the Intermediate 1 casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above.

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

- ❖ In <u>R111 Potash Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following:
   (Use this for 3 string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the capitan interval)
  - Switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
  - Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.

Page 2 of 10 BIG STAGG FEDERAL COM #603H (SUNDRY) 3. The minimum required fill of cement behind the 9-5/8 inch Intermediate 2 casing is:

#### Option 1

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### Option 2

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above.

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

- 4. The minimum required fill of cement behind the **5-1/2 inch** production casing with a tie-back to the surface is:
  - Cement should tie-back at least **50 feet** on top of Capitan Reef top. If cement does not circulate see B.1.a, c-d above.

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

PRODUCTION CASING HAS AN EXCESS OF 13%. ADDITIONAL CEMENT MAY BE NEEDED.

#### C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

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- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **2000 (2M)** psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
- 3. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the intermediate 1 and 2 casing shoe shall be **5000 (5M)** psi.
  - f. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - g. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - h. Manufacturer representative shall install the test plug for the initial BOP test.
  - i. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - j. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

#### D. SPECIAL REQUIREMENT (S)

#### **Communitization Agreement**

• The operator will submit a Communitization Agreement to the Carlsbad Field Office, 620 E Greene St. Carlsbad, New Mexico 88220, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or

Page 4 of 10 BIG STAGG FEDERAL COM #603H (SUNDRY) certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.

- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

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#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - Eddy County
     Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575)
     361-2822
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

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#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

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#### B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including

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- lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

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#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

YJ 06/01/2021

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District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

District II 811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 30147

#### **CONDITIONS**

Operator:	OGRID:
ASCENT ENERGY, LLC.	325830
1125 17th St	Action Number:
Denver, CO 80202	30147
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	None	7/26/2021