Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMLC064790 **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: Oil Well 1b. Type of Well: Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing Single Zone ✓ Multiple Zone SPANISH BAY 18/19 FED COM 526H 9. API Well No. 2. Name of Operator 30-025-53642 MEWBOURNE OIL COMPANY 3a. Address 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 Tonto/Bone Spring 4. Location of Well (Report location clearly and in accordance with any State requirements.*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 18/T19S/R33E/NMP At surface NWNE / 205 FNL / 1500 FEL / LAT 32.6669997 / LONG -103.698657 At proposed prod. zone SWSE / 100 FSL / 1980 FEL / LAT 32.6388082 / LONG -103,7003061 14. Distance in miles and direction from nearest town or post office* 12. County or Parish 13. State NM LEA 10 miles 15. Distance from proposed* 16. No of acres in lease 17. Spacing Unit dedicated to this well 210 feet location to nearest property or lease line, ft. 320.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 10008 feet / 20054 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start* 23. Estimated duration 3648 feet 08/04/2024 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 06/17/2024 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 09/25/2024 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the

Conditions of approval, if any, are attached. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency



applicant to conduct operations thereon.

eived by C-10)/3/2024 10:			State of Nev			Page 2 Revised July 9, 2024					
C li urit	el		En	C5 -		al Resources Departn TION DIVISION	nent						
	Electronicall Dermitting	У		OIL	CONSLICAT	TION DIVISION		Submit	☑ Initial Su	bmittal			
								Type:	☐ Amended	☐ Amended Report			
									☐ As Drille	d			
					WELL LOCAT	TION INFORMATION							
	0-025-53	3642	Pool Code	59470	6	Pool Name TONTO; BONE SPRING, SOUTH							
Propert	y Code 334598		Property Na	SP	ANISH BAY	′ 18/19 FED CC	M		Well Number	^{er} 526H			
OGRID	^{No.} 14	744	Operator N	ame ME	WBOURNE	OIL COMPAN	ΙΥ		Ground Lev	el Elevation 3648			
Surface	Owner: 🗆 S	State □ Fee □	Tribal 🛚 Fed	leral		Mineral Owner: □	State □ Fee	□ Tribal	XFederal				
					Surfa	ace Location							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
В	18	19S	33E		205 FNL	1500 FEL	32.6669	9997	-103.6986570	LEA			
					Bottom	Hole Location							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
0	19	19S	33E		100 FSL	1980 FEL	32.638	8082	-103.7003061	LEA			
	ı	ı	1	I	<u>l</u>								
	ted Acres 20	Infill or Defin	Defining	Well API	Overlapping Spacing N/A	Unit (Y/N)	Consolie N/A	dation Code					
Order N	Numbers. N/A	١		1		Well setbacks are un	der Common (Ownershij	p: □Yes □No				
					Kick ()	ff Point (KOP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
В	18	19	33		10 FNL	1980 FEL	32.667	5438	-103.7002133	LEA			
					First Ta	ake Point (FTP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
В	18	19	33		100 FNL	1980 FEL	32.667	2965	-103.7002147	LEA			
	1				Last Ta	ke Point (LTP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
0	19	19	33		100 FSL	1980 FEL	32.638	8082	-103.7003061	LEA			
					ı								
Unitize	d Area or Ar	ea of Uniform I	nterest	Spacing	Unit Type 🛚 Horiz	contal Vertical	Grou	nd Floor I	Elevation: 3648				
ODED :	TOP CERT	TEICATIONS				CLIDVEVOD CEDTER	CATIONS						
		IFICATIONS				SURVEYOR CERTIFIC	CATIONS						
my know organiza including location interest,	eledge and beli ution either own g the proposed pursuant to a or to a volunto	ef, and, if the weli ns a working inter bottom hole loca contract with an c ary pooling agree	l is a vertical or rest or unleased tion or has a rig owner of a work	directional water wineral intendent to drill thing interest o	rest in the land	I hereby certify that the w surveys made by me or und my belief.							
	by the division.												
consent of	of at least one tract (in the tar		rest or unleas ny part of the	sed mineral interest well's completed									
		Vhitley			3/24								
Signature			Date		-	Signature and Seal of Profes	sional Surveyor						
(CONNE	R WHITL	ΕY										
Printed N						Certificate Number	Date of Surve	ey					
	WILLIAM	EVANE	MDOLID	NE CO	N /								

Note: No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

Email Address

1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

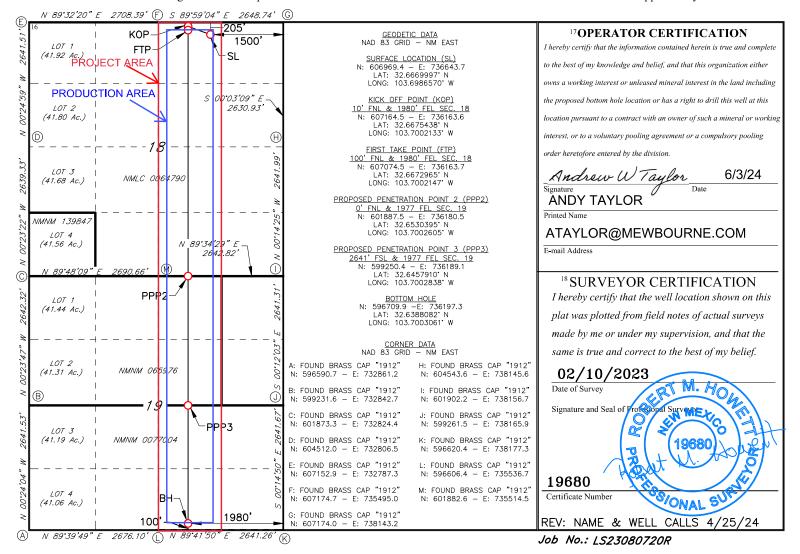
☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

¹ API Numbe	² Pool Code 59476						
⁴ Property Code		pperty Name 6 Well Nut					
7 OGRID NO. 14744		perator Name E OIL COMPANY	⁹ Elevation 3648				

¹⁰ Surface Location													
UL or lot no.	Section	ection Township		Lot Idn	Feet from the	North/South line	Feet From the	East/West line	County				
В	18	19S	33E	205		NORTH	1500	EAST	LEA				
11 Bottom Hole Location If Different From Surface													
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County				
0	19	19S	33E		100	SOUTH	1980	EAST	LEA				
12 Dedicated Acres	13 Joint	or Infill	4 Consolidation	Code 15 (Order No.								
320													

No allowable will be assigned to this completion until all interest have been consolidated or a non-standard unit has been approved by the division.



State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

	17	ATURAL G	AS MANAU	JEMIENI P	LAN			
This Natural Gas Manag	ement Plan m	ust be submitted w	ith each Applicat	ion for Permit to I	Orill (APD) for a	new or	recompleted well.	
			1 – Plan Deffective May 25,					
I. Operator: Mew	/bourne (Oil Co.	OGRID:	14744	Date:	<u>5/2</u>	/24	
II. Type: ✗ Original □	Amendment	due to □ 19.15.27	.9.D(6)(a) NMA	C □ 19.15.27.9.D((6)(b) NMAC □	Other.		
If Other, please describe:								
III. Well(s): Provide the be recompleted from a si					wells proposed to	be dril	lled or proposed to	
Well Name	API	ULSTR	Footages	Anticipated Oil BBL/D	Anticipated Gas MCF/D		Anticipated Produced Water BBL/D	
SPANISH BAY 18/19 FED COM 526	ł	B 18 19S 33E	205' FNL x 1500' F	√L 1500	1000		3000	
				Y1: 400, Y2:300, Y3:200	Y1: 800, Y2: 500, Y3: 300		Y1: 1500, Y2: 1000, Y3: 500	
IV. Central Delivery Po V. Anticipated Schedule proposed to be recomple	e: Provide the	following informa	ntion for each new				7.9(D)(1) NMAC] sed to be drilled or	
Well Name	API	Spud Date	TD Reached Date	Completion Commencement			First Production Date	
SPANISH BAY 18/19 FED COM 526	1	7/2/24	8/2/24	9/2/24	9/17	//24	9/17/24	
VI. Separation Equipm VII. Operational Pract Subsection A through F of the VIII. Best Managemen during active and planner	ices: ☑ Attac of 19.15.27.8 t Practices: §	ch a complete desc NMAC. Attach a comple	ription of the act	ions Operator wil	I take to comply	with th	ne requirements of	

Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

X Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF			

X. Natural Gas Gathering System (NGGS):

Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in				

XI. Map. \Box Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

XII. Line Capacity. The natural gas gathering system \square will \square will not have capacity to gather 100% of the anticipated natural gas production volume from the well prior to the date of first production.

XIII. Line Pressure. Operator \square does \square does not anticipate that its existing well(s) connected to the same segment, or portion, of the natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by the new well(s).

☐ Attach Operator's plan to manage production in response to the increased line pressure.

XIV. Confidentiality: □ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information provided in Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information for which confidentiality is asserted and the basis for such assertion.

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Section 3 - Certifications Effective May 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan.

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) (b) power generation for grid; compression on lease; (c) liquids removal on lease; (d) reinjection for underground storage; (e) reinjection for temporary storage; **(f)** reinjection for enhanced oil recovery; **(g)**

Section 4 - Notices

1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:

other alternative beneficial uses approved by the division.

fuel cell production; and

(h)

- (a) Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- (b) Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

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I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature:	Bradley Bishop
Printed Name:	BRADLEY BISHOP
Title:	REGULATORY MANAGER
E-mail Address:	BBISHOP@MEWBOURNE.COM
Date:	5/2/24
Phone:	575-393-5905
-	OIL CONSERVATION DIVISION
	(Only applicable when submitted as a standalone form)
Approved By:	
Title:	
Approval Date:	
Conditions of Ap	proval:

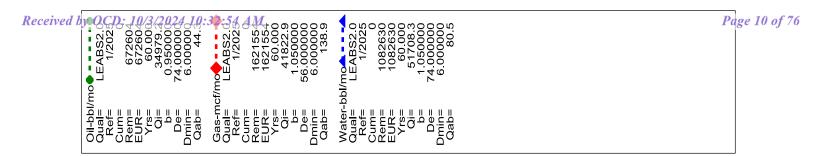
Mewbourne Oil Company

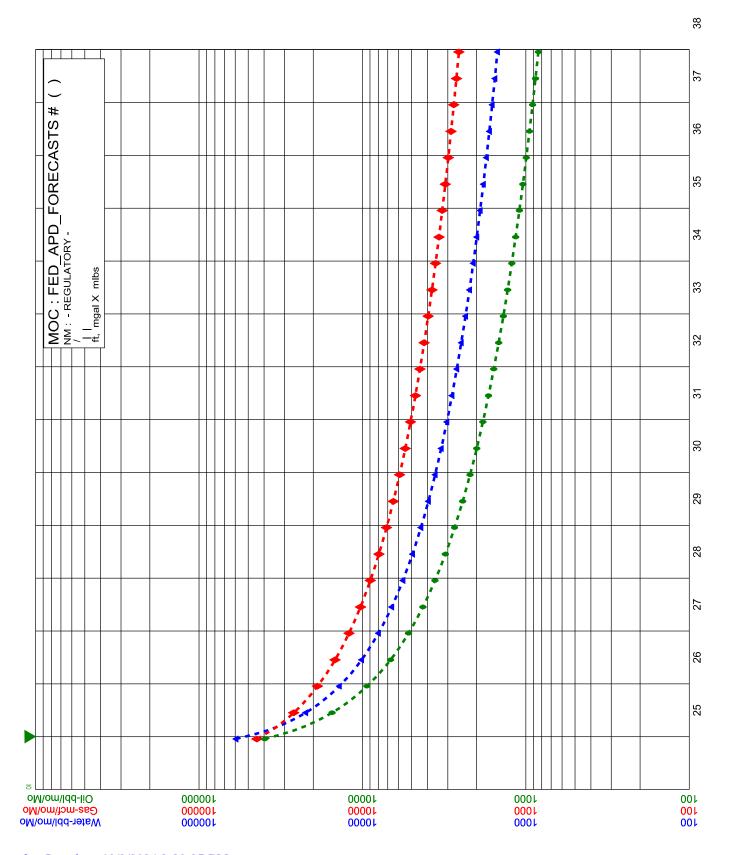
Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
 - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
 - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
 - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
 - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
 - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
 - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.







U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Drilling Plan Data Report

Submission Date: 06/17/2024

Operator Name: MEWBOURNE OIL COMPANY

Well Name: SPANISH BAY 18/19 FED COM

Well Type: OIL WELL

APD ID: 10400098866

Well Number: 526H

Well Work Type: Drill

Highlighted data reflects the most recent changes

Show Final Text

Section 1 - Geologic Formations

Formation ID	Formation Name	Elevation	True Vertical	Measured Depth	Lithologies	Mineral Resources	Producing Formatio
14214191	UNKNOWN				OTHER : Topsoil	NONE	N
14214204	RUSTLER	RUSTLER 2258		1387	ANHYDRITE, DOLOMITE	USEABLE WATER	N
14214205	TOP SALT	TOP SALT 1963 1682 1682 SALT		SALT	NONE	N	
14214192	BASE OF SALT 713 2932 2932		SALT	SALT NONE			
14214206	14214206 YATES		3166	3166	SANDSTONE	NATURAL GAS, OIL	N
14214189	214189 CAPITAN REEF		3519	3519	DOLOMITE, LIMESTONE	USEABLE WATER	N
14214203	QUEEN	-488	4133	4133	DOLOMITE, SANDSTONE	NATURAL GAS, OIL	N
14214196	LAMAR	-2162	5807	5807	DOLOMITE, LIMESTONE	NATURAL GAS, OIL	N
14214190	BONE SPRING	-4007	7652	7652	LIMESTONE	NATURAL GAS, OIL	N
14214193	BONE SPRING 1ST	-5188	8833	8833	SANDSTONE	NATURAL GAS, OIL	Y
14214207	BONE SPRING 2ND	-5737	9382	9382	SANDSTONE	NATURAL GAS, OIL	Y

Section 2 - Blowout Prevention

Pressure Rating (PSI): 5M Rating Depth: 20054

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

Choke Diagram Attachment:

Spanish_Bay_18_19_Fed_Com_526H_5M_BOPE_Choke_Diagram_20240605074003.pdf Spanish_Bay_18_19_Fed_Com_526H_Flex_Line_Specs_API_16C_20240605074012.pdf Spanish_Bay_18_19_Fed_Com_526H_5M_Multi_Bowl_WH_20240905163258.pdf

BOP Diagram Attachment:

Spanish_Bay_18_19_Fed_Com_526H_5M_BOPE_Schematic_20240605074113.pdf
Mewbourne Break Testing Variance 20240605074127.pdf

Section 3 - Casing

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	17.5	13.375	NEW	API	N	0	1480	0	1480	3648	2168	1480	H-40	48	ST&C	1.16	2.61	DRY	4.53	DRY	7.62
2	INTERMED IATE	12.2 5	9.625	NEW	API	N	0	3300	0	3300	2968	348	3300	J-55	36	LT&C	1.15	2.01	DRY	2.37	DRY	2.95
3	INTERMED IATE	12 . 2 5	9.625	NEW	API	N	3300	4300	3300	4300	348	-652	1000	J-55	40	LT&C	1.13	1.73	DRY	7.18	DRY	8.7
4	INTERMED IATE	12.2 5	9.625	NEW	API	N	4300	5110	4300	5110	-652	-1462	810	L-80	40	LT&C	1.14	2.12	DRY	22.7 5	DRY	28.2
5	PRODUCTI ON	8.75	7.0	NEW	API	N	0	9270	0	9270	2968	-5622	9270	P- 110	26	LT&C	1.34	2.14	DRY	2.88	DRY	3.44
6	LINER	6.12 5	4.5	NEW	API	N	9070	20054	9018	10008	-5370	-6360	10984	P- 110	13.5	LT&C	1.71	1.99	DRY	2.28	DRY	2.85

Casing Attachments

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Casing ID: 1

String

SURFACE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084835.pdf

Casing ID: 2

String

INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084850.pdf

Casing ID: 3

String

INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084949.pdf

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Casing ID: 4

String

INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084957.pdf

Casing ID: 5

String

PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084928.pdf

Casing ID: 6

String

LINER

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Spanish_Bay_18_19_Fed_Com_526H_CsgAssumptions_20240906084939.pdf

Section 4 - Cement

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

String Type	Lead/Tail	Stage Tool Depth	Тор МБ	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1387	910	2.12	12.5	1930	100	Class C	Salt, Gel, Extender, LCM
SURFACE	Tail		1387	1580	200	1.34	14.8	268	100	Class C	Retarder
INTERMEDIATE	Lead		0	2752	500	2.12	12.5	1060	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		2752	3100	100	1.34	14.8	134	25	Class C	Retarder
INTERMEDIATE	Lead		3100	4435	250	2.12	12.5	530	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		4435	5110	200	1.34	14.8	268	25	Class C	Retarder
PRODUCTION	Lead	3100	3465	6715	280	2.12	12.5	600	25	Class C	Gel, Retarder, Defoamer, Extender
PRODUCTION	Tail		6715	9271	400	1.18	15.6	472	25	Class H	Retarder, Fluid Loss, Defoamer
LINER	Lead		9071	2005 4	700	1.85	13.5	1300	25	Class H	Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-Settling Agent

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

Describe what will be on location to control well or mitigate other conditions: Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

Circulating Medium Table

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	ЬН	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	1580	SPUD MUD	8.4	8.6							
1580	5110	SALT SATURATED	9.5	10.2						9	
5110	9271	WATER-BASED MUD	8.6	9.7					1		
9271	2005 4	OIL-BASED MUD	8.6	10				A		1	

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

Will run GR/CNL from KOP (9271') to surface (horizontal well vertical portion of hole). Stated logs run will be in the Completion Report and submitted to

the BLM.

List of open and cased hole logs run in the well:

DIRECTIONAL SURVEY, GAMMA RAY LOG, MEASUREMENT WHILE DRILLING, MUD LOG/GEOLOGIC LITHOLOGY LOG, CEMENT BOND LOG, COMPENSATED NEUTRON LOG,

Coring operation description for the well:

None

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 5204 Anticipated Surface Pressure: 3002

Anticipated Bottom Hole Temperature(F): 140

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

H2S Plan 20240605083137.pdf

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

Spanish_Bay_18_19_Fed_Com_526H_Dir_Plot_20240605083200.pdf Spanish_Bay_18_19_Fed_Com_526H_Dir_Plan_20240605083214.pdf

Other proposed operations facets description:

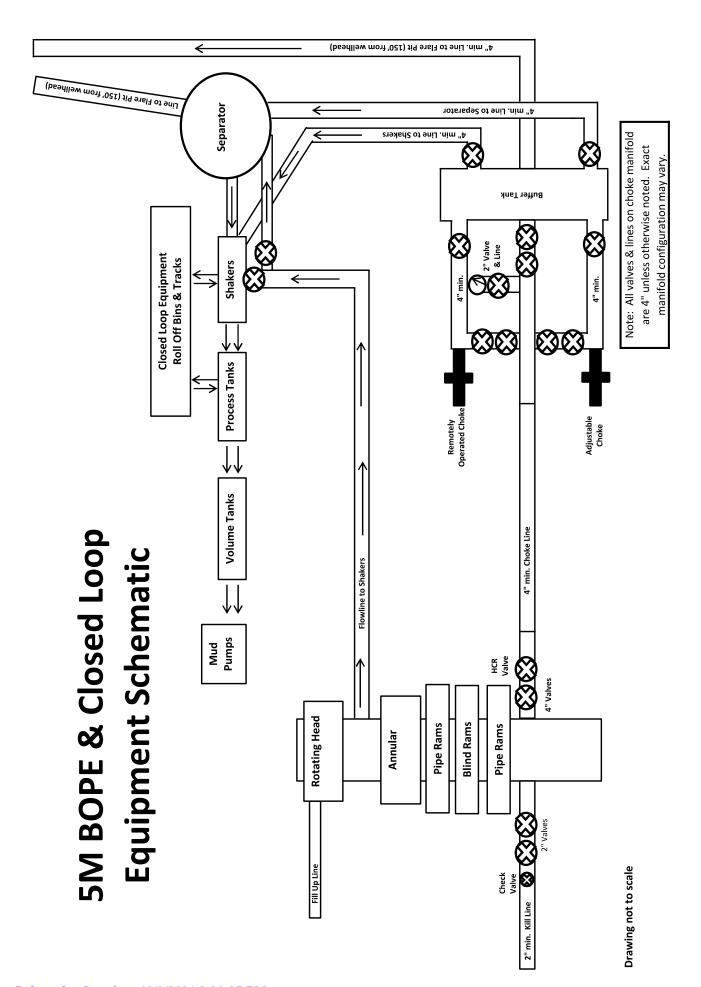
Mewbourne Oil Company also requests approval to implement Design B as described below. BLM will be notified of elected design.

Other proposed operations facets attachment:

Spanish_Bay_18_19_Fed_Com_526H_AddInfo_20240605083311.pdf Spanish_Bay_18_19_Fed_Com_526H_Drlg_Program_20240906085225.pdf

Other Variance attachment:

Mewbourne_Break_Testing_Variance_20240605083404.pdf
Mewbourne_Offline_Cementing_Variance_20240605083410.pdf
SPANISH_BAY_18_19_FED_COM__526H_NGMP_20240906090012.pdf





LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

Product Name	Cho	oke And Kill Hose		Standard	I AP	I Spec 16C 3 rd edition		
Product Specification	on 3"×1000	0psi×60ft(18.29m	1)	Serial Num	ber	7660144		
Inspection Equipme	ent MTU	J-BS-1600-3200-E		Test mediu	ım	Water		
Inspection Departm	ent (Q.C. Department			Date	2023.08.26		
		Rate of le	ength chang	ge	•			
Standard requireme	nts At working pr	essure, the rate of le	ength chang	ge should not m	nore than ±29	%		
Testing result	10000psi (69.0	MPa) ,Rate of leng	th change	0.7%				
		Hydrosta	atic testing					
Standard requirements At 1.5 times working pressure, the initial pressure-holding period of not less than three minuthe second pressure-holding period of not less than one hour, no leaks.								
Testing result	15000psi (103	.5MPa), 3 min for t	he first tim	e, 60 min for th	ne second time	, no leakage		
Graph of pressure tes	ting:					Adeca (DC		
	Table 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 2150-1 215					02754 00394 0059		
Conclusion	- 300E - 5	cted items meet stan		rements of API	000000000000000000000000000000000000000	5 10000000 10000000 100000		
Approver	Jian long Chen	aw long Chen Auditor High			Inspector	Zhansheng Wan		



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF QUALITY

LTYY/QR-5.7.1-19B

№: LT2023-126-002

Customer Name	Austin Hose							
Product Name	Chok							
Product Specification	3"×10000psi×60ft (18.29m)	Quantity	2PCS					
Serial Number	7660143~7660144	FSL	FSL3					
Temperature Range	-29℃~+121℃	Standard	API Spec 16C 3 rd edition					
Inspection Department	Q.C. Department	Inspection date	2023.08.26					

	Inspection	on Items	3		Inspection results				
	Appearance (Checkin	g		In accordance with API Spec 16C 3 rd edition				
	Size and L	engths			In accordance with API Spec 16C 3 rd edition				
Γ	Dimensions and	d Tolerar	nces		In accordance with API Spec 16C 3 rd edition				
End Connections: 4-	/16"×10000psi I	ntegral fla	ange for sour gas ser	vice	In accordance with API Spec 6A 21st edition				
End Connections: 4-	1/16″×10000psi I	ntegral fla	ange for sour gas ser	vice	In accordance with API Spec 17D 3 rd edition				
	Hydrostatic	Testing			In accordance with API Spec 16C 3 rd edition				
	product M	arking			In accordance with API Spec 16C 3 rd edition				
Inspection con	nclusion		The inspected ite	ms m	neet standard requirements of API Spec 16C 3 rd edition				
Remark	:s								
Approver	prover Jian long Chan		Auditor	1/1	nging Dong	Inspector	Zhansheng Wang		



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

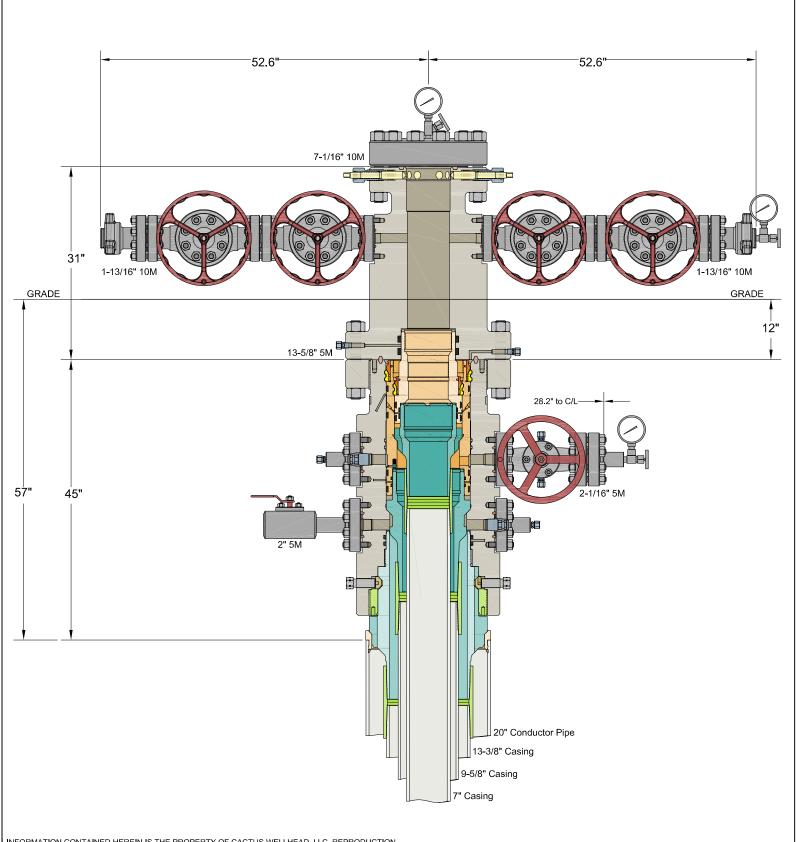
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3rd edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3rd edition.

Jian long Chen

QC Manager:

Date: Aug 26, 2023



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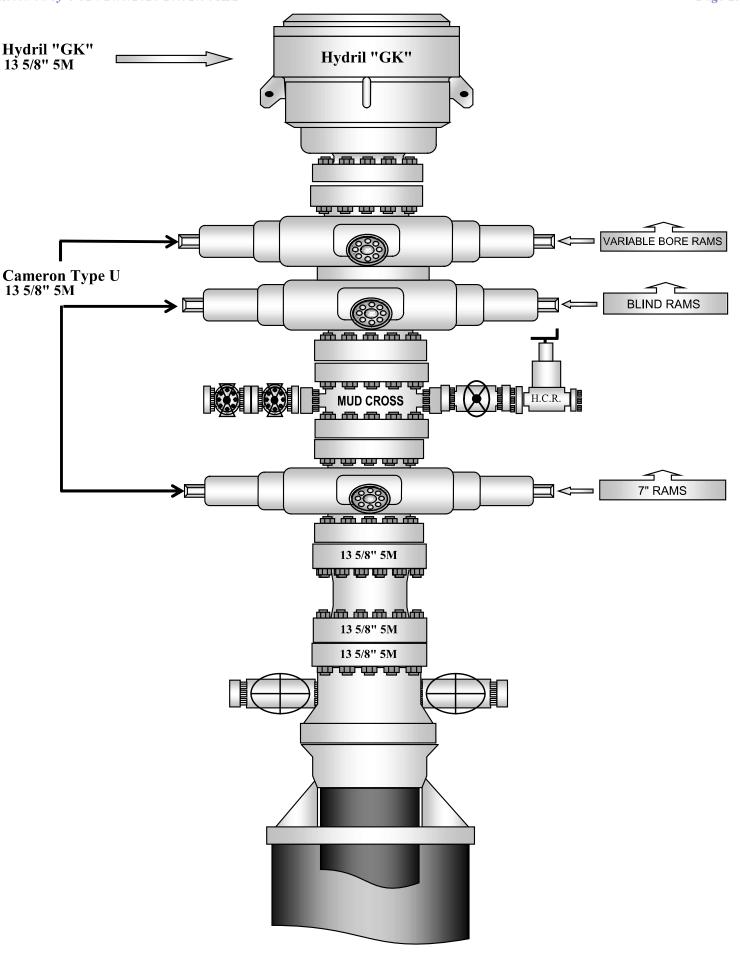
CACTUS WELLHEAD LLC

20" x 13-3/8" x 9-5/8" x 7" MBU-3T-CFL-R-DBLO Wellhead System With 9-5/8" & 7" Fluted Mandrel Casing Hangers And 13-5/8" 5M x 7-1/16" 10M CTH-DBLHPS Tubing Head

ALL DIMENSIONS APPROXIMATE MEWBOURNE OIL COMPANY NEW MEXICO

DRAWN DLE 18APR22
APPRV

DRAWING NO. HBE0000660





Mewbourne Oil Co.

BOP Break Testing Variance

Mewbourne Oil Company requests a variance from the minimum standards for well control equipment testing of 43 CFR 3172 to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with batch drilling & offline cementing operations. Modern rig upgrades which facilitate pad drilling allow the BOP stack to be moved between wells on a multi-well pad without breaking any BOP stack components apart. Widespread use of these technologies has led to break testing BOPE being endorsed as safe and reliable. American Petroleum Institute (API) best practices are frequently used by regulators to develop their regulations. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (5th Ed., Dec. 2018) Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component."

Procedures

- 1. Full BOPE test at first installation on the pad.
 - Full BOPE test at least every 21 days.
 - Function test BOP elements per 43 CFR 3172.
 - Contact the BLM if a well control event occurs.
- After the well section is secured and the well is confirmed to be static, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad. Two breaks on the BOPE will be made (Fig. 1).
 - Connection between the flex line and the HCR valve
 - Connection between the wellhead and the BOP quick connect (Fig. 5 & 6).
- 3. A capping flange will be installed after cementing per wellhead vendor procedure & casing pressure will be monitored via wellhead valve.
- 4. The BOP will be removed and carried by a hydraulic carrier (Fig. 3 & 4).
- 5. The rig will then walk to the next well.
- 6. Confirm that the well is static and remove the capping flange.
- 7. The connection between the flex line and HCR valve and the connection between the wellhead and the BOP guick connect will be reconnected.
- 8. Install a test plug into the wellhead.
- 9. A test will then be conducted against the upper pipe rams and choke, testing both breaks (Fig. 1 & 2).
- 10. The test will be held at 250 psi low and to the high value submitted in the APD, not to exceed 5000 psi.
- 11. The annular, blind rams and lower pipe rams will then be function tested.
- 12. If a pad consists of three or more wells, steps 4 through 11 will be repeated.



13. A break test will only be conducted if the intermediate section can be drilled and cased within 21 days of the last full BOPE test.

Barriers

Before Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

After Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool and/or cement head
- Capping flange after cementing

Summary

A variance is requested to only test broken pressure seals on the BOPE when moving between wells on a multi-well pad if the following conditions are met:

- A full BOPE test is conducted on the first well on the pad. API Standard 53 requires testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater.
- If the first well on the pad is not the well with the deepest intermediate section, a full BOPE test will also be performed when moving to a deeper well.
- The hole section being drilled has a MASP under 5000 psi.
- If a well control event occurs, Mewbourne will contact BLM for permission to continue break testing.
- If significant (>50%) losses occur, full BOPE testing will be required going forward.
- Full BOPE test will be required prior to drilling the production hole.

While walking the rig, the BOP stack will be secured via hydraulic winch or hydraulic carrier. A full BOPE test will be performed at least every 21 days.



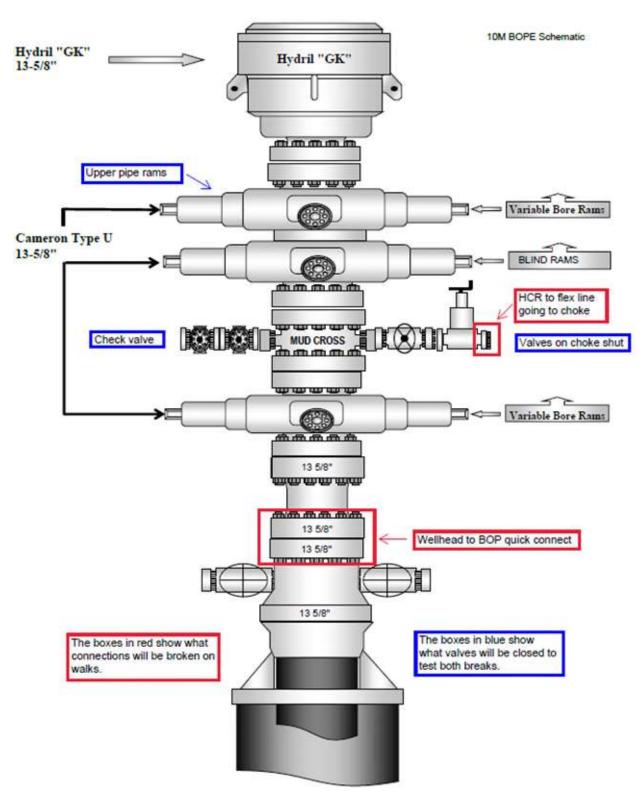


Figure 1. BOP diagram



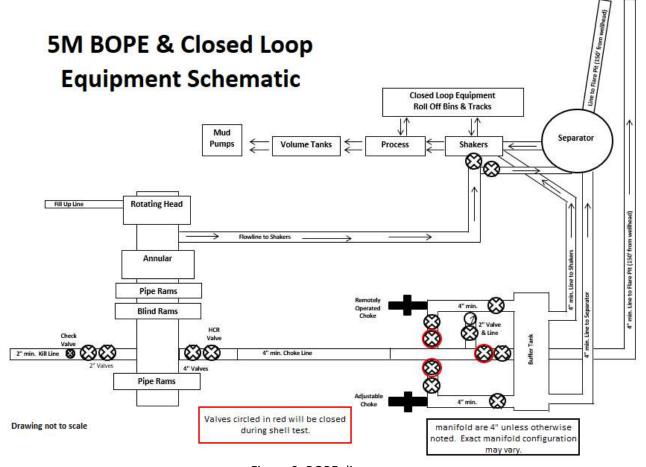


Figure 2. BOPE diagram





Figure 3. BOP handling system





Figure 4. BOP handling system



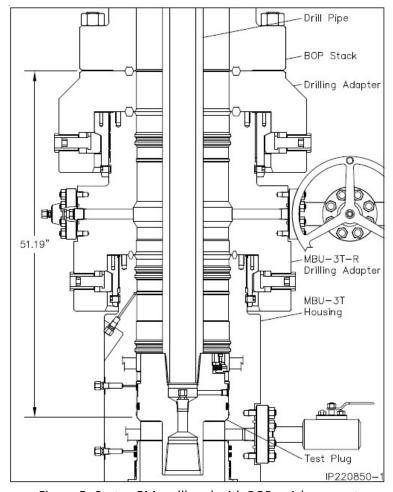


Figure 5. Cactus 5M wellhead with BOP quick connect

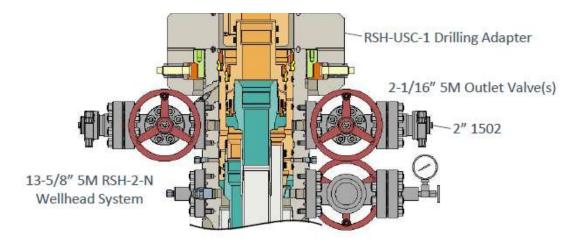


Figure 6. Vault 5M wellhead with BOP quick connect

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

		Casing Progr	ram Design A			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension	
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44
Liner	6.125"	9070'	9018'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.28	2.85

1	Lillei	

	in i rogiani										
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description			
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM			
15.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder			
1st Stg 9.625 in	LEAD 250 12.5 2.12 3100' - 4435' 530		25%	Class C: Salt, Gel, Extender, LCM							
18t 5tg 3.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder			
	9 5/8" DV Tool @ 3100'										
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM			
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder			
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer			
/ III	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer			
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent			

Design A - Mud Program

Depth	Mud Wt	Mud Type	
	8.4 - 8.6		
0' - 1480'	8.4 - 8.6	Fresh Water	
1480' - 5110'	9.5 - 10.2	Brine	
5110' - 9270'	8.6 - 9.7	Cut-Brine	
9270' - 20054.3'	10.0 - 12.	OBM	

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

	Y o'	or N
Is casing new? If used, attach certification as required in Onshore Order #1		Y
Is casing API approved? If no, attach casing specification sheet.	Y	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y	Y
Is well located within Capitan Reef?		Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?		Y
i yes, does production casing cement to eask a minimum of 30 above the Reer! Is well within the designated 4 string boundary.		N
Is well located in SOPA but not in R-111-Q?	N	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing?		
Is well located in R-111-Q and SOPA?	N	N
If yes, are the first three strings cemented to surface?		
Is 2 nd string set 100' to 600' below the base of salt?		
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.		
Is an engineered weak point used to satisfy R-111-Q?		
If yes, at what depth is the weak point planned?		
Is well located in high Cave/Karst?	N	N
If yes, are there two strings cemented to surface?		
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?		
Is well located in critical Cave/Karst?		N
If yes, are there three strings cemented to surface?	- IN	14

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

		Casing Prog	ram Design B			BLM Minimum Safety	1.125	1.0	1.6 Dry	1.6 Dry
		Casing 110g	rain Design D			Factors	1.123	1.0	1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14

4.5" 13.5# P110 LTC

Liner Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
15.375 III	TAIL	200	14.8	1.34	1289' - 1480'	268	100%	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 7.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d 3tg 9.023 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist otg / III	TAIL	400	15.6	1.18	7687' - 10160.5'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

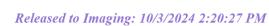
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

Mewbourne Oil Company, Spanish Bay 18/19 Fed Com 526H

Sec 18, T19S, R33E SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)



SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

	Casing Program Design A						1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44
Liner	6.125"	9070'	9018'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.28	2.85

Cement Program

Cement Frogram								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
		_			9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Sig 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	4376	Class C: Retarder
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
7 111	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9270'	8.6 - 9.7	Cut-Brine
9270' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est, Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is easing API approved? If no, attach easing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

	Casing Program Design B BLM Minimum Safety Factors 1.125 1.0							1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14
Liner	6.125"	9270'	9210'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.32	2.90

Design B - Cement Program

Design D Cement Frogram								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
15.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9:025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d 3tg 9.023 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
rst stg / III	TAIL	400	15.6	1.18	7687' - 10160.5'	472	43%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach easing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)



SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

	Casing Program Design A					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44
Liner	6.125"	9070'	9018'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.28	2.85

Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9270'	8.6 - 9.7	Cut-Brine
9270' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is easing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach easing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous easing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18)

BHL: 100' FSL 1980' FEL (Sec 19)

Casing Program Design B					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Drv 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14
Liner	6.125"	9270'	9210'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.32	2.90

Design B - Cement Program

Design D Cement 110gran								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / III	TAIL	400	15.6	1.18	7687' - 10160.5'	472	43%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est, Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production easing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous easing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)



SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

		Castas Bassa	Di 1			BLM Minimum Safety		BLM Minimum Safety			1.6 Dry	1.6 Dry
Casing Program Design A					Factors	1.125	1.0	1.8 Wet	1.8 Wet			
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension		
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62		
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95		
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70		
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27		
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44		
I iner	6.125"	9070'	90181	20054'	100081	4 5" 13 5# P110 LTC	1.71	1 00	2.28	2.95		

Cement Program

Cement Frogram								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
7 111	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9270'	8.6 - 9.7	Cut-Brine
9270' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	IN.
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
is wen rocated in high Cave Kaint: If yes, are there two strings cemented to surface?	N
Types, are treet two strings cemented to strates: (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14
Liner	6.125"	9270'	9210'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.32	2.90

Design B - Cement Program

Design D Cement 110gran								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
15.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9:025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
rst otg / m	TAIL	400	15.6	1.18	7687' - 10160.5'	472	43%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	1 11 11
	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	v
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	- 10
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)



Mewbourne Oil Company, Spanish Bay 18/19 Fed Com 526H

Sec 18, T19S, R33E SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

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SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

	Casing Program Design A						1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44
Liner	6.125"	9070'	9018'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.28	2.85

Cement Program

Cement i rogram								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Sig 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9270'	8.6 - 9.7	Cut-Brine
9270' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est, Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

Casing Program Design B						BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14
Liner	6.125"	9270'	9210'	20054'	10008'	4.5" 13.5# P110 LTC	1.71	1.99	2.32	2.90

Design B - Cement Program

Design D - Cement 110gran								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	100%	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9:025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / III	TAIL	400	15.6	1.18	7687' - 10160.5'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)



SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

Casing Program Design A					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
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Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	9270'	9210'	7" 26# P110 LTC	1.34	2.14	2.88	3.44
Liner	6.125"	9070'	9018'	20054'	10008	4 5" 13 5# P110 LTC	1.71	1 99	2.28	2.85

Cement Program

Cement Frogram								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
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1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder
7 in	LEAD	170	12.5	2.12	4910' - 6826'	370	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
7 111	TAIL	400	15.6	1.18	6826' - 9270'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9070' - 20054.3'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9270'	8.6 - 9.7	Cut-Brine
9270' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est, Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1,125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3300'	3300'	9.625" 36# J55 LTC	1.15	2.01	2.37	2.95
Int	12.25"	3300'	3300'	4300'	4300'	9.625" 40# J55 LTC	1.13	1.73	7.18	8.70
Int	12.25"	4300'	4300'	5110'	5110'	9.625" 40# L80 LTC	1.14	2.12	22.75	28.27
Production	8.75"	0'	0'	10161'	9826'	7" 26# P110 LTC	1.26	2.01	2.62	3.14
Liner	6.125"	9270'	9210'	20054'	10008'	4 5" 13 5# P110 LTC	1.71	1.99	2.32	2.90

Design B - Cement Program

Design D Cement 110gran								
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	TOC/BOC	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
15.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9:025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" D	V Tool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	250	12.5	2.12	4910' - 7687'	530	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / iii	TAIL	400	15.6	1.18	7687' - 10160.5'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9270' - 20054.3'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoame

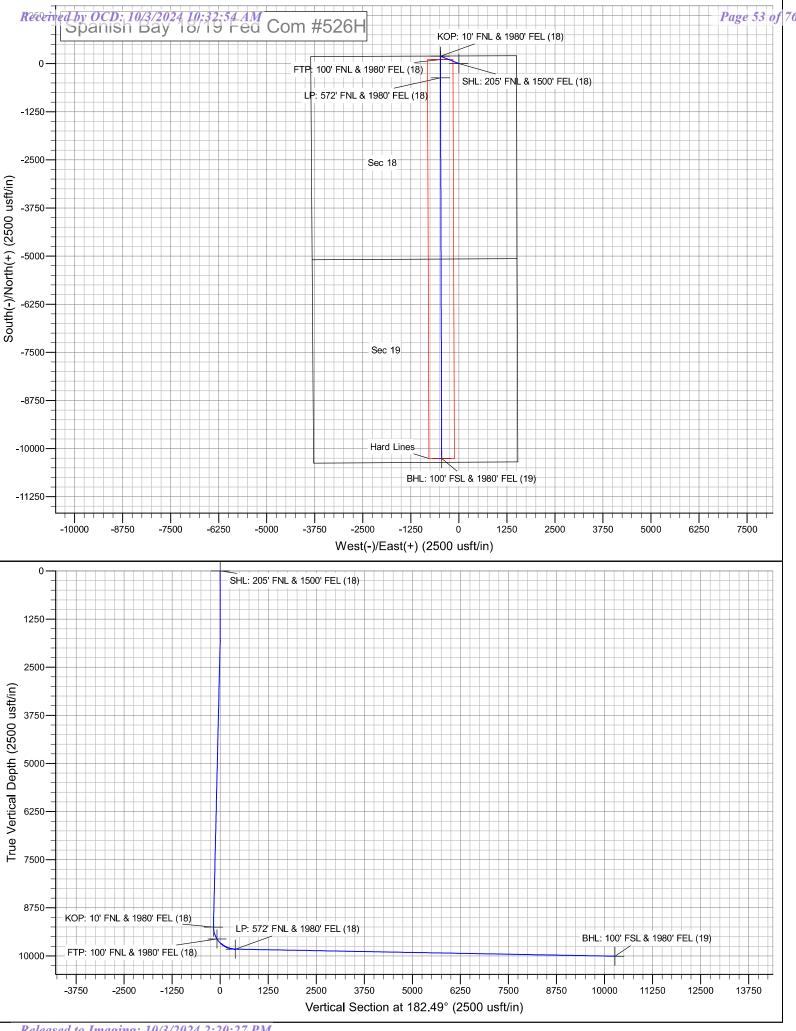
Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10160.5'	8.6 - 9.7	Cut-Brine
10160.5' - 20054.3'	10.0 - 12.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	3519'	Usable Water	Bone Spring	7652'	Oil/Natural Gas
Capitan	4133'	Oil/Natural Gas	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring		
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production easing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	



Mewbourne Oil Company

Lea County, New Mexico NAD 83 Spanish Bay 18/19 Fed Com #526H

Sec 18, T19S, R33E

SHL: 205' FNL & 1500' FEL, Sec 18 BHL: 100' FSL & 1980' FEL, Sec 19

Plan: Design #1

Standard Planning Report

31 May, 2024

Hobbs Database:

Company: Mewbourne Oil Company Project: Lea County, New Mexico NAD 83

Site: Spanish Bay 18/19 Fed Com #526H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 1980' FEL, Sec 19

Design #1 Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

Minimum Curvature

Project Lea County, New Mexico NAD 83

Map System: US State Plane 1983 North American Datum 1983 Geo Datum:

New Mexico Eastern Zone Map Zone:

System Datum:

Mean Sea Level

Spanish Bay 18/19 Fed Com #526H Site

Northing: 606,969.40 usft 32.6669997 Site Position: Latitude: From: Мар Easting: 736,643.70 usft Longitude: -103.6986570

Slot Radius: 13-3/16 " **Position Uncertainty:** 0.0 usft

Well Sec 18, T19S, R33E

Well Position +N/-S 0.0 usft 606,969.40 usft Latitude: 32.6669997 Northing: +E/-W 0.0 usft Easting: 736,643.70 usft Longitude: -103.6986570

0.0 usft Wellhead Elevation: 3,676.0 usft Ground Level: 3,648.0 usft **Position Uncertainty**

Grid Convergence: 0.34°

Wellbore BHL: 100' FSL & 1980' FEL, Sec 19

Magnetics **Model Name** Sample Date Declination Dip Angle Field Strength (°) (nT) (°) IGRF2010 12/31/2014 7.24 60.48 48,512.60289032

Design Design #1

Audit Notes:

PROTOTYPE Version: Phase: Tie On Depth: 0.0

Depth From (TVD) +N/-S +E/-W Direction Vertical Section: (usft) (usft) (usft) (°) 182.49 0.0 0.0 0.0

5/31/2024 **Plan Survey Tool Program** Date

Depth From Depth To

(usft) (usft) Survey (Wellbore) **Tool Name** Remarks

0.0 20,054.3 Design #1 (BHL: 100' FSL & 1980

lan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,600.0	0.00	0.00	1,600.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,798.8	3.98	292.12	1,798.7	2.6	-6.4	2.00	2.00	0.00	292.12	
9,072.0	3.98	292.12	9,054.4	192.5	-473.7	0.00	0.00	0.00	0.00	
9,270.9	0.00	0.00	9,253.0	195.1	-480.1	2.00	- 2.00	0.00	180.00 I	KOP: 10' FNL & 1980
10,160.5	88.95	179.82	9,826.0	-367.4	-478.3	10.00	10.00	0.00	179.82	
20,054.3	88.95	179.82	10,008.0	-10,259.5	-446.4	0.00	0.00	0.00	0.00 1	3HL: 100' FSL & 198

Database: Hobbs

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83
Site: Spanish Bay 18/19 Fed Com #526H

Well: Sec 18, T19S, R33E

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

	,	· . , · · · · . · . · . · .	
Wellbore:	BHL: 100' FSL & 1980' FEL, Sec 19		

ed Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
	NL & 1500' FEL (5.0	0.0	0.0	5.5	0.00	0.00	5.55
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
			•						
1,500.0	0.00	0.00	1,500.0	0.0	0.0	0.0	0.00	0.00	0.00
1,600.0	0.00	0.00	1,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1,700.0	2.00	292.12	1,700.0	0.7	-1.6	-0.6	2.00	2.00	0.00
1,798.8	3.98	292.12	1,798.7	2.6	-6.4	-2.3	2.00	2.00	0.00
1,800.0	3.98	292.12	1,799.8	2.6	-6.5	-2.3	0.00	0.00	0.00
1,900.0	3.98	292.12	1,899.6	5.2	-12.9	-4.7	0.00	0.00	0.00
2,000.0	3.98	292.12	1,999.4	7.8	-19.3	-7.0	0.00	0.00	0.00
2,100.0	3.98	292.12	2,099.1	10.5	-25.7	-9.3	0.00	0.00	0.00
2,200.0	3.98	292.12	2,198.9	13.1	-32.2	-11.7	0.00	0.00	0.00
2,300.0	3.98	292.12	2,298.6	15.7	-38.6	-14.0	0.00	0.00	0.00
2,400.0	3.98	292.12	2,398.4	18.3	-45.0	-16.3	0.00	0.00	0.00
2,500.0	3.98	292.12	2,498.2	20.9	-51.4	-18.6	0.00	0.00	0.00
2,600.0	3.98	292.12	2,597.9	23.5	-57.9	-21.0	0.00	0.00	0.00
2,700.0	3.98	292.12	2,697.7	26.1	-64.3	-23.3	0.00	0.00	0.00
2,800.0	3.98	292.12	2,797.4	28.7	-70.7	-25.6	0.00	0.00	0.00
2,900.0	3.98	292.12	2,897.2	31.3	-77.1	-28.0	0.00	0.00	0.00
3,000.0	3.98	292.12	2,996.9	34.0	-83.6	-30.3	0.00	0.00	0.00
3,100.0	3.98	292.12	3,096.7	36.6	-90.0	-32.6	0.00	0.00	0.00
3,200.0	3.98	292.12	3,196.5	39.2	-96.4	-35.0	0.00	0.00	0.00
3,300.0	3.98	292.12	3,296.2	41.8	-102.8	-37.3	0.00	0.00	0.00
3,400.0	3.98	292.12	3,396.0	44.4	-109.3	-39.6	0.00	0.00	0.00
3,500.0	3.98	292.12	3,495.7	47.0	-115.7	-41.9	0.00	0.00	0.00
3,600.0	3.98	292.12	3,595.5	49.6	-122.1	-44.3	0.00	0.00	0.00
3,700.0	3.98	292.12	3,695.3	52.2	-128.5	-46.6	0.00	0.00	0.00
3,800.0	3.98	292.12	3,795.0	54.8	-135.0	-48.9	0.00	0.00	0.00
3,900.0	3.98	292.12	3,894.8	57.5	-141.4	-51.3	0.00	0.00	0.00
4,000.0	3.98	292.12	3,994.5	60.1	-147.8	-53.6	0.00	0.00	0.00
4,100.0	3.98	292.12	4,094.3	62.7	-154.2	-55.9	0.00	0.00	0.00
4,200.0	3.98	292.12	4,194.1	65.3	-160.7	-58.2	0.00	0.00	0.00
4,300.0	3.98	292.12	4,293.8	67.9	-167.1	-60.6	0.00	0.00	0.00
4,400.0	3.98	292.12	4,393.6	70.5	-173.5	-62.9	0.00	0.00	0.00
4,500.0	3.98	292.12	4,493.3	73.1	-179.9	-65.2	0.00	0.00	0.00
4,600.0	3.98	292.12	4,593.1	75.7	-186.4	-67.6	0.00	0.00	0.00
4,700.0	3.98	292.12	4,692.9	78.3	-192.8	-69.9	0.00	0.00	0.00
4,800.0	3.98	292.12	4,792.6	81.0	-199.2	-72.2	0.00	0.00	0.00
4,900.0	3.98	292.12	4,892.4	83.6	-205.6	-74.6	0.00	0.00	0.00
5,000.0	3.98	292.12	4,992.1	86.2	-203.0 -212.1	-74.0 -76.9	0.00	0.00	0.00
5,100.0	3.98	292.12	5,091.9	88.8	-218.5	-70.3 -79.2	0.00	0.00	0.00

Hobbs Database: Company:

Mewbourne Oil Company Lea County, New Mexico NAD 83 Project: Spanish Bay 18/19 Fed Com #526H Site:

Well: Sec 18, T19S, R33E

Design: Design #1

BHL: 100' FSL & 1980' FEL, Sec 19 Wellbore:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

Doorgin.	<u> </u>								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0	3.98	292.12	5,191.7	91.4	-224.9	-81.5	0.00	0.00	0.00
5,300.0	3.98	292.12	5,291.4	94.0	-231.3	-83.9	0.00	0.00	0.00
5,400.0	3.98	292.12	5,391.2	96.6	-237.8	-86.2	0.00	0.00	0.00
5,500.0	3.98	292.12	5,490.9	99.2	-244.2	-88.5	0.00	0.00	0.00
5,600.0	3.98	292.12	5,590.7	101.8	-250.6	-90.9	0.00	0.00	0.00
5,700.0	3.98	292.12	5,690.4	104.5	-257.0	-93.2	0.00	0.00	0.00
5,800.0	3.98	292.12	5,790.2	107.1	-263.5	-95.5	0.00	0.00	0.00
5,900.0	3.98	292.12	5,890.0	109.7	-269.9	-97.8	0.00	0.00	0.00
6,000.0	3.98	292.12	5,989.7	112.3	-276.3	-100.2	0.00	0.00	0.00
6,100.0	3.98	292.12	6,089.5	114.9	-282.7	-102.5	0.00	0.00	0.00
6,200.0	3.98	292.12	6,189.2	117.5	-289.2	-104.8	0.00	0.00	0.00
6,300.0	3.98	292.12	6,289.0	120.1	-295.6	-107.2	0.00	0.00	0.00
6,400.0	3.98	292.12	6,388.8	122.7	-302.0	-109.5	0.00	0.00	0.00
6,500.0	3.98	292.12	6,488.5	125.3	-308.5	-111.8	0.00	0.00	0.00
6,600.0	3.98	292.12	6,588.3	128.0	-314.9	-114.1	0.00	0.00	0.00
6,700.0	3.98	292.12	6,688.0	130.6	-321.3	-116.5	0.00	0.00	0.00
6,800.0	3.98	292.12	6,787.8	133.2	-327.7	-118.8	0.00	0.00	0.00
6,900.0	3.98	292.12	6,887.6	135.8	-334.2	-121.1	0.00	0.00	0.00
7,000.0	3.98	292.12	6,987.3	138.4	-340.6	-123.5	0.00	0.00	0.00
7,100.0	3.98	292.12	7,087.1	141.0	-347.0	-125.8	0.00	0.00	0.00
7,200.0	3.98	292.12	7,186.8	143.6	-353.4	-128.1	0.00	0.00	0.00
7,300.0	3.98	292.12	7,286.6	146.2	-359.9	-130.5	0.00	0.00	0.00
7,400.0	3.98	292.12	7,386.4	148.8	-366.3	-132.8	0.00	0.00	0.00
7,500.0	3.98	292.12	7,486.1	151.5	-372.7	-135.1	0.00	0.00	0.00
7,600.0	3.98	292.12	7,585.9	154.1	-379.1	-137.4	0.00	0.00	0.00
7,700.0	3.98	292.12	7,685.6	156.7	-385.6	-139.8	0.00	0.00	0.00
7,800.0	3.98	292.12	7,785.4	159.3	-392.0	-142.1	0.00	0.00	0.00
7,900.0	3.98	292.12	7,885.1	161.9	-398.4	-144.4	0.00	0.00	0.00
8,000.0	3.98	292.12	7,984.9	164.5	-404.8	-146.8	0.00	0.00	0.00
8,100.0	3.98	292.12	8,084.7	167.1	-411.3	-149.1	0.00	0.00	0.00
8,200.0 8,300.0	3.98 3.98	292.12 292.12	8,184.4 8,284.2	169.7 172.3	-417.7 -424.1	-151.4 -153.7	0.00 0.00	0.00 0.00	0.00 0.00
8,400.0	3.98	292.12	8,383.9	175.0	-430.5	-156.1	0.00	0.00	0.00
8,500.0	3.98	292.12	8,483.7	177.6	-437.0	-158.4	0.00	0.00	0.00
8,600.0	3.98	292.12	8,583.5	180.2	-443.4	-160.7	0.00	0.00	0.00
8,700.0 8,800.0	3.98 3.98	292.12 292.12	8,683.2 8,783.0	182.8 185.4	-449.8 -456.2	-163.1 -165.4	0.00 0.00	0.00 0.00	0.00 0.00
8,900.0	3.98	292.12	8,882.7	188.0	-462.7	-167.7	0.00	0.00	0.00
9,000.0	3.98	292.12	8,982.5	190.6	-469.1	-170.1	0.00	0.00	0.00
9,072.0	3.98	292.12	9,054.4	192.5	-473.7	-171.7	0.00	0.00	0.00
9,100.0 9,200.0	3.42 1.42	292.12 292.12	9,082.3 9,182.2	193.2 194.8	-475.4 -479.3	-172.3 -173.8	2.00 2.00	-2.00 -2.00	0.00 0.00
9,270.9	0.00	0.00	9,253.0	195.1	-480.1	-174.0	2.00	-2.00	0.00
	NL & 1980' FEL (1	•	2 25 -	40		.=	46.55	4.5. 5.5	2.2-
9,300.0	2.91	179.82	9,282.2	194.4	-480.1	-173.3	10.00	10.00	0.00
9,350.0	7.91	179.82	9,331.9	189.6	-480.1	-168.6	10.00	10.00	0.00
9,400.0 9,450.0	12.91 17.91	179.82 179.82	9,381.1 9,429.3	180.6 167.3	-480.1 -480.0	-159.6 -146.3	10.00 10.00	10.00 10.00	0.00 0.00
9,500.0	22.91	179.82	9,476.1	149.9	-480.0	-128.9	10.00	10.00	0.00
9,550.0	27.91	179.82	9,521.3	128.5	-479.9	-107.5	10.00	10.00	0.00
9,596.4	32.55	179.82	9,561.3	105.1	-479.8	-84.1	10.00	10.00	0.00
	NL & 1980' FEL (0.564.4	102.2	470.0	90.0	10.00	10.00	0.00
9,600.0 9,650.0	32.91 37.91	179.82 179.82	9,564.4 9,605.1	103.2	-479.8 -479.7	-82.2 53.3	10.00 10.00	10.00 10.00	0.00 0.00
9,650.0	37.91	1/9.82	9,605.1	74.2	-4/9./	-53.3	10.00	10.00	0.00

Hobbs Database:

Company: Mewbourne Oil Company Lea County, New Mexico NAD 83 Project: Spanish Bay 18/19 Fed Com #526H Site:

Well: Sec 18, T19S, R33E

Design: Design #1

BHL: 100' FSL & 1980' FEL, Sec 19 Wellbore:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

lanned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,700.0	42.91	179.82	9,643.2	41.8	-479.6	-20.9	10.00	10.00	0.00
9,750.0	47.90	179.82	9,678.3	6.2	-479.5	14.6	10.00	10.00	0.00
9,800.0	52.90	179.82	9,710.1	-32.3	-479.4	53.1	10.00	10.00	0.00
9,850.0	57.90	179.82	9,738.5	-73.5	-479.2	94.2	10.00	10.00	0.00
9,900.0	62.90	179.82	9,763.2	-116.9	-479.1	137.6	10.00	10.00	0.00
9,950.0	67.90	179.82	9,784.0	-162.4	-478.9	183.0	10.00	10.00	0.00
10,000.0	72.90	179.82	9,800.8	-209.5	-478.8	230.1	10.00	10.00	0.00
10,050.0	77.90	179.82	9,813.4	-257.8	-478.6	278.4	10.00	10.00	0.00
10,100.0	82.90	179.82	9,821.7	-307.1	-478.5	327.6	10.00	10.00	0.00
10,150.0	87.90	179.82	9,825.7	-356.9	-478.3	377.4	10.00	10.00	0.00
40.400.5	00.04	470.00			470.0		40.00		0.00
10,160.5	88.94	179.82	9,826.0	-367.4	-478.3	387.8	10.00	10.00	0.00
	L & 1980' FEL (18	•	0.000.7	400.0	470.0	407.0	0.00	0.00	0.00
10,200.0	88.95	179.82	9,826.7	-406.9	-478.2	427.3	0.00	0.00	0.00
10,300.0	88.95	179.82	9,828.6	-506.9	-477.8	527.2	0.00	0.00	0.00
10,400.0	88.95	179.82	9,830.4	-606.9	-477.5	627.1	0.00	0.00	0.00
10,500.0	88.95	179.82	9,832.2	-706.9	-477.2	726.9	0.00	0.00	0.00
10,600.0	88.95	179.82	9,834.1	-806.8	-476.9	826.8	0.00	0.00	0.00
10,700.0	88.95	179.82	9,835.9	-906.8	-476.5	926.7	0.00	0.00	0.00
10,800.0	88.95	179.82	9,837.8	-1,006.8	-476.2	1,026.6	0.00	0.00	0.00
10,900.0	88.95	179.82	9,839.6	-1,106.8	-475.9	1,126.4	0.00	0.00	0.00
11,000.0	88.95	179.82	9,841.4	-1,206.8	-475.6	1,226.3	0.00	0.00	0.00
11,100.0	88.95	179.82	9,843.3	-1,306.8	-475.3	1.326.2	0.00	0.00	0.00
11,200.0	88.95	179.82	9,845.1	-1,406.7	-474.9	1,426.1	0.00	0.00	0.00
11,300.0	88.95	179.82	9,847.0	-1,506.7	-474.6	1,525.9	0.00	0.00	0.00
11,400.0	88.95	179.82	9,848.8	-1,606.7	-474.3	1,625.8	0.00	0.00	0.00
11,500.0	88.95	179.82	9,850.6	-1,706.7	-474.0	1,725.7	0.00	0.00	0.00
11,600.0	88.95	179.82	9,852.5	-1,806.7	-473.6	1,825.6	0.00	0.00	0.00
11,700.0	88.95	179.82	9,854.3	-1,906.7	-473.3	1,925.4	0.00	0.00	0.00
11,800.0	88.95	179.82	9,856.2	-1,900.7 -2,006.6	-473.0	2,025.3	0.00	0.00	0.00
11,900.0	88.95	179.82	9,858.0	-2,106.6	-472.7	2,125.2	0.00	0.00	0.00
12,000.0	88.95	179.82	9,859.8	-2,206.6	-472.4	2,125.2	0.00	0.00	0.00
12,100.0	88.95	179.82	9,861.7	-2,306.6	-472.0	2,324.9	0.00	0.00	0.00
12,200.0	88.95	179.82	9,863.5	-2,406.6	-471.7	2,424.8	0.00	0.00	0.00
12,300.0	88.95	179.82	9,865.4	-2,506.6	-471.4	2,524.7	0.00	0.00	0.00
12,400.0	88.95	179.82	9,867.2	-2,606.5	-471.1	2,624.5	0.00	0.00	0.00
12,500.0	88.95	179.82	9,869.0	-2,706.5	-470.7	2,724.4	0.00	0.00	0.00
12,600.0	88.95	179.82	9,870.9	-2,806.5	-470.4	2,824.3	0.00	0.00	0.00
12,700.0	88.95	179.82	9,872.7	-2,906.5	-470.1	2,924.2	0.00	0.00	0.00
12,800.0	88.95	179.82	9,874.6	-3,006.5	-469.8	3,024.0	0.00	0.00	0.00
12,900.0	88.95	179.82	9,876.4	-3,106.4	-469.5	3,123.9	0.00	0.00	0.00
13,000.0	88.95	179.82	9,878.2	-3,206.4	-469.1	3,223.8	0.00	0.00	0.00
13,100.0	88.95	179.82	9,880.1	-3,306.4	-468.8	3,323.7	0.00	0.00	0.00
13,200.0	88.95	179.82	9,881.9	-3,406.4	-468.5	3,423.5	0.00	0.00	0.00
13,300.0	88.95	179.82	9,883.8	-3,506.4	-468.2	3,523.4	0.00	0.00	0.00
13,400.0	88.95	179.82	9,885.6	-3,606.4	-467.8	3,623.3	0.00	0.00	0.00
13,500.0	88.95	179.82	9,887.4	-3,706.3	-467.5	3,723.2	0.00	0.00	0.00
13,600.0	88.95	179.82	9,889.3	-3,806.3	-467.2	3,823.0	0.00	0.00	0.00
13,600.0	88.95 88.95	179.82 179.82	9,889.3 9,891.1		-467.2 -466.9	3,823.0 3,922.9		0.00	0.00
13,700.0	88.95	179.82	9,891.1	-3,906.3 -4,006.3	-466.9 -466.6	3,922.9 4,022.8	0.00 0.00	0.00	0.00
13,800.0	88.95	179.82	9,892.9 9,894.8	-4,006.3 -4,106.3	-466.2	4,022.8 4,122.7	0.00	0.00	0.00
14,000.0	88.95	179.82	9,894.8 9,896.6	-4,106.3 -4,206.3	-465.2 -465.9	4,122.7 4,222.5	0.00	0.00	0.00
14,100.0	88.95	179.82	9,898.5	-4,306.2	-465.6	4,322.4	0.00	0.00	0.00
14,200.0	88.95	179.82	9,900.3	-4,406.2	-465.3	4,422.3	0.00	0.00	0.00

Database: Hobbs Company: Mewbo

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83
Site: Spanish Bay 18/19 Fed Com #526H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 1980' FEL, Sec 19

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

Grid

lanned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,300.0 14,400.0	88.95 88.95	179.82 179.82	9,902.1 9,904.0	-4,506.2 -4,606.2	-464.9 -464.6	4,522.2 4,622.0	0.00 0.00	0.00 0.00	0.00 0.00
14,500.0	88.95	179.82	9,905.8	-4,706.2	-464.3	4,721.9	0.00	0.00	0.00
14,600.0 14,700.0	88.95 88.95	179.82 179.82	9,907.7 9,909.5	-4,806.2 -4,906.1	-464.0 -463.7	4,821.8 4,921.7	0.00 0.00	0.00 0.00	0.00 0.00
14,800.0	88.95	179.82	9,911.3	-5,006.1	-463.7 -463.3	5,021.5	0.00	0.00	0.00
14,875.8	88.95	179.82	9,912.7	-5,081.9	-463.1	5,097.2	0.00	0.00	0.00
	NL & 1977' FEL (1	•							
14,900.0	88.95	179.82	9,913.2	-5,106.1	-463.0	5,121.4	0.00	0.00	0.00
15,000.0	88.95	179.82	9,915.0	-5,206.1	-462.7	5,221.3	0.00	0.00	0.00
15,100.0	88.95	179.82	9,916.9	-5,306.1	-462.4	5,321.1	0.00	0.00	0.00
15,200.0 15,300.0	88.95 88.95	179.82 179.82	9,918.7 9,920.5	-5,406.0 -5,506.0	-462.0 -461.7	5,421.0 5,520.9	0.00 0.00	0.00 0.00	0.00 0.00
15,400.0	88.95	179.82	9,922.4	-5,606.0	-461.4	5,620.8	0.00	0.00	0.00
15,500.0	88.95	179.82	9,924.2	-5,706.0	-461.1	5,720.6	0.00	0.00	0.00
15,600.0	88.95	179.82	9,926.1	-5,806.0	-460.8	5,820.5	0.00	0.00	0.00
15,700.0	88.95	179.82	9,927.9	-5,906.0	-460.4	5,920.4	0.00	0.00	0.00
15,800.0	88.95	179.82	9,929.7	-6,005.9	-460.1	6,020.3	0.00	0.00	0.00
15,900.0	88.95	179.82	9,931.6	-6,105.9	-459.8	6,120.1	0.00	0.00	0.00
16,000.0	88.95	179.82	9,933.4	-6,205.9	-459.5	6,220.0	0.00	0.00	0.00
16,100.0	88.95	179.82	9,935.3	-6,305.9	-459.1	6,319.9	0.00	0.00	0.00
16,200.0 16,300.0	88.95 88.95	179.82 179.82	9,937.1 9,938.9	-6,405.9 -6,505.9	-458.8 -458.5	6,419.8 6,519.6	0.00 0.00	0.00 0.00	0.00 0.00
16,400.0	88.95	179.82	9,940.8	-6,605.8	-458.2	6,619.5	0.00	0.00	0.00
16,500.0 16,600.0	88.95 88.95	179.82 179.82	9,942.6 9,944.5	-6,705.8 -6,805.8	-457.9 -457.5	6,719.4 6,819.3	0.00 0.00	0.00 0.00	0.00 0.00
16,700.0	88.95	179.82	9,946.3	-6,905.8	-457.3 -457.2	6,919.1	0.00	0.00	0.00
16,800.0	88.95	179.82	9,948.1	-7,005.8	-456.9	7,019.0	0.00	0.00	0.00
16,900.0	88.95	179.82	9,950.0	-7,105.8	-456.6	7,118.9	0.00	0.00	0.00
17,000.0	88.95	179.82	9,951.8	-7,205.7	-456.2	7,218.8	0.00	0.00	0.00
17,100.0	88.95	179.82	9,953.7	-7,305.7	-455.9	7,318.6	0.00	0.00	0.00
17,200.0	88.95	179.82	9,955.5	-7,405.7	-455.6	7,418.5	0.00	0.00	0.00
17,300.0 17,400.0	88.95 88.95	179.82 179.82	9,957.3 9,959.2	-7,505.7 -7,605.7	-455.3 -455.0	7,518.4 7,618.3	0.00 0.00	0.00 0.00	0.00 0.00
•			·	•		·			
17,500.0	88.95	179.82	9,961.0	-7,705.6	-454.6	7,718.1	0.00	0.00	0.00
17,513.4	88.95	179.82	9,961.3	-7,719.0	-454.6	7,731.5	0.00	0.00	0.00
17,600.0	l ' FSL & 1977' FEI 88.95	- (19) 179.82	9,962.9	-7,805.6	-454.3	7.818.0	0.00	0.00	0.00
17,700.0	88.95	179.82	9,964.7	-7,905.6	-454.0	7,917.9	0.00	0.00	0.00
17,800.0	88.95	179.82	9,966.5	-8,005.6	-453.7	8,017.7	0.00	0.00	0.00
17,900.0	88.95	179.82	9,968.4	-8,105.6	-453.3	8.117.6	0.00	0.00	0.00
18,000.0	88.95	179.82	9,970.2	-8,205.6	-453.0	8,217.5	0.00	0.00	0.00
18,100.0	88.95	179.82	9,972.0	-8,305.5	-452.7	8,317.4	0.00	0.00	0.00
18,200.0	88.95	179.82	9,973.9	-8,405.5	-452.4	8,417.2	0.00	0.00	0.00
18,300.0	88.95	179.82	9,975.7	-8,505.5	-452.1	8,517.1	0.00	0.00	0.00
18,400.0	88.95	179.82	9,977.6	-8,605.5	-451.7	8,617.0	0.00	0.00	0.00
18,500.0	88.95	179.82	9,979.4	-8,705.5	-451.4	8,716.9	0.00	0.00	0.00
18,600.0	88.95	179.82	9,981.2	-8,805.5 8,005.4	-451.1	8,816.7 8,916.6	0.00	0.00	0.00
18,700.0 18,800.0	88.95 88.95	179.82 179.82	9,983.1 9,984.9	-8,905.4 -9,005.4	-450.8 -450.4	9,016.5	0.00 0.00	0.00 0.00	0.00 0.00
18,900.0 19,000.0	88.95 88.95	179.82 179.82	9,986.8 9,988.6	-9,105.4 -9,205.4	-450.1 -449.8	9,116.4 9,216.2	0.00 0.00	0.00 0.00	0.00 0.00
19,100.0		179.82	9,900.6	-9,205.4 -9,305.4	-449.6 -449.5	9,216.2	0.00	0.00	0.00
19,200.0		179.82	9,992.3	-9,405.3	-449.2	9,416.0	0.00	0.00	0.00

Database: Hobbs Company: Mewbo

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83
Site: Spanish Bay 18/19 Fed Com #526H

Well: Sec 18, T19S, R33E

 Wellbore:
 BHL: 100' FSL & 1980' FEL, Sec 19

 Design:
 Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #526H WELL @ 3676.0usft (Original Well Elev) WELL @ 3676.0usft (Original Well Elev)

Grid

anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
19,300.0	88.95	179.82	9,994.1	-9,505.3	-448.8	9,515.9	0.00	0.00	0.00
19,400.0	88.95	179.82	9,996.0	-9,605.3	-448.5	9,615.7	0.00	0.00	0.00
19,500.0	88.95	179.82	9,997.8	-9,705.3	-448.2	9,715.6	0.00	0.00	0.00
19,600.0	88.95	179.82	9,999.6	-9,805.3	-447.9	9,815.5	0.00	0.00	0.00
19,700.0	88.95	179.82	10,001.5	-9,905.3	-447.5	9,915.4	0.00	0.00	0.00
19,800.0	88.95	179.82	10,003.3	-10,005.2	-447.2	10,015.2	0.00	0.00	0.00
19,900.0	88.95	179.82	10,005.2	-10,105.2	-446.9	10,115.1	0.00	0.00	0.00
20,000.0	88.95	179.82	10,007.0	-10,205.2	-446.6	10,215.0	0.00	0.00	0.00
20,054.3	88.95	179.82	10,008.0	-10,259.5	-446.4	10,269.2	0.00	0.00	0.00
BHL: 100' F	SL & 1980' FEL (19)							

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL: 205' FNL & 1500' - plan hits target ce - Point		0.01	0.0	0.0	0.0	606,969.40	736,643.70	32.6669997	-103.6986570
KOP: 10' FNL & 1980' I - plan hits target ce - Point		0.00	9,253.0	195.1	-480.1	607,164.50	736,163.60	32.6675438	-103.7002133
FTP: 100' FNL & 1980' - plan hits target ce - Point		0.00	9,561.3	105.1	-479.8	607,074.50	736,163.89	32.6672964	-103.7002141
LP: 572' FNL & 1980' F - plan hits target ce - Point		0.00	9,826.0	-367.4	-478.3	606,602.00	736,165.41	32.6659977	-103.7002183
PPP2: 0' FNL & 1977' F - plan hits target ce - Point		0.00	9,912.7	-5,081.9	-463.1	601,887.50	736,180.61	32.6530394	-103.7002603
PPP3: 2641' FSL & 197 - plan hits target ce - Point		0.00	9,961.3	-7,719.0	-454.6	599,250.40	736,189.11	32.6457911	-103.7002837
BHL: 100' FSL & 1980' - plan hits target ce - Point		0.00	10,008.0	-10,259.5	-446.4	596,709.90	736,197.30	32.6388082	-103.7003063

SHL: 205' FNL 1500' FEL (Sec 18) BHL: 100' FSL 1980' FEL (Sec 19)

Operator Nar	ne:	Property Name:	Well Number
Mewbourne Oil C	ompany	Spanish Bay 18/19 Fed Com	526H

Kick Off Point (KOP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
В	18	19	33	_	10'	FNL	1980'	FEL	Lea
Latitude						NAD			
32.6675438				-103.70021	33			83	

First Take Point (FTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
В	18	19	33	-	100'	FNL	1980'	FEL	Lea
Latitude						NAD			
32.6672965	5				-103.70021	47			83

Last Take Point (LTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
О	19	19	33	_	100'	FSL	1980'	FEL	Lea
Latitude						NAD			
32.638808	2				-103.70030	061			83

32.6388082	-103.7003061	83
Is this well the defining well for the Horizontal Is this well an infill well? If infill is yes please provide API if available, C Spacing Unit.	Spacing Unit? Y Operator Name and well number for Defining well for Horizontal	
API#		
Operator Name:	Property Name:	Well Number

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: MEWBOURNE OIL COMPANY

WELL NAME & NO.: SPANISH BAY 18/19 FED COM 526H

APD ID: 10400098866

LOCATION: Section 18, T.19 S., R.33 E. NMP

COUNTY: Lea County, New Mexico

COA

H ₂ S	0	Yes		
Potash /	None	O Secretary	O R-111-Q	☐ Open Annulus
WIPP				□ WIPP
Cave / Karst	• Low	O Medium	O High	Critical
Wellhead	Conventional	Multibowl	O Both	Diverter
Cementing	☐ Primary Squeeze	☐ Cont. Squeeze	☐ EchoMeter	DV Tool
Special Req	Capitan Reef	☐ Water Disposal	\square COM	☐ Unit
Waste Prev.	Self-Certification	• Waste Min. Plan	○ APD Submitted ₁	prior to 06/10/2024
Additional	✓ Flex Hose	☐ Casing Clearance	☐ Pilot Hole	Break Testing
Language	☐ Four-String	Offline Cementing	▼ Fluid-Filled	

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H₂S) Drilling Plan shall be activated **AT SPUD**. As a result, the Hydrogen Sulfide area must meet **title 43 CFR 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING

Primary Casing Program

- 1. The 13-3/8 inch surface casing shall be set at approximately 1,480 ft. (a minimum of 25 feet (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8 hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 5,110 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, and Capitan Reef.

Option 1 (Single Stage): Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

If Capitan Reef is the loss zone, a DV tool shall be set a maximum of 200 ft. above the top of Capitan Reef.

Option 2 (Two-Stage): The operator has proposed utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

Note: excess cement is below the BLM's recommendation of 25%. More cement might be needed.

Note: The intermediate casing must be kept fluid-filled to meet minimum requirement for collapse design safety factor.

- ❖ In Capitan Reef Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following: (Use this for 3

string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)

- Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
- O Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.
- **3.** Operator has proposed to set 7" (26# P-110) production casing at approximately **9,270 ft.** (9,210 ft. TVD). The minimum required fill of cement behind the 7 inch production casing is:
 - Cement should tie-back at least **50 feet** above Capitan Reef top or **200 feet** into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

Note: Operator has estimated the Capitan reef top is at approximately 3,519 ft. Cement volume is insufficient to bring cement to at least 50 feet above Capitan Reef top. More cement is needed.

- 4. The minimum required fill of cement behind the 4-1/2 inch production liner is:
 - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

Alternate Casing Program

- 1. The 13-3/8 inch surface casing shall be set at approximately 1,480 ft. (a minimum of 25 feet (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8 hours or 500 psi compressive strength, whichever is greater. (This is to

- include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 5,110 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, and Capitan Reef.

Option 1 (Single Stage): Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

If Capitan Reef is the loss zone, a DV tool shall be set a maximum of 200 ft. above the top of Capitan Reef.

Option 2 (Two-Stage): The operator has proposed utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

Note: excess cement is below the BLM's recommendation of 25%. More cement might be needed.

Note: The intermediate casing must be kept fluid-filled to meet minimum requirement for collapse design safety factor.

- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following: (Use this for 3 string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)

- Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
- Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.
- **3.** Operator has proposed to set 7" (26# P-110) production casing at approximately **10,161 ft.** (9,826 ft. TVD). The minimum required fill of cement behind the 7 inch production casing is:
 - Cement should tie-back at least **50 feet** above Capitan Reef top or **200 feet** into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

Note: Operator has estimated the Capitan reef top is at approximately 3,519 ft. Cement volume is insufficient to bring cement to at least 50 feet above Capitan Reef top. More cement is needed.

- 4. The minimum required fill of cement behind the 4-1/2 inch production liner is:
 - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

Offline Cementing

Operator has been (**Approved**) to pump the proposed cement program offline in the **Surface and intermediate(s) intervals**. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to the commencement of any offline cementing procedure at **Lea County:** 575-689-5981.

C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Before drilling

the surface casing shoe out, the BOP/BOPE and annular preventer shall be pressuretested in accordance with title 43 CFR 3172 and API Standard 53.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP
- d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Contact Lea County Petroleum Engineering Inspection Staff:

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - i. Notify the BLM when moving in and removing the Spudder Rig.
 - ii. Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum

- compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- **4.** Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- **5.** No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for

- review. These documents shall be posted in the company man's trailer and on the rig floor.
- **3.** 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - iii. Manufacturer representative shall install the test plug for the initial BOP test.
 - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
 - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- **5.** The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
 - iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent

tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crewintensive operations.

SA 09/12/2024

Hydrogen Sulfide Plan Summary

- A. All personnel shall receive proper H2S training in accordance with Onshore Order III.C.3.a.
- B. Briefing Area: two perpendicular areas will be designated by signs and readily accessible.
- C. Required Emergency Equipment:
 - Well control equipment
 - a. Flare line 150' from wellhead to be ignited by flare gun.
 - b. Choke manifold with a remotely operated choke.
 - c. Mud/gas separator
 - Protective equipment for essential personnel.

Breathing apparatus:

- a. Rescue Packs (SCBA) 1 unit shall be placed at each breathing area, 2 shall be stored in the safety trailer.
- b. Work/Escape packs —4 packs shall be stored on the rig floor with sufficient air hose not to restrict work activity.
- c. Emergency Escape Packs —4 packs shall be stored in the doghouse for emergency evacuation.

Auxiliary Rescue Equipment:

- a. Stretcher
- b. Two OSHA full body harness
- c. 100 ft 5/8 inch OSHA approved rope
- d. 1-20# class ABC fire extinguisher
- H2S detection and monitoring equipment:

The stationary detector with three sensors will be placed in the upper dog house if equipped, set to visually alarm @ 10 ppm and audible @ 14 ppm. Calibrate a minimum of every 30 days or as needed. The sensors will be placed in the following places: Rig floor / Bell nipple / End of flow line or where well bore fluid is being discharged.

(Gas sample tubes will be stored in the safety trailer)

- Visual warning systems.
 - a. One color code condition sign will be placed at the entrance to the site reflecting the possible conditions at the site.
 - b. A colored condition flag will be on display, reflecting the current condition at the site at the time.
 - c. Two wind socks will be placed in strategic locations, visible from all angles.

MEWBOURNE OIL COMPANY

ALTHEA 18 FED #101H

■ Mud program:

The mud program has been designed to minimize the volume of H2S circulated to surface. The operator will have the necessary mud products to minimize hazards while drilling in H2S bearing zones.

■ Metallurgy:

All drill strings, casings, tubing, wellhead, blowout preventer, drilling spool, kill lines, choke manifold and lines, and valves shall be suitable for H2S service.

■ Communication:

Communication will be via cell phones and land lines where available.

Operator Name: MEWBOURNE OIL COMPANY

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Section 7 - Methods for Handling

Waste type: DRILLING

Waste content description: Drill cuttings

Amount of waste: 940 barrels

Waste disposal frequency: One Time Only

Safe containment description: Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.)

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located

on HWY 62/180, Sec. 27 T20S R32E.

Waste type: SEWAGE

Waste content description: Human waste & grey water

Amount of waste: 1500 gallons

Waste disposal frequency: Weekly

Safe containment description: 2,000 gallon plastic container

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: City of Carlsbad Water Treatment facility

Waste type: GARBAGE

Waste content description: Garbage & trash

Amount of waste: 1500 pounds

Waste disposal frequency : One Time Only

Safe containment description: Enclosed trash trailer

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: Waste Management facility in Carlsbad.

Reserve Pit

Reserve Pit being used? NO

Operator Name: MEWBOURNE OIL COMPANY

Well Name: SPANISH BAY 18/19 FED COM Well Number: 526H

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Cuttings Area

Cuttings Area being used? NO

Are you storing cuttings on location? N

Description of cuttings location

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area volume (cu. yd.) Cuttings area depth (ft.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary

Are you requesting any Ancillary Facilities?: N

Ancillary Facilities

Comments:

Section 9 - Well Site

Well Site Layout Diagram:

SPANISH_BAY_18_19_FED_COM__526H_WellSiteLayout_20240605083811.pdf

Comments: NONE

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720 District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 389646

CONDITIONS

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	389646
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

CONDITIONS

Created By	Condition	Condition Date
pkautz	Will require a File As Drilled C-102 and a Directional Survey with the C-104	10/3/2024
pkautz	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string	10/3/2024
pkautz	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system	10/3/2024
pkautz	Cement is required to circulate on both surface and intermediate1 strings of casing	10/3/2024
pkautz	If cement does not circulate on any string, a CBL is required for that string of casing	10/3/2024