Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMLC064790 **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: Oil Well 1b. Type of Well: Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing Single Zone ✓ Multiple Zone SPANISH BAY 18/19 FED COM 9. API Well No. 30-025-53655 2. Name of Operator MEWBOURNE OIL COMPANY 10. Field and Pool, or Exploratory 3a. Address 3b. Phone No. (include area code) P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 Tonto/Bone Spring 4. Location of Well (Report location clearly and in accordance with any State requirements.\*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 18/T19S/R33E/NMP At surface NENE / 205 FNL / 1460 FEL / LAT 32.666999 / LONG -103.6985271 At proposed prod. zone SESE / 100 FSL / 660 FEL / LAT 32.6388057 / LONG -103.696019 14. Distance in miles and direction from nearest town or post office\* 12. County or Parish 13. State NM LEA 10 miles 15. Distance from proposed\* 16. No of acres in lease 17. Spacing Unit dedicated to this well 210 feet location to nearest property or lease line, ft. 320.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location\* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 10033 feet / 20075 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start\* 23. Estimated duration 3648 feet 08/04/2024 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 06/11/2024 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 10/04/2024 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.



eived by	OCD: 10	/7/2024 7:54	4:51 AM							Page 2 o			
<u>C-10</u>				arov Mir	State of Nev	v Mexico il Resources Departn	nent		ı	Revised July 9, 2024			
Submit	Electronical	v	Elle			TION DIVISION	пепі		T				
	Permitting	,						Submit	tal Initial Su				
								Type:	☐ Amended				
					WELL LOCAT	☐ As Drilled							
API Nu	mber 20 0	25 52655	Pool Code			Dool Nama	DONE	0001	10.001.171				
Property		)25-53655	Property Na	59476	Ď	TONTO	<u>*</u>	SPRI	NG; SOUTH				
	334	598		5P/	ANISH BAY	′ 18/19 FED CC	)M			528H			
OGRID	<sup>No.</sup> 147	744	Operator Na	<sup>ime</sup> ME	WBOURNE	E OIL COMPNA	·Υ		Ground Leve	el Elevation 648			
Surface	Owner: 🗆 S	State □ Fee □	Tribal 🛚 Fed	eral		Mineral Owner:	State □ Fee	□ Tribal	X Federal				
					Surfa	ace Location							
UL				Ft. from E/W	Latitude		Longitude	County					
В	18	19S	33E		205 FNL	1460 FEL	32.6669	9990	-103.6985271	LEA			
	I	I	Γ_		1	Hole Location	T	- 1					
UL P	Section 19	Township 19S	Range 33E	Lot	Ft. from N/S 100 FSL	Ft. from E/W 660 FEL	Latitude <b>32.638</b> 8	8057	Longitude -103.6960190	County <b>LEA</b>			
'	13	130	JOL		10010L	000122	32.0000	3001	-103.0900190	LL/\			
Dedicated Acres Infill or Defining Well Defining Well API 320 DEFINING						Overlapping Spacing Unit (Y/N) Consolidation Code							
Order N	Order Numbers.					Well setbacks are un	der Common (	Ownership	o: □Yes □No				
					Kick O	ff Point (KOP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County			
Α	18	19	33		10 FNL	660 FEL	32.6675211 -1		-103.6959248	LEA			
	1	ı		1		ake Point (FTP)							
UL A	Section 18	Township 19	Range 33	Lot	Ft. from N/S 100 FNL	Ft. from E/W 660 FEL	Latitude <b>32.6672</b>	2738	Longitude -103.6959263	County LEA			
	ı	ı	1		ı	ke Point (LTP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	0057	Longitude	County			
Р	19	19	33		100 FSL	660 FEL	32.6388	3057	-103.6960190	LEA			
Unitize	d Area or Ar	ea of Uniform I	nterest	Spacing <sup>1</sup>	Unit Type 🛚 Horiz	contal   Vertical	Grou	nd Floor I	Elevation: 36	48			
OPER A	TOR CERT	IFICATIONS				SURVEYOR CERTIFI	CATIONS						
			ained herein is 1	rue and com	plete to the best of	I hereby certify that the w		wn on thic	nlat was plotted from	m field notes of actual			
my know organiza including location interest,	ledge and beli tion either own g the proposed pursuant to a d	ef, and, if the well s a working inter bottom hole locat contract with an o ury pooling agreen	is a vertical or a est or unleased tion or has a rig wner of a worki	directional w mineral inter ht to drill thi ng interest of	vell, that this rest in the land	surveys made by me or une my belief.							
consent of in each t	If this well is a horizontal well, I further certify that this organization has received the consent of at least one lessee or owner of a working interest or unleased mineral interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the division.												
C:			D-+-		10/7/24	Ciomotrus I C- 1 CD C	aianal C						
Signature			Date			Signature and Seal of Profes	Sionai Surveyor						
Printed N		AYLOR				Certificate Number	Date of Surve	ev					
		MEWRC	II IDNE (	'OM				-					

Note: No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

Email Address

District I 1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720
District II 8 First St., Artesia, NM 88210
Phone: (575) 748-1283 Fax: (575) 748-9720 District III
1000 Rio Brazos Road, Aztec, NM 87410
Phone: (505) 334-6178 Fax: (505) 334-6170
District IV
1120 S. St. Francis Dr., Santa Fe, NM 87505
Phone: (505) 476-3460 Fax: (505) 476-3462

Energy, Minerals & Natural Resources Department **OIL CONSERVATION DIVISION** 1220 South St. Francis Dr. State of New Mexico Santa Fe, NM 87505

Form C-102
Revised August 1, 2011 d
Submit one copy to appropriate
District Office

☐ AMENDED REPORT

# WELL LOCATION AND ACREAGE DEDICATION PLAT

		6 Well Number	528H	9 Elevation	3648'		County	LEA	
	IE SPRING			6			East/West line	EAST	
3 Pool Name	TONTO; BONE SPRING		y				Feet From the	1460	im Surface
T0		ıme	SPANISH BAY 18/19 FED COM	ame	MEWBOURNE OIL COMPANY	Location	North/South line	NORTH	" Bottom Hole Location If Different From Surface
		5 Property Name	H BAY 18,	8 Operator Name	OURNE OI	<sup>10</sup> Surface Location	Feet from the	202	ole Location
2 Pool Code	59476		SPANIS		MEWB		Lot Idn		<b>Bottom</b> H
							Range	33E	111 ]
							Township	19S	
1 API Number		de		NO.	4		Section	18	
		4Property Code		7 OGRID NO	14744		UL or lot no.	В	

Dedicated Acres 320

LEA

East/West line

Feet from the

North/South line

EAST

099

SOUTH

100

Range

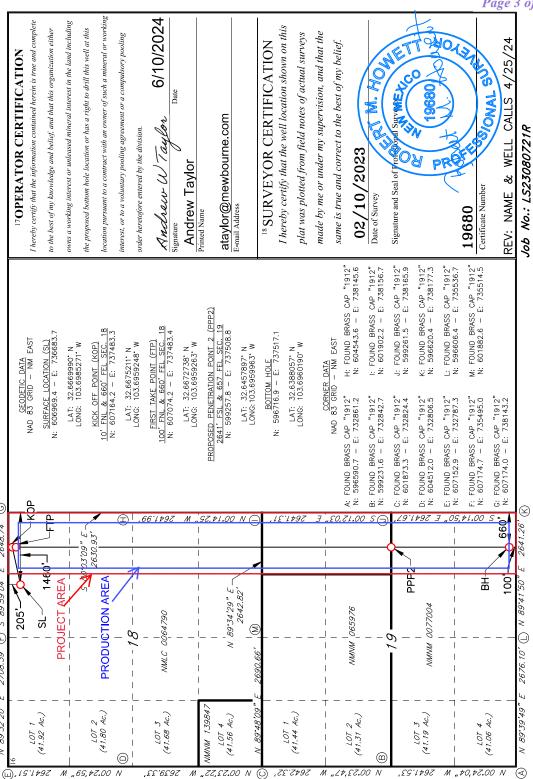
33E

19S Infill

19

UL or lot no.

No allowable will be assigned to this completion until all interest have been consolidated or a non-standard unit has been approved by the division.



# State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

# NATURAL GAS MANAGEMENT PLAN

This Natural Gas M	Ianagement Pl	an must be submitted w	vith each Applicat	ion for Permit to I	Orill (APD) for a	new or recompleted well.			
Section 1 — Plan Description <u>Effective May 25, 2021</u>									
I. Operator:	Mewbourr	ne Oil Co.	OGRID:	14744	Date:	5/2/24			
II. Type: 💢 Origin	nal 🗆 Amendi	ment due to $\Box$ 19.15.27	7.9.D(6)(a) NMA	C □ 19.15.27.9.D(	(6)(b) NMAC 🗆 (	Other.			
If Other, please des	cribe:								
		ng information for each I pad or connected to a			wells proposed to	be drilled or proposed to			
Well Name		ULSTR	Footages	Anticipated Oil BBL/D	Anticipated Gas MCF/D	Anticipated Produced Water BBL/D			
SPANISH BAY 18/19 FED Co	OM 528H	B 18 19S 33E	205' FNL x 1460' F	L 1500	1000	3000			
				Y1: 400, Y2:300, Y3:200	Y1: 800, Y2: 500, Y3: 300	Y1: 1500, Y2: 1000, Y3: 500			
IV. Central Delive	·	e:	ANISH BAY 18/19			9.15.27.9(D)(1) NMAC] s proposed to be drilled or			
		a single well pad or co			ven or set of went	s proposed to be diffied of			
Well Name	API	Spud Date	TD Reached Date	Completion Commencement					
SPANISH BAY 18/19 FED C	OM 528H	7/2/24	8/2/24	9/2/24	9/17	/24 9/17/24			
VII. Operational Subsection A throu	Practices: 🛛 gh F of 19.15 ement Practic	Attach a complete desc 27.8 NMAC. ces: ☑ Attach a comple	cription of the act	ions Operator wil	l take to comply	at to optimize gas capture.  with the requirements of tices to minimize venting			

# Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

X Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

### IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF		

### X. Natural Gas Gathering System (NGGS):

Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in			
				22 27 27 22 22 22 22 22 22 22			

**XI.** Map.  $\Box$  Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

XII. Line Capacity. The natural gas gathering system $\Box$ will $\Box$ will not have capacity to gather 100% of the anticipate	d natural gas
production volume from the well prior to the date of first production.	

XIII. Line Pr	ressure. Operator	$\square$ does $\square$ does no	t anticipate that its	s existing well(s) co	onnected to the	he same segment	i, or portion,	, of the
natural gas ga	thering system(s)	described above w	ill continue to mee	et anticipated increa	ases in line p	ressure caused by	y the new w	ell(s).

☐ Attach Operator's plan to manage production in response to the increased line pressure.

**XIV. Confidentiality:** □ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information provided in Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information for which confidentiality is asserted and the basis for such assertion.

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# Section 3 - Certifications Effective May 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan. 

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) (b) power generation for grid; compression on lease; (c) liquids removal on lease; (d)

- reinjection for underground storage; (e)
- reinjection for temporary storage; **(f)**
- reinjection for enhanced oil recovery; **(g)**
- fuel cell production; and (h)
- other alternative beneficial uses approved by the division.

# **Section 4 - Notices**

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

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I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature:	Bradley Bishop
Printed Name:	BRADLEY BISHOP
Title:	REGULATORY MANAGER
E-mail Address:	BBISHOP@MEWBOURNE.COM
Date:	5/2/24
Phone:	575-393-5905
-	OIL CONSERVATION DIVISION
	(Only applicable when submitted as a standalone form)
Approved By:	
Title:	
Approval Date:	
Conditions of Ap	proval:

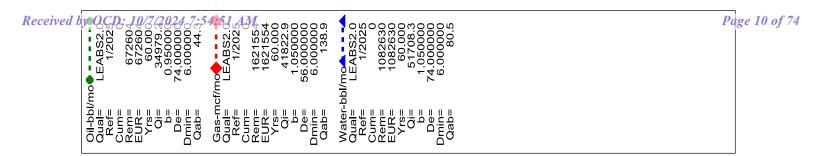
## Mewbourne Oil Company

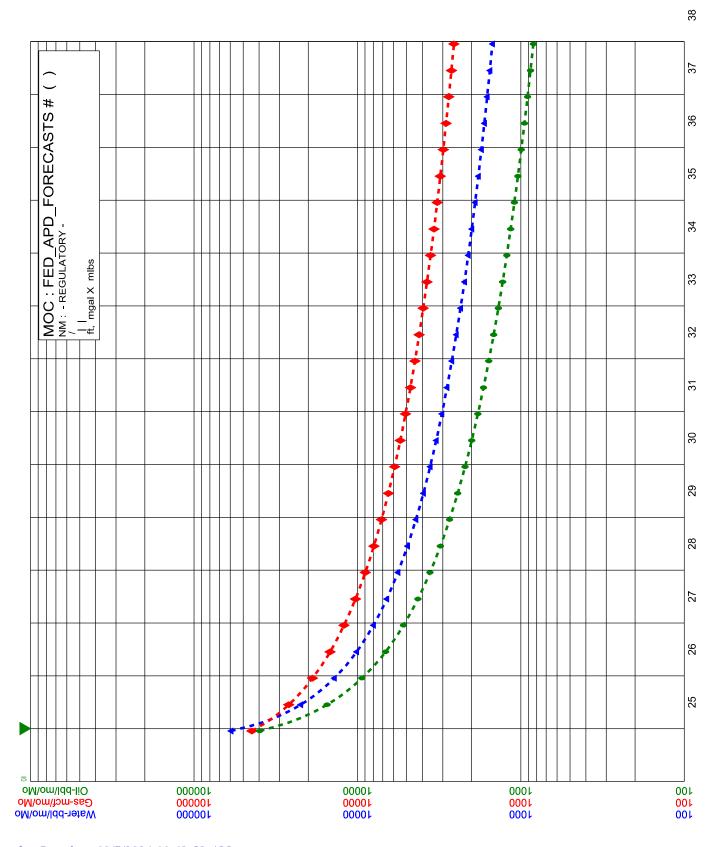
### Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
  - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
  - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
  - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
  - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
  - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
  - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.





U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

# **Drilling Plan Data Report** 10/04/2024

**APD ID**: 10400098985 Submission Date: 06/11/2024

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: SPANISH BAY 18/19 FED COM

Well Type: OIL WELL

Well Number: 528H

Well Work Type: Drill

**Show Final Text** 

Highlighted data reflects the most

recent changes

# **Section 1 - Geologic Formations**

Formation ID	Formation Name	Elevation	True Vertical	Measured Depth	Lithologies	Mineral Resources	Producing Formatio
14264388	UNKNOWN	3645	28	28	OTHER : Topsoil	NONE	N
14264401	RUSTLER	2258	1387	1387	ANHYDRITE, DOLOMITE	USEABLE WATER	N
14264402	TOP SALT	1963	1682	1682	SALT	NONE	N
14264389	BASE OF SALT	713	2932	2932	SALT	NONE	N
14264403	14264403 YATES		3166	3166 SANDSTONE		NATURAL GAS, OIL	N
14264386	CAPITAN REEF	126	3519	3519	DOLOMITE, LIMESTONE	USEABLE WATER	N
14264400	QUEEN	-488	4133	4133	DOLOMITE, SANDSTONE	NATURAL GAS, OIL	N
14264393	LAMAR	-2162	5807	5807	DOLOMITE, LIMESTONE	NATURAL GAS, OIL	N
14264387	BONE SPRING	-4007	7652	7652	LIMESTONE	NATURAL GAS, OIL	N
14264390	BONE SPRING 1ST	-5188	8833	8833	SANDSTONE	NATURAL GAS, OIL	Y
14264404	BONE SPRING 2ND	-5737	9382	9382	SANDSTONE	NATURAL GAS, OIL	Y
14264385	BONE SPRING 3RD	-6460	10105	10105	SANDSTONE	NATURAL GAS, OIL	N

### **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M Rating Depth: 20075

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

**Testing Procedure:** BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

### **Choke Diagram Attachment:**

5M\_BOPE\_Choke\_Diagram\_20240610084420.pdf

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_Flex\_Line\_Specs\_API\_16C\_20240905163140.pdf

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_5M\_Multi\_Bowl\_WH\_20240905163140.pdf

### **BOP Diagram Attachment:**

5M BOPE Schematic 20240610084536.pdf

Mewbourne\_Offline\_Cementing\_Variance\_20240610084545.pdf

# **Section 3 - Casing**

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	17.5	13,375	NEW	API	N	0	1480	0	1480	3648	2168	1480	H-40	48	ST&C	1.16	2.61	DRY	4.53	DRY	7.62
2	INTERMED IATE	12 <b>.</b> 2 5	9.625	NEW	API	N	0	3200	0	3200	3648	448	3200	J-55	36	LT&C	1.19	2.07	DRY	2.36	DRY	2.94
3	INTERMED IATE	12 <b>.</b> 2 5	9.625	NEW	API	N	3200	4100	3200	4100	448	-452	900	J-55	40	LT&C	1.18	1.82	DRY	6.81	DRY	8.25
4	INTERMED IATE	12.2 5	9,625	NEW	API	N	4100	5000	4100	5000	-452	-1352	900	L-80	40	LT&C	1.17	2.17	DRY	18.2 4	DRY	22.6 7
5	INTERMED IATE	12.2 5	9.625	NEW	API	N	5000	5110	5000	5110	-1352	-1462	110	HCL -80	40	LT&C	1.56	2.12	DRY	99.9 9	DRY	99.9 9
6	PRODUCTI ON	8.75	7.0	NEW	API	N	0	9298	0	9238	2968	-5590	9298	P- 110	26	LT&C	1.34	2.14	DRY	2.87	DRY	3.43
7	LINER	6.12 5	4.5	NEW	API	N	9098	20075	9046	10033	-5398	-6385	10977	P- 110	13.5	LT&C	2.05	2.38	DRY	2.28	DRY	2.85

### **Casing Attachments**

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

Casing	Attach	ıments
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Casing ID: 1

String

SURFACE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103512.pdf

Casing ID: 2

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103459.pdf

Casing ID: 3

String

INTERMEDIATE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103527.pdf

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

Casing	Attach	ıments
--------	--------	--------

Casing ID: 4

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103615.pdf

Casing ID: 5

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103625.pdf

Casing ID: 6

7

**String** 

**PRODUCTION** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103557.pdf

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

### **Casing Attachments**

Casing ID: 7

String

**LINER** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_CsgAssumptions\_20240906103605.pdf

# **Section 4 - Cement**

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1289	850	2.12	12.5	1810	100	Class C	Salt, Gel, Extender, LCM
SURFACE	Tail		1289	1480	200	1.34	14.8	268	100	Class C	Retarder
INTERMEDIATE	Lead		0	2752	500	2.12	12.5	1060	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		2752	3100	100	1.34	14.8	134	25	Class C	Retarder
INTERMEDIATE	Lead		3100	4435	250	2.12	12.5	530	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		4435	5110	200	1.34	14.8	268	25	Class C	Retarder
PRODUCTION	Lead	3100	3469	6732	280	2.12	12.5	600	25	Class C	Gel, Retarder, Defoamer, Extender
PRODUCTION	Tail		6732	9298	400	1.18	15.6	472	25	Class H	Retarder, Fluid Loss, Defoamer
LINER	Lead		9098	2007 5	700	1.85	13.5	1300	25	Class H	Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-Settling Agent

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

# **Section 5 - Circulating Medium**

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

**Describe what will be on location to control well or mitigate other conditions:** Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

# **Circulating Medium Table**

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	ЬН	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	1480	SPUD MUD	8.4	8.6		9					
1480	5110	SALT SATURATED	9.5	10.2							
5110	9298	WATER-BASED MUD	8.6	9.7							
9298	2007 5	OIL-BASED MUD	10	10							

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

# Section 6 - Test, Logging, Coring

### List of production tests including testing procedures, equipment and safety measures:

No logs are planned based on well control or offset log information. Offset Well: Spanish Bay 18/19 Fed Com #526H

### List of open and cased hole logs run in the well:

GAMMA RAY LOG,MEASUREMENT WHILE DRILLING,MUD LOG/GEOLOGIC LITHOLOGY LOG,COMPENSATED NEUTRON LOG.

Coring operation description for the well:

None

### **Section 7 - Pressure**

Anticipated Bottom Hole Pressure: 5217 Anticipated Surface Pressure: 3009

**Anticipated Bottom Hole Temperature(F): 140** 

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

**Contingency Plans geoharzards description:** 

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

H2S Plan 20240605083137.pdf

### Section 8 - Other Information

### Proposed horizontal/directional/multi-lateral plan submission:

SPANISH\_BAY\_18\_19\_FED\_COM\_\_528H\_dir\_plan\_20240610090949.pdf SPANISH\_BAY\_18\_19\_FED\_COM\_\_528H\_dir\_plot\_20240610090954.pdf

### Other proposed operations facets description:

Mewbourne Oil Company also requests approval to implement Design B as described below. BLM will be notified of elected design.

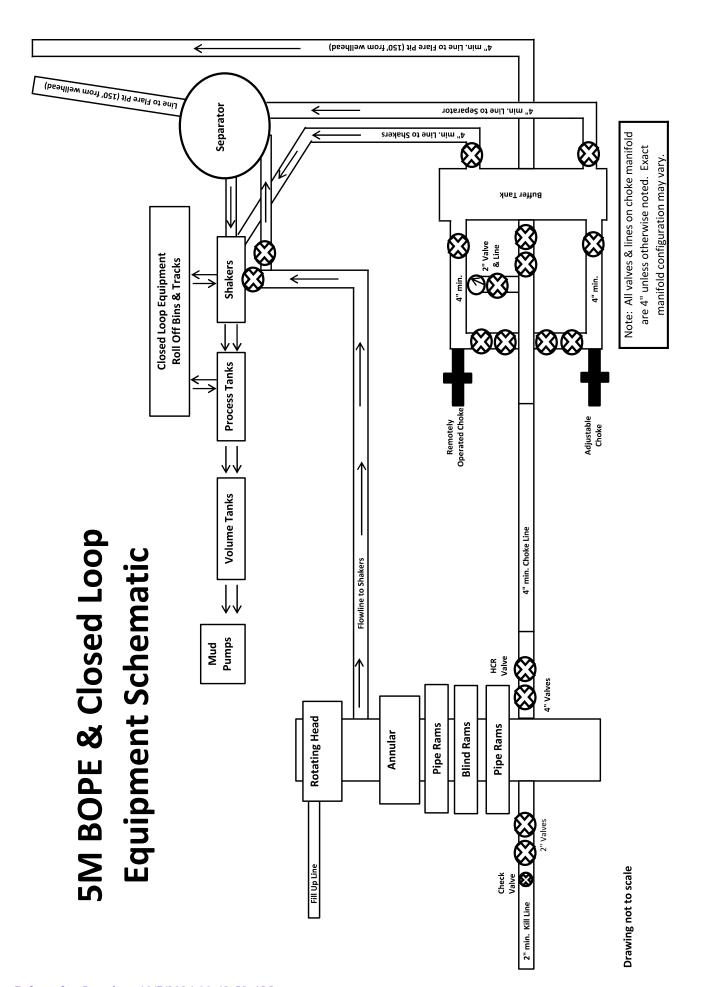
### Other proposed operations facets attachment:

Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_AddInfo\_20240610091007.pdf Spanish\_Bay\_18\_19\_Fed\_Com\_528H\_Drlg\_Program\_20240906103645.pdf

### Other Variance attachment:

Mewbourne\_Break\_Testing\_Variance\_20240605083404.pdf
Mewbourne\_Offline\_Cementing\_Variance\_20240605083410.pdf
SPANISH BAY 18 19 FED COM 528H NGMP 20240906103652.pdf







# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

# HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

Product Name										
	Cho	ke And Kill Hose		Standard API Spec 16C 3 <sup>rd</sup> edition						
Product Specification	3″×1000	0psi×60ft (18.29m)	)	Serial Num	ber	7660144				
Inspection Equipment	MTU	J-BS-1600-3200-E		Test mediu	ım	Water				
Inspection Departmen	t (	C. Department		Inspection I	Date	2023.08.26				
		Rate of len	ngth change	;						
Standard requirements	At working pro	At working pressure ,the rate of length change should not more than $\pm 2\%$								
Testing result	10000psi (69.0	10000psi (69.0MPa) ,Rate of length change 0.7%								
		Hydrostat	tic testing							
Standard requirements		orking pressure, the ssure-holding period				less than three minutes				
Testing result	15000psi (103	.5MPa), 3 min for the	e first time	, 60 min for th	e second tim	ne, no leakage				
Graph of pressure testing	g:									
			110							
100   90   100   1			100 90 80 70 60 70 10 40 40 40 70							
36 - 16 - 16 - 16 - 16 - 16 - 16 - 16 -	। अर्डका अर्डका अर्डका अर्डका अर्डका अर्	M21 22:06:21 22:06:21 22:06:21 22:06:21 22:06	50 - 50 - 50 - 50 - 50 - 50 - 50 - 50 -	SI 23:09:58 23:59:		(10)				
56 (Federal CZ3) 10 (Fe	। अर्डका अर्डका अर्डका अर्डका अर्डका अर्		50 - 50 - 50 - 50 - 50 - 50 - 50 - 50 -	ements of API	S\$ 00:09:S\$ 00	Section Section Section 1100				



# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

# **CERTIFICATE OF QUALITY**

# LTYY/QR-5.7.1-19B

№: LT2023-126-002

Customer Name	Austin Hose						
Product Name	Choke And Kill Hose						
Product Specification	3"×10000psi×60ft (18.29m)	Quantity	2PCS				
Serial Number	7660143~7660144	FSL	FSL3				
Temperature Range	-29℃~+121℃	Standard	API Spec 16C 3 <sup>rd</sup> edition				
Inspection Department	Q.C. Department	Inspection date	2023.08.26				

	Inspection	Items		Inspection results						
	Appearance Ch	necking		In accordance with API Spec 16C 3 <sup>rd</sup> edition						
	Size and Len	ngths		In accordance with API Spec 16C 3 <sup>rd</sup> edition						
Γ	Dimensions and Tolerances					In accordance with API Spec 16C 3 <sup>rd</sup> edition				
End Connections: 4-	End Connections: 4-1/16"×10000psi Integral flange for sour gas service					In accordance with API Spec 6A 21st edition				
End Connections: 4-	End Connections: 4-1/16"×10000psi Integral flange for sour gas service					In accordance with API Spec 17D 3 <sup>rd</sup> edition				
	Hydrostatic To	esting			In accordance with API Spec 16C 3 <sup>rd</sup> edition					
	product Marking					In accordance with API Spec 16C 3 <sup>rd</sup> edition				
Inspection conclusion The inspected items m					eet standard require	ments of API Spec	16C 3 <sup>rd</sup> edition			
Remarks										
Approver Jian long Chan			Auditor	1/1	iging Dong	Inspector	Zhansheng Wang			



# LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

### CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

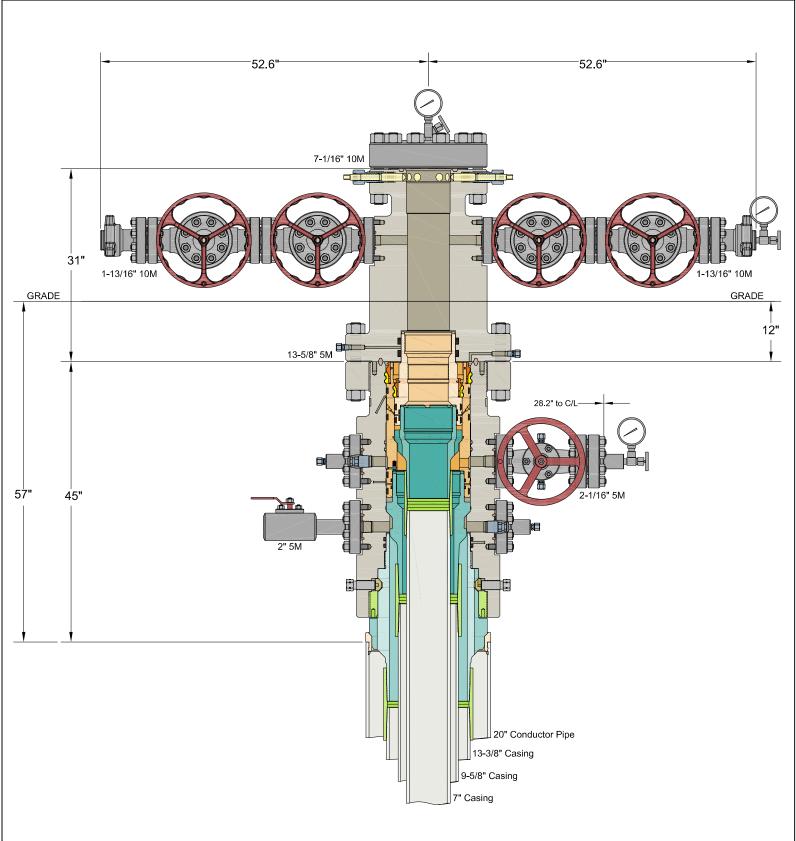
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3<sup>rd</sup> edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3<sup>rd</sup> edition.

Jiaulong Chen

QC Manager:

Date: Aug 26, 2023



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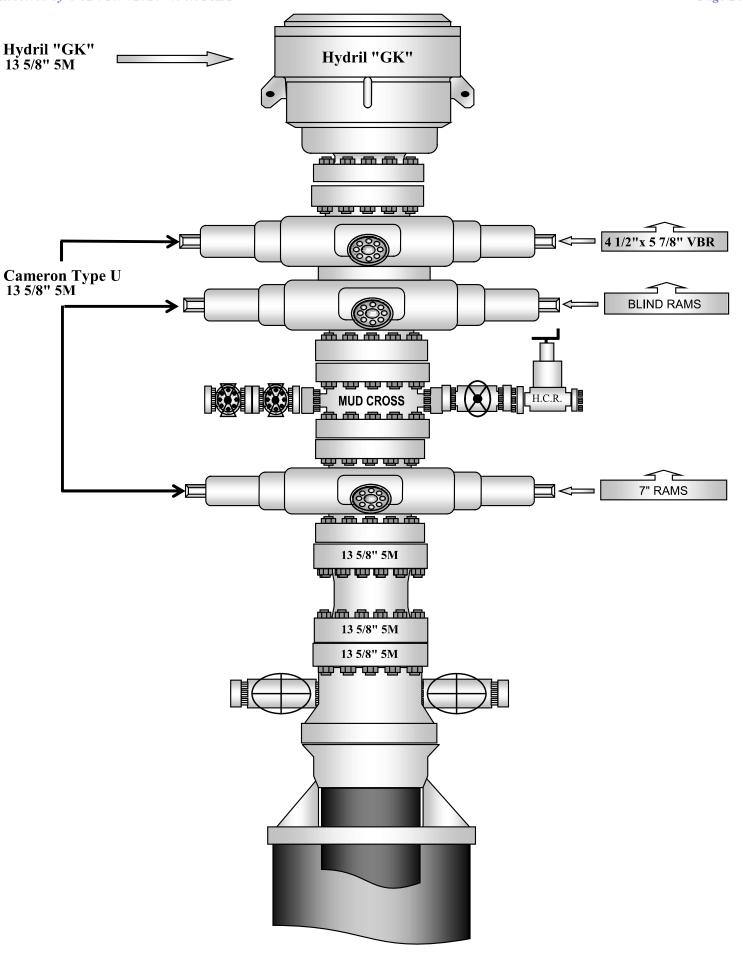
# CACTUS WELLHEAD LLC

20" x 13-3/8" x 9-5/8" x 7" MBU-3T-CFL-R-DBLO Wellhead System With 9-5/8" & 7" Fluted Mandrel Casing Hangers And 13-5/8" 5M x 7-1/16" 10M CTH-DBLHPS Tubing Head

# ALL DIMENSIONS APPROXIMATE MEWBOURNE OIL COMPANY

DRAWN DLE 18APR22
APPRV

DRAWING NO. HBE0000660





# Mewbourne Oil Co.

# Surface & Intermediate Offline Cementing Variance

Mewbourne Oil Company requests a variance to perform offline cementing for surface and intermediate casing strings with the following conditions:

- Offline cementing will not be performed on production casing.
- Offline cementing will not be performed on a hole section with MASP > 5000 psi.
- Offline cementing will not be performed concurrently with offset drilling.

# **Surface Casing Order of Operations:**

- 1. Run 13 3/8" surface casing as per normal operations (TPGS and float collar).
- 2. Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Confirm well is static.
- 4. Make up 13 %" wellhead or wellhead landing ring assembly and land on 20" conductor.
- 5. Fill pipe, circulate casing capacity and confirm float(s) are still holding.
- 6. Confirm well is static.
- 7. Back out landing joint and pull to rig floor. Lay down landing joint.
- 8. Walk rig to next well on pad with cement crew standing by to rig up.
- 9. Make up offline cement tool with forklift per wellhead manufacturer (Fig. 1 & 2).
- 10. Make up cement head on top of offline cement tool with forklift.
- 11. Commence cement operations.
- 12. If cement circulates, confirm well is static and proceed to step 16.
- 13. If cement does not circulate, notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 14. Use 1" pipe for remedial cement job until the surface casing is cemented to surface.
- 15. Confirm well is static.
- 16. Once cement job is complete, the cement head and offline cementing tool are removed. The wellhead technician returns to cellar to install wellhead/valves.
- 17. Install wellhead capping flange.

# **Barriers**

### **Before Walk:**

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus



### After Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Offline cementing tool tested to 5000 psi and cement head
- Capping flange after cementing

# 20" Surface Casing Order of Operations (4 string area):

- 1. Run 20" surface casing as per normal operations (TPGS and float collar).
- Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Fill pipe, circulate casing capacity and confirm float(s) are still holding.
- 4. Confirm well is static.
- 5. Back out landing joint and pull to rig floor. Lay down landing joint.
- 6. Make up cement head.
- 7. Walk rig to next well on pad with cement crew standing by to rig up.
- 8. Commence cement operations.
- 9. If cement circulates, confirm well is static and proceed to step 13.
- 10. If cement does not circulate, notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 11. Use 1" pipe for remedial cement job until the surface casing is cemented to surface.
- 12. Confirm well is static.
- 13. Once cement job is complete, remove cement head and install cap.

# **Barriers**

### **Before Walk:**

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Cement Head

### After Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Cement head
- Capping flange after cementing



# **Intermediate Casing Order of Operations:**

- 1. Run casing as per normal operations (float shoe and float collar).
- 2. Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Confirm well is static (if running SBM).
- 4. Land casing.
- 5. Fill pipe, circulate casing capacity and confirm floats are still holding.
- 6. Confirm well is static.
- 7. Back out landing joint and pull to rig floor. Lay down landing joint. Install packoff & test.
- 8. Nipple down BOP.
- 9. Walk rig to next well on pad with cement crew standing by to rig up.
- 10. Make up offline cement tool using forklift per wellhead manufacturer (Fig. 3 8).
- 11. Make up cement head on top of offline cement tool.
- 12. Commence cement operations.
- 13. If cement circulates, confirm well is static and proceed to step 16.
- 14. If cement does not circulate (when required), notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 15. Pump remedial cement job if required.
- 16. Confirm well is static.
- 17. Remove cement head and offline cementing tool.
- 18. Install wellhead capping flange and test.

### **Barriers**

### **Before Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

### **After Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool tested to 5000 psi and cement head
- Capping flange after cementing



# **Risks:**

- Pressure build up in annulus before cementing
  - Contact BLM if a well control event occurs.
  - Rig up 3<sup>rd</sup> party pump or rig pumps to pump down casing and kill well.
  - Returns will be taken through the wellhead valves to a choke manifold (Fig 9 & 10).
  - Well could also be killed through the wellhead valves down the annulus.

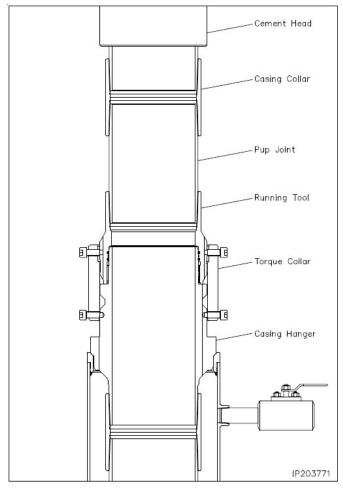


Figure 1. Cactus 13 3/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 13 3/8" pup joint and casing.



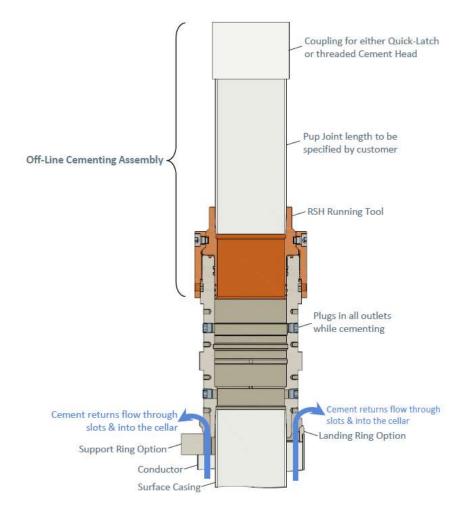


Figure 2. Vault 13 3/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 13 3/8" pup joint and casing.



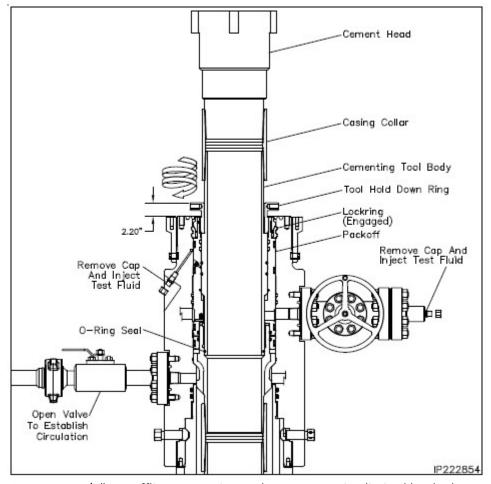


Figure 3. Cactus 9 5/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 9 5/8" pup joint and casing.



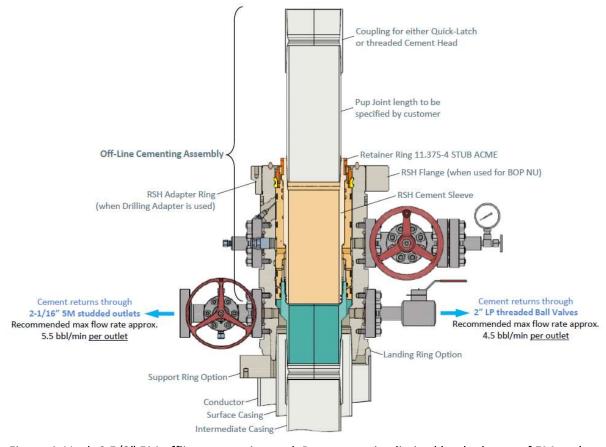


Figure 4. Vault 9 5/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 9 5/8" pup joint and casing.



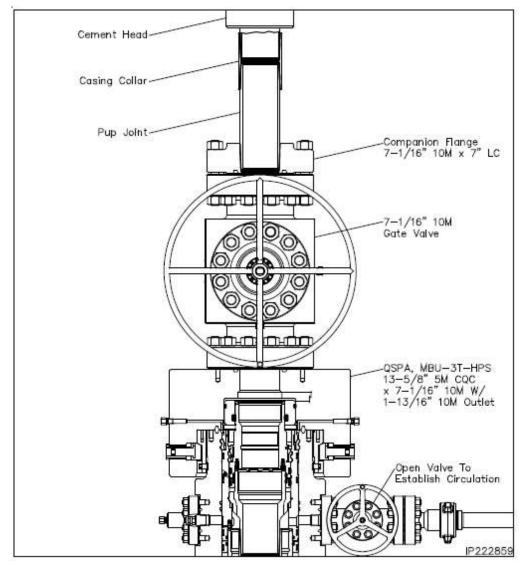


Figure 5. Cactus 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



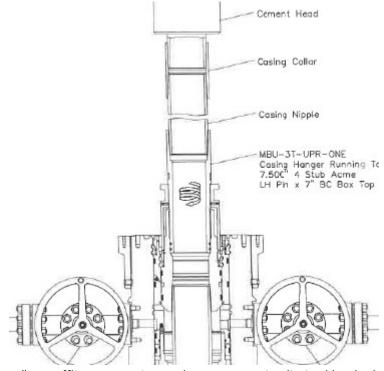


Figure 6. Cactus 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



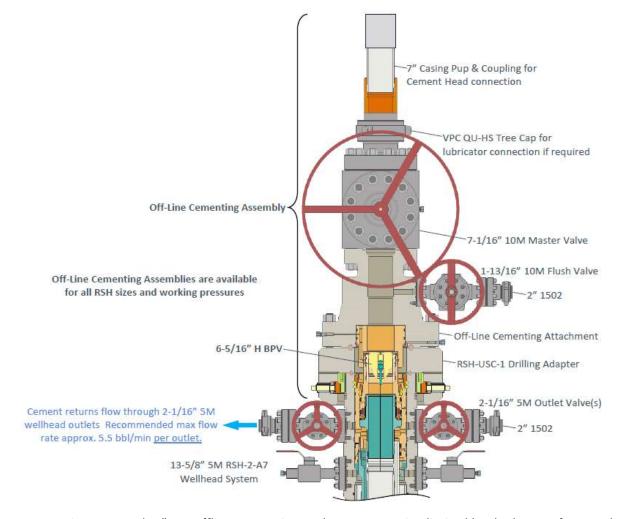


Figure 7. Vault 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



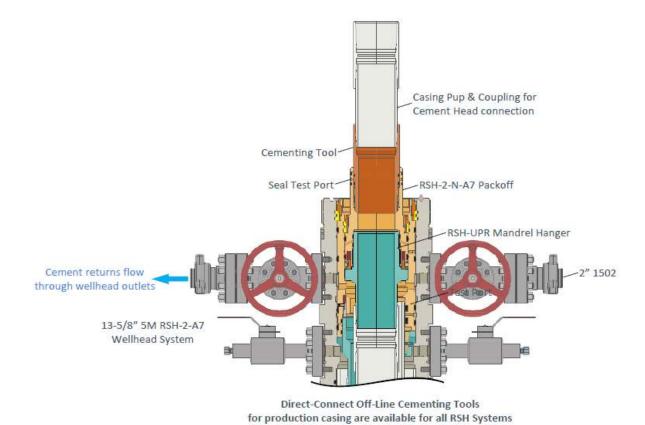


Figure 8. Vault 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



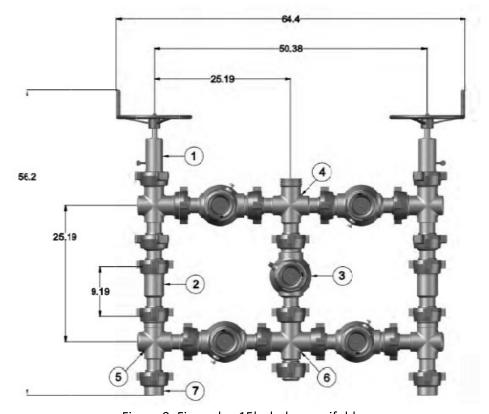


Figure 9. Five valve 15k choke manifold.

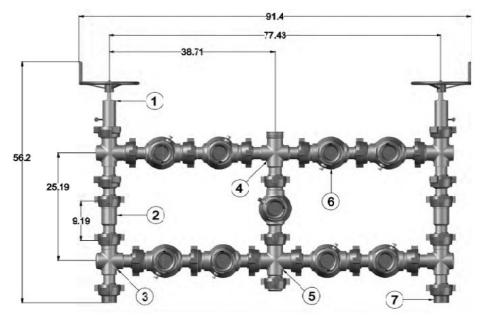


Figure 10. Nine valve 15k choke manifold.

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

		Casing Prog	ram Design A	•		BLM Minimum Safety	1.125	1.0	1.6 Dry	1.6 Dry
		O HOLLING T. TOP				Factors	11120	1.0	1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211u Stg 9.023 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	6732' - 9298'	472	2570	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9298'	8.6 - 9.7	Cut-Brine
9298' - 20075'	10.0 - 10.	OBM

Geology

scology						
Formation	Est. Top (TVD)	Mineral Resources	Iineral Resources Formation		Mineral Resources	
Rustler	1387'	Usable Water	Yeso			
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas	
Salt Top	1682'	None	Bell Canyon			
Salt Base	2932'	None	Cherry Canyon			
Yates	3166'	Oil/Natural Gas	Manzanita Marker			
Seven Rivers			Basal Brushy Canyon			
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas	
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas	
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas	
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas	
Glorieta			Wolfcamp			

	Y or N					
Is casing new? If used, attach certification as required in Onshore Order #1	Y					
Is casing API approved? If no, attach casing specification sheet.	Y					
Is premium or uncommon casing planned? If yes attach casing specification sheet.						
Does the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).						
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?						
Is well located within Capitan Reef?	Y					
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y					
Is well within the designated 4 string boundary.	N					
Is well located in SOPA but not in R-111-Q?	N					
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?						
Is well located in R-111-Q and SOPA?	N					
If yes, are the first three strings cemented to surface?						
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?						
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.						
Is an engineered weak point used to satisfy R-111-Q?						
If yes, at what depth is the weak point planned?						
Is well located in high Cave/Karst?	Y					
If yes, are there two strings cemented to surface?	Y					
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?						
Is well located in critical Cave/Karst?	N					
If yes, are there three strings cemented to surface?						

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

	Casing Program Design B					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	25%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1ot Sto 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg 7 in	TAIL	400	15.6	1.18	7641' - 10199'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

	Casing Program Design A					BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Chick Flogram								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 111	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
7 111	TAIL	400	15.6	1.18	6732' - 9298'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type	
	8.4 - 8.6		
0' - 1480'	8.4 - 8.6	Fresh Water	
1480' - 5110'	9.5 - 10.2	Brine	
5110' - 9298'	8.6 - 9.7	Cut-Brine	
9298' - 20075'	10.0 - 10.	OBM	

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres	1		3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N						
Is casing new? If used, attach certification as required in Onshore Order #1	Y						
Is casing API approved? If no, attach casing specification sheet.	Y						
s premium or uncommon casing planned? If yes attach casing specification sheet.							
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y						
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y						
Is well located within Capitan Reef?	Y						
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y						
Is well within the designated 4 string boundary.	N						
Is well located in SOPA but not in R-111-Q?	N						
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?							
Is well located in R-111-Q and SOPA?	N						
If yes, are the first three strings cemented to surface?							
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?							
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.							
Is an engineered weak point used to satisfy R-111-Q?							
If yes, at what depth is the weak point planned?							
Is well located in high Cave/Karst?	Y						
If yes, are there two strings cemented to surface?	Y						
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?							
Is well located in critical Cave/Karst?	N						
If yes, are there three strings cemented to surface?							

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

Casing Program Design B						BLM Minimum Safety Factors	1.125	1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2376	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist otg / in	TAIL	400	15.6	1.18	7641' - 10199'	472	45%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geolog

Geology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production easing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is $2^{\text{nd}}$ string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

•		Casing Prog	ram Design A		•	BLM Minimum Safety	1.125	1.0	1.6 Dry	1.6 Dry
		O HOLLING T. TOP				Factors	11120	1.0	1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13.375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.023 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
211d Stg 9.023 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	6732' - 9298'	472	2570	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type	
	8.4 - 8.6		
0' - 1480'	8.4 - 8.6	Fresh Water	
1480' - 5110'	9.5 - 10.2	Brine	
5110' - 9298'	8.6 - 9.7	Cut-Brine	
9298' - 20075'	10.0 - 10.	OBM	

Geology

Jeology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta	1		Wolfcamp		

	Y or N
Is easing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach easing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is $2^{\text{nd}}$ string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

Casing Program Design B					BLM Minimum Safety Factors	1.125	1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.375 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	23%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9,625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / in	TAIL	400	15.6	1.18	7641' - 10199'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

•	Casing Program Design				•	BLM Minimum Safety	BLM Minimum Safety	1.0	1.6 Dry	1.6 Dry
	Cuonig I rogram Design A					Factors	11120	1.0	1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description	
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM	
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder	
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM	
18t Stg 9.023 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder	
	9 5/8" DV Tool @ 3100'								
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM	
211d Stg 9.023 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder	
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer	
/ III	TAIL	400	15.6	1.18	6732' - 9298'	472	2570	Class H: Retarder, Fluid Loss, Defoamer	
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent	

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9298'	8.6 - 9.7	Cut-Brine
9298' - 20075'	10.0 - 10.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta	1		Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

Casing Program Design B					BLM Minimum Safety Factors	1.125	1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

_ 0								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	23%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9,625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / in	TAIL	400	15.6	1.18	7641' - 10199'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is $2^{\text{nd}}$ string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

	Casing Program Design A						BLM Minimum Safety 1.125	1.0	1.6 Dry	1.6 Dry
						Factors			1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	6732' - 9298'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9298'	8.6 - 9.7	Cut-Brine
9298' - 20075'	10.0 - 10.	OBM

Geology

Jeology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N					
Is casing new? If used, attach certification as required in Onshore Order #1	Y					
Is casing API approved? If no, attach casing specification sheet.	Y					
Is premium or uncommon casing planned? If yes attach casing specification sheet.						
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y					
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y					
Is well located within Capitan Reef?	Y					
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y					
Is well within the designated 4 string boundary.	N					
Is well located in SOPA but not in R-111-Q?	N					
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?						
Is well located in R-111-Q and SOPA?	N					
If yes, are the first three strings cemented to surface?						
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?						
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.						
Is an engineered weak point used to satisfy R-111-Q?						
If yes, at what depth is the weak point planned?						
Is well located in high Cave/Karst?	Y					
If yes, are there two strings cemented to surface?	Y					
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?						
Is well located in critical Cave/Karst?	N					
If yes, are there three strings cemented to surface?						

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

_ 0								
Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	23%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stg 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
ist stg / in	TAIL	400	15.6	1.18	7641' - 10199'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geolog

Geology					
Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
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Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
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If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>ad</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

	Casing Program Design A						1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
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Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
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Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description		
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13.5/5 III	TAIL	200	14.8	1.34	1289' - 1480'	268	10076	Class C: Retarder		
1st Stg 9,625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM		
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder		
	9 5/8" DV Tool @ 3100'									
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM		
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2376	Class C: Retarder		
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer		
/ III	TAIL	400	15.6	1.18	6732' - 9298'	472	2370	Class H: Retarder, Fluid Loss, Defoamer		
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent		

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9298'	8.6 - 9.7	Cut-Brine
9298' - 20075'	10.0 - 10.	OBM

Geology

Jeology					
Formation	Est. Top (TVD)	Mineral Resources	Mineral Resources Formation		Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta	1		Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach easing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and $3^{rd}$ string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	
is wen rocated in N-111-Q and SOFA:  If yes, are the first three strings cemented to surface?	N
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

Casing Program Design B				BLM Minimum Safety Factors		1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet		
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.3/5 III	TAIL	200	14.8	1.34	1289' - 1480'	268	100%	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	23%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1 of Sta 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg 7 in	TAIL	400	15.6	1.18	7641' - 10199'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

se casing new? If used, attach certification as required in Onshore Order #1  versing API approved? If no, attach casing specification sheet.  premium or uncommon casing specification sheet.  premium or uncommon casing planned? If yes attach casing specification sheet.  premium or uncommon casing planned? If yes attach casing specification sheet.  premium or uncommon casing planned? If yes attach casing specification sheet.  y y y lift the pipe be kept at a minimum I/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  y well located within Capitan Reer?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  y If yes, are the first 2 strings cement do surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  y well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  y well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  y an open annulus used to satisfy R-111-Q? If yes, see cement design.  y an open annulus used to satisfy R-111-Q? If yes, see cement design.  y well located in high Cave/Karst?  y well located in high Cave/Karst?  y y y life yes, is there a contingency casing if lost circulation occurs?  y well located in critical Cave/Karst?		
se casing API approved? If no, attach easing specification sheet.  Premium or uncommon casing planned? If yes attach easing specification sheet.  No sees the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  You will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement desting boundary.  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement desting cement desting the string cement desting the string cement desting the string cement desting the string cement desting the strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salf?  If yes, are the first three strings cemented to surface?  If yes, are what depth is the weak point planned?  If yes, are the rew to strings cemented to surface?  If yes, are where two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?		Y or N
s pemium or uncommon casing planned? If yes attach casing specification sheet.  Noes the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Y if the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  Y If yes, does production casing cement tie back a minimum of 50° above the Reef?  If yes, does production casing cement tie back a minimum of 50° above the Reef?  If yes, does production casing cement tie back a minimum of 50° above the Reef?  If yes, are the first 2 strings cemented to surface and 3°d string cement tied back 500° into previous casing?  If yes, are the first 2 strings cemented to surface and 3°d string cement tied back 500° into previous casing?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the depth is the weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are the first first weak point planned?  If yes, are three first first weak point planned?  If yes, are three first first weak point planned?  If yes, are three first first weak point planned?  If yes, are three first first weak point planned?  If yes, are three first first weak point planned?  If yes, are three first first weak point planned?	Is casing new? If used, attach certification as required in Onshore Order #1	Y
sees the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Yill the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  Y If yes, does production casing cement tie back a minimum of 50' above the Reef?  Y If yes, does production casing cement tie back a minimum of 50' above the Reef?  Y If yes, does production casing cement tie back a minimum of 50' above the Reef?  Y If yes, are the designated 4 string boundary.  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  In one namulus used to satisfy R-111-Q? If yes, see cement design.  If yes, are what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, is there a contingency casing if lost circulation occurs?  If yes, is there a contingency casing if lost circulation occurs?  N If yes, is there a contingency casing if lost circulation occurs?  N If yes, is there a contingency casing if lost circulation occurs?	Is casing API approved? If no, attach casing specification sheet.	Y
will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?  swell located within Capitan Reef? If yes, does production casing cement tie back a minimum of 50° above the Reef? If yes, does production casing cement tie back a minimum of 50° above the Reef? If yes, does production casing cement tie back a minimum of 50° above the Reef? If yes, are the first 2 strings oemented to surface and 3°d string cement tied back 500° into previous easing?  If yes, are the first 2 strings cemented to surface and 3°d string cement tied back 500° into previous easing?  If yes, are the first three strings cemented to surface?  Is 2°d string set 100° to 600° below the base of salf?  If yes, are the first three strings cemented to sarface?  If yes, are the first three strings cemented to sarface?  If yes, are the first three three strings cemented to sarface?  If yes, are the first three three strings cemented to sarface?  If yes, are then two strings cemented to sarface?  If yes, are then two strings cemented to sarface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, is there a contingency casing if lost circulation occurs?  If yes, are there two strings cemented to surface?  If yes, is there a contingency casing if lost circulation occurs?	Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
is well located within Capitan Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, does production casing cement tie back a minimum of 50' above the Reef?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  If yes, are the first 1 and SOPA?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, at what depth is the weak point planned?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are there there is the first three	Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?  Is well within the designated 4 string boundary.  Is well within the designated 4 string boundary.  Is well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  If yes, are the first 12 strings cemented to surface?  Is 2 <sup>rd</sup> string set 100° to 600° below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to	Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?  Is well within the designated 4 string boundary.  Is well within the designated 4 string boundary.  Is well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  If yes, are the first 12 strings cemented to surface?  Is 2 <sup>rd</sup> string set 100° to 600° below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to		
Is well within the designated 4 string boundary.  Note that the strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  Note that the strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  Note that the strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point planned?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  You for 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  Note that the designated 4 string boundary.  Note that the designa	Is well located within Capitan Reef?	Y
is well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous easing?  If yes, are the first 1 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous easing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it wo strings cemented to surface?  If yes, are there it is a surface?  If yes, are the first it is a surface?  If yes, are the first it is a surface?  If yes, are the first it is a surface?  If yes, are the first it is a surface?  If yes, are there it is a surface?  If yes, are the first it is a surface?  If	If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous easing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  Y  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  N  N  N	Is well within the designated 4 string boundary.	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous easing?  If yes, are the first three strings cemented to surface?  Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  Is an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  Y  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  N  N  N		
is well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt? Is an open annulus used to satisfy R-111-Q? If yes, see cement design. If yes, at what depth is the weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  If yes well located in critical Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	Is well located in SOPA but not in R-111-Q?	N
If yes, are the first three strings cemented to surface?  Is 2 <sup>m2</sup> string set 100' to 600' below the base of salt?  sa no open annulus used to satisfy R-111-Q? If yes, see cement design.  sa negineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  N	If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
If yes, are the first three strings cemented to surface?  Is 2 <sup>m2</sup> string set 100' to 600' below the base of salt?  sa no open annulus used to satisfy R-111-Q? If yes, see cement design.  sa negineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  N		
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt? an open annulus used to satisfy R-111-Q? If yes, see cement design. an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  N		N
an open amulus used to satisfy R-111-Q? If yes, see cement design.  an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  swell located in critical Cave/Karst?	If yes, are the first three strings cemented to surface?	
s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  N	Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	
If yes, at what depth is the weak point planned?  swell located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  swell located in critical Cave/Karst?  N	Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  N	Is an engineered weak point used to satisfy R-111-Q?	
If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  well located in critical Cave/Karst?  N	If yes, at what depth is the weak point planned?	
If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  well located in critical Cave/Karst?  N		
(For 2 string wells) If yes, is there a contingency easing if lost circulation occurs?  swell located in critical Cave/Karst?  N		Y
s well located in critical Cave/Karst?  N		Y
	(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
If yes, are there three strings cemented to surface?	Is well located in critical Cave/Karst?	N
	If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

		Casing Prog	ram Design A	•	•	BLM Minimum Safety	1.125	1.0	1.6 Dry	1.6 Dry
						Factors			1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2.12	190.23	208.18
Production	8.75"	0'	0'	9298'	9238'	7" 26# P110 LTC	1.34	2.14	2.87	3.43
Liner	6.125"	9098'	9046'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.28	2.85

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	тос/вос	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
15.575 III	TAIL	200	14.8	1.34	1289' - 1480'	268	100%	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t 5tg 5.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	2370	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	2370	Class C: Retarder
7 in	LEAD	280	12.5	2.12	3469' - 6732'	600	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
7 111	TAIL	400	15.6	1.18	6732' - 9298'	472	2370	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	700	13.5	1.85	9098' - 20075'	1300	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 9298'	8.6 - 9.7	Cut-Brine
9298' - 20075'	10.0 - 10.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso	•	
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta	1		Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 3 <sup>nd</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Drv 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	1480'	1480'	13.375" 48# H40 STC	1.16	2.61	4.53	7.62
Int	12.25"	0'	0'	3200'	3200'	9.625" 36# J55 LTC	1.19	2.07	2.36	2.94
Int	12.25"	3200'	3200'	4100'	4100'	9.625" 40# J55 LTC	1.18	1.82	6.81	8.25
Int	12.25"	4100'	4100'	5000'	5000'	9.625" 40# L80 LTC	1.17	2.17	18.24	22.67
Int	12.25"	5000'	5000'	5110'	5110'	9.625" 40# HCL80 LTC	1.56	2,12	190.23	208.18
Production	8.75"	0'	0'	10199'	9826'	7" 26# P110 LTC	1.26	2.01	2.61	3.13
Liner	6.125"	9298'	9238'	20075'	10033'	4.5" 13.5# P110 LTC	2.05	2.38	2.32	2.90

#### Design B - Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft <sup>3</sup> /sack	TOC/BOC	Volume ft <sup>3</sup>	% Excess	Slurry Description
13,375 in	LEAD	850	12.5	2.12	0' - 1289'	1810	100%	Class C: Salt, Gel, Extender, LCM
13.3/5 III	TAIL	200	14.8	1.34	1289' - 1480'	268	100%	Class C: Retarder
1st Stg 9.625 in	LEAD	250	12.5	2.12	3100' - 4435'	530	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 III	TAIL	200	14.8	1.34	4435' - 5110'	268	23%	Class C: Retarder
					9 5/8" DV T	ool @ 3100'		
2nd Stg 9.625 in	LEAD	500	12.5	2.12	0' - 2752'	1060	25%	Class C: Salt, Gel, Extender, LCM
2110 Stg 9.025 III	TAIL	100	14.8	1.34	2752' - 3100'	134	23%	Class C: Retarder
1st Stor 7 in	LEAD	360	12.5	2.12	3469' - 7641'	770	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg 7 in	TAIL	400	15.6	1.18	7641' - 10199'	472	25%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	680	13.5	1.85	9298' - 20075'	1260	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant,

#### Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 1480'	8.4 - 8.6	Fresh Water
1480' - 5110'	9.5 - 10.2	Brine
5110' - 10199'	8.6 - 9.7	Cut-Brine
10199' - 20075'	10.0 - 10.	OBM

#### Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler	1387'	Usable Water	Yeso		
Castile			Delaware (Lamar)	5807'	Oil/Natural Gas
Salt Top	1682'	None	Bell Canyon		
Salt Base	2932'	None	Cherry Canyon		
Yates	3166'	Oil/Natural Gas	Manzanita Marker		
Seven Rivers			Basal Brushy Canyon		
Queen	4133'	Oil/Natural Gas	Bone Spring	7652'	Oil/Natural Gas
Capitan	3519'	Usable Water	1st Bone Spring	8833'	Oil/Natural Gas
Grayburg			2nd Bone Spring	9382'	Oil/Natural Gas
San Andres			3rd Bone Spring	10105'	Oil/Natural Gas
Glorieta			Wolfcamp		

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 <sup>ad</sup> string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there strings cemented to surface?	

# **Mewbourne Oil Company**

Lea County, New Mexico NAD 83 Spanish Bay 18/19 Fed Com #528H

Sec 18, T19S, R33E

SHL: 205' FNL & 1460' FEL (Sec 18) BHL: 100' FSL & 660' FEL (Sec 19)

Plan: Design #1

# **Standard Planning Report**

05 June, 2024

Hobbs Database:

Company: Mewbourne Oil Company

Project: Lea County, New Mexico NAD 83 Site: Spanish Bay 18/19 Fed Com #528H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 660' FEL (Sec 19)

Design #1 Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Grid

Minimum Curvature

Project Lea County, New Mexico NAD 83

Map System: US State Plane 1983 North American Datum 1983 Geo Datum: Map Zone:

New Mexico Eastern Zone

System Datum:

Mean Sea Level

Spanish Bay 18/19 Fed Com #528H Site

Northing: 606,969.40 usft 32.6669990 Site Position: Latitude: From: Мар Easting: 736,683.70 usft Longitude: -103.6985270

Slot Radius: 13-3/16 **Position Uncertainty:** 0.0 usft

Well Sec 18, T19S, R33E

**Well Position** +N/-S 0.0 usft 606,969.40 usft Latitude: 32.6669990 Northing: +E/-W 0.0 usft Easting: 736,683.70 usft Longitude: -103.6985270

0.0 usft Wellhead Elevation: 3,676.0 usft Ground Level: 3,648.0 usft **Position Uncertainty** 

**Grid Convergence:** 0.34°

BHL: 100' FSL & 660' FEL (Sec 19) Wellbore

Field Strength Magnetics **Model Name** Sample Date Declination Dip Angle (°) (nT) (°) **I**GRF2010 12/31/2014 7.24 60.48 48,512.61634347

Design Design #1

Audit Notes:

PROTOTYPE Version: Phase: Tie On Depth: 0.0

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°) 175.35 0.0 0.0 0.0

6/5/2024 Plan Survey Tool Program Date

**Depth From** Depth To

(usft) (usft) Survey (Wellbore) **Tool Name** Remarks

Design #1 (BHL: 100' FSL & 660' 0.0 20,075.0

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,600.0	0.00	0.00	1,600.0	0.0	0,0	0.00	0.00	0.00	0.00	
1,920.2	6.40	76.31	1,919.5	4.2	17.4	2.00	2.00	0.00	76.31	
8,978.2	6.40	76.31	8,933.5	190.6	782.2	0.00	0.00	0.00	0.00	
9,298.4	0.00	0.00	9,253.0	194.8	799.6	2.00	-2.00	0.00	180.00	KOP: 10' FNL & 660' I
10,186.6	88.80	179.81	9,826.0	-366.3	801.4	10.00	10.00	0.00	179.81	
20,075.0	88.80	179.81	10,033.0	-10,252.5	833.4	0.00	0.00	0.00	0.00	BHL: 100' FSL & 660'

Database: Hobbs

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83
Site: Spanish Bay 18/19 Fed Com #528H

**Well:** Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 660' FEL (Sec 19)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Grid

ned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
SHL: 205' I	FNL & 1460' FEL (	Sec 18)							
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0		0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0		0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0		0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0		0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0		0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0		0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0		0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0		0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	0.00	0.00	1,500.0	0.0	0.0	0.0	0.00	0.00	0.00
1,600.0		0.00	1,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1,700.0		76.31	1,700.0	0.4	1.7	-0.3	2.00	2.00	0.00
1,800.0		76.31	1,799.8	1.7	6.8	-1.1	2.00	2.00	0.00
1,900.0		76.31	1,899.5	3.7	15.2	-2.5	2.00	2.00	0.00
1,920,2		76,31	1,919 <u>.</u> 5	4,2	17.4	-2.8	2,00	2,00	0,00
2,000.0		76,31	1,998.8	6,3	26.0	-4.2	0.00	0.00	0.00
2,100.0		76,31	2,098,2	9.0	36.9	-6.0	0.00	0.00	0.00
2,200.0		76,31	2,197.6	11,6	47.7	-7.7	0.00	0.00	0.00
2,300.0	6.40	76,31	2,297.0	14.3	58,5	-9.5	0.00	0.00	0.00
2,400.0	6.40	76.31	2,396.3	16.9	69.4	-11.2	0.00	0.00	0.00
2,500.0	6.40	76.31	2,495.7	19.5	80.2	<b>-</b> 13.0	0.00	0.00	0.00
2,600.0	6.40	76.31	2,595.1	22.2	91.0	-14.7	0.00	0.00	0.00
2,700.0	6.40	76.31	2,694.5	24.8	101.9	-16.5	0.00	0.00	0.00
2,800.0	6.40	76.31	2,793.8	27.5	112.7	-18.2	0.00	0.00	0.00
0.000.0	0.40	70.04	0.000.0	20.4	400 F	20.0	0.00	0.00	0.00
2,900.0		76.31	2,893.2	30.1	123.5	-20.0	0.00	0.00	0.00
3,000.0		76.31	2,992.6	32.7	134.4	-21.7	0.00	0.00	0.00
3,100.0		76.31	3,092.0 3.191.3	35.4	145.2	-23.5 25.3	0.00	0.00	0.00
3,200.0		76.31	,	38.0 40.7	156.1	-25.3	0.00	0.00	0.00
3,300.0	6.40	76.31	3,290.7	40.7	166.9	-27.0	0.00	0.00	0.00
3,400.0		76.31	3,390.1	43.3	177.7	-28.8	0.00	0.00	0.00
3,500.0		76.31	3,489.5	45.9	188.6	-30.5	0.00	0.00	0.00
3,600.0	6.40	76.31	3,588.9	48.6	199.4	-32.3	0.00	0.00	0.00
3,700.0	6.40	76.31	3,688.2	51.2	210.2	-34.0	0.00	0.00	0.00
3,800.0	6.40	76.31	3,787.6	53.9	221.1	-35.8	0.00	0.00	0.00
3,900.0	6.40	76.31	3,887.0	56.5	231.9	-37.5	0.00	0.00	0.00
4,000.0		76.31 76.31	3,986.4	59.1	242.8	-37.3 -39.3	0.00	0.00	0.00
4,000.0		76.31 76.31	4,085.7	61.8	2 <del>4</del> 2.6 253.6	-39.3 -41.0	0.00	0.00	0.00
4,200.0		76.31	4,185.1	64.4	264.4	-41.0 -42.8	0.00	0.00	0.00
4,200.0		76.31 76.31	4,185.1	67.1	275.3	-42.6 -44.5	0.00	0.00	0.00
4,400.0		76.31	4,383.9	69.7	286.1	-46.3	0.00	0.00	0.00
4,500.0		76.31	4,483.2	72.3	296.9	-48.0	0.00	0.00	0.00
4,600.0		76.31	4,582.6	75.0	307.8	-49.8	0.00	0.00	0.00
4,700.0		76.31	4,682.0	77.6	318.6	-51.6	0.00	0.00	0.00
4,800.0	6.40	76.31	4,781.4	80.3	329.4	-53.3	0.00	0.00	0.00
4,900.0	6.40	76.31	4,880.7	82.9	340.3	-55.1	0.00	0.00	0.00
5,000.0		76.31 76.31	4,980.1	85.5	351.1	-56.8	0.00	0.00	0.00
5,000.0 5,100.0		76.31 76.31	5,079.5	88.2	362.0	-58.6	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83

Site: Spanish Bay 18/19 Fed Com #528H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 660' FEL (Sec 19)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0 5,300.0	6.40 6.40	76.31 76.31	5,178.9 5,278.2	90.8 93.5	372.8 383.6	<b>-</b> 60.3 <b>-</b> 62.1	0.00 0.00	0.00 0.00	0.00 0.00
5,400.0	6.40	76.31	5,377.6	96.1	394.5	-63.8	0.00	0.00	0.00
5,500.0	6.40	76.31	5,477.0	98.7	405.3	-65.6	0.00	0.00	0.00
5,600.0	6.40	76.31	5,576.4	101.4	416.1	-67.3	0.00	0.00	0.00
5,700.0	6.40	76.31	5,675.7	104.0	427.0	-69.1	0.00	0.00	0.00
5,800.0	6.40	76.31	5,775.1	106.7	437.8	<del>-</del> 70.8	0.00	0.00	0.00
5,900.0	6.40	76,31	5,874.5	109.3	448.7	-72.6	0.00	0.00	0.00
6,000.0	6.40	76.31	5,973.9	111.9	459.5	-74.3	0.00	0.00	0.00
6,100.0	6.40	76.31	6,073.3	114.6	470.3	-76.1	0.00	0.00	0.00
6,200.0	6.40	76.31	6,172.6	117.2	481.2	-77.9	0.00	0.00	0.00
6,300.0	6.40	76.31	6,272.0	119.9	492.0	-79.6	0.00	0.00	0.00
6,400.0	6.40	76.31	6,371.4	122.5	502.8	-81.4	0.00	0.00	0.00
6,500.0	6.40	76.31	6,470.8	125.1	513.7	-83.1	0.00	0.00	0.00
6,600.0	6.40	76.31	6,570.1	127.8	524.5	-84.9	0.00	0.00	0.00
6,700.0	6.40	76.31	6,669.5	130.4	535.3	-86.6	0.00	0.00	0.00
6,800.0	6.40	76.31	6,768.9	133.1	546.2	-88.4	0.00	0.00	0.00
6,900.0	6.40	76,31	6,868,3	135.7	557.0	-90.1	0.00	0,00	0.00
7,000.0	6.40	76,31	6,967.6	138,3	567.9	-91.9	0.00	0.00	0,00
7,100.0	6.40	76,31	7,067.0	141.0	578.7	-93,6	0.00	0.00	0.00
7,200.0	6.40	76,31	7,166.4	143.6	589,5	-95.4	0.00	0.00	0.00
7,300.0	6.40	76,31	7,265,8	146,3	600,4	-97.1	0,00	0,00	0.00
7,400.0	6.40	76.31	7,365.1	148.9	611.2	-98.9	0.00	0.00	0.00
7,500.0	6.40	76.31	7,464.5	151.5	622.0	-100.6	0.00	0.00	0.00
7,600.0	6.40	76.31	7,563.9	154.2	632.9	-102.4	0.00	0.00	0.00
7,700.0	6.40	76.31	7,663.3	156.8	643.7	-104.2	0.00	0.00	0.00
7,800.0	6.40	76.31	7,762.6	159.5	654.6	-105.9	0.00	0.00	0.00
7,900.0	6.40	76,31	7,862,0	162,1	665,4	-107.7	0.00	0,00	0,00
8,000.0	6.40	76,31	7,961.4	164,7	676,2	-109.4	0.00	0.00	0.00
8,100.0	6.40	76,31	8,060.8	167.4	687.1	-111.2	0.00	0.00	0.00
8,200.0	6.40	76,31	8,160.1	170.0	697.9	-112.9	0.00	0.00	0.00
8,300.0	6.40	76,31	8,259.5	172,7	708.7	-114.7	0,00	0.00	0.00
8,400.0	6.40	76.31	8,358.9	175.3	719.6	-116.4	0.00	0.00	0.00
8,500.0	6.40	76.31	8,458.3	177.9	730.4	-118.2	0.00	0.00	0.00
8,600.0	6.40	76.31	8,557.7	180.6	741.2	-119.9	0.00	0.00	0.00
8,700.0	6.40	76.31	8,657.0	183.2	752.1	-121.7	0.00	0.00	0.00
8,800.0	6.40	76.31	8,756.4	185.9	762.9	-123.4	0.00	0.00	0.00
8,900.0	6.40	76.31	8,855.8	188.5	773.8	-125.2	0.00	0.00	0.00
8,978.2	6.40	76.31	8,933.5	190.6	782.2	-126.6	0.00	0.00	0.00
9,000.0	5.97	76.31	8,955.2	191.1	784.5	-126.9	2.00	-2.00	0.00
9,100.0	3.97	76.31	9,054.8	193.2	792.9	-128.3	2.00	-2.00	0.00
9,200.0	1.97	76.31	9,154.6	194.4	798.0	-129.1	2,00	-2.00	0.00
9,298.4	0.00	0.00	9,253.0	194.8	799.6	-129.4	2.00	-2.00	0.00
KOP: 10' FN	L & 660' FEL (Se	ec 18)							
9,300.0	0.16	179.81	9,254.6	194.8	799.6	<b>-</b> 129.4	10.00	10.00	0.00
9,350.0	5.16	179.81	9,304.6	192.5	799.6	<b>-</b> 127.1	10.00	10.00	0.00
9,400.0	10.16	179.81	9,354.1	185.8	799.6	<b>-</b> 120.4	10.00	10.00	0.00
9,450.0	15.16	179.81	9,402.9	174.9	799.7	<b>-</b> 109.5	10.00	10.00	0.00
9,500.0	20.16	179.81	9,450.5	159.7	799.7	-94.4	10.00	10.00	0.00
9,550,0	25.16	179,81	9,496.6	140.4	799,8	-75.2	10,00	10,00	0,00
9,600.0	30.15	179,81	9,540.9	117,2	799.9	-52,1	10,00	10,00	0,00
9,623.9	32.54	179,81	9,561,3	104.8	799,9	-39.7	10.00	10,00	0.00
FTP: 100' FN	IL & 660' FEL (Se	ec 18)							
9,650.0	35.15	179.81	9,583.0	90.3	799.9	-25.2	10.00	10.00	0.00

Hobbs Database: Company:

Mewbourne Oil Company

Lea County, New Mexico NAD 83 Spanish Bay 18/19 Fed Com #528H

Well: Wellbore:

Project:

Site:

Sec 18, T19S, R33E BHL: 100' FSL & 660' FEL (Sec 19)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Plann	ned Survey									
	Measured			Vertical			Vertical	Dogleg	Build	Turn
	Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Section (usft)	Rate (°/100usft)	Rate (°/100usft)	Rate (°/100usft)
	9,700.0	40.15	179.81	9,622.6	59.7	800.0	5.3	10.00	10.00	0.00
	9,750.0	45.15	179,81	9,659.3	25.9	800.1	39.0	10.00	10.00	0,00
	9,800.0	50.15	179.81	9,693.0	-11.1	800.3	75.9	10.00	10.00	0.00
	9,850.0	55 <b>.</b> 15	179.81	9,723.3	-50.8	800.4	115.5	10.00	10.00	0.00
	9,900.0	60.15	179.81	9,750.1	-93.0	800.5	157.6	10.00	10.00	0.00
	9,950.0	65.14	179.81	9,773.0	-137.4	800.7	201.8	10.00	10.00	0.00
	10,000.0	70.14	179,81	9,792.0	-183.6	8.00.8	247.9	10.00	10.00	0.00
	10,050.0	75.14	179.81	9,807.0	-231.3	801.0	295.5	10.00	10.00	0.00
	10,100.0	80.14	179.81	9,817.7	-280.2	801.1	344.2	10.00	10.00	0.00
	10,150.0	85.14	179.81	9,824.1	-329.7	801.3	393.6	10.00	10.00	0.00
	10,186.6	88.80	179.81	9,826.0	-366.3	801.4	430.1	10.00	10.00	0.00
	10,198.5	88.80	179.81	9,826.2	-378.2	801.5	441.9	0.00	0.00	0.00
	LP: 583' FNL	. & 660' FEL (Sed	c 18)							
	10,200.0	88.80	179.81	9,826.3	-379.7	801.5	443.4	0.00	0.00	0.00
	10,300.0	88.80	179.81	9,828.4	-479.7	801.8	543.0	0.00	0.00	0.00
	10,400.0	88.80	179.81	9,830.5	-579.6	802.1	642.7	0.00	0.00	0.00
	10,500.0	88.80	179.81	9,832.6	-679.6	802.4	742.4	0.00	0.00	0.00
	10,600.0	88.80	179.81	9,834.7	-779.6	802.8	842.1	0.00	0.00	0.00
	10,700.0	88.80	179,81	9,836.7	-879.6	803.1	941.7	0.00	0.00	0.00
	10,800.0	88.80	179,81	9,838.8	-979.5	803.4	1,041.4	0.00	0.00	0,00
	10,900.0	88.80	179,81	9,840.9	-1,079.5	803.7	1,141.1	0.00	0.00	0,00
	11,000.0	88.80	179.81	9,843.0	<b>-</b> 1,179.5	804.0	1,240.8	0.00	0.00	0.00
	11,100.0	88.80	179.81	9,845.1	<b>-</b> 1,279.5	804.4	1,340.4	0.00	0.00	0.00
	11,200.0	88.80	179.81	9,847.2	-1,379.5	804.7	1,440.1	0.00	0.00	0.00
	11,300.0	88.80	179.81	9,849.3	-1,479.4	805.0	1,539.8	0.00	0.00	0.00
	11,400.0	88.80	179.81	9,851.4	<b>-</b> 1,579.4	805.3	1,639.5	0.00	0.00	0.00
	11,500.0	88.80	179,81	9,853,5	-1,679.4	805.7	1,739,1	0.00	0,00	0,00
	11,600.0	88.80	179.81	9,855.6	-1,779.4	806.0	1,838.8	0.00	0,00	0.00
	11,700.0	88.80	179.81	9,857.7	-1,879.3	806.3	1,938.5	0.00	0.00	0.00
	11,800.0	88.80	179,81	9,859.8	-1,979.3	806.6	2,038.2	0.00	0.00	0.00
	11,900.0	88.80	179.81	9,861.9	-2,079.3	807.0	2,137.8	0.00	0.00	0.00
	12,000.0	88.80	179.81	9,864.0	-2,179.3	807.3	2,237.5	0.00	0.00	0.00
	12,100.0	88.80	179.81	9,866.1	-2,279.3	807.6	2,337.2	0.00	0.00	0.00
	12,200.0	88.80	179.81	9,868.1	-2,379.2	807.9	2,436.9	0.00	0.00	0.00
	12,300.0	88.80	179.81	9,870.2	-2,479.2	808.3	2,536.5	0.00	0.00	0.00
	12,400.0	88.80	179.81	9,872.3	<b>-</b> 2,579.2	808.6	2,636.2	0.00	0.00	0.00
	12,500.0	88.80	179.81	9,874.4	-2,679.2	808.9	2,735.9	0.00	0.00	0.00
	12,600.0	88.80	179.81	9,876.5	-2,779.1	809.2	2,835.6	0.00	0.00	0.00
	12,700.0	88.80	179.81	9,878.6	-2,879.1	809.5	2,935.2	0.00	0.00	0.00
	12,800.0	88.80	179.81	9,880.7	-2,979.1	809.9	3,034.9	0.00	0.00	0.00
	12,900.0	88.80	179.81	9,882.8	-3,079.1	810.2	3,134.6	0.00	0.00	0.00
	13,000.0	88.80	179.81	9,884.9	<b>-</b> 3,179.1	810.5	3,234.3	0.00	0.00	0.00
	13,100.0	88.80	179.81	9,887.0	-3,279.0	810.8	3,333.9	0.00	0.00	0.00
	13,200.0	88.80	179.81	9,889.1	<b>-</b> 3,379.0	811.2	3,433.6	0.00	0.00	0.00
	13,300.0	88.80	179.81	9,891.2	<b>-</b> 3,479.0	811.5	3,533.3	0.00	0.00	0.00
	13,400.0	88.80	179.81	9,893.3	<b>-</b> 3,579.0	811.8	3,633.0	0.00	0.00	0.00
	13,500.0	88.80	179.81	9,895.4	-3,678.9	812.1	3,732.6	0.00	0.00	0.00
	13,600.0	88.80	179.81	9,897.5	-3,778.9	812.5	3,832.3	0.00	0.00	0.00
	13,700.0	88.80	179.81	9,899.5	-3,878.9	812.8	3,932.0	0.00	0.00	0.00
	13,800.0	88.80	179,81	9,901.6	-3,978.9	813,1	4,031.7	0.00	0.00	0,00
	13,900.0	88.80	179,81	9,903.7	-4,078.9	813.4	4,131.3	0.00	0.00	0.00
	14,000.0	88.80	179.81	9,905.8	-4,178.8	813.7	4,231.0	0.00	0.00	0.00
	14,100.0	88.80	179.81	9,907.9	<b>-</b> 4,278.8	814.1	4,330.7	0.00	0.00	0.00
	., •			,	,		,			

Database: Hobbs

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83
Site: Spanish Bay 18/19 Fed Com #528H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 660' FEL (Sec 19)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Grid

Planned Su	rvey									
	asured Depth Jusft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	14,200.0	88.80	179,81	9,910.0	-4,378.8	814.4	4,430.4	0.00	0.00	0.00
	14,300.0	88.80	179,81	9,912.1	<b>-</b> 4,478.8	814.7	4,530.0	0.00	0.00	0.00
	14,400.0	88.80	179,81	9,914.2	<b>-</b> 4,578.7	815.0	4,629.7	0.00	0.00	0.00
	14,500.0	88.80	179,81	9.916.3	-4,678.7	815.4	4,729.4	0.00	0.00	0.00
	14,600.0	88.80	179.81	9,918.4	-4,778.7	815.7	4,829.1	0.00	0.00	0.00
	14,700.0	88.80	179.81	9,920.5	-4,878.7	816.0	4,928.7	0.00	0.00	0.00
	14,800.0	88.80	179.81	9,922.6	-4,978.7	816.3	5,028.4	0.00	0.00	0.00
	14,900.0	88.80	179.81	9,924.7	-5,078.6	816.7	5,128.1	0.00	0.00	0.00
	15,000.0	88.80	179.81	9,926.8	-5,178.6	817.0	5,227.8	0.00	0.00	0.00
	15,000.0	88.80	179.81	9,928.9	-5,278.6	817.3	5,327.4	0.00	0.00	0.00
	15,200.0	88.80	179.81	9,930.9	-5,378.6	817.6	5,427.1	0.00	0.00	0.00
	15,300.0	88.80	179.81	9,933.0	-5,478.5	818.0	5,526.8	0.00	0.00	0.00
	15,400.0	88.80	179.81	9,935.1	-5,578.5	818.3	5,626.5	0.00	0.00	0.00
	15,500.0	88.80	179.81	9,937.2	-5,678.5	818.6	5,726.1	0.00	0.00	0.00
	15,600.0	88.80 88.80	179.81 179.81	9,939.3 9,941.4	-5,778.5 5.878.4	818.9	5,825.8 5,925.5	0.00	0.00 0.00	0.00
	15,700.0				-5,878.4 5,078.4	819.2		0.00		0.00
	15,800.0 15,900.0	88.80 88.80	179.81 179.81	9,943.5 9,945.6	-5,978.4 -6,078.4	819.6 819.9	6,025.2 6,124.8	0.00 0.00	0.00 0.00	0.00 0.00
	15,900.0									
	16,000.0	88.80	179,81	9,947.7	-6,178.4	820,2	6,224,5	0.00	0,00	0,00
	16,100.0	88.80	179,81	9,949.8	-6,278.4	820,5	6,324,2	0,00	0.00	0,00
	16,200.0	88.80	179,81	9,951.9	-6,378.3	820,9	6,423,9	0,00	0.00	0.00
	16,300.0	88.80	179,81	9,954.0	-6,478.3	821.2	6,523,5	0.00	0.00	0.00
	16,400.0	88.80	179,81	9,956.1	-6,578.3	821,5	6,623,2	0,00	0.00	0.00
	16,500.0	88.80	179.81	9,958.2	-6,678.3	821.8	6,722.9	0.00	0.00	0.00
	16,600.0	88.80	179.81	9,960.3	-6,778.2	822.2	6,822.6	0.00	0.00	0.00
	16,700.0	88.80	179.81	9,962.3	-6,878.2	822.5	6,922.3	0.00	0.00	0.00
	16,800.0	88.80	179.81	9,964.4	-6,978.2	822.8	7,021.9	0.00	0.00	0.00
	16,900.0	88.80	179.81	9,966.5	-7,078.2	823.1	7,121.6	0.00	0.00	0.00
	17,000.0	88.80	179,81	9,968,6	-7,178,2	823.5	7,221,3	0.00	0,00	0.00
	17,100.0	88.80	179,81	9,970.7	-7,278.1	823.8	7,321.0	0.00	0,00	0.00
	17,200.0	88.80	179,81	9,972.8	-7,378.1	824.1	7,420.6	0.00	0,00	0.00
	17,300.0	88.80	179,81	9,974.9	-7,478.1	824.4	7,520.3	0.00	0.00	0.00
	17,400.0	88.80	179,81	9,977.0	-7,578.1	824.7	7,620.0	0.00	0.00	0.00
	17 500 0		170.91				7 740 7	0.00	0.00	0.00
	17,500.0 17,533.6	88.80 88.80	179.81 179.81	9,979.1 9,979.8	-7,678.0 -7,711.6	825.1 825.2	7,719.7 7,753.1	0.00	0.00	0.00 0.00
				9,979.0	-7,711.0	023.2	7,755.1	0.00	0.00	0.00
		FSL & 657' FEL	•	0.004.0	<b>-</b> 7,778,0	925 4	7 940 9	0.00	0.00	0.00
	17,600.0 17,700.0	88.80 88.80	179.81 179.81	9,981.2 9,983.3	-7,778.0 -7,878.0	825.4 825.7	7,819.3 7,919.0	0.00 0.00	0.00 0.00	0.00 0.00
	17,700.0	88.80	179.81	9,985.4	-7,676.0 -7,978.0	826.0	7,919.0 8,018.7	0.00	0.00	0.00
					,		•			
	17,900.0	88.80	179.81	9,987.5	-8,078.0	826.4	8,118.4	0.00	0.00	0.00
	18,000.0	88.80	179.81	9,989.6	-8,177.9	826.7	8,218.0	0.00	0.00	0.00
	18,100.0	88.80	179.81	9,991.7	-8,277.9	827.0	8,317.7	0.00	0.00	0.00
	18,200.0	88.80	179.81	9,993.7	-8,377.9 8,477.0	827.3	8,417.4	0.00	0.00	0.00
	18,300.0	88.80	179.81	9,995.8	-8,477.9	827.7	8,517.1	0.00	0.00	0.00
	18,400.0	88.80	179.81	9,997.9	<b>-</b> 8,577.8	828.0	8,616.7	0.00	0.00	0.00
	18,500.0	88.80	179.81	10,000.0	<b>-</b> 8,677.8	828.3	8,716.4	0.00	0.00	0.00
	18,600.0	88.80	179.81	10,002.1	<b>-</b> 8,777.8	828.6	8,816.1	0.00	0.00	0.00
	18,700.0	88.80	179.81	10,004.2	-8,877.8	829.0	8,915.8	0.00	0.00	0.00
	18,800.0	88.80	179.81	10,006.3	-8,977.8	829.3	9,015.4	0.00	0.00	0.00
	18,900.0	88.80	179,81	10,008.4	-9,077.7	829,6	9,115,1	0.00	0.00	0.00
	19,000.0	88.80	179.81	10,010.5	-9,177.7	829.9	9,214.8	0.00	0.00	0.00
	19,100.0	88.80	179,81	10,012,6	-9,277.7	830,2	9,314.5	0,00	0.00	0.00
	19,200.0	88.80	179,81	10,014.7	-9,377.7	830,6	9,414.1	0.00	0.00	0.00
	19,300.0	88.80	179,81	10,016.8	-9,477.6	830.9	9,513,8	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company
Project: Lea County, New Mexico NAD 83

Site: Spanish Bay 18/19 Fed Com #528H

Well: Sec 18, T19S, R33E

Wellbore: BHL: 100' FSL & 660' FEL (Sec 19)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

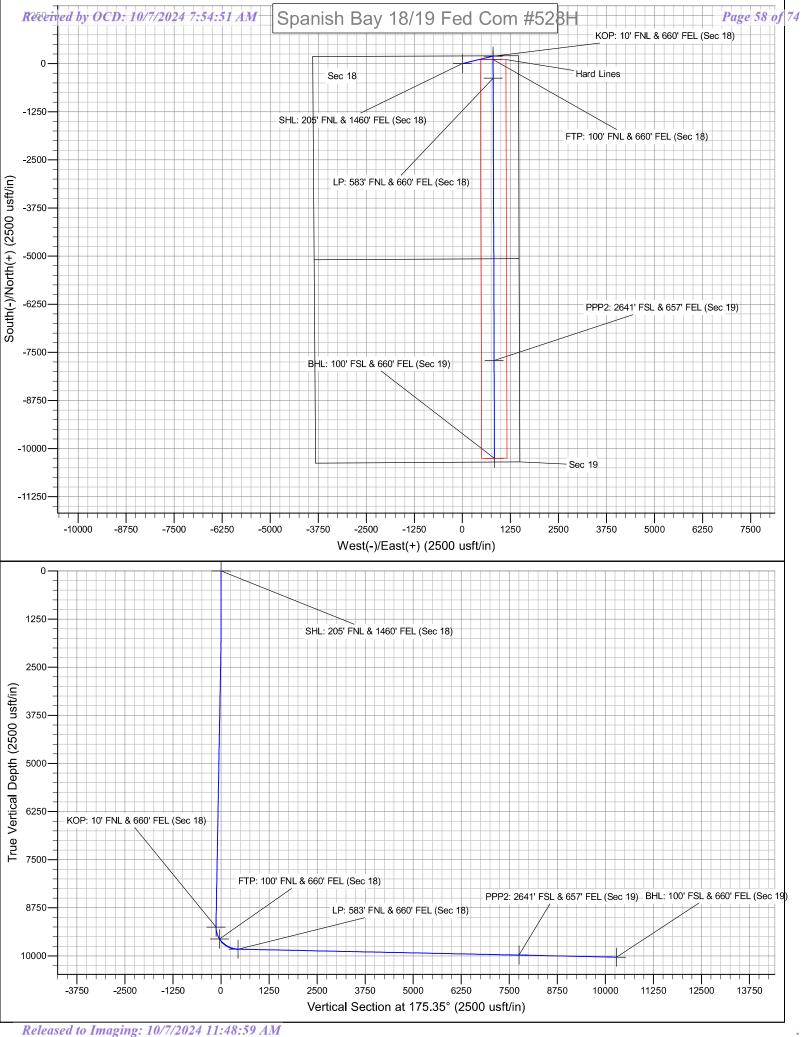
Site Spanish Bay 18/19 Fed Com #528H

Original Well @ 3676.0usft Original Well @ 3676.0usft

Grid

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
19,400,0	88.80	179.81	10,018,9	-9.577,6	831,2	9,613,5	0.00	0.00	0,00
19,500,0	88.80	179.81	10,021,0	-9,677.6	831.5	9.713.2	0.00	0.00	0.00
19,600,0	88.80	179,81	10,023,1	-9,777,6	831,9	9,812,8	0.00	0,00	0,00
19,700,0	88.80	179,81	10,025,1	-9,877,6	832,2	9,912,5	0.00	0,00	0.00
19,800.0	88.80	179.81	10,027.2	-9,977.5	832.5	10,012.2	0.00	0.00	0.00
19,900.0	88.80	179,81	10,029.3	-10,077.5	832.8	10,111.9	0.00	0.00	0.00
20,000.0	88.80	179.81	10,031.4	-10,177.5	833.2	10,211.5	0.00	0.00	0.00
20,075,0	88.80	179,81	10,033,0	-10,252,5	833,4	10,286,3	0,00	0,00	0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL: 205' FNL & 1460' F - plan hits target cent - Point	0.00 er	0.00	0.0	0.0	0.0	606,969.40	736,683.70	32.6669990	-103.6985270
KOP: 10' FNL & 660' FE - plan hits target cent - Point	0.00 er	0.00	9,253.0	194.8	799.6	607,164.20	737,483.30	32.6675212	-103.6959249
FTP: 100' FNL & 660' FE - plan hits target centi - Point	0.00 er	0.00	9,561.3	104.8	799.9	607,074.20	737,483.60	32.6672739	<b>-</b> 103.6959257
LP: 583' FNL & 660' FEL - plan hits target cent - Point	0.00 er	0.00	9,826.2	<b>-</b> 378.2	801.5	606,591.18	737,485.15	32,6659462	<b>-</b> 103 <u>.</u> 6959301
PPP2: 2641' FSL & 657' - plan hits target cent - Point	0.00 er	0.00	9,979.8	<b>-</b> 7,711.6	825.2	599,257.80	737,508.88	32.6457897	<b>-</b> 103.6959960
BHL: 100' FSL & 660' FE - plan hits target cent - Point	0.00 er	0.00	10,033.0	-10,252.5	833.4	596,716.90	737,517.10	32.6388058	-103.6960188



SHL: 205' FNL 1460' FEL (Sec 18) BHL: 100' FSL 660' FEL (Sec 19)

Operator Name:	Property Name:	Well Number
Mewbourne Oil Company	Spanish Bay 18/19 Fed Com	528H

#### Kick Off Point (KOP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County		
A	18	19	33	-	10'	FNL	660'	FEL	Lea		
	Latitude					Longitude					
32.6675211	Į.				-103.69592	248			83		

#### First Take Point (FTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
Α	18	19	33	-	100'	FNL	660'	FEL	Lea
		Latitude				Long	itude		NAD
32.6672738	}				-103.69592	263			83

#### Last Take Point (LTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County		
P	19	19	33	-	100'	FSL	660'	FEL	Lea		
	Latitude					Longitude					
32.6388057	7				-103.69601	90			83		

Is this well the defining well for the Horizontal Is this well an infill well?	Spacing Unit? Y	
If infill is yes please provide API if available, C Spacing Unit.	Operator Name and well number for Defining well for Horizontal	
API#		
Operator Name:	Property Name:	Well Number

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** MEWBOURNE OIL COMPANY

WELL NAME & NO.: SPANISH BAY 18/19 FED COM 528H

**APD ID:** 10400098985

**LOCATION:** Section 18, T.19 S., R.33 E. NMP

**COUNTY:** Lea County, New Mexico

COA

H <sub>2</sub> S	0	No	•	Yes
Potash /	None	O Secretary	O R-111-Q	☐ Open Annulus
WIPP				□ WIPP
Cave / Karst	• Low	O Medium	O High	Critical
Wellhead	Conventional	<ul><li>Multibowl</li></ul>	O Both	<ul><li>Diverter</li></ul>
Cementing	☐ Primary Squeeze	☐ Cont. Squeeze	☐ EchoMeter	DV Tool
Special Req	Capitan Reef	☐ Water Disposal	$\square$ COM	☐ Unit
Waste Prev.	Self-Certification	• Waste Min. Plan	○ APD Submitted 1	prior to 06/10/2024
Additional	✓ Flex Hose	☐ Casing Clearance	☐ Pilot Hole	Break Testing
Language	$\square$ Four-String	Offline Cementing	▼ Fluid-Filled	

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H<sub>2</sub>S) Drilling Plan shall be activated **AT SPUD**. As a result, the Hydrogen Sulfide area must meet **title 43 CFR 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

#### **B. CASING**

### **Primary Casing Program**

- 1. The 13-3/8 inch surface casing shall be set at approximately 1,480 ft. (a minimum of 25 feet (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8 hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 5,110 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, and Capitan Reef.

**Option 1 (Single Stage): Cement to surface.** If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

If Capitan Reef is the loss zone, a DV tool shall be set a maximum of 200 ft. above the top of Capitan Reef.

**Option 2** (Two-Stage): The operator has proposed utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

**Note:** Excess cement is below the BLM's recommendation of 25%. More cement might be needed.

**Note:** The intermediate casing must be kept fluid-filled to meet minimum requirement for collapse design safety factor.

- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following: (Use this for 3

# string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)

- Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
- O Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.
- **3.** Operator has proposed to set 7" (26# P-110) production casing at approximately **9,298 ft.** (9,238 ft. TVD). The minimum required fill of cement behind the 7 inch production casing is:
  - Cement should tie-back at least 50 feet above Capitan Reef top or 200 feet into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

**Note:** Operator has estimated the Capitan reef top is at approximately 3,519 ft. Cement volume is insufficient to bring cement to at least 50 feet above Capitan Reef top. More cement might be needed.

- 4. The minimum required fill of cement behind the 4-1/2 inch production liner is:
  - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

# **Alternate Casing Program**

- 1. The 13-3/8 inch surface casing shall be set at approximately 1,480 ft. (a minimum of 25 feet (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8 hours or 500 psi compressive strength, whichever is greater. (This is to

- include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 5,110 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, and Capitan Reef.

**Option 1 (Single Stage): Cement to surface.** If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

If Capitan Reef is the loss zone, a DV tool shall be set a maximum of 200 ft. above the top of Capitan Reef.

**Option 2** (Two-Stage): The operator has proposed utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

**Note:** excess cement is below the BLM's recommendation of 25%. More cement might be needed.

**Note:** The intermediate casing must be kept fluid-filled to meet minimum requirement for collapse design safety factor.

- ❖ In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3<sup>rd</sup> casing string must come to surface.
- ❖ Special Capitan Reef requirements. If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall do the following: (Use this for 3 string wells in the Capitan Reef, if 4 string well ensure FW based mud used across the Capitan interval)

- Switch to freshwater mud to protect the Capitan Reef and use freshwater mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.
- Daily drilling reports from the Base of the Salt to the setting of the intermediate casing are to be submitted to the BLM CFO engineering staff via e-mail by 0800 hours each morning. Any lost circulation encountered is to be recorded on these drilling reports. The daily drilling report should show mud volume per shift/tour. Failure to submit these reports will result in an Incidence of Non-Compliance being issued for failure to comply with the Conditions of Approval. If not already planned, the operator shall run a caliper survey for the intermediate well bore and submit to the appropriate BLM office.
- **3.** Operator has proposed to set 7" (26# P-110) production casing at approximately **10,199 ft.** (9,826 ft. TVD). The minimum required fill of cement behind the 7 inch production casing is:
  - Cement should tie-back at least **50 feet** above Capitan Reef top or **200 feet** into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to Capitan Reef.

**Note:** Operator has estimated the Capitan reef top is at approximately 3,519 ft. Cement volume is insufficient to bring cement to at least 50 feet above Capitan Reef top. More cement is needed.

- 4. The minimum required fill of cement behind the 4-1/2 inch production liner is:
  - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

# **Offline Cementing**

Operator has been (**Approved**) to pump the proposed cement program offline in the **Surface and intermediate(s) intervals**. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to the commencement of any offline cementing procedure at **Lea County:** 575-689-5981.

#### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Before drilling

the surface casing shoe out, the BOP/BOPE and annular preventer shall be pressure-tested in accordance with title 43 CFR 3172 and API Standard 53.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

## **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

# **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

# **Contact Lea County Petroleum Engineering Inspection Staff:**

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - i. Notify the BLM when moving in and removing the Spudder Rig.
    - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum

- compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- **4.** Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- **5.** No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

### **B. PRESSURE CONTROL**

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for

- review. These documents shall be posted in the company man's trailer and on the rig floor.
- **3.** 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- **5.** The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
  - iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent

tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

## D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crewintensive operations.

SA 09/30/2024

# **Hydrogen Sulfide Plan Summary**

- A. All personnel shall receive proper H2S training in accordance with Onshore Order III.C.3.a.
- B. Briefing Area: two perpendicular areas will be designated by signs and readily accessible.
- C. Required Emergency Equipment:
  - Well control equipment
    - a. Flare line 150' from wellhead to be ignited by flare gun.
    - b. Choke manifold with a remotely operated choke.
    - c. Mud/gas separator
  - Protective equipment for essential personnel.

# Breathing apparatus:

- a. Rescue Packs (SCBA) 1 unit shall be placed at each breathing area, 2 shall be stored in the safety trailer.
- b. Work/Escape packs —4 packs shall be stored on the rig floor with sufficient air hose not to restrict work activity.
- c. Emergency Escape Packs —4 packs shall be stored in the doghouse for emergency evacuation.

# Auxiliary Rescue Equipment:

- a. Stretcher
- b. Two OSHA full body harness
- c. 100 ft 5/8 inch OSHA approved rope
- d. 1-20# class ABC fire extinguisher
- H2S detection and monitoring equipment:

The stationary detector with three sensors will be placed in the upper dog house if equipped, set to visually alarm @ 10 ppm and audible @ 14 ppm. Calibrate a minimum of every 30 days or as needed. The sensors will be placed in the following places: Rig floor / Bell nipple / End of flow line or where well bore fluid is being discharged.

(Gas sample tubes will be stored in the safety trailer)

- Visual warning systems.
  - a. One color code condition sign will be placed at the entrance to the site reflecting the possible conditions at the site.
  - b. A colored condition flag will be on display, reflecting the current condition at the site at the time.
  - c. Two wind socks will be placed in strategic locations, visible from all angles.

### MEWBOURNE OIL COMPANY

### **ALTHEA 18 FED #101H**

# ■ Mud program:

The mud program has been designed to minimize the volume of H2S circulated to surface. The operator will have the necessary mud products to minimize hazards while drilling in H2S bearing zones.

# ■ Metallurgy:

All drill strings, casings, tubing, wellhead, blowout preventer, drilling spool, kill lines, choke manifold and lines, and valves shall be suitable for H2S service.

# ■ Communication:

Communication will be via cell phones and land lines where available.

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

# **Section 7 - Methods for Handling**

Waste type: DRILLING

Waste content description: Drill cuttings

Amount of waste: 940 barrels

Waste disposal frequency: One Time Only

Safe containment description: Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.)

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

**FACILITY** 

Disposal type description:

Disposal location description: NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located

on HWY 62/180, Sec. 27 T20S R32E.

Waste type: SEWAGE

Waste content description: Human waste & grey water

Amount of waste: 1500 gallons

Waste disposal frequency: Weekly

Safe containment description: 2,000 gallon plastic container

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

**FACILITY** 

Disposal type description:

Disposal location description: City of Carlsbad Water Treatment facility

Waste type: GARBAGE

Waste content description: Garbage & trash

Amount of waste: 1500 pounds

Waste disposal frequency : One Time Only

Safe containment description: Enclosed trash trailer

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

**Disposal location description:** Waste Management facility in Carlsbad.

# **Reserve Pit**

Reserve Pit being used? NO

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: SPANISH BAY 18/19 FED COM Well Number: 528H

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

# **Cuttings Area**

Cuttings Area being used? NO

Are you storing cuttings on location? N

**Description of cuttings location** 

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

**WCuttings** area liner

Cuttings area liner specifications and installation description

# **Section 8 - Ancillary**

Are you requesting any Ancillary Facilities?: N

**Ancillary Facilities** 

#### Comments:

### **Section 9 - Well Site**

Well Site Layout Diagram:

SPANISH\_BAY\_18\_19\_FED\_COM\_\_528H\_WellSiteLayout\_20240610091844.pdf

Comments: NONE

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720 District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

# **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 390298

### **CONDITIONS**

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	390298
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	Will require a File As Drilled C-102 and a Directional Survey with the C-104	10/7/2024
pkautz	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string	10/7/2024
pkautz	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system	10/7/2024
pkautz	Cement is required to circulate on both surface and intermediate1 strings of casing	10/7/2024
pkautz	If cement does not circulate on any string, a CBL is required for that string of casing	10/7/2024