

PRODUCTION DEPARTMENT SOUTHWESTERN DIVISION



December 10, 1987

Downhole Commingling Request Squaw Federal #3 Sheep Draw Field Eddy County, New Mexico

New Mexico Oil Conservation Division P. O. Box 2088 Santa Fe, New Mexico 87504-2088

Attention: Mr. David R. Catanach

Exxon respectfully requests an exception to New Mexico Oil Conservation Division Rule 303(a) to permit us to commingle the production from the Morrow and Atoka pools in the subject wellbore. No reservoir damage or waste will result from such downhole commingling, and correlative rights will not be violated.

The Squaw Federal #3 was drilled in late 1985 and completed in the Morrow. The Morrow completion proved to be too poor to pay out and the well was subsequently recompleted to the Atoka using a retriev-This was done with the intention of eventually comminable plug. gling the Morrow with the Atoka when the Atoka pressure had drawn down to the Morrow pressure. After completion in the Atoka, it was found that the pressure was virtually identical to the pressure found in the Morrow. Therefore, we would like to proceed with commingling at this time.

Attached are exhibits supporting our commingling application. there are any questions, please contact Bill Duncan at (915) 686-4105.

James D. Howell

JDH/kw Attachments

c: Certified Mail - w/Attachments Offset Operators District II - NMOCD Artesia, NM Bureau of Land Management, Carlsbad, NM

ATTACHMENT 1

Exxon Squaw Federal #3 - Downhole Commingling Requirements

The Sheep Draw Atoka and Sheep Draw Morrow formations in the above well satisfy the requirements for downhole commingling of two gas zones pursuant to: Rule 303(C)(1)(b) (items 1 through 6):

- 1. The commingling is necessary to permit a zone or zones to be produced which would not otherwise be economically producible. The Sheep Draw Morrow zone is not economical to produce separately in order to make a commercial well. The expected deliverability is about 150 MCFPD, and rather than totally abandon these Morrow reserves, provision was made on original recompletion to install a retrievable plug for commingling purposes.
- 2. There will be no crossflow between the zones to be commingled. The bottom hole pressure in the Atoka is 4072 psia, and in the Morrow, 4159 psia. Adjusted to a common datum of 7300'ss, the two pressures are 4102 psia and 4129 psia, respectively. The two pressures are virtually identical and no crossflow should occur.
- 3. Any zone which is producing from fluid sensitive sands, which may be subject to damage from water or other produced liquids, is protected from contact from such liquids produced from other zones in the well. Both the Atoka sands and Morrow sands are very water sensitive. However, neither zone produces any water or condensate (dry gas only).
- 4. The fluids from each zone are compatible with the fluids from the other(s), and combining the fluids will not result in the formation of precipitates which might damage any of the reservoirs. Neither zone produces any water or condensate (dry gas only).
- 5. Ownership of the zones to be commingled is common (including working interest, royalty and overriding royalty). All ownership is common on both zones.
- 6. The bottom hole pressure of the lower pressure zone is not less than 50 percent of the bottom hole pressure of the higher pressure zone adjusted to a common datum. Adjusted to a common datum of 7300'ss, the Atoka pressure is 4102 psia and the Morrow pressure is 4129 psia, which is a difference of only 0.7%.

ATTACHMENT 2

Exxon Squaw Federal #3 - Downhole Commingling - Data Required

To obtain approval for downhole commingling, we have enclosed the following data pursuant to Rule 303(C)(2)(a through j):

a. Exxon's name and address:

Exxon Corporation
P. O. Box 1600
Midland, Texas 79702
Attention: New Mexico Operations

b. Lease name, well number, well location, and name of pools to be commingled:

Squaw Federal No. 3 2479' FSL & 1880' FWL Section 1, Township 23-S, Range 25-E Eddy County, New Mexico

Pools to be commingled: Sheep Draw Morrow and Sheep Draw Atoka

- c. A plat of the area showing the acreage dedicated to the well and the ownership of all offsetting leases: Attached.
- d. A 24-hour productivity test showing the amount of oil, gas, and water produced from each zone. See attached four point tests and well resume. The well is not yet connected to sales. Sustainable deliverability from the Morrow is estimated at 150 MCFPD, and from the Atoka, 375 MCFPD. There is no condensate or water production.
- e. <u>Newly completed well: A complete resume of the well's completion history including description of treating, testing, etc. of each zone, and a prognostication of future production from each zone.</u> See attached resume.
- f. A current bottomhole pressure for each zone capable of flowing: Both gas zones are capable of flowing:

Measured BHP - Atoka: 4072 psia (4102 psia @ 7300' ss datum)
Extrapolated BHP - Morrow: (3263 psia S.I.T.P.) 4159 psia (4129 psia @ 7300' ss datum)

BHP Bomb data & Form C-122G are attached.

- g. A description of the fluid characteristics of each zone showing that the fluids will not be incompatible in the wellbore. There is no water or condensate production, and therefore, no incompatible fluids. Hydrocarbon analyses of the two gases are attached.
- h. A computation showing that the value of the commingled production will not be less than the sum of the values of the individual streams. There is no condensate production to consider. The gas is sold by dollar per MMBTU, and therefore, the gas value is constant whether it is sold separately or commingled. Both zones are sweet with similar levels of nitrogen and CO₂.

A formula for the allocation of production to each of the commingled zones i. and a description of the factor or data used in determining such a formula:

Gas Allocation

Gas Rate at time of commingling, Morrow:

150 MCFPD

Gas Rate at time of commingling, Atoka:

375 MCFPD

Total, both zones:

525 MCFPD

Sheep Draw Morrow: 150/525 = 0.29 Gas Allocation Factor

Sheep Draw Atoka: 375/525 = 0.71 Gas Allocation Factor

Allocation based upon production rate compares favorably to allocation based upon Exxon's reserve information for each zone.

<u>Condensate Allocation</u>: Neither zone produces any condensate on test. However, some minor amounts of condensate may fall out in the separators during cold weather. It is proposed to use GPM content of the gas to allocate condensate as follows:

GPM content Morrow = 0.953 Gal/MCF GPM content Atoka = 1.407 Gal/MCF

Total gallons, Morrow = $0.953 \times 150 = 143 \text{ gallons/day}$ Total gallons, Atoka = $1.407 \times 375 = 528 \text{ gallons/day}$ Total gallons, both zones = 671 gallons/day

Sheep Draw Morrow: 143/671 = 0.21 Condensate Allocation Factor

Sheep Draw Atoka: 528/671 = 0.79 Condensate Allocation Factor

A statement that all offset operators, and, in case of a well on Federal j. land, the United States Geological Survey, has been notified in writing of the proposed commingling: All offset operators (list attached) and the United States Geological Survey have been notified by copy of this application. A list is attached.

ACREAGE DEDICATED TO SQUAW FEDERAL # 3

US State State 2 HNG Exxon 1 Corinne Grace 6 LG 2082 0453201 (Oper) Yates Pet Yates VB95 VB95 VB95 Cueva Unit								ſ	1			
Corinne Grace Coper Chevron				R2	5E				R	26E		
Finnel 38827		1		35				36		1 .	OII	
Corinne Grace 6 Coper	T22S		<u></u>									
2 HNG LG2082 0453201 (Oper) 6 Yates Pet VB95 VB95 Cueva Unit State Exxon 12 Exxon 5 Exxon K4781 Corinne Grace 6 (Oper) 6 Cueva Unit State Squaw-Fed State Exxon 12 Exxon 7 Exxon K4781 Cueva Unit State Exxon 7 Exxon K4781		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	**TY		HNG LG5764			1				
LG 2082		u	T S			Sto	ate -	·	S	tate		
Yates Pet VB95 VB95 HNG LH2082 Cueva Unit State State State Exxon 12 Exxon K4781 T Ramuz Est Exxon K4781 Exxon K4781 Exxon Faxon K4781						~~~		1		: e j.	6	
Cueva Unit Cueva Unit Cueva Unit Cueva Unit Cueva Un										1		
State State		:	i 1 mm.						垛	1 .		
0426782 0453201 State Exxon	D D			Squaw-Fed								
Exxon V710 Ramuz Est Exxon V710 Exxon K4781	7 -			11				12	K 4 7 6 1	7		
Exxon Exxon K4781				*		-(}-			Exxon		Exxon V710	-
Mary-Fed Squaw-Fed Grandt et al State					本 :				on 781			
		Mary-Fed		Squaw-Fed		Grandt et a	Sto	ıte				
			1							-p		

Well Resume

Exxon's Squaw Federal #3

Sheep Draw Morrow Operations:

- 9/14/85 Spud well.
- Set 5-1/2" casing @ 11,665'. T.D. @ 11,670' 11/01/85
- 11/09/85
- Clean out well to 11,630'. Pressure tested casing integrity o.k. Perforated Morrow at 11,218-233', 11,430-439', and 11,616-621'. Set 11/12/85 packer at 11,042'
- Swabbed well for 6 hours, well kicked off flowing 15' flare and kCl 11/13/85
- 11/14/85 13-1/2 hour flow test, flowed at rate of 450 MCFPD, 2900 psig F.T.P., 8/64" choke. No water or condensate.
- 13 hour flow test, 1060 MCFPD rate, 1120 psig F.T.P., 15/64" choke. 11/15/85 No water or condensate.
- 11/16/85 24 hour flow test, 1060 MCFPD rate, 1120 psig F.T.P., 15/64" choke. No water or condensate.
- 6 hour flow test, 900 MCFPD rate, 955 psig F.T.P., 15/64" choke. No 11/17/85 water or condensate.
- 70 hour SI well pressure: 2376 psig 11/19/85 70 hour SI bottom hole pressure measurement (BOMB): 3169 psig Ran 4 point test. C.A.O.F. 915 MCFPD, no water or condensate. well in to evaluate and solicit gas contract.
- 11/21/85 Cost to date: \$1,677,000.

Prognosis:

Based upon the 4 point test, the sustainable rate is estimated at 150 MCFPD.

Although this well did test for three days at about 1000 MCFPD, the Morrow had not been sufficiently produced to attain pseudo steady-state rate, which is estimated at around 150 MCFPD, and which would take at least several weeks to attain. The Morrow has very low permeability which is evidenced by the fact that after producing only 2300 MCF, the shut-in bottom hole pressure had declined from an original 4129 psia to 3182 psia. (Even after allowing the S.I. BHP to buildup for 70 hours.) When the BHP was measured on 6/24/87 (19 months later) it was found to be back at original of 4129 psia, based upon extrapolation of shut-in wellhead pressure of 3263 psia (see attached C-122G).

Based upon the well expenditure to date, and faced with an additional expenditure to hook up the well, it would have been more economical to plug the well as a dry hole than the produce the Morrow singly.

Sheep Draw Atoka Operations

10/21/86 Mr. David Catanach (NMOCD - Santa Fe), Mr. Les Clements (NMOCD -Artesia) and Mr. W. T. Duncan (Exxon) verbally discussed strategy of recompleting to the Atoka with the intent of eventual downhole commingling with the Morrow (internal memo attached).

(Continued)

- 5/27/87 Notice of intent to recomplete and eventually down hole commingle filed with BLM (attached).
- 6/24/87 19 month S.I. wellhead pressure of 3263 psia recorded for Morrow. Attached C-122-G calculates a static BHP of 4129 psia (back to original). Well was flowed down and killed with KCl brine.
- 6/25/87 Pulled packer. Ran new packer with wireline retrievable plug. Set new packer at 11,150', between Morrow and Atoka.
- 6/29/87 Perforated Atoka, one shot, at 10,469', 10,484', 10,501', 10,552', 10,561', 10,593', 10,795', 10,805', 10,819', 10,843', and 10,857'. (13,561) shots for limited entry fracture design).
- 7/03/87 Pumped 105 Bbls of diesel to break down perforations.
- 7/08/87 Fractured the Atoka with 44,000 gallons diesel and 64,000 lbs. of Bauxite, with maximum surface treating pressure of 12,400 psig. Total load oil: 1210 Bbls to recover.
- 7/10/87 SI wellhead pressure: 1375 psig. Flow back load, recovered only 219 Bbls diesel.
- 7/11/87 Well flowing on 20/64" choke, 1700 psig F.T.P., 2665 MCFPD rate. Recovered a total of 320 Bbls of load oil with 890 Bbls. left to recover.
- 7/13/87 Well flowing on 26/64" choke, 1500 psig F.T.P. 3500 MCFPD rate. Still cleaning up and getting stronger. Shut well in.
- 7/16/87 S.I.T.P. 2850 psig. Ran coil tubing unit with diesel to clean out fill to 11,080'.
- 7/17/87 Well flowing on 15/64" choke, 1800 psig F.T.P., 1638 MCFPD rate. Shut in for 72 hour static bottom hole pressure measurement.
- 7/20/87 Measured BHP to be 4072 psia (and not 6400 psia as originally expected).

Ran 4 point test. C.A.O.F. 4760 MCFPD, no water or condensate. Shut well in waiting on expenditure to hook up well and produce to sales.

Prognosis:

The estimated sustainable rate from the Atoka is 375 MCFPD. Assuming a decline rate of 30% per year applied to the 375 MCFPD rate approximates the future flowstream.

(Continued)

Well Resume Exxon's Squaw Federal #2 Page 3

Commingling will recover significant additional reserves from the Morrow. The Morrow reserves will otherwise be left behind when the well is plugged because it will not be economical to recomplete the well deeper solely to produce the Morrow. For this reason the packer with retrievable plug was set between the Atoka and Morrow, until such time as the pressure in the two zones is approximately equal. On recompletion, the pressures were found to be equal.

P. O. BOX 2088

STATE OF NEW MEXICO

ENERGY MO MINERALS DEPARTMENT

SANTA FE, NEW MEXICO 87501

Form C-122 Revised 10-1-78

T.1.

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

_										Test D					
	ype Teet [X Initia	ol			nnual		☐ Spec	:ial		11/19/	85			:
C	Exxon (Co. U.	s.A.			None									
P	Sheep Draw Fermetten Morrow									Unit		''' -			
1	Compision Date Total Depth Plug Beek TD Elevation								Fore	or Lease !	1000				
	11/1/85	;		11	646		116	30	Į				quaw Fe		1
[c	5 Size	20.	R	4,156	5-1	1646	Perioration From	11218			:04	Well	No.		
+	Q. BIAO	W1.		4.130	501		Perloration		Te	110	021	Unit	Sec.	Tw	Aye.
	2 7/8	6.5		2.441		042	From	0pen	T	• End	1	K	1	23	
**	re Well - Sim Single	ile — Divi	denheed	1 – G.G. er G	.O. Mul	itiple		Packer Sot	A1 .04	2		Cous	-		
1.0	ducing Thru			rois Temp. • F	1	Jean Annual	Temp. 'F	Baro. Pres	•	Pa		Stole	JУ		
	Tbg.		184	• 11042		60			3.2			Ne	Mexic)	
	11042	H 110	142	.589		1.161	# N 2	211	H ₂ S		Prover		er Aun-	Top	
				OW DATA				TUBI	NG	DATA	7		3.826 DATA	1 	lg.
NO	Prover	× (Orilles	Press.		Diff.	Temp.	Press.		Tom		71000,	Temp	\Box	01
SI	Stee		5110	p.e.l.q.		<u>~~</u>	•F	p.e.i.g.		· · · · · · · · · · · · · · · · · · ·			• •	_	Flow
".	3.826	X .750		300		2	67	2376 2220		 			 	-	1 hr.
Z.	3.826			300		10	88	2155							1 hr
3.	3.826			200 300		52 40	88 88	1730			#				i hr.
4. 5.	3.020	1.00		300			-00	1225		 			 		1 hr.
						RATEO	FLOW	CALCULA	TIC	NS			· · · · · · · · · · · · · · · · · · ·		
			1				l l								
	Coellic	ioni	I _	7/2	• [Pressure		Temp.		Cuantilà	1.	Super		Rate o	(Flow
1 0.	Coellic (24 Ho		-	√h _w P _m	•	Presewe	F	Temp. setor F1.		Factor Factor		Super Compress actor, Fp	.		of Flow Meid
ю. 1	(24 Ho		_	25.03	•	P _m 313.2	.99	PI.	1	Factor Fa		Compress actor, Fp 1.024	.	88	Meid
1 2.	2.662 2.662		_	25.03 55.96		313.2 313.2	.9	933 741	1	Feetor Fe .303 .303	F	1.024 1.021	.	88 193	Meld 3
1 2. 3.	(24 Ho		_	25.03		P _m 313.2	.9	PI.	1 1	Factor Fa	F	Compress actor, Fp 1.024	.	88 193 440	3)
ī	2.662 2.662 2.662			25.03 55.96 127.62		313.2 313.2 313.2	.9	933 741	1 1	.303 .303 .303 .303	F	1.024 1.021	.	88 193	3)
2. 3. 4.	2.662 2.662 2.662		• R	25.03 55.96 127.62	2	313.2 313.2 313.2 313.2	.99 .9 .9	933 741 741 741		.303 .303 .303 .303	F	1.024 1.021	.	88 193 440	Meld 3)) Mel/bbl.
1 2. 3.	2.662 2.662 2.662 2.662 4.758	Temp.	• • • • • • • • • • • • • • • • • • • •	25.03 55.96 127.62 111.93	z .95	313.2 313.2 313.2 313.2	.9 .9 .9 .9	933 741 741 741 rocarbon Rai	droce	.303 .303 .303 .303	F	1.024 1.021	v	88 193 440 690	Meld 3))
2. 3. 4. 5.	2.662 2.662 2.662 2.662 4.758	Temp. 527	·A	25.03 55.96 127.62 111.93 T. 1.51	.95	313.2 313.2 313.2 313.2 313.2	.9 .9 .9 .9 .9 Liquid Hyd	933 741 741 741	droce	.303 .303 .303 .303	Dry	1.024 1.021 1.021 1.021	v	88 193 440 690	Meld 3)) Mel/bbl.
1 2. 3. 4. 5.	2.662 2.662 2.662 2.662 4.758 Ph .46 .46	Temp. 527 548 548	• A	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57	.956 .960	313.2 313.2 313.2 313.2 313.2 313.2 Gae A.P. Spec Spec Critic	.9 .9 .9 .9 .9 Liquid Hyd I. Gravity of the Gravity title Gravity	933 741 741 741 rocarbon Rate of Liquid Hyce Procarbon File of	droce	303 .303 .303 .303 .303	Dry 89	1.024 1.021 1.021 1.021	v	88 193 440 690	Meld 3))
1 2. 3. 4. 5. 10.	2.662 2.662 2.662 2.662 4.758 P. .46 .46 .46	Temp. 527 548 548 548		25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57	.95	313.2 313.2 313.2 313.2 313.2 313.2 Gae A.P. Spec Spec Critic	.9 .9 .9 .9 .9 Liquid Hyd	933 741 741 741 rocarbon Rate of Liquid Hyce Procarbon File of	droce	.303 .303 .303 .303	Dry 89	1.024 1.021 1.021 1.021	v	88 193 440 690	Meld 3))
1 2. 3. 4. 5. 10.	2.662 2.662 2.662 4.758 4.758 4.46 .46 .46 .46	Temp. 527 548 548 548		25.03 55.96 127.62 111.93 7 1.51 1.57 1.57	.956 .960 .960	313.2 313.2 313.2 313.2 313.2 313.2 Cae A.P. Spec Critic	J. 99 .99 .99 .99 .99 .99 .99 .99 .99 .9	peter Ft. 933 741 741 741 Tocarbon Rational Liquid Hyce Separator Gr Flowing Fire eature 3	droce :00_ uid _ 49	303 .303 .303 .303 .303 .303	Dry 89 ***	Compressed actor, Fp 1.024 1.021 1.021 1.021	X X X X	88 193 440 690	Meld 3) Mel/bbl. Deq. XXXX P.S.I.A.
1 2. 3. 4. 5. 10. 1. 2. 3. 4.	2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46	Temp. 527 548 548 548	708.3	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57	.956 .960 .960	313.2 313.2 313.2 313.2 313.2 313.2 Coe A.P. Spec Critic	J. 99 .99 .99 .99 .99 .99 .99 .99 .99 .9	933 741 741 741 rocarbon Rate of Liquid Hyce Procarbon File of	droce :00_ uid _ 49	303 .303 .303 .303 .303 .303	Dry 89 ***	Compressed actor, Fp 1.024 1.021 1.021 1.021	X X X X	88 193 440 690	Meld 3) Mel/bbl. Deq. XXXX P.S.I.A.
1 2. 3. 4. 5. 10. 1. 2. 3. 4. 5.	2.662 2.662 2.662 4.758 4.758 4.46 .46 .46 .46	Temp. 527 548 548 548	708.3	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .960	313.2 313.2 313.2 313.2 313.2 313.2 Cae A.P. Spec Spec Critic	John John John John John John John John	peter Ft. 933 741 741 741 recorbon Ret of Liquid Hye of Separator G of Flowing Fi te ature 3	49	303 .303 .303 .303 .303	Dry 89 ** × ×	Compressed actor, Fp 1.024 1.021 1.021 1.021	X X X X	88 193 440 690	Meld 3) Mel/bbl. Deq. XXXX P.S.I.A.
1 2. 3. 4. 5. 10. 11. 2. 3. 4.	2.662 2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46 .46 .2398.2 P. ² 2233.2 2168.2 1743.2	Temp. 527 548 548 548 2233 2168 1774	708.3 .2 .4	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .960	313.2 313.2 313.2 313.2 313.2 313.2 Cae A.P. Spec Spec Critic	John John John John John John John John	peter Ft. 933 741 741 741 recorbon Ret of Liquid Hye of Separator G of Flowing Fi te ature 3	49	303 .303 .303 .303 .303	Dry 89 ** × ×	Compressed actor, Fp 1.024 1.021 1.021 1.021	X X X X	88 193 440 690	Meld 3) Mel/bbl. Deq. XXXX P.S.I.A.
1 2. 3. 4. 5. 10. 11. 2. 3. 1. 5.	2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46 .46 .2398.2 P. ² 2233.2 2168.2	Temp. 527 548 548 548	708.3 .2 .4	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .960	313.2 313.2 313.2 313.2 313.2 313.2 Cae A.P. Spec Spec Critic	John John John John John John John John	peter Ft. 933 741 741 741 Tocarbon Rational Liquid Hyce Separator Gr Flowing Fire eature 3	49	303 .303 .303 .303 .303	Dry 89 ** × ×	Compressed actor, Fp 1.024 1.021 1.021 1.021	X X X X	88 193 440 690	Meld 3) Mel/bbl. Deq. X X X X P.S.I.A.
3. 4. 5. 10. 1. 2. 3. 4. 5. 0 1	2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46 .2398.2 .233.2 2168.2 1743.2 1238.2	Temp. 527 548 548 548 2233 2168 1774 1242	708.3 .2 .4 .4 .5	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .960	313.2 313.2 313.2 313.2 313.2 313.2 Cae A.P. Spec Spec Critic	Liquid Hyd I. Gravity III Gravity III Gravity Cal Pressur Cal Temper	peter Ft. 933 741 741 741 recerbon Reference Grand Flowing Fire endure 3	49	.303 .303 .303 .303 .303 .5676	Dry 89 ** × × ×	20mpress dector, Fp 1.024 1.021 1.021 1.021 2.02	X X X X X X X X X X X X X X X X X X X	88 193 440 690	McId 3)) — McI/bbl. — Deg. — X X X X — P.S.I.A. — R
3. 4. 5. 10. 1. 2. 3. 4. 5. 0 1	2.662 2.662 2.662 2.662 4.758 .46 .46 .46 .46 .46 .2398.2 P. ² 2233.2 2168.2 1743.2 1238.2	527 548 548 548 548 2233 2168 1774 1242	708.3 .2 .4 .4 .5	25.03 55.96 127.62 111.93 T, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .966 .966 .966 .966 .966	313.2 313.2 313.2 313.2 313.2 313.2 4 Spec Critic Critic	Liquid Hyd Liquid Hyd Cravity Coll Pressur Coll Temper Pc 2 R2 - H2 Mold 0	pettor Ft. 933 741 741 741 Tocarbon Rational Liquid Hyror Separator Graduite = 1 Ref 2 Ref 2 Ref 2 15.025 Ar	49	303 .303 .303 .303 .303 .303	Dry 89 ** × × × 4	25	X X X X X X X X X X X X X X X X X X X	88 193 440 690	McId 3)) — McI/bbl. — Deg. — X X X X — P.S.I.A. — R
2. 3. 4. 5. 10. 1. 2. 3. 4. 5. 7. 0.	2.662 2.662 2.662 2.662 4.758 .46 .46 .46 .46 .46 .2398.2 P. ² 2233.2 2168.2 1743.2 1238.2	527 548 548 548 548 2233 2168 1774 1242	708.3 .2 .4 .4 .5	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .966 .966 .966 .966 .966	313.2 313.2 313.2 313.2 313.2 313.2 4 Spec Critic Critic	Liquid Hyd Liquid Hyd Cravity Coll Pressur Coll Temper Pc 2 R2 - H2 Mold 0	pettor Ft. 933 741 741 741 Tocarbon Rational Liquid Hyror Separator Graduite = 1 Ref 2 Ref 2 Ref 2 15.025 Ar	49	303 .303 .303 .303 .303 .303	Dry 89 ** × × × 4	25	X X X X X X X X X X X X X X X X X X X	88 193 440 690	McId 3)) — McI/bbl. — Deg. — X X X X — P.S.I.A. — R
1 2. 3. 4. 5. 10. 11. 2. 3. 1. 5.	2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46 .2398.2 p. ² 2233.2 2168.2 1743.2 1238.2	527 548 548 548 548 2233 2168 1774 1242	708.3 .2 .4 .4 .5	25.03 55.96 127.62 111.93 T, 1.51 1.57 1.	.956 .966 .966 .966 .966 .966 4166	313.2 313.2 313.2 313.2 313.2 313.2 4 Spec Critic Critic	Liquid Hyd I. Gravity illic Gravity cal Pressus cal Temper Pc ² R ² - H ² Meld e	pettor Ft. 933 741 741 741 741 Tecorron Rad If Liquid Hyre Separator G Flowing Fi Tecorron 1 1 1 1 1 1 1 1 1 1 1 1 1	49	303 .303 .303 .303 .303 .303	Dry 89 ** × × × 4	25 dd	XXX	88 193 440 690	McId 3)) — McI/bbl. — Deg. — X X X X — P.S.I.A. — R
1 2. 3. 4. 5. 10. 12. 33. 4. 5. 70.	2.662 2.662 2.662 2.662 4.758 4.758 .46 .46 .46 .46 .46 .2398.2 P. ² 2233.2 2168.2 1743.2	527 548 548 548 548 2233 2168 1774 1242	708.3 .2 .4 .4 .5	25.03 55.96 127.62 111.93 7, 1.51 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57 1.57	.956 .966 .966 .966 .966 .966 4164	313.2 313.2 313.2 313.2 313.2 313.2 4.P. Spec Critic Critic Critic	John John John John John John John John	pettor Ft. 933 741 741 741 Tocarbon Rational Liquid Hyror Separator Graduite = 1 Ref 2 Ref 2 Ref 2 15.025 Ar	49	.303 .303 .303 .303 .303 .5676	Dry 89 ** × × × 4	25	XXX	88 193 440 690	McId 3)) — McI/bbl. — Deg. — X X X X — P.S.I.A. — R

JUMPANY:

EXXON CO. U.S.A.

LEASE:

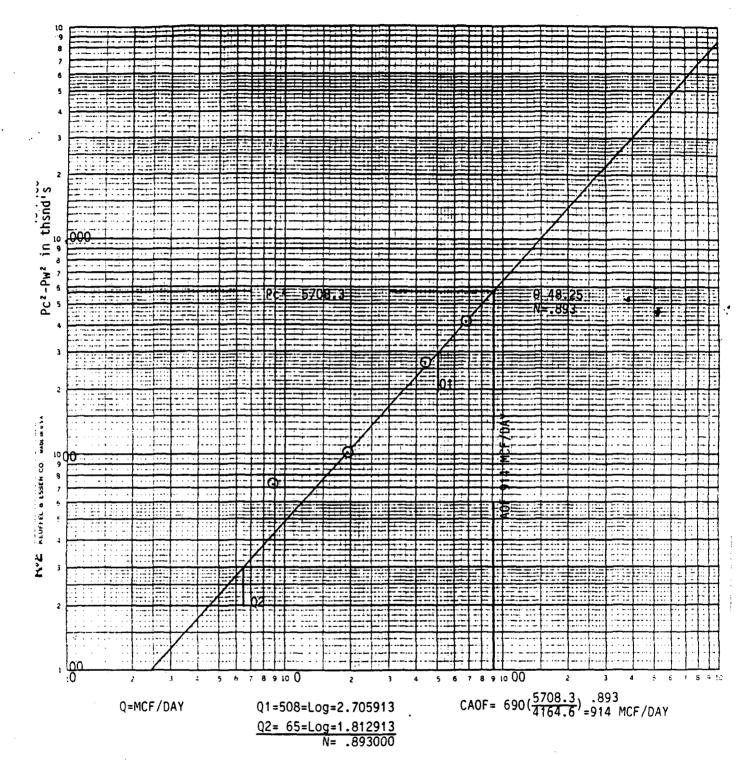
SQUAW FEDERAL #3

COUNTY:

EDDY

DATE:

11/19/85



JAAREL SERVICES,VC.

POST OFFICE BOX 1664

PHONES 506 398-6300 -- 365-6274

HOSSE, NEW MEXICO 68349

OPERATOR_	Exxon	Company	USA	
FIELD	Sheep	Draw		
FORMATION	Morrov	7		
LEASE	Squaw	Federal		WELL No. 3
COUNTY	Eddy		STATE	New Mexico
DATE	11/19/	/85	TIME	11:00 AM
Status	Shut i	n		
Test Depth	11022			
Time S. L. 70	0 hrs.	Last test	date	_
Tub Pres	23 90	_BHP last		-
Cas. Pres	PKK	_BHP char		
Elev. 373	4'KB	_Fluid top		None
Datum (-76	86)**	_Water to		None
Temp.	181 F	_Run by		JSI #29
Cal. No	22693	_Chart No		2

BOTTOM HOLE PRESSURE RECORD

Depth	Pressure	Gradient
0.	2390	-
2 000	2521	.066
4000	265 8	.069
6000	2792	.067
8000	. 2933	.071
10000	3069	.068
11022	3141	.071
11420 (-7686)	3169 • ••	(.071)
A 5245.6		

* EXTRAPOLATED PRESSURE

** MIDPOINT OF CASING PERFORATIONS

)	1000	2000	3000	4000	Pressure
2000					
1000					
6000					
3000					
30ණු ජී					
۵					
1000					
1102					
-4 , t	¥1				
				1	
111	1 <u></u> 1 <u></u> 1 <u></u>		r		
	7 i 4 i i i i i i i i i i i i i i i i i	+" -5-			771





PHONE 505/393-3561

P. O. BOX 1161

611 W. SNYDER

ENI 1

HOBBS, NEW MEXICO 88240

ANALYSIS CERTIFICATE

CLIENT: ADDRESS: DUKE SERVICES INC.

2400 N GRIMES - SUITE 273

HOBBS, NM 88240

ANALYSIS NUMBER:

DATE OF RUN: DATE SECURED:

8335 11 20 85 11 19 85

CITY, STATE: SAMPLE IDENT:

EXXON CO USA - SQUAW FEDERAL #3

SAMPLING TEMP:88 DEG F

REMARKS: 700 MCFD

SAMPLING PRESS:300 PSIG

MORROW GAS ANALYSIS

****** GAS ANALYSIS ******

	PERCENT	MCF
NITROGEN CARBON DIOXIDE METHANE ETHANE PROPANE ISO-BUTANE NORMAL BUTANE ISO-PENTANE NORMAL PENTANE HEXANES	0.211 1.161 95.163 2.791 0.347 0.079 0.100 0.052 0.036 0.060	0.744 0.095 0.026 0.031 0.019 0.013 0.025
TOTAL	100.000	0.953

MOLE

PROPANE GPM:

0.09

BUTANES GPM:

0.06

ETHANE GPM:

0.74

PENTANES PLUS GPM:

0.06

SPECIFIC GRAV (CALC):

MOLE WEIGHT:

0.5888 17.05

HHV-BTU/CU FT

PRESSURE (PSIA) WET 14.696

DRY 1032

14.650

1013 1010

1028

14.730

1016

1034

14.735

1016

1034

DEANE SIMPSON

I contacted both David Catanach (NMOCD-Santa Fe) and Les Clements (NMOCD-Artesia) today and described why we would like to set a retrievable plug above the Morrow in the captioned well. Neither party had any objection to the proposal, saying that no formal approval was required until Exxon wanted to obtain a permit to downhole commingle the Morrow and the Atoka. Both agreed that obtaining authority to commingle should be no problem when the pressure in the two zones is more nearly equal.

In addition, I asked Bob Pitschke with the BLM in Carlsbad what the BLM would require. He said they wanted a Sundry Notice before we moved uphole and another before downhole commingling, but that no specific authorization to use a packer and plug above the Morrow is required.

WTD:tt

xc: R. M. Chiquito
J. L. Schaumburg

Form 3160-3 (November 1983) (formerly 9-331C)

UNITED STATES DEPARTMENT OF THE INTERIOR

BUBMIT IN T. (Other instructions on reverse side) Form approved.
Budget Bureau No. 1004-0136
Expires August 31, 1985

	BUREAU OF	LAND MANA	GEMEN	NT.		NM-0453201	AND BERIAL NO.	,
APPLICATION	N FOR PERMIT				BACK	6. IF INDIAN, ALLOTTES	OR TRIBE HAME	
1a. TYPE OF WORK		io bilice,	<u> </u>	LIV, OR TEOU	DACK			
b. Type of Wall		DEEPEN		PLUG BA	CK 🖪	7. UNIT AGREEMENT N	MB	•
WELL L. W	AR VELL X OTHER		81 80	NGLE MULTI	PLB	8. FARM OR LEASE NAM	19	
2. HAMB OF OPERATOR				-		Squaw Fede:	ral	
EXXON COTPO	ration Attr	: David A	. Mur	ray		9. WELL NO.		
				*		3		
P. O. Box 1	.600, Midland, Teport location clearly and	X 79702	A 0	(4.4		10. FIELD AND FOOL, O		
At surface			_	cate requirements.")		Undes. Sheep		Gas
At proposed prod. son	FSL and 1880' F	WL OI Sec.	•			11. SEC., T., E., M., OR S AND SURVEY OR AR	RA .	
A DISSINCE IN MILES	AND DIRECTION FROM NEAD					Sec. 1, T23S,		
		ESST TOWN OF POS	or Oppici	,		12. COUNTY OR PARISH		
5 MILES SW	from Carlsbad		16 WO	. OF ACRES IN LEASE	1 17 WO	Eddy	NM	
PROPERTY OR LEASE I (Also to bearest drig	r .IME, FT. g. unit line, if any)	O' FWL	14	40.84		HIS WELL 320		
18. DISTANCE FROM FROF TO NEAREST WELL, D OR APPLIED FOR, ON TH	RILLING, COMPLETED,	lone	1	0008ED DEPTH 10,857	20. BOTA	BY OR CABLE TOOLS N/A		
21. ELEVATIONS (Show who	ether DF, RT, GR, etc.)		•		· 	22. APPEOX. DATE WOL	K WILL START	
23.		PROPOSED CAS	ING AND	CEMENTING PROGRA	M	-'		
SIZE OF HOLE	SIZE OF CASING	WEIGHT PER F	T00	SETTING DEPTH		QUANTITY OF CREEK	r	
26	20	94		85	25	0 sx		
17 1/2	13 3/8	54.5		1510	-]	5 sx		
12 1/4 8 1/2	9 5/8 5	40 20.8		2604 11665	1	'5 sx 0 sx		
to set a CI will be pro	s currently come the Moduced until the les will be come on the Class 1.	rrow, then Morrow an	perf	orate and stime	ulate t	he Atoka. The	Atoka	
N ABOVE SPACE DESCRIBE one. If proposal is to preventer program, if any	PROPOSED PROGRAM: If partitions of the proposed in the propose	lly, give pertinen	t data o	lug back, give data on p n subsurface locations ar rmits Supervise	resent prod	Detive sone and proposed and true vertical depths	Give blowout	
(This space for Feder	ral or State office use)							
PERMIT NO.			Tin	APPROVAL DATE	··- <u>-</u>			
APPROVED BY CONDITIONS OF APPROV	y Girc	Tir	,	A MANAGER 1890 RESOURCE AREA		DATE 6.16	87	

*See Instructions On Reverse Side

Title 18 U.S.C. Section 1001, makes it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.



Morrow BHP @ 7300' Subsea from Shut-In Wellhead Pressure Measurement

WORKSHEET FOR CALCULATION OF STATIC COLUMN PRESSURE AT GAS LIQUID INTERFACE

(From Wellhead Shut-In Pressure of 3263 PSIA)

Form C-122G Adopted 9-1-65

One copy to be filed in District Office (Work copy acceptable) DATE June 24, 1987 TABLE 1X & X PCI 673 TCI % H₂S- $% N_2 = 2.1$ 1.16 WELL NO. % CO₂— G 0.589 сн 6726 LEASE Squaw Federal Sohaney 1.00 L/H_ Morrow BHP 17,046 528.3 1.60110,647 zero 546 589 12.73 3263 4129 3696 5.49 632 0.897 0.897 1.697 11,034 COMPANY EXXON CORD. 16 | Fw=L/H(FcQm)2(1-ers) 9 | 1 - e^{-S} (Table XIV) $P_{\mathbf{w}}^2 = P_{\mathbf{t}}^2 + F_{\mathbf{w}}$ es (Table XIV) 15 L/H (F_cQ_m) ² Fr (Table XV) 4 | T = (Tw + Ts) $P_f^2 = e^s P_c^2$ 2 Tw (W.H. °R) Z (Table XI) 3 T_s (BH °R) 20 P=(Pc+Pf) $F_c = F_r TZ$ Z (Est.) GH/TZ 14 FcQm 11 Pc2 ZL10 P_C Ŋ 12 ន Ø 6 ξ ō ဖ

STATE OF NEW MEXICO

P. O. BOX 2088 ENERGY AND MINERALS DEPARTMENT SANTA FE, NEW MEXICO 87501

Form C-122 Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

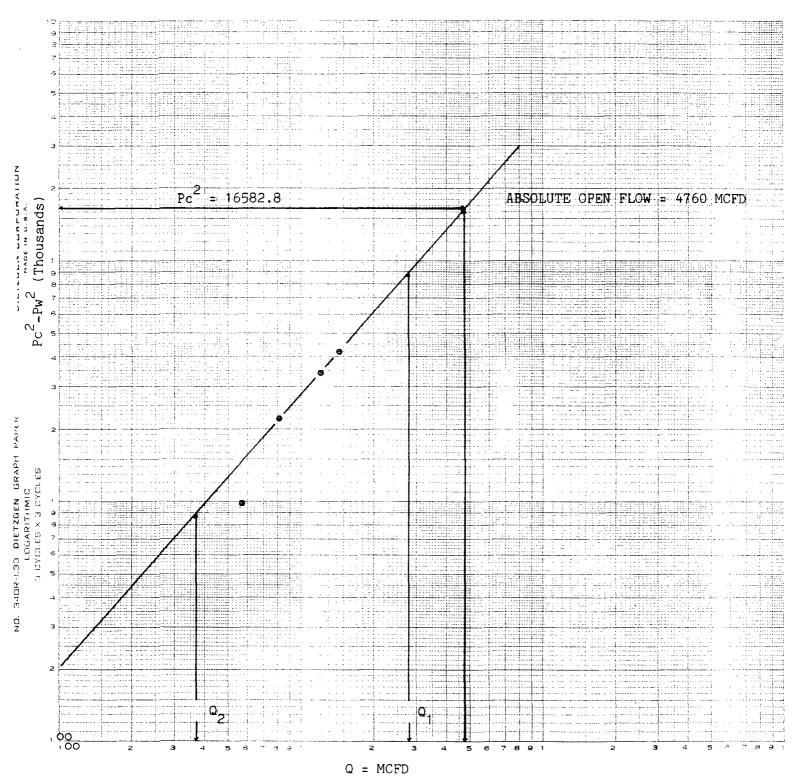
Typ	• T••I	Initial		{	Annual			Spc	cial	7/20/8	37				
Ces	p any Ex	xon Co	mpany	y USA	. Com	ection None			·						
Foc	i	eep Dra			Form	Atok	a						Unit		
Com	pletion Date 6/29/8	7 .	T	otal Cepth 11630'		F*	lug Back 11150						Form or Lease Name Squaw Federal		
Ceq		we.	ه. پ		Set At		erloralio			10057		Well No			
Tro	5"	20.8	o# 	4.154	11630 501 A1	1	Setiotatio Liou	104691	To	10857	<u> </u>	3 Unii	Sec.	Twp. Riges	
7	2 7/8"	6.5		2.441	10400	<u>' '</u>	From	Open		Ended	` `	K	I	23s 25e	
<i>"</i>	Sin			- 0.0. 0.				104	00'			Eddy	у		
1.100	The	1	164 •	tr Temp. °F	i	innudi T	•mp. •F	Baro. Pr	•••. — F	•		State	Marria		
	Tbg	H	104	10633 C	% CO.		1 % N 2	L	% H ₂ S	13.2 Pro	vet	New	Mexico	Taps	
	1			0.59		0.425	0	483					026	Flg	
NO.	Prover	x 0	ilice	OW DATA	Dill	.	Temp.	Pres	BING D	Temp.	Pres	SING	Temp.	Duration	
	Line Size		5120	p.e.1.g.	<u> </u>		•F		TWG •	•••	p. s. i		• F	Flow	
51	4.026	4/64	1.5	00 515		3	77	318 309		63 63		PAC	KER	75.5 hrs	
2.	4.026	7/64	1.5			5	77	298		61				1.0 hrs	
3.	4.026	10/64					77	281		61				1.0 hrs	
4.	4.026	14/64	1.5	00 530	18	3	76	264	0	61				1.0 hrs	
5.								L							
<u> </u>		<u>_</u>	÷		RAT	EOF	FLOW	CALCU	LATIO	NS					
1	Coeffic						Flor	Temp	1 (Gravity	1	Super	i .	ate of Flow	
	-			7/20	.] [0 W 0			1	F	1 0-			die of Fide	
NO.	(24 Ho			VhwP _M	1	P _m		actor Ft.	1	Factor Fq	1	mpress. tor, Fpv		Q, kicia	
9 -	10.84			√h,,P,, 39.81	1	P _m	F	actor	'		Fac	•			
	10.84 10.84		ľ	39.81 56.56	528 533	. 2	0.	9840 9840	1.	.296 .296	1 1	.039 .039		Q, kicia	
1	10.84 10.84 10.84		; {	39.81 56.56 83.65	528 533 538	.2 .2 .2	0.	9840 9840 9840	1.	.296 .296 .296	1 1 1	.039 .039 .040		572 812 1203	
1 2. 3 4.	10.84 10.84		; {	39.81 56.56	528 533	.2 .2 .2	0.	9840 9840	1.	.296 .296	1 1 1	.039 .039		9. kicia 572 812	
1 2. 3 4. 5.	10.84 10.84 10.84 10.84		; {	39.81 56.56 83.65	528 533 538	.2 .2 .2 .2 .2	0.0.0.	9840 9840 9840 9840 9850	1.1.1.1.	.296 .296 .296	1 1 1 1	.039 .039 .040		572 812 1203	
1 2. 3 4.	10.84 10.84 10.84 10.84			39.81 56.56 83.65	528 533 538	.2 .2 .2 .2	0. 0. 0.	9840 9840 9840 9850 9850	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1	.039 .039 .040		572 812 1203 1423	
1 2. 3 4. 5.	10.84 10.84 10.84 10.84	Temp. 537		39.81 56.56 83.65 98.88	528 533 538 543	.2 .2 .2 .2	O. O. O.	9840 9840 9840 9840 9850	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1	.039 .039 .040		572 812 1203 1423	
1 2. 3 4. 5.	10.84 10.84 10.84 10.84 10.84 0.78	Temp. 537		39.81 56.56 83.65 98.88 1.53	528 533 538 543 543 2 0.927 0.926	.2 .2 .2 .2 .2 .2 .2 .2 .2 .2	O. O. O. Liquid Hy Gravity	9840 9840 9840 9840 9850 drocarbon of Liquid	1. 1. 1. 1. 1. Hydroca	.296 .296 .296 .296	1 1 1 1 Dry595	.039 .039 .040 .040		9. kicia 572 812 1203 1423 Mc(/ub).	
1 2. 3 4. 5. NO. 1 2.	10.84 10.84 10.84 10.84 10.84 0.78 0.78	Temp. 537 537 537		39.81 56.56 83.65 98.88 1.53 1.53	528. 533. 538. 543. 2 0.927 0.926 0.925	Cas I. A.P.I. Speci	O. O. O. Iquid Hy Gravity	9840 9840 9840 9850 drocarbon of Liquid	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	x x x	9. kicia 572 812 1203 1423 Mc(/ub).	
1 2. 3 4. 5. NO. 1 2. 3.	10.84 10.84 10.84 10.84 10.84 0.78	Temp. 537		39.81 56.56 83.65 98.88 1.53	528 533 538 543 543 2 0.927 0.926	Cae I. A.P.I. Speci	O. O. O. O. Iquid Hy Gravity fic Gravity fic Gravity	9840 9840 9840 9850 drocarbon of Liquid y Separate	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 Dry595	.039 .039 .040 .040	x x x	9. kicia 572 812 1203 1423 McC/ubl.	
1 2. 3 4. 5. NO. 1 2. 3. 4.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	Temp. 537 537 537 536	? R	39.81 56.56 83.65 98.88 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925	Gae I. A.P.I. Speci Critic	O. O. O. O. Liquid Hy Gravity fic Gravity fic Gravit fic Gravit cal Present	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	Temp. 537 537 537 536	? R	39.81 56.56 83.65 98.88 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925	Gae I. A.P.I. Speci Critic	O. O. O. O. Liquid Hy Gravity fic Gravity fic Gravit fic Gravit cal Present	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	537 537 537 536 9,2	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53	528. 533. 538. 543. 2 0.927 0.926 0.925 0.925	Gas I. A.P.I. Speci Critic Critic	O. O. O. O. Liquid Hy Gravity fic Gravity fic Gravit fic Gravit cal Present	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. kicia 572 812 1203 1423 Mc(/ubl	
1 2. 3 4. 5. NO. 1 2. 3. 4 5 F _C	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	Temp. 537 537 537 536	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925 0.925	Gas L A.P.I. Speci Critic Critic	O. O. O. O. O. Iquid Hy Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 Pr.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	537 537 537 536 Pc ² Ru	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925 0.925	Gas L A.P.I. Speci Critic Critic	O. O. O. O. O. Iquid Hy Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 Fr. NO. 1 2. 3. 4. 3. 4. 3. 4. 4. 5. 7. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	537 537 537 536 9,2 9,3 3950 3792	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925 0.925	Gas L A.P.I. Speci Critic Critic	O. O. O. O. O. Iquid Hy Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 Pr. Pr. Pr. Pr. Pr. Pr. Pr. Pr. Pr. Pr.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80	537 537 537 536 9,2 3950 3792 3628	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53 1.53 1.53 1.53	528 533 538 543 543 2 0.927 0.926 0.925 0.925 0.925	Gas L A.P.I. Speci Critic Critic	O. O. O. O. O. Iquid Hy Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 PC. NO. 1 2 3. 4. 5 7 7 8 7 8 8 9 1 1 2 8 9 1 1 1 2 8 1 1 1 2 8 1 1 1 2 1 2 1 2 1 2	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80 4072.2* Pt ²	Temp. 537 537 536 536 9,2 3950 3792 3628 3519	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53 1.53 1.53 1.53	528. 533. 538. 543. 543. 2 0.927 0.926 0.925 0.925 0.925 978.7 2202.0 3419.0 4198.0	Can I. A.P.I. Speci Critic Critic	O. O. O. O. Cravity fic Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing are return R2 R2 R2 R3 15.025	Ratio Hydroca or Gas Fluid	296 .296 .296 .296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mel/ubl. Deg. (X X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 Fr. NO. 1 2 3. 4. 5 5 A. A. A. A. A. A. A. A. A. A. A. A. A.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80 4072.2* Pt ²	Temp. 537 537 536 536 9,2 3950 3792 3628 3519	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53 1.53 1.53 1.53	528. 533. 538. 543. 2 0.927 0.926 0.925 0.925 0.925 P. 1 - P. 2 978.7 2202.0 3419.0 4198.0	Can I. A.P.I. Speci Critic Critic	O. O. O. O. Cravity fic Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing are return R2 R2 R2 R3 15.025	Ratio Hydroca or Gas Fluid	296 .296 .296 .296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mcl/ubl. Drg. (X X X X X X	
1 2. 3 4. 5. NO. 1 2. 3. 4. 5 Fr. NO. 1 2 3 4 5 5 Abe.	10.84 10.84 10.84 10.84 10.84 0.78 0.79 0.80 0.80 4072.2* Pt ²	Temp. 537 537 536 536 9,2 3950 3792 3628 3519	16582	39.81 56.56 83.65 98.88 1.53 1.53 1.53 1.53 1.53 1.53 1.53	528. 533. 538. 543. 543. 2 0.927 0.926 0.925 0.925 0.925 978.7 2202.0 3419.0 4198.0	Can I. A.P.I. Speci Critic Critic	O. O. O. O. Cravity fic Gravity fic Gravit	9840 9840 9840 9850 drocarbon of Liquid y Separate y Flowing are return R2 R2 R2 R3 15.025	Ratio Hydroca or Gas Fluid	296 .296 .296 .296 .296 .296 .296 .296	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.039 .039 .040 .040 .040	X X X	9. Nicia 572 812 1203 1423 Mcl/ubl. Deg. X X X X X X	

Exxon Company USA COMPANY: Squaw Federal, No. 3 WELL:

LOCATION: K 1 23_s 25_e

COUNTY: Eddy

DATE: July 20, 1987



 $Q_1 = 2800 \text{ MCFD: } Log Q_1 = 3.447158$ $Log Q_2 = 2.568202$ 370 MCFD:

N = 0.878956 = 0.879

JARREL SERVICES, INC.

POST OFFICE BOX 1654

PHONES 505 393-5396 — 393-8274

HOBBS, NEW MEXICO 88240

COMPANY: Exxon Company USA

WELL: Squaw Federal, No. 3 FIELD: Sheep Draw - Atoka

CHRONOLOGICAL PRESSURE DATA

	omanus on and	MT.	ELASPED	· 		PRESSURE		(- 6899)	
DATE	STATUS OF WELL	TIME	HRS.	MIN.	TBG DWT	CSG	10350	10633 ps	sig
1987									
7/20	Shut in 73.5 hrs. Run Bombs to 10350'	9:30 AM	73	30	3180	PKR	4033	4059	
	Started 1st Rate Flowing	11:30	75	30	3180	- MCFD	4033	4059	
	Finished 1st Rate & Started 2nd Rate	12:30 PM	1	00	3095	572	3911	3937	
	Finished 2nd Rate & Started 3rd Rate	1;30	1	00	2985	812	3753	3779	
	Finished 3rd Rate & Started 4th Rate	2:30	1	00	2810	1203	3589	3615	
	Finsihed 4th Rate & Pulled Bombs	3:30	1	00	2640	1423	3480	3506	

NEW-TEX LAB

P.O. Box 1161 Hobbs: New Mexico 88240

ANALYSIS CERTIFICATE

CLIENT:

BENNETT & CATHEY INC.,

1632

ADDRESS:

80X 787

ANALYSIS NUMBER: DATE OF RUN:

Ø7 21 87

CITY, STATE: ARTESIA, NM 88210

DATE SECURED:

07 21 87

SAMPLE IDENT:

EXXON - SQUAW FEDERAL #3

SAMPLING PRESS: 150 PSIG

SAMPLING TEMP: 60 DEG F

AtoKA ****** GAS ANALYSIS ******

	MOLE	GAL/
	PERCENT	MCF
NITROGEN	0.483	
CARBON DIOXIDE	Ø.425	
METHANE	93.981	
ETHANE	3.835	1.023
PROPANE	Ø.789	0.217
ISO-BUTANE	Ø. 161	0.053
NORMAL BUTANE	0. 143	0.045
ISO-PENTANE	Ø. Ø8Ø	0.029
NORMAL PENTANE	Ø. Ø 55	0.020
HEXANES	Ø. Ø48	0.020
TOTAL	1 (2)(2) _ (2)(2)(2)	1 . 407

PROPANE GPM:

0.22

BUTANES GPM:

0.10

ETHANE GPM:

1.02

PENTANES PLUS GPM: 0.07

SPECIFIC GRAV (CALC):

MOLE WEIGHT:

0.5945

17.22

HHV-BTU/CU FT	PRESSURE	(PSIA) WET	DRY
	14.696	1036	1.055
	14.650	1033	1051
	14.730	1038	1057
	14.735	1039	1057

ANALYZED BY:

DEANE SIMPSON

APPROVED BY:

JARREL SERVICES, INC. Box 1230 Hobbs, New Mexico 88240

<<Static Gradient Survey>>

Date: 07/20/87 @ 9:30 am

COMPANY: Exxon Company USA CONTACT: James Fort

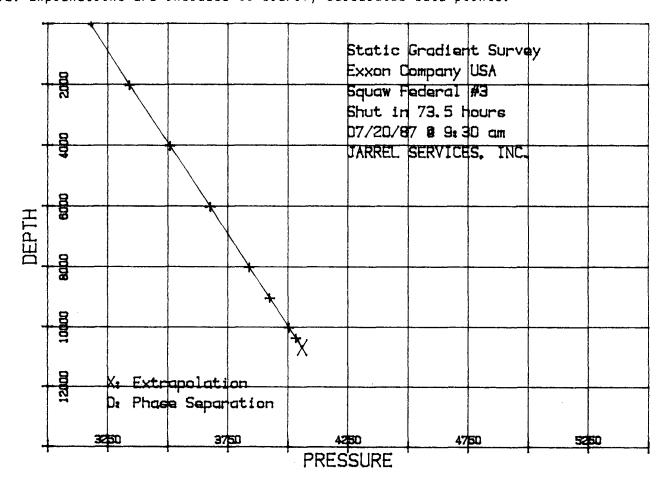
LEASE: Squaw Federal WELL: #3
FIELD: Sheep Draw ZONE: Atoka
COUNTY: Eddy STATE: New Mexico
STATUS: Shut in 73.5 hours OPERATOR: Standefer

DEPTH: 10350 ft TEMPERATURE: 161'F

TABULAR DATA

DEPTH (ft)	PRESSURE (psi)	GRADIENT (psi/ft)	EXPLANATIONS
0	3177		
2000	3339	0.081	
4000	3509	0.085	
6000	3676	0.084	
8000	3839	0.082	
9000	3924	0.085	
10000	4004	0.080	
10350	4033	0.083	
10663	4059	0.083	<=Extrapolated BHP

NOTE: Explanations are included to clarify calculated data points.



Exxon Squaw Federal No. 3 Offset Operators Eddy County, New Mexico

HNG Oil Company
P. O. Box 2267
Midland, Texas 79702

Yates Petroleum 207 S. 4th Artesia, New Mexico 88210

Bureau of Land Management P. O. Box 1449 Santa Fe, New Mexico 87504

EXON COMPANY, U.S.A. POST OFFICE BOX 1600 • MIDLAND, TEXAS 79702-1600

DEC 2 8 1987

OIL CONSERVATION DIVISIONS

PRODUCTION DEPARTMENT SOUTHWESTERN DIVISION

December 10, 1987

Downhole Commingling Request Squaw Federal Well No. 3 Sheep Draw (Morrow) and (Atoka) Pools Eddy County, New Mexico

HNG Oil Company P. O. Box 2267 Midland, Texas 79702

Exxon has applied to the New Mexico Oil Conservation Division for permission to downhole commingle the Morrow and Atoka production in the captioned wellbore. A copy of that application is attached. If you, as an offset operator or lessor have no objection to the granting of this application, we would appreciate your waiver of objection by executing and returning one copy of this letter to the NMOCD and another copy to Exxon in the attached postage paid envelopes.

Sincerely,

James D. Howell

JDH:def

Attachment

Approved

Date

Company ENVIN OUS

EXON COMPANY, U.S.A.

POST OFFICE BOX 1600 • MIDLAND, TEXAS 79702-1600

PRODUCTION DEPARTMENT SOUTHWESTERN DIVISION

December 10, 1987

Downhole Commingling Request Squaw Federal Well No. 3 Sheep Draw (Morrow) and (Atoka) Pools Eddy County, New Mexico

Yates Petroleum 207 S. 4th Artesia, New Mexico 88210

Exxon has applied to the New Mexico Oil Conservation Division for permission to downhole commingle the Morrow and Atoka production in the captioned wellbore. A copy of that application is attached. If you, as an offset operator or lessor have no objection to the granting of this application, we would appreciate your waiver of objection by executing and returning one copy of this letter to the NMOCD and another copy to Exxon in the attached postage paid envelopes.

Sincerely,

James D. Howel

JDH:def

Attachment

Approved

Company

Attorney-M-Fact YATES PETROLEUM CORPORATION Date

December 30, 1987

S. P. YATES PRESIDENT JOHN A. YATES VICE PRESIDENT

December 31, 1987

Exxon Company, U.S.A. P. O. Box 1600 Midland, Texas 79702-1600

TELEPHONE (505) 748-1471

Attention: James D. Howell

Re: Downhole Commingling Request Squaw Federal Well No. 3 Sheep Draw (Morrow) and (Atoka) Pools Eddy County, New Mexico

Gentlemen:

As requested in your letter dated December 10, 1987, we are enclosing a copy of your waiver of objection on the captioned, executed by Yates Petroleum Corporation.

Very truly yours,

SANTAFE

YATES PETROLEUM CORPORATION

Randy 6. Patterson

Land Manager

RGP/bp

Enclosure

cc: NMOCD