

AMERADA HESS CORPORATION

Drawer "D"
Monument, New Mexico 88265

AUGUST 21, 1989

NEW MEXICO OIL CONSERVATION COMMISSION
P.O. BOX 2088
SANTA FE, NEW MEXICO 87501

RECEIVED

SEP - 1 1989

RE: E.W. WALDEN #2
REQUEST TO DOWNHOLE COMMINGLED
THE BLINEBRY AND DRINKARD GAS
ZONES

OIL CONSERVATION DIV.
SANTA FE

DEAR SIR;

AMERADA HESS CORPORATION IS REQUESTING APPROVAL FOR AN EXCEPTION TO RULE 303-C TO PERMIT DOWNHOLE COMMINGLING OF THE BLINEBRY AND DRINKARD GAS ZONES IN THE WELLBORE OF THE E.W. WALDEN #2. PRESENTLY THE BLINEBRY ZONE IS PRODUCING 1 BO AND 168 MCFPD AND THE DRINKARD ZONE IS CI DUE TO ZERO PRODUCTION. REPEATED SWABS IN THE DRINKARD ZONE HAVE PROVEN UNECONOMICAL TO CONTINUE DUE TO FLUID ENCROACHMENT. IF THIS APPLICATION IS APPROVED, BOTH GAS ZONES WILL BE TURNED TOGETHER AND PLACED ON SUCKER ROD PUMP SO AS TO APPLY A CONTINUOUS SWABBING ACTION IN THE WELLBORE AND PERMIT THE FLOW OF NATURAL GAS INTO THE WELLBORE FROM BOTH ZONES AT AN ECONOMICAL RATE.

IN THE WELLBORE, THE BLINEBRY ZONE IS PERFORATED FROM 5483' TO 5605' AND THE DRINKARD ZONE IS PERFORATED FROM 6262'-6376'. BOTTOM HOLE PRESSURES WERE CALCULATED WITH THE METHOD DOCUMENTED IN THE FOLLOWING ATTACHMENTS.

THE RESULTS OF THESE CALCULATIONS WERE:

BLINEBRY:	302 PSIA @ 5544', 24 HOUR SHUT IN
DRINKARD:	356 PSIA @ 6319', 24 HOUR SHUT IN
	ADJUSTED TO A COMMON DATUM
BLINEBRY:	308 PSIA @ 6319'
DRINKARD:	356 PSIA @ 6319'

NO FORMATION PRECIPITATION WHICH MIGHT DAMAGE THE FORMATION IS ANTICIPATED BASED ON PREVIOUS EXPERIENCE. ASSUMING 200 MCFPD TOTAL PRODUCTION WITH 38 MCFPD ALLOCATED TO THE DRINKARD AND 162 MCFPD TO THE BLINEBRY, THE COMBINED STREAM VALUE OF \$262/DAY WOULD BE EQUAL TO THE TWO INDIVIDUAL STREAMS.

NO SECONDARY RECOVERY PROJECT INVOLVING THIS WELLBORE IS UNDER CONSIDERATION AT THIS TIME. IF FUTURE RECOVERY PROJECTS WERE TO BE CONSIDERED, NO PROBLEMS WITH THIS COMMINGLING PROSPECT JEOPARDIZING THE EFFICIENCY OF A SECONDARY RECOVERY OPERATION IS ANTICIPATED.

AMERADA HESS CORPORATION WILL BE THE OPERATOR OF THE SAID WELL ON UNIT K, 2009' FSL, 1911' FWL, SEC. 15, T-22S, R-37E, LEA COUNTY, NEW MEXICO. AMERADA HESS CORPORATION HAS COMMON OWNERSHIP OF BOTH ZONES WITH A WORKING INTEREST OF 100%, 1/8 ROYALTY AND NO OVERRIDING ROYALTY.

A PLAT OF THE AREA IS ATTACHED AT THE END OF THIS LETTER. A DIVISION FORM C-116 WHICH SHOWS THE PRODUCTION FROM THE BLINEBRY ZONE IS INCLUDED.

PRODUCTION DECLINE CURVES HAVE BEEN SUPPLIED FOR BOTH PRODUCING FORMATIONS. USING THESE RATES, A COMBINED RATE WAS CALCULATED AS 17.0%/YR.

OFFSET OPERATORS HAVE BEEN NOTIFIED OF THIS PROPOSAL BY A COPY OF THIS LETTER.

IF THERE ARE ANY QUESTIONS REGARDING THIS PROPOSAL, PLEASE CONTACT ME AT (505) 393-0087.

SINCERLY,

DENISE WARD-WANN
SENIOR PETROLEUM ENGINEER

Anadarko Petroleum
P.O. Box 2497
Midland, Texas 79702

Two States
P.O. Box 176
Eunice, New Mexico 88231

Conoco, Inc.
P.O. Box 460
Hobbs, New Mexico 88240

Wagner & Brown
P.O. Box 1714
Midland, Texas 79702

Exxon
P.O. Box 1600
Midland, Texas 79701

Warrior
P.O. Box 17479
Ft. Worth, Texas 76102

John Hendrix
222 W. Wall
Suite 525
Midland, Texas 79701

Aqua
P.O. Box 1976
Hobbs, New Mexico 88240

Oryx Energy Co.
P.O. Box 1861
Midland, Texas 79702

Arch
777 Taylor Street
Suite II-A
Ft. Worth, Texas 76102

Presidio Exploration
3131 Turtle Creek Blvd.
Suite 400
Dallas, Texas 75219

Meridian
21 Desta Drive
Midland, Texas 79705

Sohio Petroleum Co.
P.O. Box 4587
Houston, Texas 77210

New Mexico Oil Conservation Commission
P.O. Box 1980
Hobbs, New Mexico

Chevron
P.O. Box 670
Hobbs, New Mexico 88240

Dekalb Energy Company
800 Central
Odessa, Texas 79761

The map displays the Gulf of Mexico and surrounding land areas, including parts of Texas, Louisiana, and Mississippi. It is divided into 22 numbered sections, each representing a different oil field or production zone. The sections are labeled as follows:

- 1. Gulf
- 2. Penrose et al
- 3. Cont'l
- 4. Penrose et al
- 5. Rowan
- 6. Elliott
- 7. Elliott
- 8. Elliott
- 9. Penrose
- 10. Anadarko
- 11. Tex Pac
- 12. Magnolia
- 13. Cary
- 14. Humble
- 15. Sohio
- 16. Vanda
- 17. Elliott
- 18. Parker
- 19. Gulf
- 20. Cont'nent
- 21. Skelly
- 22. Humble

Each section contains numerous small circles representing oil wells, some with numbers next to them. The map also shows major cities like Houston, Dallas, and San Antonio, and the Gulf of Mexico coastline. The map is a black and white reproduction of a technical drawing, likely a map for an oil company.

37 EAST

Submit 2 copies to Appropriate District Office.

DISTRICT I
P.O. Box 1980, Hobbs, NM 88240
DISTRICT II
P.O. Drawer DD, Artesia, NM 88210
DISTRICT III
1000 Rio Brazos Rd., Aztec, NM 87410

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-116
Revised 1/1/89

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

GAS - OIL RATIO TEST

Operator AMERADA HESS CORPORATION		Pool Blinebry Gas		County Lea								
Address Drawer "D", Monument, NM 88265		TYPE OF TEST - (X)		Scheduled <input checked="" type="checkbox"/> X								
LEASE NAME E.W. Wallden	WELL NO. 2	LOCATION U S T R	DATE OF TEST 9-10-88	SIZE OF CHOKE 2"	TBG. PRESS. 55	DAILY ALLOW-ABLE GAS WELL	LENGTH OF TEST 24 HOURS	Completion <input type="checkbox"/>		Special <input type="checkbox"/>		
								WATER BBL.S.	PROD. DURING TEST GRAV. OIL	OIL BBL.S.	GAS M.C.F.	GAS - OIL RATIO CU FT/BBL.
								0	--	1	194	194,000

Instructions:

During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well is located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned increased allowables when authorized by the Division.
Gas volumes must be reported in MCF measured at a pressure base of 15.025 psia and a temperature of 60° F.
Specific gravity base will be 0.60.
Report casing pressure in lieu of tubing pressure for any well producing through casing.

(See Rule 301, Rule 1116 & appropriate pool rules.)

I hereby certify that the above information is true and complete to the best of my knowledge and belief.

Signature

Denise Mann - Senior Petroleum Engineer

Printed name and title

August 23, 1989

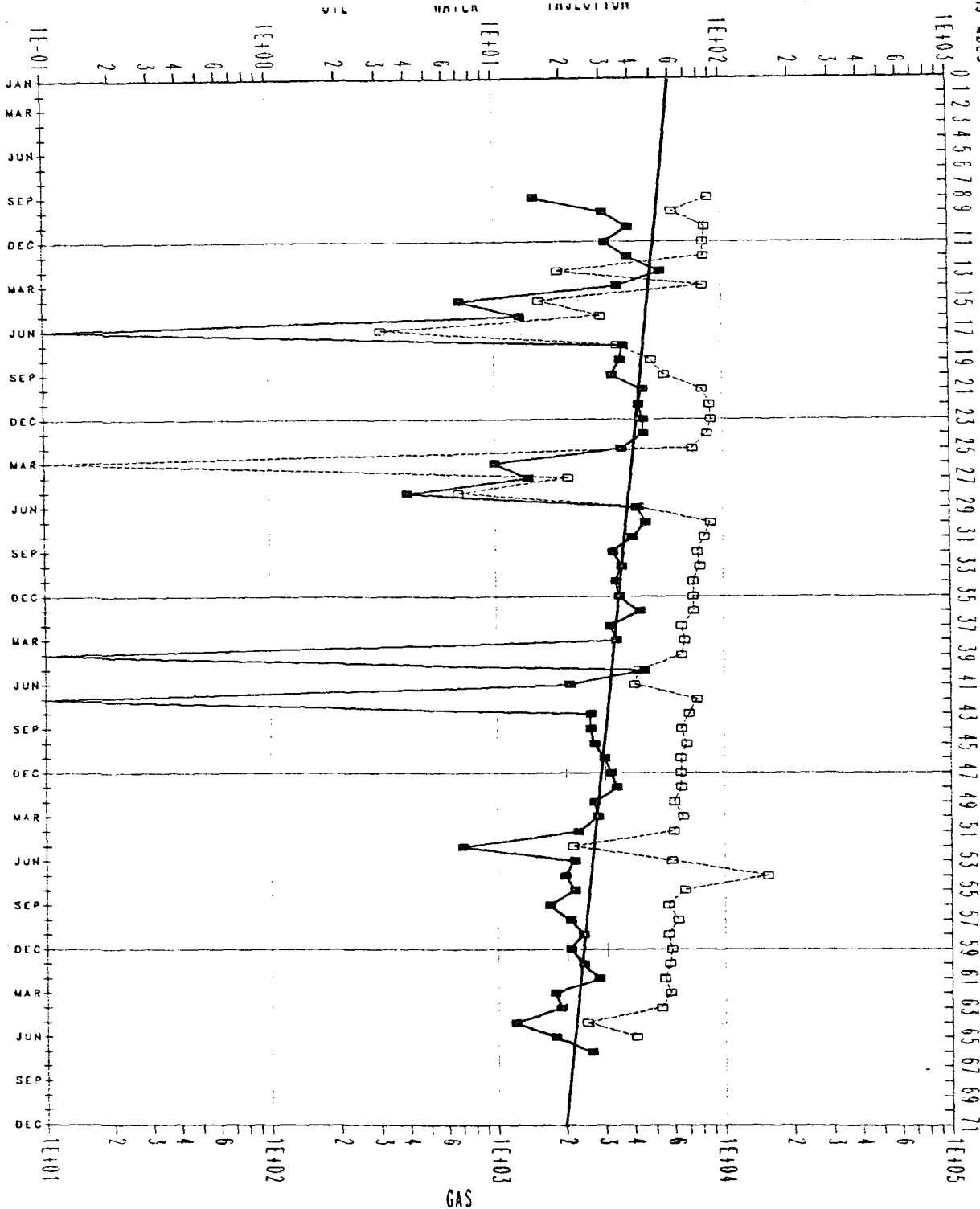
(505) 393-2144

Date

Telephone No.

PRODUCTION PLOT

CUMULATIVES:
 1 MBLS 5.3
 2 MBLS 894.0
 3 MBLS 5.5
 4 MBLS 956.6
 5 MBLS 1028.6
 6 MBLS 1105.8
 7 MBLS 1185.0
 8 MBLS 1219.6



1E-01 = 10
 1E+00 = 100
 1E+01 = 1000

Oil BBL/MO
 Gas MCF/MO

NOTE
 1E+02 = 100
 1E+03 = 1000
 1E+04 = 10000

PLOT DATE: 8/9/88
 PLOT NO.: 1334

REGION: SOUTHWEST ARIZONA
 FIELD: EUNICE FIELD 268
 POOL: /BLINBERT GAS/
 LEASE: 02645 MADEN, CV
 WELL: 21
 STATE CODE: 30 NEW MEXICO
 PROD CODE: 623

STATUS:
 41 ON 6/14/88

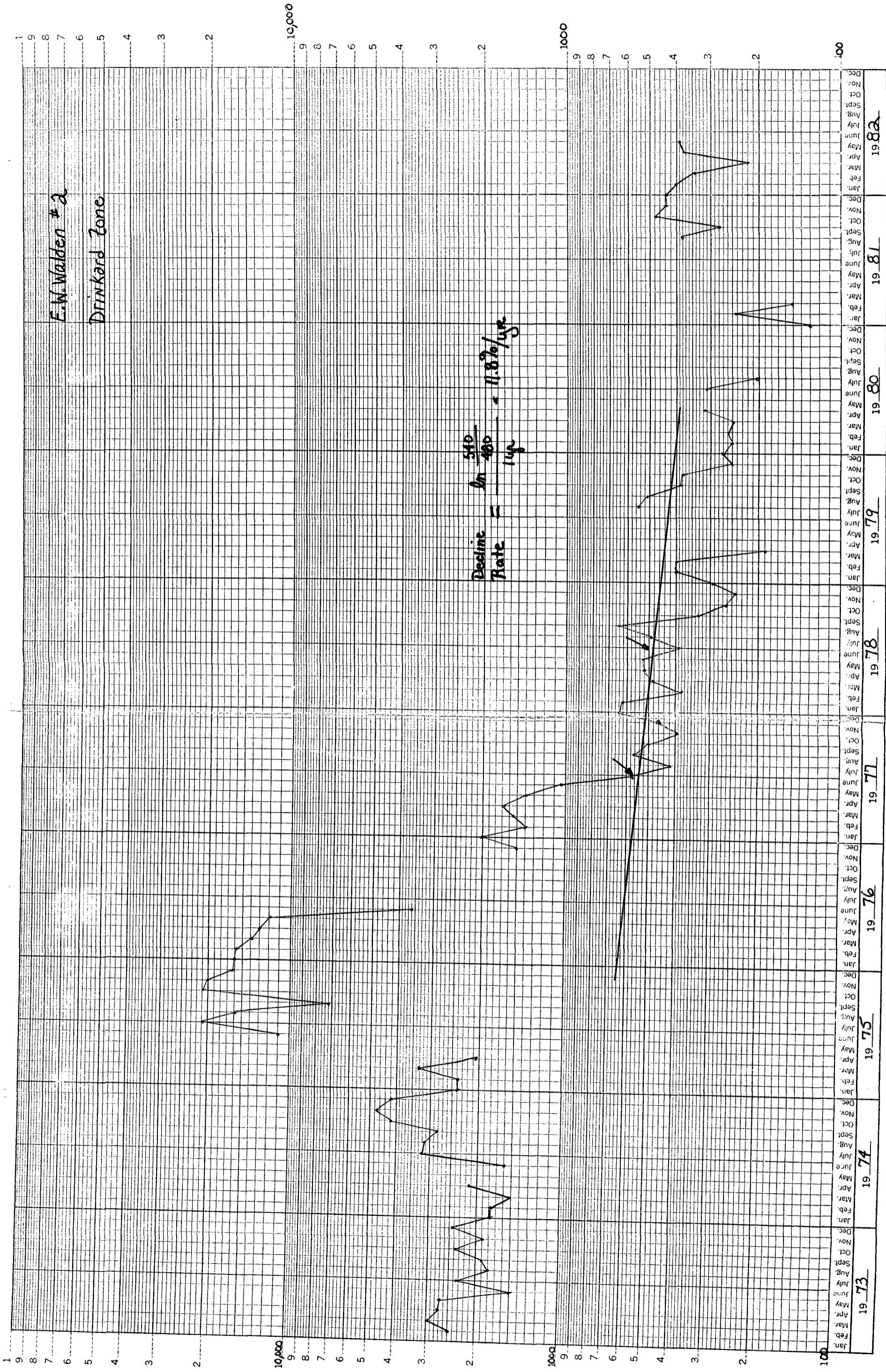
GAS
 FLOWING

$$\text{Decline Rate} = \frac{\ln \frac{2400}{2000}}{1y} = 18.2\%/y$$

WORK OVER CODES:

- X - CHEMICAL SQUEEZE
- J - PARAFFIN INHIBITOR
- R - WELL HEAD
- P - SCALE INHIBITOR
- N - RODS AND/OR PUMP
- L - PULVER ROO
- J - LINER
- H - HOT OIL
- T - FRESH WATER
- D - CLEAN OUT
- B - CONVERT TO SALTWATER
- 9 - CONVERT TO OIL
- 7 - FISH
- 5 - ACIDIZE
- 3 - FERTIGRILL
- 1 - SQUEEZE
- 0 - ABANDONED
- S - CORROSION INHIBITOR
- Q - TUBING
- O - SWAB
- M - SUBMERISABLE EQUIP.
- K - PACTER
- I - HYDRAULIC EQUIPMENT
- G - GAS LIFT VALVES
- E - CUT PARAFFIN
- C - CASING
- A - CONVERT TO NI
- B - GRAVEL PACK
- S - GRILL OUT
- 4 - FRAC
- 2 - PLUG BACK

MCFFPM



SOUTHEAST NEW MEXICO PACKER LEAKAGE TEST

Operator Amerada Hess Corp.				Lease E. W. Walden		Well No. 2	
Location of Well	Unit K	Sec 15	Twp 22S	Rge 37E	County Lea		
Name of Reservoir or Pool			Type of Prod (Oil or Gas)	Method of Prod Flow, Art Lift	Prod. Medium (Tbg or Csg)		Choke S
Upper Compl	Blinebry		Gas	Flow	Tbg.		2"
Lower Compl	Drinkard		Gas	Flow	Tbg.		2"

FLOW TEST NO. 1

Both zones shut-in at (hour, date): 9:00 A.M. 4-3-89

Well opened at (hour, date): 9:00 A.M. 4-4-89

	Upper Completion	Lower Comple
Indicate by (X) the zone producing.....	X	
Pressure at beginning of test.....	250	290
Stabilized? (Yes or No).....	YES	YES
Maximum pressure during test.....	250	290
Minimum pressure during test.....	50	290
Pressure at conclusion of test.....	50	290
Pressure change during test (Maximum minus Minimum).....	200	--
Was pressure change an increase or a decrease?.....	decrease	--

Well closed at (hour, date): 9:00 A.M. 4-5-89

Oil Production During Test: 1 bbls; Grav. --

Gas Production During Test: 168 MCF; GOR 168,000

Remarks

FLOW TEST NO. 2

	Upper Completion	Lower Comple
Well opened at (hour, date):		
Indicate by (X) the zone producing.....		
Pressure at beginning of test.....		
Stabilized? (Yes or No).....		
Maximum pressure during test.....		
Minimum pressure during test.....		
Pressure at conclusion of test.....		
Pressure change during test (Maximum minus Minimum).....		
Was pressure change an increase or a decrease?.....		

Well closed at (hour, date):

Oil Production During Test: bbls; Grav. ;

Gas Production During Test: MCF; GOR

Remarks Drinkard Zone is TA'd.

I hereby certify that the information herein contained is true and complete to the best of my knowledge.

APR 13 1989

Approved _____
New Mexico Oil Conservation Commission

ORIGINAL SIGNED BY JERRY SEXTON
DISTRICT I SUPERVISOR

By _____
Title _____

Operator Amerada Hess Corp.

By Linda Johnson

Title Production Technician

Date 4-10-89

FIG. 16-4
Compressibility factors at low reduced pressures

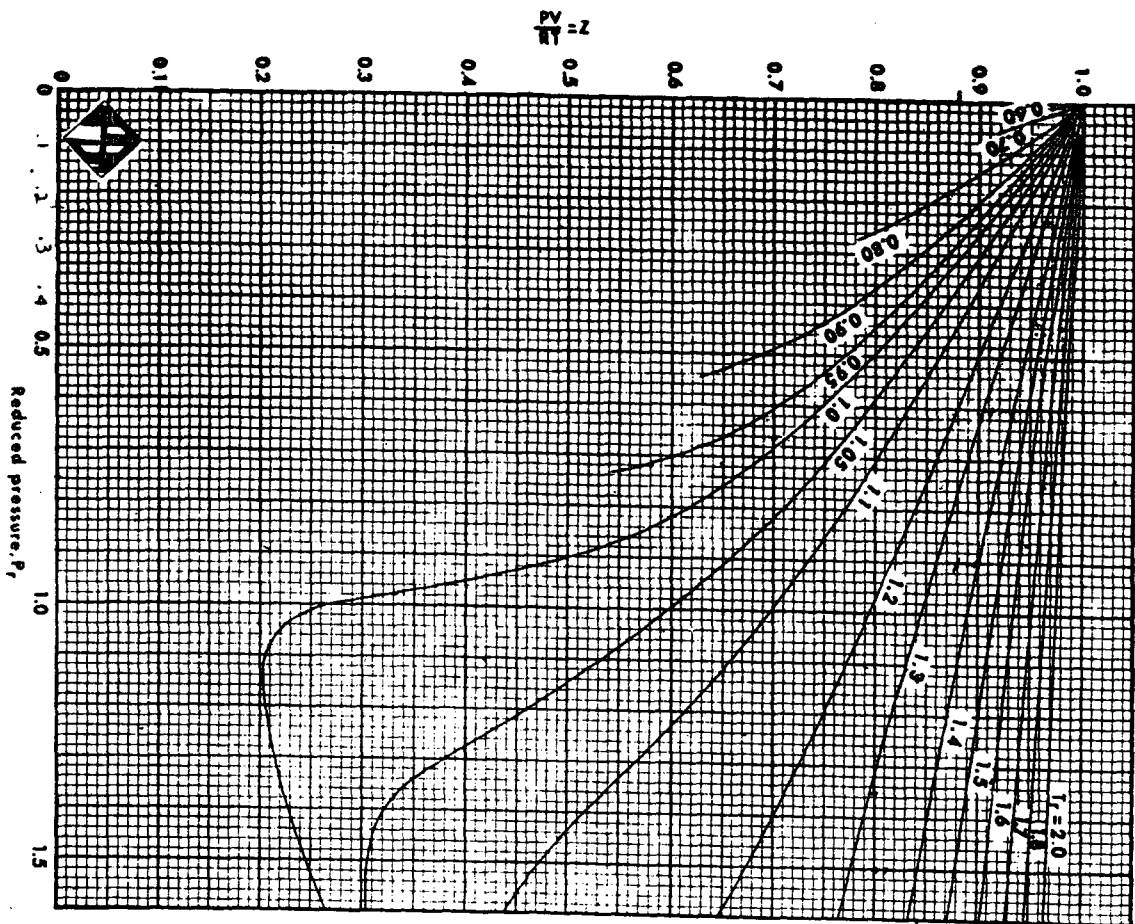
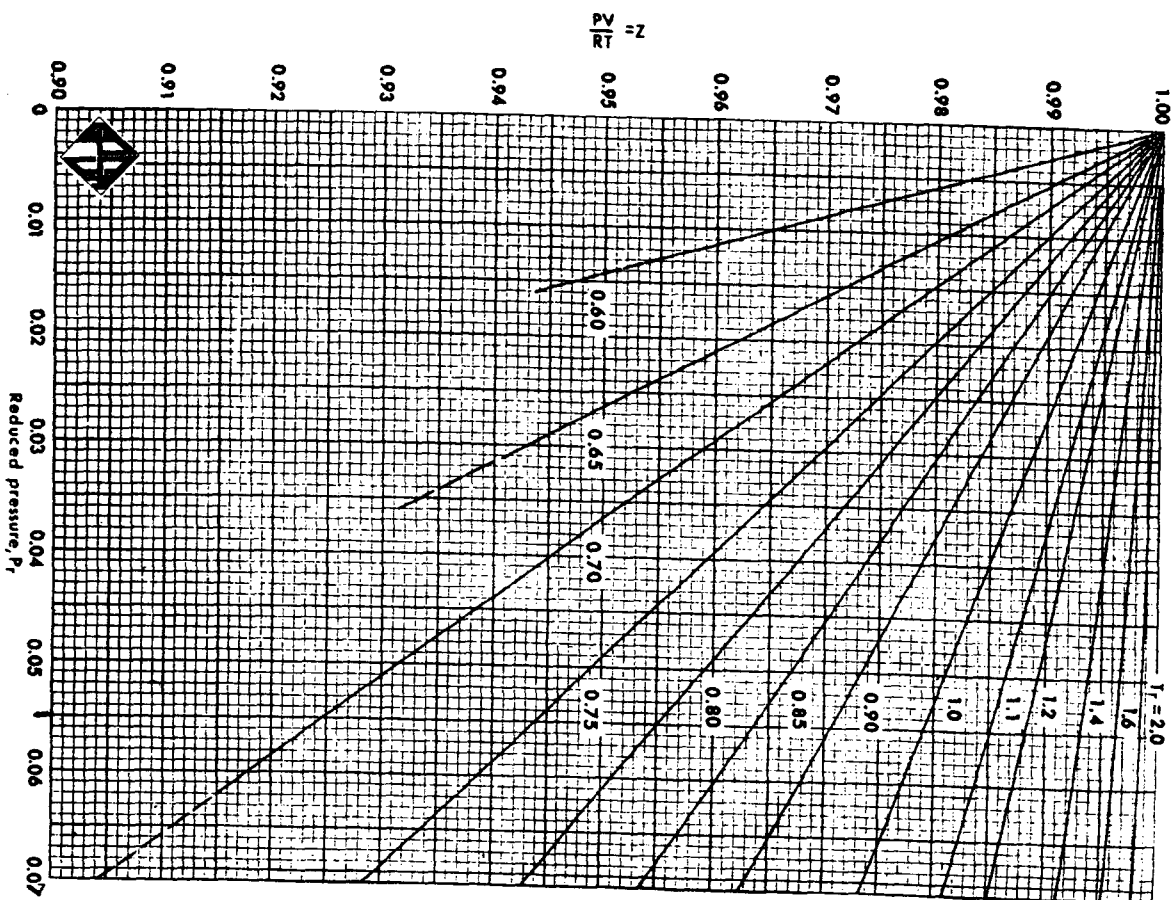


FIG. 16-5
Compressibility factors for gases near atmospheric pressure



vapors. For example for propane at 300 psia and 140°F., turn to the Mollier chart for propane, Fig. 17-6, locate the 300 psia and 140°F. point, and interpolate on the constant specific volume lines to obtain 0.33 cu ft/lb. Dividing this into 1 gives 3.03 lb/cu ft as the density, D_v . If the compressibility is required,

$$Z = \frac{M P}{10.73 T D_v}$$

Symbols have been defined previously. Then

$$Z = \frac{(44.09) (300)}{(10.73) (460+140) (3.03)} = 0.68$$

ACID GASES

Natural gases which contain H_2S and/or CO_2 frequently exhibit different compressibility factor behavior than do sweet gases. Wichert and Aziz (Gas Processing/Canada, pp 20-25, January/February 1971; Hydrocarbon Processing, pp 119-122, May 1972) present a simple easy to use calculational procedure to account for these differences. The method uses the standard gas compressibility factor chart (Figure 16-3) and provides accurate sour gas compressibili-

ties for gas compositions that contain as much as 80% total acid gas.

Wichert and Aziz define a "Critical temperature adjustment factor" which is a function of the concentrations of CO_2 and H_2S in the sour gas. This correction factor is then used to adjust the pseudo critical temperature and pressure of the sour gases according to the equations:

$$T_c^I = T_c - \epsilon$$

$$P_c^I = \frac{P_c T_c^I}{[T_c + B(1-B)\epsilon]}$$

Where:

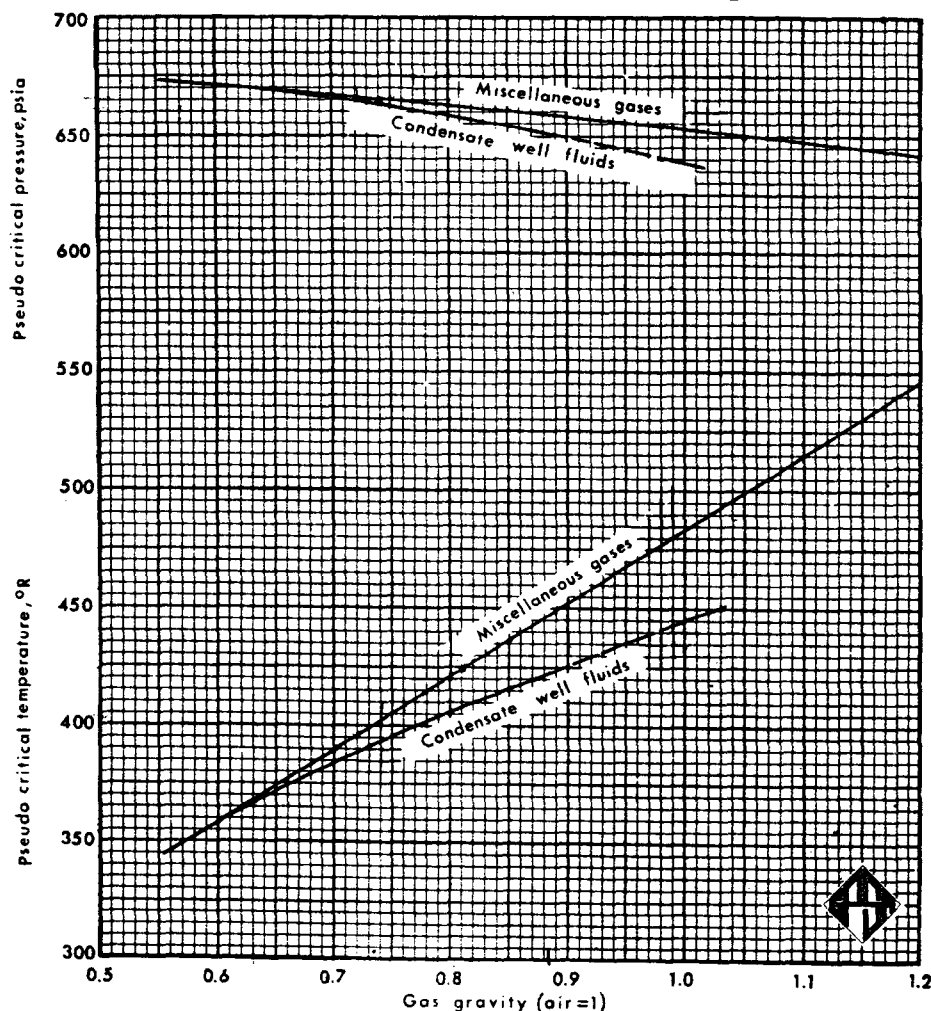
T_c = Mole Fraction average pseudo critical temperature

P_c = Mole Fraction average pseudo critical pressure

T_c^I = Pseudo critical temperature adjusted for acid gas composition

(Text cont'd. p. 16-15)

FIG.16-6
Pseudocritical properties of natural gases



BLINEBRY DECLINE RATE

$$\begin{aligned}q_i &= 2400 \text{ MCFPM} \\q &= 2000 \text{ MCFPM} \\t &= 1 \text{ yr}\end{aligned}$$

$$a = \frac{\ln \frac{2400}{2000}}{1}$$

$$\begin{aligned}a &= .182 \\a &= 18.2\%\end{aligned}$$

DRINDARD DECLINE RATE

$$\begin{aligned}q_i &= 540 \text{ MCFPM} \\q &= 480 \text{ MCFPM} \\t &= 1 \text{ yr}\end{aligned}$$

$$a = \frac{\ln \frac{540}{480}}{1}$$

$$\begin{aligned}a &= .118 \\a &= 11.8\%\end{aligned}$$

COMBINED DECLINE RATE

$$\begin{aligned}q_i &= 2940 \text{ MCFPM} \\q &= 2480 \text{ MCFPM} \\t &= 1 \text{ yr}\end{aligned}$$

$$a = \frac{\ln \frac{2940}{2480}}{1}$$

$$\begin{aligned}a &= .170 \\a &= 17.0\%\end{aligned}$$

ALLOCATION BASED ON DECLINE RATES

If: $x = \text{Blinebry}$
 $1-x = \text{Drinkard}$

$$a_c = x(a)_{\text{blinebry}} + (1-x)(a)_{\text{drinkard}}$$

$$.170 = x(.182) + 1-x (.118)$$

$$.170 = .182x + .118 - .118x$$

$$.170 - .118 = .182x - .118x$$

$$.052 = .064x$$

$$x = .052/.064$$

$$x = .812$$

$$1 - x = .188$$

Blinebry allocation = 81%
Drinkard allocation = 19%

E.W. WALDEN #2

Blinebry Perfs - 5483'-5605' avg. depth (\bar{L}) = 5544'

Drinkard Perfs - 6262'-6376' avg. depth (\bar{L}) = 6319'

Blinebry = .694

$\begin{matrix} G \\ \text{Drinkard} \end{matrix}$ = .702

Assume Patm = 13.2 psia

Assume temp. grad. = 0.4 F/100'

Assume avg. surface temp. = 74 degrees F

BHT = 74 F + 5544' (.4/100') = 96°F
(Blinebry)

BHT = 74 F + 6319' (.4/100') = 99°F
(Drinkard)

Psw = 250 + 13.2 = 263.2 psia
(Blinebry)

Psw = 290 + 13.2 = 303.2 psia
(Drinkard)

BLINEBRY ZONE

SBHP

Formula: Psfs = Pwhs $e^{\frac{c}{z}}$

$$\frac{\bar{T}}{2} = \frac{74^{\circ}\text{F} + 96^{\circ}\text{F}}{2} + 460^{\circ}\text{R} = 545^{\circ}\text{R}$$

$$C = \frac{\gamma_g \bar{L}}{53.34 \bar{T}} = \frac{(.694)(5544)}{53.34 (545)} = 0.131$$

Fig. 16-6

$$P_{pc} = 666 \text{ psia}$$

$$T_{pc} = 388 \text{ R}$$

$$T_r = \frac{\bar{T}}{T_{pc}} = \frac{545}{388} = 1.40$$

TRIAL & ERROR METHOD

$$\text{Assume: } P_{sfs} = 302 \text{ psia} \quad \bar{P} = \frac{302 + 263}{2} = 282 \text{ psia}$$

$$P_r = \frac{\bar{P}}{P_{pc}}$$

$$P_r = 282 \text{ psia} / 666 \text{ psia} = 0.42$$

$$T_r = 1.40$$

FIG. 16-4

$$Z = .952$$

$$P_{sfs} = P_{whs} e^{c/z}$$
$$P_{sfs} = 263 e^{.131/.952}$$

$$P_{sfs} = 302 \text{ psia}$$

DRINKARD ZONE

$$\bar{T} = \frac{74^{\circ} + 99^{\circ}}{2} + 460^{\circ} = 546^{\circ} \text{R}$$

$$C = \frac{(.702)(6319)}{53.34 (546)} = .152$$

FIG. 16-6

$$P_{pc} = 665 \text{ psia}$$

$$T_{pc} = 390^{\circ} \text{R}$$

$$T_r = \frac{\bar{T}}{T_{pc}} = \frac{546}{390} = 1.40$$

TRIAL & ERROR METHOD

$$\text{Assume: } P_{sfs} = 356 \text{ psia}$$

$$P = \frac{356 + 303}{2} = 330 \text{ psia}$$

$$P_r = \frac{\bar{P}}{P_{pc}} = \frac{330}{665} = .50$$

$$T_r = 1.40$$

Fig. 16-4

$$Z = .945$$

$$P_{sfs} = P_{whs} e^{c/z}$$

$$P_{sfs} = 303 e^{.152/.945}$$

$$P_{sfs} = 356 \text{ psia}$$

BLINEBRY SBHP @ 5544' = 302 psia
 DRINKARD SBHP @ 6319' = 356 psia

Adjusted to a common datum @ 6319'
 ∴ Blinebry zone SBHP needs to be adjusted 775'

$$\bar{T} = \frac{96^{\circ} + 99^{\circ}}{2} + 460^{\circ} = 557.5^{\circ} \text{ R}$$

$$P_{pc} = 666 \text{ psia}$$

$$T_{pc} = 388^{\circ} \text{ R}$$

$$T_r = \frac{557}{388} = 1.44$$

$$C = \frac{(.694)(775)}{(53.34)(557)} = .018$$

TRIAL & ERROR METHOD

$$\text{Assume: } P_{sfs} = 307 \text{ psia} \qquad \bar{P} = \frac{307 + 302}{2} = 304.5$$

$$P_r = \frac{\bar{P}}{P_{pc}} = \frac{304.5 \text{ psia}}{666 \text{ psia}} = 0.46$$

$$T_r = 1.44$$

Fig. 16-4

$$Z = .96$$

$$P_{sfs} = 302 \text{ e}^{.018/.96}$$

$$P_{sfs} = 308 \text{ psia} \quad \text{close to } 307 \text{ psia}$$

∴ Psfs = 308 psia

Blinebry adjusted to common datum of 6319'

BLINEBRY ZONE	SBHP	= 308 psia
DRINKARD ZONE	SBHP	= 356 psia

E.W. WALDEN #2

GAS STREAM VALUES

Gas Price as of AUGUST 1989

Drinkard - \$1.31 /mcf
Blinebry - \$1.31 /mcf

Assuming 200 mcfpd total production:

Drinkard production	-	(20 mcfpd) (\$1.31 mcf)	= \$ 26.20
Blinebry production	-	(180 mcfpd) (\$1.31 mcf)	= \$235.80

\$262.00 /day

Combined stream value = (200 mcfpd) (\$1.31 /mcf) = \$262.00 /day

Values are equal.



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION
HOBBS DISTRICT OFFICE

GABRIEL CARROLL
GOVERNOR

8-28-89

POST OFFICE BOX 1980
HOBBS, NEW MEXICO 88241-1980
(505) 393-6161

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

RE: Proposed:

MC _____
DHC X _____
NSL _____
NSP _____
SWD _____
WFX _____
PMX _____

Gentlemen:

I have examined the application for the:

Amerada Hess Corp. E.W. Walden #2-K 15-22-37
Operator Lease & Well No. Unit S-T-R

and my recommendations are as follows:

OK

Yours very truly,

Jerry Sexton
Jerry Sexton
Supervisor, District 1

/ed

RECEIVED

AUG 31 1989

OIL CONSERVATION DIV.
SANTA FE