

GW – 022

**2009 only
PERMIT,
Application**

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September 24, 2009

Mr. Leonard Lowe
Environmental Engineer
New Mexico Oil Conservation Division
1220 S St. Francis Drive
Santa Fe, New Mexico 87505

RE: Frontier Field Service Discharge Permit Renewal
Empire Abo Gas Plant - GW-022
Eddy County, New Mexico

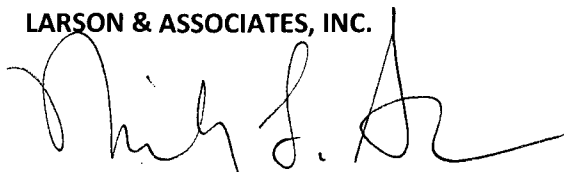
Dear Mr. Lowe:

On behalf of Frontier Field Services, Larson & Associates, Inc., submits this renewal permit for the Empire Abo Gas Plant. Please find enclosed the renewal application, public notice (in English and Spanish) and the filing fee.

If you have any questions or require additional information, please call me at 432.687.0901 to discuss.

Sincerely,

LARSON & ASSOCIATES, INC.



Michelle L. Green
Environmental Scientist
michelle@laenvironmental.com

Enclosure Discharge Permit Renewal Application
Public Notice
Filing Fee

District I
1625 N. French Dr., Hobbs, NM 88240
District II
1301 W. Grand Avenue, Artesia, NM 88210
District III
1000 Rio Brazos Road, Aztec, NM 87410
District IV
1220 S. St. Francis Dr., Santa Fe, NM 87505

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
1220 South St. Francis Dr.
Santa Fe, NM 87505

Revised June 10, 2003

Submit Original
Plus 1 Copy
to Santa Fe
1 Copy to Appropriate
District Office

**DISCHARGE PLAN APPLICATION FOR SERVICE COMPANIES, GAS PLANTS,
REFINERIES, COMPRESSOR, GEOTHERMAL FACILITIES
AND CRUDE OIL PUMP STATIONS**

(Refer to the OCD Guidelines for assistance in completing the application)

☐ New ☒ Renewal ☐ Modification

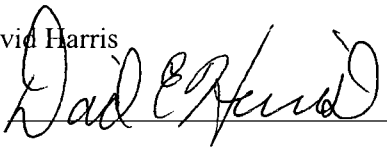
1. Type: Gas Plant
2. Operator: Frontier Field Services, LLC

Address: 257 Empire Road, Artesia, New Mexico, 88210

Contact Person: David Harris Phone: 505-677-5177
3. Location: Unit I (NE/4, SE/4), Section 3, Township 18, South, Range 27 East
Submit large scale topographic map showing exact location.
4. Attach the name, telephone number and address of the landowner of the facility site.
5. Attach the description of the facility with a diagram indicating location of fences, pits, dikes and tanks on the facility.
6. Attach a description of all materials stored or used at the facility.
7. Attach a description of present sources of effluent and waste solids. Average quality and daily volume of waste water must be included.
8. Attach a description of current liquid and solid waste collection/treatment/disposal procedures.
9. Attach a description of proposed modifications to existing collection/treatment/disposal systems.
10. Attach a routine inspection and maintenance plan to ensure permit compliance.
11. Attach a contingency plan for reporting and clean-up of spills or releases.
12. Attach geological/hydrological information for the facility. Depth to and quality of ground water must be included.
13. Attach a facility closure plan, and other information as is necessary to demonstrate compliance with any other OCD rules, regulations and/or orders.
14. CERTIFICATION I hereby certify that the information submitted with this application is true and correct to the best of my knowledge and belief.

Name: David Harris

Title: Plant Manager

Signature: 

Date: 1 Sept 2009

E-mail Address: dharris@frontierfieldservices.com

DISCHARGE PERMIT RENEWAL APPLICATION

GW-022

Frontier Field Services, LLC
Empire Abo Gas Plant
Eddy County, New Mexico

Project No. 9-0111

August 28, 2009

Prepared for:
Frontier Field Services, LLC
257 Empire Road
Artesia, New Mexico 88210

Prepared by:
Michelle L. Green
Environmental Scientist

Larson & Associates, Inc.
507 North Marienfeld, Suite 200
Midland, Texas 79701

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1.0 Type of Operation

Frontier Field Services, LLC (Frontier) operates the Empire Abo Gas Plant located in Eddy County, New Mexico. The facility is a 56 MMcfd cryogenic gas plant and gathering system. The facility utilizes a cryogenic process to remove simple alkanes (i.e. ethane, propane, pentane and hexane) from natural gas and third party y-grade (liquid hydrocarbons). The unprocessed material is transported to the facility via pipelines. The gas is compressed and sent to an amine system to remove carbon dioxide and hydrogen sulfide, dehydrated and cooled. Natural gas liquid and residue gas products leave the facility by means of pipelines. The facility uses scrubbers, exchangers, separators, chillers, flash tanks, and compressors for the various processes.

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2.0 Name of Operator or Legally Responsible Party and Local Representative

Facility Operator and Responsible Party: Frontier Field Services, LLC
257 Empire Road
Artesia, New Mexico 88210

Local Representatives: David Harris
Plant Manager
Office: 575-677-5117
Cell: 575-703-0891

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3.0 Location of the Discharge Plan Facility

The facility is located at Latitude 32° 46' 37.4" North and Longitude 104° 15' 32.7" West, in the NE/4, SE/4, (Unit I), Section 3, Township 18 South, Range 27 East, Eddy County, New Mexico. A topographic map, aerial based map and facility drawing are presented in Figures 1, 2, and 3, respectively.

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4.0 Landowners

The landowner of record, according to the Eddy County Tax Assessor's Office is:

Frontier Field Services, LLC
4200 E. Skelly Drive
Suite 700
Tulsa, Oklahoma 74135

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5.0 Facility Description

The Empire Abo Gas Plant is a cryogenic gas plant and associated gathering system. The plant accepts inlet gas from the various fields. The end products, residue gas and natural gas liquids, are sold to various Petroleum based companies.

A facility diagram depicting locations of storage, disposal and processing areas is presented in Figure 4. Process flow diagrams are presented in Appendix A.

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6.0 Material Stored or Used at the Facility

The following materials are stored and used at the Empire Abo Gas Plant facility:

A. Process specific chemicals (TEG, Amine, Lean Oil, etc.)

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Monoethanolamine	Liquid	1 – 210 bbl Tank	100 bbls	Plastic lined Earthen berm	East of Evap Pond
MR Solvent, Kerosene	Liquid	1 – 500 gallon tank	500 gallons	Fiberglass with earthen berm	South of Shop

B. Acids/Caustics

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Sulfuric acid	Liquid	1000 gallon poly tank	1000 gallon	Concrete berm	East of Cooling Tower
Sodium hydroxide	Liquid	1000 gallon tank	500 gallon	Concrete berm	West of #1 Amine System
Bleach	Liquid	1000 gallon poly tank	1000 gallon	Concrete berm	East of Cooling Tower
Unichem 3941, NaOH based	Liquid	100 gallon tank	100 gallon	Concrete berm	East of Cooling Tower
Sodium Carbonate	Solid	80 lb bag	5 bags	None	Chemical building
Unichem 1304, KOH based	Liquid	100 gallon tank	100 gallon	Concrete berm	East of Cooling Tower
Unichem 1702, Phosphonic acid based	Liquid	100 gallon tank	100 gallon	Concrete berm	East of Cooling Tower
Unichem 3033, TKPP, $K_4P_2O_7$	Liquid	100 gallon tank	100 gallon	Concrete berm	East of Cooling Tower
Caustic Soda Beads, KOH	Solid	2-2500 gallon Old Dehydrator Vessels	28.274 feet ² per vessel	N/A	North Cryogenic Plant
Citric Acid	Solid	80 lb bag	15 bags	None	Chemical building

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C. Detergents/soaps

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Bio-degradable Industrial Detergent	Liquid	Poly Tank	500 gallon	Concrete berm	East of Comp Building

D. Solvents, inhibitors and degreasers

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Unichem 3270, Volatile based amine	Liquid	110 gallon Tank	100 gallons	Concrete berm	East of Cooling Tower
Methanol	Liquid	1000 gallon Tank	1000 gallon	Concrete berm	West of Comp Engine Room
Carb/Choke Cleaner	Liquid	12 oz aerosol can & 3 gallon pail	15 gallons	Flammable Cabinet	Shop Building
Safety Kleen Solvent 150, Petroleum naptha	Liquid	1 - 15 gallon 1 - 30 gallon	45 gallons	N/A	Comp Building, Welding, Warehouse

E. Paraffin Treatment/Emulsion breakers

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Unichem 985, silicone based	Solid	5 gallon pail	1 pail	N/A	Chemical Building

F. Biocides

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Unichem 3141, Oxygen scavenger	Liquid	110 gallon Tank	100 gallon	Concrete berm	East of Cooling Tower
Alpha 120	Liquid	5 gallon pail 65 gallon tank	3 pails 60 gallons	Fiberglass	Chemical Bldg East of Cooling Tower
Alpha 512	Liquid	5 gallon pail 65 gallon tank	3 pails 60 gallons	Fiberglass	Chemical Bldg East of Cooling Tower

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G. Others (other liquids or solids such as diesel or cement, etc.)

Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Lubrication Oils	Liquid	2 - 400 bbl tanks	800 bbls	Metal berm with liner	South of Shop building
ISO 22 Oil	Liquid	1000 gallon Tank	700 gallon	Concrete berm	East of Comp building
Rental Lube Oil	Liquid	Tank	500 gallon	Fiberglass	SE corner of plant
Chevron 541 Oil	Liquid	2 - 322 bbl Tanks	400 bbl	Earthen berm	South of Shop
Condensate	Liquid	400-bbl Gunbarrel 2-400 bbl Tank	1200 bbl	Metal berm with liner	Condensate storage area
Diesel	Liquid	2 - 500 gallon Tanks	1000 gallon	Fiberglass	SE of Comp Building
Gasoline	Liquid	1 - 1000 gallon 1 - 500 gallon Tanks	1000 gallon 500 gallon	Fiberglass	South of Comp building
Propane	Liquid	1400 bbl Tank	250 bbls	Earthen berm	Tank Farm
Propylene Glycol	Liquid	55 gallon drum	4 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
Methanol	Liquid	1000 gallon Tank	1000 gallon	Concrete berm	Cryo
Ethyl Mercaptan	Liquid	500 gallon Tank	55 gallons	Concrete berm, enclosed system	Loading Rack
Process Drains	Liquid	550 bbls & 210 bbl Tanks	700 bbl	Earthen berm	West side of Plant
Aluminum Oxide	Solid	2000 lb Super Sack	1 super sack	N/A	North of Evap Pond
Sulfur	Molten	Tank	13 short tons	Concrete vault	NW corner of Plant-underground
Engine Lubricant	Liquid	55 gallon drum	4 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
Activated Alumina	Solid	2000 lb sack	2 sacks	N/A	Warehouse

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Material Name	Solid or Liquid	Type of Container	Estimated Volume	Secondary Containment	Location
Cylinder Oil-680	Liquid	55 gallon drum	2 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
Epoxy Resin	Liquid	1 gallon pail	20 pails	N/A	Chemical building
Gear Compound ESP - Oil	Liquid	55 gallon drum	2 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
Unichem 2310, Sodium nitrate, corrosion inh.	Liquid	100 gallon	100 gallon	Fiberglass containment	East of #9 Inlet Gas Comp Building
American Industrial Oil #150	Liquid	55 gallon drum	2 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
American Industrial Oil #46	Liquid	55 gallon drum	2 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
American Industrial Oil #68	Liquid	55 gallon drum	2 drums	Concrete berm with grates	East of #9 Inlet Gas Comp Building
Activated Charcoal	Solid	Filter Towers	N/A	Concrete berm	Amine System Area
Glass Beads, Sodium aluminum silicate	Solid	50 lb bag	5 bags	N/A	Welding Shop
y-Grade	Liquid	1000 gallon tank	1000 gallons	N/A	Holding Tank in Amine System Area
Slop Oil	Liquid	2 - 1000 gallon tanks	2000 gallons	Earthen berm	South of Tank Farm
Sodium chloride	Solid	50 lb bags	147 bags	N/A	R/O Building
Heat Transfer Salt Mixture	Solid	Block	5 blocks	N/A	Salt Bath Heater

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7.0 Sources and Quantities of Effluent and Waste Solids Generated at the Facility

The facility generates the following:

1. Separators, Scrubbers, Slug Catchers

Gunbarrel Waste Tank

The facility generates produced water and condensate mixture from the dehydration units, closed header tanks, and inlet scrubbers. The water and condensate mixture is separated out in the gunbarrel. The condensate and oil is recovered as a product and is sold. The waste water is transported via pipeline to an OCD approved Class II Disposal Well operated by BP. The facility generates approximately 3,000 barrels (bbls) per month of waste water. This waste water is considered RCRA exempt.

2. Boilers, Waste Heat Recovery Units, cogeneration facilities, and cooling towers/fans

Amine Drain Tank

The facility uses monoethanolamine (amine) to remove hydrogen sulfide and carbon dioxide gases from the gas stream. The amine is recycled back into the system. Spent amine is transferred to an open drain sump. Contents of the sump are then transferred to the Process Drain Tank. The waste water is disposed quarterly by trucking to an OCD approved disposal facility, I & W, Inc.

Evaporation Pond Water

The facility generates waste water from blow-down of the cooling tower, backwash system processes and back-flush/rejection water from the reverse osmosis system. Approximately 200 to 400 bbls of waste water are generated on a daily basis. The waste water is transferred to the evaporation pond. Excess waste water from the evaporation pond is transferred to the Waste Water Tank located directly north of the pond. The waste water is transported via pipeline to an OCD approved Class II Well, operated by BP.

Representative grab samples from the North and South ends of the Pond were collected on April 30, 2009 and submitted for Benzene, Toluene, Ethylbenzene and Xylenes (BTEX), metals, anions, alkalinity, total dissolved solids (TDS) and pH parameters. The sample was determined to be non-hazardous based on analytical data (work order 0905016) provided by DHL Analytical, Inc. (DHL).

Laboratory analytical reports are presented in Appendix B.

3. Wash down/Steam out effluent from process and storage equipment internals and externals

Process Drain Tank Waste

The facility generates a mixture of amine and waste water from various processes (blow-down and drains in the amine and coolant systems). The amine and waste water from the open drain storage area is transferred to the Process Drain Tank. The facility generates approximately 70 bbls of waste water

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per month. The waste water is disposed quarterly by trucking to an OCD approved disposal facility, I & W, Inc.

Dirty Slop Oil Tanks

The facility generates waste oil from the compressor engine pit drains. The waste oil is transferred to the Dirty Slop Oil Tanks. The facility generates approximately 400 bbls of oil waste per week.

A representative sample was collected on September 2 and September 23, 2009 and submitted for waste characterization parameters. The waste oil is disposed of weekly at an OCD approved disposal facility, I & W, Inc.

4. Solvent/degreaser use

Safety Kleen 150 Solvent

The solvent (Petroleum naptha) is used in the parts washer to degrease and clean small parts. The facility disposes of approximately 45 gallons of the solvent every three months by Safety Kleen.

Methanol

The facility uses methanol in the cryogenic unit. The methanol is recycled in the process.

5. Spent acids or caustics

Sulfuric Acid

The sulfuric acid is used to control the pH in the cooling tower. The neutralized and spent acid is transferred as cooling tower blow-down to the evaporation pond. The waste water is transported via pipeline to an OCD approved Class II Disposal Well operated by BP.

Sodium carbonate – soda ash

Sodium carbonate is used to neutralize acid spills. The sodium carbonate is spent during the neutralization process.

Sodium hydroxide

Sodium hydroxide is used in boilers for alkalinity treatment. The spent waste is transferred to the evaporation pond and transported via pipeline to an OCD approved Class II Well operated by BP.

Bleach

The facility uses bleach as a chlorine source in the cooling tower. The waste water is transferred to the cooling tower as blow-down to the evaporation pond. The waste water is transported via pipeline to an OCD approved Class II Well operated by BP.

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6. Used engine coolants (antifreeze)

Propylene glycol

The facility uses propylene glycol in the Jacket #9 Water Tank. The water and antifreeze mixture is recycled in the process.

7. Used lubrication and motor oils

Lubrication, Gear and Synthetic Oils

The oils are used to lube engines, pumps, and compressors. The used oil is transferred to the Dirty Slop Oil Tanks for proper disposal.

8. Used lube oil and process filters

Process Filters

Process filters (sock filters, pre and after charcoal filters and bag filters) and oil filters are collected and placed in the Used Filter Bin located at the South end of the plant. The filters are recycled by US Filter or Procycle, an approved recycling facility about every six (6) months.

9. Solids and sludges from tanks

Sludges

Sludge waste from the sumps is removed by I & W, Inc. The sludge is disposed "as needed" by trucking to an OCD approved disposal facility, I & W, Inc.

10. Painting wastes

Paint Cans

The facility utilizes paint for marking the safety hazard awareness areas (steps, uneven surfaces, etc.) and for maintaining process equipment. The empty cans and pails are placed in the Scrap Metal recycling bin.

11. Sewage

Septic Tank

The facility is not connected to a publicly owned treatment works; however two septic systems are utilized at the facility. The septic tanks are located near the northeast corner of the office and in the southwest area of the Amine System. Septic system maintenance is performed by J.C. Septic Tank Service Company. The septic tank complies with applicable requirements.

12. Laboratory wastes

Non-applicable

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13. Other waste liquids

Stormwater

Stormwater collects in secondary containments and is removed using procedures described in the facility Spill Control and Countermeasures Plan (SPCC). Stormwater is disposed when necessary by trucking to an OCD approved disposal facility, I & W, Inc.

14. Other waste solids

Metal

The facility recycles various un-usable metal parts and metal shavings. These are placed in a metal recycling dumpster.

Aluminum oxide

The plant uses aluminum oxide balls as a catalyst in the sulfur recovery process. Depleted aluminum oxide balls are placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Activated carbon

The plant uses activated charcoal in the amine system. Depleted activated charcoal is placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Molecular sieve/zeolite

The plant uses molecular sieves during the gas separation process. Depleted molecular sieves are placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Oily Soil

The plant personnel remediate oil spills around the yard as they occur. The soil is stockpiled, tested and disposed of at an OCD approved disposal facility, CRI, Inc., or treated onsite.

Sulfur

The plant recovers sulfur from the acid gas. The recovered sulfur is a product that is sold to various customers.

Ceramic balls, Molecular sieves, Aluminum silicate

The plant uses various media: ceramic balls in conjunction with catalysts, molecular sieves and aluminum silicate to increase the production of clean fuels, absorb water from the air, filter various compounds and protect catalysts. Depleted media is placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Activated Alumina

The plant uses activated alumina in the sulfur plant reactors. The activated alumina is consumed in the process.

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8.0 Description of Current Liquid and Solid Waste Collection/Storage/Disposal Procedures

Gunbarrel Waste Water

The oil and produced water mixture from the dehydration units, closed header tanks and inlet scrubbers are transferred to the Gunbarrel Waste Tank which is located in the Condensate Storage Area near the south end of the plant. The water and oil mixture is separated in the 400 bbl capacity gunbarrel tank. The condensate and oil is recovered as a product and sold to various oil related customers. The plant disposes of approximately of 3,000 bbls of waste water per month. The waste water is sent offsite via pipeline to a permitted OCD Class II disposal well operated by BP.

Process Drain Tank Waste

The spent amine and water is collected in the 500 bbl Process Drain Tank located east of the Evaporation Pond. The plant disposes of approximately of 200 bbls of spent amine and waste water every three months in a permitted OCD Class II disposal well operated by I & W, Inc.

Evaporation Pond Water Waste

The waste water from the blow-down of the cooling towers, backwash system processes and rejection water from the reverse osmosis system is transferred to the evaporation pond. Excess waste water in the pond maybe transferred to the 300 bbl Waste Water Storage Tank located directly north of the pond. The plant disposes of approximately of 200 to 400 bbls of waste water daily which is sent offsite via pipeline to a permitted OCD Class II disposal well operated by BP.

Safety Kleen 150 – Petroleum Naptha

The solvent is used in the parts washer to clean small parts. The parts washer vessels are leased from Safety Kleen. The facility disposes approximately 45 gallons on a quarterly basis by Safety Kleen.

Carb/Choke Cleaner - Aerosol Cans and Pails

The facility utilizes carb/choke cleaner to clean electrical parts and contacts. The cleaner is used according to manufacturer instructions. The empty cans and pails are placed in a trash bin for proper disposal as unregulated solid waste.

Dirty Slop Oil Tank Waste

The used oil generated by the plant and the compressor units is transferred to the Dirty Slop Oil Tanks located south of the tank farm. The plant has two tanks with a capacity of 400 bbls each. The plant disposes of approximately of 40 bbls of used oil and waste water per week. The used oil and waste water is trucked offsite to an OCD approved facility operated by I & W, Inc.

Sludges

Sludge waste from the sumps is removed and disposed of monthly to an OCD approved facility operated by I & W, Inc.

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Metal

The facility collects un-usable metal parts and scrap metal. The scrap metal is placed in a metal recycling dumpster located west of the condensate storage tank area. Scrap metal is taken to a local metal recycling facility.

Septic System Waste

The facility is not connected to a publically owned treatment works; however two septic systems are located near the northeast corner of the office and in the southwest area of the Amine System. Septic system maintenance is performed on an "as needed basis", J.C. Septic Tank Service Company.

The septic waste is managed in leach fields on-site.

Aluminum oxide

The plant uses aluminum oxide balls as a catalyst in the sulfur recovery process. Depleted aluminum oxide balls are placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Activated carbon

The plant uses activated charcoal in the amine system process. Depleted activated charcoal is placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Molecular sieve/zeolite

The plant uses molecular sieves during the gas separation process. Depleted molecular sieves are placed in drums and disposed at an OCD approved disposal facility, CRI, Inc.

Oily Soil

The plant is in the process of remediating oil spills in the vicinity of the flare sump. Removed soil is stockpiled and tested. Oily soil is disposed of at an OCD approved facility, CRI, Inc. or treated onsite.

Ceramic balls, Molecular sieves, Aluminum silicate

The plant uses various media: ceramic balls in conjunction with catalyst, molecular sieves and aluminum silicate to increase the production of clean fuels, absorb water from the air, filter various compounds and protect catalyst. Depleted media is placed in 55 gallons drums and disposed at an OCD approved disposal facility, CRI, Inc. on an "as needed basis".

Process Filters

Process filters (sock filters, pre and after charcoal filters and bag filters) and oil filters are collected and placed in the Used Filter Bin located at the South end of the plant. The filter bin is picked up for recycling every six months by US Filter or Procycle, and transferred to an approved recycling facility.

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9.0 Proposed Modifications

Dirty Slop Oil Tanks

The Old Dirty Oil Slop Tanks will be decommissioned in the near future. The tanks are currently located within an earthen berm near the east side of the plant. The plant will remove the two metal tanks. Soil samples will be collected from below the tanks to investigate the potential for a release according to guidelines "*Guidelines for Remediation of Leaks, Spills and Releases, August 13, 1993*".

A 400 bbl replacement tank has been installed in the lined secondary containment of the condensate storage area located near the south side of the plant.

Condensate Tank Storage Area

The condensate tank storage area has a metal retaining wall with a poly-liner. Four tanks, each with a 400 bbl capacity, are located inside the containment. Two of the tanks are used for condensate storage, which is sold as product. The gunbarrel and the new Dirty Slop Oil tanks are also located inside the containment. The tanks are placed on a raised platform to allow visual inspection of the tank bottoms.

Engine #9 Jacket Water Storage Tank

The leaking water tank for Engine #9 Jacket will be removed from service. A leak was noted during the OCD inspection on April 22, 2009. The water tank will be replaced with a new tank that will be placed inside secondary containment with an impermeable liner.

Sulfur Tank Removal

On April 5, 2009, the plant removed the Sulfur Tank located in the northwest corner. The tank was removed for proper disposal. Confirmation soil samples were collected below the tank. The removal and closure were performed with OCD approval.

Groundwater Sampling Event

On May 8, 2008, LAI requested permission to modify the groundwater sampling schedule from quarterly to semi-annually. This request was approved via email on the same day. A copy of the email requests and approvals are provided as Appendix C.

Frontier request to maintain the semi-annual (twice annular) groundwater monitoring frequency, but reduce the parameter list to BTEX, chloride, sulfate and TDS analyses. Metal samples will also be collected for MW-02 (arsenic) and EB-04 (chromium). Annual groundwater monitoring reports will be submitted to the OCD during the first quarter of the calendar year.

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10.0 Inspection, Maintenance and Reporting

Drum Storage Area

The drum storage area is a concrete structure with secondary containment with curbing. The secondary containment stores empty and full drums. Drums are properly labeled and the containment and drums are inspected daily as described in the SPCC Plan.

Underground Lines

The plant has underground lines from various processes and wastewater. The lines were hydrostatically pressure tested to demonstrate mechanical integrity between April 21 and May 10, 2005. Services were provided by TRS Resources, LLC (TRS). All underground lines met the requirements of the mechanical integrity test. All above ground surface piping were visually inspected for leaks after the test pressure was stabilized. The summary report *Hydrostatic Pressure Testing of Underground Drain Piping* conducted by TRS, is presented in Appendix D.

The underground and surface lines will be hydrostatically pressure tested in the first semi-annual of 2010.

Containments and Sumps

All containments and sumps are visually inspected weekly as described in the SPCC Plan.

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11.0 Spill/Leak Prevention and Reporting Procedures (Contingency Plan)

The facility has a site specific Contingency Plan. A copy of the plan is located in Appendix E.

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12.0 Site Characteristics

1. Surface Water Hydrology

The facility is located approximately nine miles east-southeast of Artesia, on the edge of a plateau's southerly slope. The location is hydrologically bound by Scoggins Draw (aka Coggins Draw on some early maps) to the south, and incised tributary drainages to the west and the east. Scoggins Draw is an ephemeral watercourse flowing southwest about three miles into the ephemeral Chalk Bluff Draw. Approximately 1.8 miles further downstream, Chalk Bluff Draw discharges into the Pecos River approximately two miles south of Brainard Lake and about six miles north of Lake McMillan.

Comparing the elevation of Scoggins Draw and the depth to groundwater from the nearest monitoring points (P-04, EB-07, and EB-01), groundwater is approximately 25 feet below ground surface (bgs) in the drainage. This watercourse is a losing stream without groundwater affecting surface water or discharging to the surface. There are no documented groundwater discharge sites, e.g. springs, seeps, marshes or swamps, within a mile of the outside perimeter of the facility.

A search of the State Engineer's New Mexico Water Rights Reporting System (NMWRRS) database did not identify any points of diversion within ¼-mile of the facility's perimeter. A copy of the database and ancillary documentation of two points of discharge beyond the area of concern is attached in Appendix F.

2. Groundwater Characteristics

1. Groundwater Flux and Gauging Results

Historic groundwater flow direction was reported to be towards the south-southwest consistent with vicinity surface water drainage (Hendrickson and Jones, 1952). During LAI's investigation, groundwater mounding is obvious in the north central portion of the facility, and appears to have affected the groundwater flow direction. Current potentiometric maps depict groundwater south of the mound moving towards the southeast, while groundwater to the north of the mound appears to be moving towards the north. The groundwater mound may be due to perched water in discontinuous clay and silty-clay units present in the north central area of the plant.

Three groundwater gauging events have been performed since the last OCD reporting. These events occurred on September 15, 2008, March 10, 2009, and July 13, 2009, after the installation of additional monitor wells. Groundwater elevations in the more peripheral monitor wells remained relatively stable for this site – about two feet or less fluctuation – between September 2008 and July 2009. This high degree of fluctuation in all wells may indicate a high permeability and response to meteoric influences. Seven central wells (MW-02-03, MW-02-06, MW-02-09, MW-02-10, MW-02-13, MW-06, and MW-07) exhibited fluctuations between 4.21 feet (MW-02-06) and 17.14 feet (MW-02-03), which may indicate a water source artificially recharging the aquifer.

During the most recent gauging event (July 13, 2009), groundwater beneath the facility is encountered between 3.73 (MW-07) and 94.00 (MW-16) feet bgs (3,466.54 and 3,618.66 feet elevation NGVD 1929, respectively). Shallow groundwater was observed near MW-02-02 and MW-02-05 where a repaired leak occurred, while the deepest groundwater was encountered from the well farthest north and upgradient

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from the site (MW-16). Similar results were observed during the September 2008 and March 2009 monitoring events. Table 1 is a summary of groundwater monitoring data since LAI began investigation activities at this facility in 2007. Figures 5a and 5b are Groundwater Gradient/Potentiometric Maps for the September 2008 and July 2009 gauging events, respectfully. Figures 5c and 5d present Depth to Groundwater Maps for the March 2009 and July 2009 gauging events, respectfully. The groundwater maps presented were generated using Surfer® data contouring program.

Phase-separated hydrocarbons (PSH) found impacting facility groundwater are primarily light-end gas condensates. Some monitor wells have a product emulsion. This emulsion may be the result of high-pH water reacting with hydrocarbons in a saponification process. PSH or emulsion was observed in the following monitor wells during the past three gauging events:

- MW-02-04 – sheen, July 2009
- MW-02-09 – 8.83 feet, September 2008; 3.89 feet, March 2009
- MW-02-10 – 8.78 feet, September 2008; emulsion, March and July 2009
- MW-02-11 – 0.55 feet, September 2008; emulsion, March 2009
- MW-02-12 – emulsion, all three events
- MW-02-13 – sheen, September 2008; 3.17 feet, March 2009
- MW-02-14 – 0.56 feet, September 2008; 0.28 feet, March 2009
- MW-03 – 3.05 feet, September 2008; 2.67 feet, March 2009
- MW-03-01 – 15.49 feet, September 2008; 10.69 feet, March 2009; 11.16 feet, July 2009
- MW-03-02 – emulsion, all three events
- MW-03-03 – 0.01 feet, September 2008; sheen, March 2009
- MW-03-04 – 0.79 feet, September 2008; 0.82 feet, March 2009; 0.83 feet, July 2009
- MW-04 – 5.09 feet, September 2008; 4.65 feet, March 2009; 5.80 feet, July 2009
- MW-06 – 13.39 feet, September 2008; 7.34 feet, March 2009
- MW-07 – 0.11 feet, September 2008; 0.30 feet, March 2009; sheen, July 2009
- MW-09 – 0.23 feet, September 2008; 0.06 feet, March 2009; 0.09 feet, July 2009
- MW-10 – 0.66 feet, September 2008; 16.90 feet, March 2009; 5.61 feet, July 2009
- MW-11 – 19.27 feet, September 2008; 14.86 feet, March 2009; 15.40 feet, July 2009
- MW-12 – 0.01 feet, September 2008; sheen, March 2009
- MW-14 – 0.29 feet, September 2008; 1.65 feet, March 2009; 1.19 feet, July 2009
- MW-15 – sheen, March 2009
- MW-19 – 5.35 feet, July 2009
- MW-20 – 17.29 feet, July 2009
- MW-21 – 0.20 feet, July 2009
- EB-03 – 0.43 feet, September 2008; 0.94 feet, March 2009; 1.67 feet, July 2009
- EB-05 – sheen, March 2009

Figures 6a, 6b and 6c are Apparent PSH Thickness Maps for the September 2008, March 2009, and July 2009 gauging events, respectfully.

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2. Groundwater Chemistry

Background groundwater quality in the vicinity of the facility is difficult to determine, as the water-bearing strata is within an evaporite dominated lithology that is believed to naturally exceed State of New Mexico Water Quality Control Commission (WQCC) standards. Evaporites are easily dissolved by groundwater, and this area has known secondary porosity voids believed to be a result of groundwater interaction. During the March/July 2009 monitoring events, groundwater total dissolved solids (TDS) concentrations vary from 2,310 (MW-03-03, eastern portion of facility) to 517,000 (MW-02-05, north portion of facility) milligrams per liter (mg/l, aka parts per million, ppm). The lower TDS value water within the plant is considered to be the result of mixing previously lost low-TDS water and connate water, while the high TDS value water is thought to be the result of the same lost water mining a sulfate-based evaporite salt (gypsum) within the subsurface. This "water" is extremely viscous and quickly begins crystallizing when physical parameters are upset, such as when a bailer of water is poured into an aliquot container.

Three monitoring wells placed to the north of the facility, and in the apparent groundwater upgradient direction, have TDS values between 3,190 (MW-17) and 73,200 (MW-15) mg/l. MW-16, the monitor well farthest away (approximately 1,300 feet north and upgradient from the facility) exhibited a TDS concentration of 13,900 mg/l in July 2009.

Groundwater samples were collected from gauged and purged monitor wells, with aliquots being submitted to DHL Analytical, a National Environmental Laboratory Accreditation Program (NELAP) accredited laboratory. Laboratory samples were analyzed for benzene, toluene, ethylbenzene, and total xylenes (BTEX, EPA SW method 8021B), water chemistry cations and RCRA metals (EPA SW method 6020 for As, Ba, Cd, Ca, Pb, Mg, K, Se, Ag, Na, and EPA SW method 7470A for Hg), chloride, nitrate, sulfate, (EPA method E300), alkalinity (Standard Method M2320B, 18th Edition), and TDS (Standard Method M2540C, 18th Edition). Duplicate samples for a quality control (QC) check were submitted as blind samples to DHL. Quantitative laboratory analytical data and QC results for the 2008 and 2009 monitoring events are included as a CDROM (Appendix B).

September 2008 Groundwater Sampling Event

Table 2 presents a summary of the BTEX analyses. Benzene is a common volatile organic compound (VOC) in natural gas condensate and crude oil, but toluene, ethylbenzene, and total xylenes were quantified above the established WQCC human health standard in MW-02, MW-02-06, and EB-08. Analytical data indicates the following samples exhibited benzene concentrations in excess of the 0.01 milligrams per liter (parts per million, mg/l) WQCC human health standard:

- P-01 (0.0127 mg/l)
- MW-08 (0.0254 mg/l)
- MW-02-15 (0.0294 mg/l)
- MW-13 (0.767 mg/l)
- MW-02-07 (4.59 mg/l)
- MW-02-06 (5.36 mg/l)
- EB-08 (5.77 mg/l)
- MW-02 (8.91 mg/l)
- MW-02-18 (15.0 mg/l)

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A comparison of benzene in the primary (MW-13, 0.767 mg/l) and Duplicate-01 (0.760 mg/l) samples indicate a deviation of 0.92%; Duplicate-02 has a deviation of 3.7% (4.42 mg/l and 4.59 mg/l for MW-02-07 primary). No data quality exceptions were noted in the DHL case narratives. Figure 7a is a drawing of the observed benzene concentration for the September 2008 monitoring event.

During the September 2008 monitoring event only two metals were detected at concentrations above WQCC human health standards. Arsenic was detected in MW-02 (0.127 mg/l) and chromium was detected in EB-04 (0.0565 mg/l). Table 3 presents a summary of RCRA metals and major cations in groundwater.

Major anions – chloride, nitrate, and sulfate – are a groundwater quality concern. Only nitrate is classified by the WQCC as a human health concern; chloride and sulfate are domestic water supply quality standards. Nitrate concentrations exceeding the 10 mg/l standard were only observed in samples from MW-02-02 (10.7 mg/l). This value may be affected by the high chloride and sulfate concentrations in the parent sample. Observed chloride concentrations exceeding the WQCC standard (250 mg/l) were identified in samples from:

- MW-08 (333 mg/l)
- EB-08 (374 mg/l)
- P-04 (508 mg/l)
- EB-04 (598 mg/l)
- P-03 (659 mg/l)
- MW-15 (1,430 mg/l)
- MW-02-05 (5,490 mg/l)
- MW-02-02 (11,400 mg/l)

Table 4 presents inorganics other metals and groundwater quality parameters. Chloride value distribution is graphically displayed in Figure 8a, Chloride Isocon Map.

Sulfate concentrations – and conversely TDS concentrations – exceed the domestic water quality standards (600 mg/l and 1,000 mg/l, respectfully) for all monitor wells established at the facility. Sulfate concentrations range from 899 mg/l (MW-03-03) to 366,000 mg/l (MW-02-05), while TDS value range from 2,460 mg/l (EB-05) to 517,000 mg/l (MW-02-05).

Although groundwater impacts figure prominently in the elevated sulfate and TDS values, Figure 9a, Sulfate Isocon Map, and Figure 10a, TDS Isocon Map, hint at the possibility of natural groundwater density stratification, particularly apparent in the TDS map.

March 2009 and July 2009 Groundwater Sampling Events

Chemical distribution data for March and July 2009 are combined for graphic presentation. This is not a normal procedure for LAI, but the July data collected for the newly installed MW-16 through MW-23 does not lend to a suitable presentation as a stand-alone data set. Groundwater gradient maps are presented separately for each event.

Ethylbenzene, and total xylenes were quantified above the established WQCC human health standard in EB-08 only (1.43 and 2.31 mg/l, respectfully) during this monitoring event. Analytical data indicates the

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following samples exhibited benzene concentrations in excess of the 0.01 milligrams per liter (parts per million, mg/l) WQCC human health standard in the following samples:

- MW-18 (0.0130 mg/l)
- MW-08 (0.0174 mg/l)
- MW-20 (0.0176 mg/l)
- MW-05 (0.106 mg/l)
- MW-02-03 (0.0224 mg/l)
- MW-02-15 (0.169 mg/l)
- MW-12 (0.708 mg/l)
- MW-03-03 (1.49 mg/l)
- MW-02 (1.73 mg/l)
- MW-23 (2.26 mg/l)
- EB-08 (5.04 mg/l)
- MW-02-06 (5.35 mg/l)
- MW-02-07 (5.85 mg/l)
- MW-22 (6.35 mg/l)
- MW-02-18 (16.4 mg/l)

A comparison of benzene in the primary (MW-13, 0.00133 mg/l) and Duplicate-01 (0.00148 mg/l) sample for the March 2009 event indicate a deviation of 10.1%; Duplicate-02 has a deviation of 2.1% (0.723 mg/l and 0.708 mg/l for MW-12 primary). During the July 2009 monitoring event there was no deviation between the primary (MW-16) and the duplicate because both samples did not exhibit the benzene above the method detection level. No data quality exceptions were noted in the DHL case narratives. Figure 7b is drawing of the observed benzene concentration for the March/July 2009 monitoring events.

During the March and July 2009 monitoring events no metals were detected above WQCC human health standards. The chromium observed in the down and cross gradient well, EB-04, decreased below the human health standard of 0.05 mg/l.

During the March monitoring event nitrate concentrations exceeding the 10 mg/l standard were observed in samples from MW-02-02 (12.8 mg/l) and MW-02-05 (14.7 mg/l). Again, these values may be affected by the high chloride and sulfate concentrations in the parent sample. Observed chloride concentrations exceeding the WQCC standard (250 mg/l) were identified in samples from:

- MW-23 (265 mg/l)
- MW-02-15 (280 mg/l)
- MW-08 (290 mg/l)
- EB-08 (358 mg/l)
- P-04 (575 mg/l)
- EB-04 (604 mg/l)
- P-03 (702 mg/l)
- MW-16 (1,500 mg/l)
- MW-15 (3,170 mg/l)
- MW-02-05 (5,440 mg/l)

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- MW-02-02 (9,460 mg/l)

Table 4 presents inorganics other metals and groundwater quality parameters. Chloride value distribution is graphically displayed in Figure 8b, Chloride Isocon Map.

Sulfate and TDS concentrations exceed the domestic water quality standards for all monitor wells at the facility. Sulfate concentrations range from 1,340 mg/l (MW-02-07) to 297,000 mg/l (MW-02-05), while TDS value range from 2,310 mg/l (MW-03-03) to 510,000 mg/l (MW-02-02). The elevated TDS and chloride near the cooling tower, northwest corner of the plant, may have been associated with a water leak in the cooling tower basin that has been corrected.

Figure 9b, Sulfate Isocon Map, and Figure 10b, TDS Isocon Map, graphically depict parameter distribution.

3. Soil and Aquifer Information

Surface soils are dominated by gypsite soils derived from evaporite parent rocks. The Natural Resource Conservation Service Soil Survey for Eddy County identify the surface soil underlying most of the facility as "RG", Reeves-Gypsum land complex, 0 to 3 percent slopes, while the exposed flanks of Scoggins Draw and its tributary drains are comprised of Gypsum land-Cottonwood complex, 0 to 3 percent slopes (GC). Both soil types exhibit similar characteristics and properties. However, the calcium carbonate (25%) and gypsum (80%) of the RG soil is much greater than the GC soil, which is 15% calcium carbonate and 5% gypsum. A copy of the *Custom Soil Resource Report* is included in Appendix G.

Typical drilling logs consist of a veneer of detritus-based soil from two to five feet thick, multicolored layers of gypsum with thin beds of clay, sand, or carbonate increasing in frequency with depth, and an aquiclude of red clay/shale/mudstone. Soil boring and monitor well logs from LAI investigation activities are included as Appendix H.

Groundwater occurrence is reported as being within the Permian-aged, Three Twins Member of the Guadalupe Series Chalk Bluff Formation by Hendrickson and Jones (1952). A later interpretation of the water-bearing formations by Kelley (1971) identifies two units, the Artesia Group Tansill Formation and Yates Formation. The younger Tansill Formation (Pat) is described as "Dolomite inter-tonguing northward into gypsum", and the older Yates Formation (Paye) is described as "Gypsum, dolomite and siltstone." The base of the water-bearing strata is interpreted as the red shale encountered between 3,460' and 3,480' elevation. Cross sections depicting interpretations of boring logs are included in Appendix I.

4. Surface Flooding and Protection Measures

The facility is located on a south-facing toe of a plateau, above Scoggins Draw. This location is not within a flood plain, and would not be subject to flooding even during extreme precipitation events. Overland flow from the north is intercepted by the entrance road and diverted to the east and west, away from the facility. Earthen berms protecting the northern portion of the west perimeter and the northeast portion of the facility prevent run-on or run-off. Run-off in the southern portion of the facility is retarded by stone and earthen berms which follows historic overland flow features south to Scoggins Draw.

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5. *Geology and Stratigraphy Profile*

The dominant regional feature is the Pecos Slope, a broad, low eastward dip of about 50 to 100 feet per mile. The western extents of the Pecos Slope are the Mescalero Arch, and the Sacramento and Guadalupe uplift structural divides (Kelley, 1971). The eastern extents of the Pecos Slope are the extramontane Delaware and Midland Basins. This monocline is imprinted with other structural features, including the southern flank of the Artesia-Vacuum Arch, which reflects the underlying Abo reef trend.

The Artesia-Vacuum Arch extends from beneath the Pecos Valley fill to the west, extending through Townships 17 to 19 South, eastward to Range 35 East in Lea County (Kelley, 1971). The arch is covered by post-Permian strata, except in a four to five mile stretch near Chalk Bluff Draw, the vicinity of the facility. In the vicinity of the facility, the plunging south limb of Yates and Tansill Formations dip about 4° South 47° East. Brittle deformation of the Artesia Group members causes fractures that are subject to dissolution by meteoric and phreatic groundwater interactions. Process water discharging to the subsurface and interacting with the formation material may be the source of the highest TDS concentrations observed at the facility. Conversely, dissolution from leaked process water may cause "mini-sinks", small sinkholes observed within the facility.

The lowest encountered formation in the facility's vicinity is the aforementioned Permian Artesia Group Yates Formation. The Yates is named for the Ira and An Yates oilfield in Pecos County, Texas, and has wide areal extent in both surface exposures and subsurface wells samples. The 250 to 350 feet thick Yates Formation is documented as siltstone north of Roswell, New Mexico, carbonate and evaporites west and northwest of Carlsbad, and as gypsum north of Lake McMillan to near Roswell (the vicinity of the facility). At the facility it appears that red mudstone/shale/clay reported at the base of monitor well borings is the top of the Yates formation.

Above the Yates Formation is the Permian-aged Artesia Group Tansill Formation. The type section of the Tansill Fm. is found along US Highway 285 about 2 miles north of Carlsbad and is reported to be predominantly dolomite of the reef shelf margin about 300 – 325 feet thick (Kelley, 1971), however, this facies gives way to evaporite facies about 10 miles north of the type section. In the vicinity of the site the Tansill is part of irregularly shaped north-trending belt generally less than a mile wide that is comprised of anhydrite and salt about 100 feet thick in subsurface sections. At the facility the anhydrite, gypsum and salts of the Tansill Fm. appear to be the bulk of the strata encountered during monitor well borings, and is the perched aquifer of concern.

6. *Aquifer Maps and Cross Sections*

Three cross sections have been prepared using primarily LAI subsurface investigation data, filling in with previous consultant data (Appendix I). These cross sections focus on the main processing area, which is the northwest portion of the facility. In, general the cross sections depict a subsurface dominated by gypsum, with a surface veneer of detritus-based silty-clayey soil, while the base of the water-bearing zone is recorded as mudstone, shale, or clay. Figure 3 presents the cross section locations.

Figures depicting the corrected groundwater potentiometric surface, Light non-aqueous liquids (LNAPL) thickness isopachs, and chloride, sulfide and total dissolved solids (TDS) isocons are included in the "Figures" section of this report.

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Synthesizing the data depicted in these maps and cross sections confirms the known process water and pipeline leaks at the facility are affecting groundwater movement and its relative quality. Water mounding is obvious in the north central portion of the facility. Current potentiometric maps depict groundwater south of the mounds moving towards the southeast, while groundwater to the north of the mounds appears to be moving towards the north. The mounding may be due to perched water in discontinuous clay and silty-clay units.

The north-south cross section (A to A') depicts what seems to be a natural water bearing system with a 20 foot thickness to the north, thinning to approximately eight feet thick to the south, with a mound in the process area of the facility.

Cross section B to B' is oriented west to east through the process area. This cross section depicts groundwater mounding through the middle of the plant, with an LNAPL "bubble" in the western portion of the facility. Of note in this cross section is the emulsion "bubble" in the middle of the facility. This emulsion has a potentiometric head approximately 8 feet above the top of screen, with no gauge-able groundwater in monitor well MW-02-10.

Cross section C to C' cuts a diagonal from the northwest to the southeast across the facility near the corners. Groundwater mounding is centered about MW-02, with an LNAPL "bubble" in the vicinity of MW-20, based on gauging and boring log interpretations, the southeast portion of the facility may have a connected product sheen on the groundwater extending to MW-14 where greater LNAPL thicknesses have been recorded.

7. Aquifer Testing Results

Aquifer slug testing was conducted to provide hydraulic conductivity, transmissivity, and storativity estimates for the design of a remediation plan. Slug tests were conducted on July 31, and August 3, 2009, in five wells that circumscribe the facilities. A total of 13 falling head, and 9 rising head tests were performed. The wells tested include MW-15, MW-17, EB-08, P-01, and P-05. Testing consisted of up to three iterations of falling head and rising head cycles. A synopsis of the procedures and data interpretation follows. Slug test data curves are presented as Appendix J.

Slug Test Introduction

A slug test consists of measuring groundwater head recovery in a well after a near-instantaneous change in head at that well. This is done by rapidly introducing a solid object or a volume of water (the "slug"), or removing the same, into the well causing an abrupt change in water level. The water level in the well returns to static conditions as fluid moves in or out of formation media in response to the gradient forced by the sudden change in head. The hydraulic head changes through time, the response data, can be used to estimate the hydraulic conductivity of the formation through comparisons with theoretical models of test response. This data can be used to predict the subsurface movement of a contaminant, and to design a remediation plan. The analysis of response data from slug tests involves fitting straight lines or type curves to plots of field data. To ensure the quality of response data, LAI used an In-Situ® Troll 700 pressure transducer to log the aquifer response in one-second intervals.

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AQTESOLV® Software

AQTESOLV® software provides a variety of slug test response solutions based upon the aquifer conditions encountered. At the Empire Abo Gas Plant, the water bearing zone is multiple thin beds of evaporite sequences. This stratigraphy is considered an unconfined aquifer under water table condition. Based upon the observed aquifer conditions, the Bouwer-Rice slug test solution (1976) was chosen to evaluate the response data.

Bouwer-Rice (1976) developed a method for the analysis of an overdamped slug test in a fully or partially penetrating well in an unconfined aquifer. The Bouwer-Rice method employs a quasi-steady-state model that ignores elastic storage in the aquifer. Assumptions used in the Bouwer-Rice solution include:

- Aquifer has infinite areal extent
- Aquifer is homogeneous and of uniform thickness in the vicinity of the test well
- Test well is fully or partially penetrating
- Flow to well is quasi-steady-state (storage is negligible)
- Volume of the slug is injected into or discharged from the well instantaneously

To perform the slug test analysis, a graph of the slug test data is made by plotting the head difference logarithmically on the Y-axis versus time (t) on the X-axis. The section of the graph which best approximates a straight line slope is used to determine y_0 , y_t , and t. Once the values for y_0 , y_t , t, and natural logarithm of the effective well radius are obtained, they are used to calculate the hydraulic conductivity (K).

Response Data Interpretation

The falling head conductivity extremes were 0.0593 ft/day (MW-15 Test 2) and 14.92 ft/day (P-01 Test 1); the rising head conductivity extremes were 0.1135 (P-05 Test 3) and 19.24 (P-01 Test 1). Test data from monitor well P-01 were up to two orders of magnitude greater than the highest values returned from the other four monitor wells. Biasing the data to not include the first test of P-01 produces a mean hydraulic conductivity of 0.3574 ft/day; unbiased test data had a mean hydraulic conductivity of 1.8796 ft/day.

These numeric values may be skewed with a low bias. A test curve generally has three curve parts – a near vertical initial segment that represents the forcing of water into/out-of the well bore and the sand filter pack; the main curve that reflects movement of water into/out-of the aquifer; and a near horizontal tailing line that indicates the water table returning to static conditions. Plotted test data from falling head tests lack the vertical and curved response portions in most of these tests. This may indicate secondary porosity – either karstic solution cavities or intercepted normal jointing or fractures – contribute to the migration pathway for groundwater.

Product Recovery Testing

Product recovery testing was conducted on September 17 – 18, 2008 using the method outlined in *Determination of a Realistic Estimate of the Actual Formation Product Thickness Using Monitor Wells: A Field Bailout Test* (Gruszczenski, 1987). "This empirical test is similar to a rising head slug test. Product that has accumulated in a monitor well is bailed out and the rising water/product levels are recorded

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with time using an oil/water interface probe." (Gruszczenski, 1987) A copy of the test procedure and test result graphs are provided as Appendix K.

The test procedure consists of a nine step process. Steps one, two, and three are field measurement, bailout, and recovery monitoring. The remaining steps are data reduction procedures. Testing was performed on MW-11, MW-10, MW-14, and MW-02-11.

MW-11's test was conducted as a pump-down and recovery test. Initially, 19.7 feet of light non-aqueous phase liquids (LNAPL) was observed on the groundwater in this well. LNAPL (and a small amount of water) was evacuated using a pump until a static fluid level was achieved. The pump was then turned off, and the rising fluid levels were recorded. Using the Gruszczenski correction method, the actual product thickness in this well is 0.55 feet, with a calculated capillary fringe height of 4.49 feet. MW-11's capillary fringe height (53.88 inches) correlates to a silty soil type. Uncorrected LNAPL thickness, calculated actual product thickness, calculated capillary fringe height, and correlated soil for all tests are as follow:

Monitor Well ID	Uncorrected LNAPL Thickness (inches)	Calculated LNAPL Thickness (inches)	Calculated Capillary Fringe Height (inches)	Soil Type Correlation
MW-11	236.4	6.6	53.88	Silt
MW-10	137.88	7.32	1.68	Coarse Sand
MW-14	2.76	1.56	1.32	Coarse Sand
MW-2-11	6.72	0.48	1.92	Coarse Sand

8. Electromagnetic Conductivity Survey Results

On June 4, 2008, LAI personnel performed an electromagnetic (EM-34) terrain conductivity survey of the area north of the cooling tower and plant. The EM survey was performed using an EM-34-3 terrain conductivity meter manufactured by Geonics, Ltd., Toronto, Canada. The survey was performed over an area measuring 800 x 1200 feet or approximately 22 acres for the purpose of assessing the TDS in groundwater. The EM-34-3 measures the electrical properties of soil and rock, as well as the electrical properties of groundwater, which is influenced by TDS concentration of the formation water. The EM-34-3 utilizes current flow induced into the subsurface materials by a surface transmitter that generates an alternating magnetic field to induce current flow through the earth material. The alternating magnetic field creates a secondary magnetic field that is sensed by a surface receiver. The primary magnetic field, current frequency, and coil separation can be accounted for, leaving ground conductivity as the only unknown variable to be measured. The EM-34-3 has exploration capabilities ranging from approximately 0 to 196.9 feet below ground surface (bgs) depending on the separation of the transmitter and receiver coils (i.e., 10, 20 or 40 meters) and coil orientation (i.e., horizontal dipole [HD]) mode or vertical dipole [VD] mode). The EM-34-3 was operated in the HD and VD modes using 10 and 20 meter coil separations. The EM-34-3 20-meter VD survey was selected to assess the TDS since groundwater occurs between about 60 to 90 feet Figure 12 presents the EM-34-3 20 meter VD survey (0 to 98.4 feet) drawing. Appendix L presents the EM-34 survey field sheets.

Referring to Figure 11, an anomaly of elevated EM-34-3, 20-meter VD readings between 107.2 and 153.3 millimhos per meter (mmhos/m) was observed in the area north of the cooling tower and decreased to

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below 20 mmhos/m approximately 400 feet north of the plant. This anomaly suggests groundwater containing elevated TDS is moving north and decreasing in concentration. An anomaly of elevated EM-34-3 20-meter VD readings was also observed about 1,000 feet northwest of the plant.

Two (2) monitoring wells (MW-15 and MW-16) were installed northwest of the cooling plant and recorded TDS concentrations of 73,200 mg/L (MW-15) and 13,900 mg/L (MW-16) demonstrating that the TDS decreases in concentration northwest of the plant and correlates with the EM-34-3 20-meter VD readings.

References

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- Kelley, Vincent C., 1971. *Geology of the Pecos country, southeastern New Mexico.* Memoir 24. New Mexico Bureau of Mines & Mineral Resources. Socorro, NM.

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13.0 Other Compliance Information

NM OCD conducted a facility inspection on April 22, 2009.

Table 1
Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-02	12/29/1991	37.5	4	3,545.3	19 - 34	2.89	3,548.19	2/13/2007	--	32.75	3,515.44
								3/26/2007	--	32.85	3,515.34
								6/18/2007	--	33.90	3,514.29
								9/17/2007	--	33.83	3,514.36
								12/10/2007	--	34.02	3,514.17
								3/11/2008	--	34.03	3,514.16
								9/15/2008	--	33.96	3,514.23
								3/9/2009	--	34.00	3,514.19
								7/13/2009	--	33.91	3,514.28
MW-02-02	10/6/1992	45	4	3,549.3	35 - 45	2.96	3,552.26	10/6/1992	--	39.00	3,513.26
								3/26/2007	--	26.50	3,525.76
								6/18/2007	--	26.86	3,525.40
								9/17/2007	--	27.00	3,525.26
								12/10/2007	--	27.03	3,525.23
								3/11/2008	--	27.13	3,525.13
								9/15/2008	--	27.25	3,525.01
								3/9/2009	--	26.96	3,525.30
								7/13/2009	--	27.06	3,525.20
MW-02-03	9/28/1992	105	4	3,553.0	95 - 105	3.03	3,556.03	9/28/1992	--	97.00	3,459.03
								2/12/2007	63.15	63.20	3,492.87
								3/27/2007	--	62.96	3,493.07
								6/18/2007	--	62.26	3,493.77
								9/17/2007	--	62.08	3,493.95
								12/10/2007	--	62.56	3,493.47
								3/11/2008	--	62.01	3,494.02
								9/15/2008	--	79.15	3,476.88
								3/9/2009	--	64.20	3,491.83
								7/13/2009	--	63.95	3,492.08
MW-02-04	9/30/1992	55	4	3,550.9	45 - 55	2.89	3,553.79	9/30/1992	--	50.00	3,503.79
								3/26/2007	--	53.35	3,500.44
								6/18/2007	--	50.67	3,503.12
								9/17/2007	--	51.69	3,502.10
								12/10/2007	--	52.32	3,501.47
								3/11/2008	--	52.74	3,501.05
								9/15/2008	--	51.52	3,502.27
								3/9/2009	--	53.06	3,500.73
								7/13/2009	sheen	53.20	3,500.59

Table 1
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Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-02-05	10/6/1992	50	4	3,549.9	40 - 50	2.79	3,552.69	10/6/1992	--	43.00	3,509.69
								3/26/2007	--	27.21	3,525.48
								6/18/2007	--	27.40	3,525.29
								9/17/2007	--	27.56	3,525.13
								12/10/2007	--	27.58	3,525.11
								3/11/2008	--	27.76	3,524.93
								9/15/2008	--	27.50	3,525.19
								3/9/2009	--	27.53	3,525.16
								7/13/2009	--	27.62	3,525.07
MW-02-06	9/29/1992	21	4	3,548.3	11 - 21	2.52	3,550.82	9/29/1992	--	18.00	3,532.82
								3/26/2007	--	18.18	3,532.64
								6/18/2007	--	16.48	3,534.34
								9/17/2007	--	15.60	3,535.22
								12/10/2007	--	16.83	3,533.99
								3/11/2008	--	17.96	3,532.86
								9/15/2008	--	14.98	3,535.84
								3/9/2009	--	17.34	3,533.48
								7/13/2009	--	19.19	3,531.63
MW-02-07	10/5/1992	63	4	3,544.2	53 - 63	2.80	3,547.00	10/5/1992	--	57.00	3,490.00
								3/26/2007	--	46.75	3,500.25
								6/18/2007	--	45.89	3,501.11
								9/17/2007	--	44.31	3,502.69
								12/10/2007	--	46.51	3,500.49
								3/11/2008	--	46.73	3,500.27
								9/15/2008	--	45.78	3,501.22
								3/9/2009	--	48.64	3,498.36
								7/13/2009	--	46.95	3,500.05
MW-02-09	10/7/1992	40	4	3,543.5	30 - 40	3.02	3,546.52	10/7/1992	--	31.00	3,515.52
								3/27/2007	34.84	38.41	3,510.97
								6/18/2007	35.45	35.62	3,511.04
								9/17/2007	35.66	38.72	3,510.25
								12/10/2007	35.78	39.18	3,510.06
								3/11/2008	38.19	39.01	3,508.17
								9/15/2008	25.89	34.72	3,518.86
								3/9/2009	35.18	39.07	3,510.56
								7/14/2009	--	33.11	3,513.41

Table 1
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Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-02-10	9/29/1992	75	4	3,545.4	65 - 75	3.00	3,548.40	9/29/1992	--	64.00	3,484.40
								3/27/2007	52.38	*	--
								6/18/2007	52.74	58.38	3,494.53
								9/17/2007	52.48	58.76	3,494.66
								12/10/2007	53.18	58.22	3,494.21
								3/11/2008	53.22	55.14	3,494.80
								9/15/2008	54.12	62.90	3,492.52
								3/9/2009	54.60	*	--
								7/14/2009	54.12	*	--
MW-02-11	9/29/1992	20	4	3,544.0	10 - 20	2.79	3,546.79	9/29/1992	--	--	--
								3/26/2007	--	22.62	3,524.17
								6/18/2007	18.05	19.30	3,528.49
								9/17/2007	20.82	22.02	3,525.73
								12/10/2007	21.67	22.18	3,525.02
								3/11/2008	23.79	26.79	3,522.40
								9/15/2008	21.72	22.27	3,524.96
								3/9/2009	22.52	*	--
								7/14/2009	--	22.91	3,523.88
MW-02-12	10/1/1992	80	4	3,540.3	70 - 80	3.02	3,543.32	10/1/1992	--	74.00	3,469.32
								2/12/2007	emulsion	55.15	3,488.17
								3/27/2007	55.10	55.50	3,487.82
								6/18/2007	emulsion	54.20	3,489.12
								9/17/2007	emulsion	54.29	3,489.03
								12/10/2007	emulsion	--	--
								3/11/2008	emulsion	54.32	3,489.00
								9/15/2008	emulsion	55.89	3,487.43
								3/9/2009	emulsion	56.04	3,487.28
								7/14/2009	emulsion	56.23	3,487.09
MW-02-13	10/7/1992	46	4	3,542.7	36 - 46	2.89	3,545.59	10/7/1992	--	40.00	3,505.59
								2/12/2007	41.20	42.65	3,504.10
								3/27/2007	41.25	42.23	3,504.14
								6/18/2007	36.66	39.81	3,508.30
								9/17/2007	38.31	41.44	3,506.65
								12/10/2007	39.90	43.00	3,505.07
								3/11/2008	41.03	43.24	3,504.12
								9/15/2008	sheen	36.65	3,508.94
								3/9/2009	40.81	43.98	3,504.15
								7/14/2009	--	39.61	3,505.98

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Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-02-14	10/5/1992	73	4	3,541.3	63 - 73	3.23	3,544.53	10/5/1992	--	67.00	3,477.53
								3/27/2007	46.4	46.78	3,498.05
								6/18/2007	46.44	46.89	3,498.00
								9/17/2007	46.09	46.58	3,498.34
								12/10/2007	46.94	47.60	3,497.46
								3/11/2008	47.53	48.01	3,496.90
								9/15/2008	47.31	47.87	3,497.11
								3/9/2009	49.40	49.68	3,495.07
								7/14/2009	--	48.75	3,495.78
MW-02-15	10/2/1992	70	4	3,540.2	60 - 70	3.09	3,543.29	10/2/1992	--	64.00	3,479.29
								3/27/2007	--	50.76	3,492.53
								6/18/2007	--	50.73	3,492.56
								9/17/2007	--	50.78	3,492.51
								12/10/2007	--	51.41	3,491.88
								3/11/2008	--	51.34	3,491.95
								9/15/2008	--	52.09	3,491.20
								3/9/2009	--	53.08	3,490.21
								7/13/2009	--	52.62	3,490.67
MW-02-16	9/30/1992	80	4	3,541.0	70 - 80	3.24	3,544.24	9/30/1992	--	74.00	3,470.24
								2/12/2007	--	55.92	3,488.32
								3/27/2007	--	55.59	3,488.65
								6/18/2007	--	55.09	3,489.15
								9/17/2007	--	55.18	3,489.06
								12/10/2007	--	55.63	3,488.61
								3/11/2008	--	55.53	3,488.71
								9/15/2008	--	56.40	3,487.84
								3/9/2009	--	56.32	3,487.92
								7/13/2009	--	56.50	3,487.74
MW-02-18	10/7/1992	36	4	3,542.7	26 - 36	3.00	3,545.70	10/7/1992	--	30.00	3,515.70
								2/12/2007	--	21.84	3,523.86
								3/26/2007	--	21.36	3,524.34
								6/18/2007	--	17.48	3,528.22
								9/17/2007	--	20.23	3,525.47
								12/10/2007	--	20.69	3,525.01
								3/11/2008	--	21.73	3,523.97
								9/15/2008	--	20.34	3,525.36
								3/9/2009	--	21.65	3,524.05
								7/13/2009	--	22.04	3,523.66

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Frontier Field Services - Empire Abo Gas Plant (GW-022)
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Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-03	12/20/1991	91.5	4	3,552.4	69 - 89	2.90	3,555.30	3/27/2007	--	59.51	3,495.79
								6/18/2007	58.74	59.23	3,496.46
								9/17/2007	58.39	59.46	3,496.70
								12/10/2007	59.10	60.28	3,495.96
								3/11/2008	58.47	61.11	3,496.30
								9/15/2008	60.98	64.03	3,493.71
								3/9/2009	60.93	63.60	3,493.84
								7/13/2009	--	63.36	3,491.94
MW-03-01	5/3/1994	70	4	3,539.9	50 - 70	2.66	3,542.56	3/27/2007	--	43.78	3,498.78
								6/18/2007	--	43.65	3,498.91
								9/17/2007	--	43.22	3,499.34
								12/10/2007	--	44.09	3,498.47
								3/11/2008	--	43.98	3,498.58
								9/15/2008	40.88	56.37	3,498.58
								3/9/2009	44.73	55.42	3,495.69
								7/13/2009	44.00	55.16	3,496.33
MW-03-02	5/4/1994	100	4	3,538.6	60 - 100	2.48	3,541.08	3/27/2007	--	56.33	3,484.75
								6/18/2007	--	56.13	3,484.95
								9/17/2007	emulsion	56.19	3,484.89
								12/10/2007	--	56.38	3,484.70
								3/11/2008	emulsion	53.91	3,487.17
								9/15/2008	emulsion	56.40	3,484.68
								3/9/2009	emulsion	59.60	3,481.48
								7/14/2009	emulsion	56.60	3,484.48
MW-03-03	5/4/1994	80	4	3,542.3	55 - 80	2.42	3,544.72	3/26/2007	59.59	59.60	3,544.72
								6/18/2007	--	58.96	3,485.76
								9/17/2007	--	59.28	3,485.44
								12/10/2007	emulsion	59.52	3,485.20
								3/11/2008	emulsion	59.43	3,485.29
								9/15/2008	60.61	60.62	3,484.11
								3/9/2009	sheen	60.69	3,484.03
								7/14/2009	--	60.92	3,483.80

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Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-03-04	5/4/1994	110.0	4	3,555.7	65 - 110	2.75	3,558.45	3/26/2007	60.85	60.98	3,497.57
								6/18/2007	60.68	61.51	3,497.60
								9/17/2007	60.28	61.44	3,497.94
								12/10/2007	60.43	61.34	3,497.84
								3/11/2008	61.01	61.98	3,497.25
								9/15/2008	62.16	62.95	3,496.13
								3/9/2009	62.02	62.84	3,496.27
								7/14/2009	61.67	62.50	3,496.61
MW-04	12/21/1991	62.5	4	3,547.8	45 - 60	3.19	3,550.99	3/26/2007	--	48.15	3,502.84
								6/18/2007	47.18	48.23	3,503.60
								9/17/2007	emulsion	44.41	3,506.58
								12/10/2007	45.49	47.45	3,505.11
								3/11/2008	47.81	50.18	3,502.71
								9/15/2008	45.57	50.66	3,504.40
								3/9/2009	46.90	51.55	3,503.16
								7/14/2009	42.20	48.00	3,507.63
MW-05	12/22/1991	99.0	4	3,540.6	71 - 96	3.17	3,543.77	3/27/2007	--	54.69	3,489.08
								6/18/2007	--	54.18	3,489.59
								9/17/2007	--	54.22	3,489.55
								12/10/2007	--	54.71	3,489.06
								3/11/2008	--	54.58	3,489.19
								9/15/2008	--	55.92	3,487.85
								3/9/2009	--	55.84	3,487.93
								7/13/2009	--	55.97	3,487.80
MW-06	12/22/1991	53.0	4	3,541.8	30 - 50	2.70	3,544.50	3/27/2007	43.40	44.75	3,500.83
								6/18/2007	35.93	36.10	3,508.54
								9/17/2007	37.89	37.96	3,506.60
								12/10/2007	39.84	40.03	3,504.62
								3/11/2008	40.18	41.09	3,504.14
								9/15/2008	31.74	45.13	3,510.08
								3/9/2009	38.32	45.66	3,504.71
								7/14/2009	--	37.57	3,506.93

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Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-07	12/22/1991	28.5	4	3,546.0	11 - 26	0.49	3,546.49	3/26/2007	--	8.20	3,538.29
								6/18/2007	--	8.13	3,538.36
								9/17/2007	--	8.06	3,538.43
								12/10/2007	--	8.58	3,537.91
								3/11/2008	--	9.38	3,537.11
								9/15/2008	7.50	7.61	3,538.97
								3/9/2009	9.20	9.50	3,537.23
								7/13/2009	sheen	3.73	3,542.76
MW-08	12/29/1991	92.0	4	3,540.5	69 - 89	3.23	3,543.73	2/13/2007	--	54.19	3,489.54
								3/27/2007	--	54.62	3,489.11
								6/18/2007	--	53.20	3,490.53
								9/17/2007	--	53.29	3,490.44
								12/10/2007	--	53.92	3,489.81
								3/11/2008	--	53.82	3,489.91
								9/15/2008	--	54.42	3,489.31
								3/9/2009	--	55.13	3,488.60
								7/13/2009	--	55.11	3,488.62
MW-09	12/29/1991	74.5	4	3,540.4	52 - 72	2.42	3,542.82	2/13/2007		44.05	3,498.58
								3/27/2007		43.88	3,498.87
								6/18/2007		43.90	3,498.86
								9/17/2007		43.34	3,499.38
								12/10/2007	emulsion	44.25	3,498.57
								3/11/2008		44.28	3,498.21
								9/15/2008		43.79	3,498.98
								3/9/2009		46.51	3,496.30
								7/14/2009		45.60	3,497.20
MW-10	7/28/2008	50.4	4	3,541.8	15 - 50	2.64	3,544.44	7/31/2008	27.62	53.04	3,511.74
								9/15/2008	25.11	25.77	3,519.20
								3/9/2009	40.96	57.82	3,500.11
								7/14/2009	41.00	46.61	3,502.32
MW-11	7/29/2008	57	4	3,540.2	21 - 56	2.53	3,542.73	7/31/2008	38.70	57.58	3,500.25
								9/15/2008	38.39	57.66	3,500.49
								3/9/2009	42.93	57.79	3,496.83
								7/14/2009	42.10	57.50	3,497.55

Table 1
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Frontier Field Services - Empire Abo Gas Plant (GW-022)
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Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
MW-12	7/29/2008	74.1	4	3,522.6	36 - 71	2.65	3,525.25	7/31/2008	47.49	47.55	3,477.75
								9/15/2008	47.81	47.82	3,477.44
								3/9/2009	sheen	47.57	3,477.68
								7/14/2009	--	47.98	3,477.27
MW-13	7/29/2008	88.6	4	3,558.5	50 - 85	2.90	3,561.40	7/31/2008	--	62.80	3,498.60
								9/15/2008	--	63.64	3,497.76
								3/9/2009	--	62.49	3,498.91
								7/13/2009	--	62.18	3,499.22
MW-14	7/30/2008	72.5	4	3,517.7	33 - 68	2.62	3,520.32	7/31/2008	--	44.10	3,476.22
								9/15/2008	44.89	45.18	3,475.37
								3/9/2009	44.55	46.20	3,475.44
								7/13/2009	45.31	46.50	3,474.77
MW-15	7/30/2008	80.2	4	3,559.7	42 - 77	2.75	3,562.45	7/31/2008	--	61.05	3,501.40
								9/15/2008	--	61.62	3,500.83
								3/9/2009	sheen	61.19	3,501.26
								7/13/2009	--	61.35	3,501.10
MW-16	6/24/2009	115	4	3,582.6	80 - 115	2.86	3,585.46	7/13/2009	--	94.00	3,491.46
MW-17	6/23/2009	95	4	3,568.0	60 - 95	2.84	3,570.84	7/13/2009	--	78.61	3,492.23
MW-18	6/24/2009	54	4	3,529.7	33 - 53	2.93	3,532.63	7/13/2009	--	37.33	3,495.30
MW-19	6/17/2009	77	4	3,540.6	41 - 76	2.74	3,543.34	7/14/2009	57.01	62.36	3,485.26
MW-20	6/18/2009	77	4	3,538.7	41 - 76	2.77	3,541.47	7/14/2009	55.71	73.00	3,482.30
MW-21	6/18/2009	78	4	3,540.2	43 - 78	2.95	3,543.15	7/14/2009	56.20	56.40	3,486.91
MW-22	6/19/2009	38	4	3,542.9	13 - 38	2.97	3,545.87	7/13/2009	--	22.31	3,523.56
MW-23	6/19/2009	84	4	3,539.2	49 - 84	3.01	3,542.21	7/13/2009	--	62.42	3,479.79

Table 1
Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
EB-01	3/29/2004	40.3	1	3,491.5	33 - 38	0.65	3,492.15	3/26/2007	--	23.71	3,468.44
								6/18/2007	--	23.06	3,469.09
								9/17/2007	--	22.81	3,469.34
								12/10/2007	--	22.83	3,469.32
								3/10/2008	--	23.09	3,469.06
								9/15/2008	--	23.18	3,468.97
								3/9/2009	--	22.67	3,469.48
								7/13/2009	--	23.43	3,468.72
EB-02	3/29/2004	55	2	3,522.6	35 - 55	2.74	3,525.34	3/26/2007	--	43.83	3,481.51
								6/18/2007	--	43.02	3,482.32
								9/17/2007	--	42.68	3,482.66
								12/10/2007	--	42.29	3,483.05
								3/10/2008	--	40.84	3,484.50
								9/15/2008	--	42.33	3,483.01
								3/9/2009	--	40.88	3,484.46
								7/13/2009	--	40.50	3,484.84
EB-03	3/30/2004	67	2	3,517.8	46 - 66	3.25	3,521.05	3/26/2007	46.04	46.35	3,474.95
								6/18/2007	45.41	45.55	3,475.61
								9/17/2007	45.81	46.16	3,475.17
								12/10/2007	45.89	46.28	3,475.08
								3/11/2008	43.27	45.79	3,477.28
								9/15/2008	45.95	46.38	3,475.01
								3/9/2009	45.69	46.63	3,475.17
								7/14/2009	46.03	47.70	3,474.69
EB-04	3/31/2004	62.7	2	3,505.3	31 - 51	3.08	3,508.38	3/26/2007	--	40.91	3,467.47
								6/18/2007	--	40.19	3,468.19
								9/17/2007	--	40.51	3,467.87
								12/10/2007	--	40.74	3,467.64
								3/10/2008	--	42.18	3,466.20
								9/15/2008	--	41.14	3,467.24
								3/9/2009	--	40.88	3,467.50
								7/13/2009	--	41.58	3,466.80

Table 1
Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
EB-05	3/31/2004	56	2	3,523.7	44 - 54	2.91	3,526.61	3/26/2007	--	35.08	3,491.53
								6/18/2007	--	35.61	3,491.00
								9/17/2007	--	35.79	3,490.82
								12/10/2007	--	35.70	3,490.91
								3/10/2008	--	40.84	3,485.77
								9/15/2008	--	33.78	3,492.83
								3/9/2009	sheen	35.60	3,491.01
								7/13/2009	--	35.24	3,491.37
EB-06	3/31/2004	83	1	3,555.6	72 - 82	1.03	3,556.63	3/26/2007	--	54.39	3,502.24
								6/18/2007	--	54.37	3,502.26
								9/17/2007	--	54.66	3,501.97
								12/10/2007	--	55.83	3,500.80
								3/10/2008	--	54.73	3,501.90
								9/15/2008	--	55.38	3,501.25
								3/9/2009	--	55.92	3,500.71
								7/13/2009	--	57.51	3,499.12
EB-07	4/1/2004	53	2	3,501.3	43 - 53	2.67	3,503.97	3/26/2007	--	35.74	3,468.23
								6/18/2007	--	33.82	3,470.15
								9/17/2007	--	34.64	3,469.33
								12/10/2007	--	34.85	3,469.12
								3/10/2008	--	35.17	3,468.80
								9/15/2008	--	35.48	3,468.49
								3/9/2009	--	35.62	3,468.35
								7/13/2009	--	36.44	3,467.53
EB-08	4/2/2004	81	2	3,533.8	66 - 81	3.27	3,537.07	3/26/2007	--	57.19	3,479.88
								6/18/2007	--	56.47	3,480.60
								9/17/2007	--	56.85	3,480.22
								12/10/2007	--	57.03	3,480.04
								3/10/2008	--	56.99	3,480.08
								9/15/2008	--	57.86	3,479.21
								3/9/2009	--	57.68	3,479.39
								7/13/2009	--	58.26	3,478.81

Table 1
Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
P-01	12/29/2005	50	2	3,527.9	40 - 50	2.31	3,530.21	3/26/2007	--	29.73	3,500.48
								6/18/2007	--	28.93	3,501.28
								9/17/2007	--	29.23	3,500.98
								12/10/2007	--	29.14	3,501.07
								3/10/2008	--	34.78	3,495.43
								9/15/2008	--	30.76	3,499.45
								3/9/2009	--	36.96	3,493.25
								7/13/2009	--	35.32	3,494.89
P-02	12/27/2005	22.5	2	3,542.3	19.5 - 22.5	2.43	3,544.73	3/26/2007	--	22.22	3,522.51
								6/18/2007	--	19.90	3,524.83
								9/17/2007	--	20.98	3,523.75
								12/10/2007	--	21.29	3,523.44
								3/10/2008	--	24.01	3,520.72
								9/15/2008	--	21.87	3,522.86
								3/9/2009	--	22.18	3,522.55
								7/13/2009	--	22.33	3,522.40
P-03	12/27/2005	78	2	3,534.4	58 - 78	2.43	3,536.83	3/26/2007	--	65.45	3,471.38
								6/18/2007	--	63.15	3,473.68
								9/17/2007	--	63.34	3,473.49
								12/10/2007	--	63.78	3,473.05
								3/10/2008	--	64.12	3,472.71
								9/15/2008	--	65.37	3,471.46
								3/9/2009	--	65.17	3,471.66
								7/13/2009	--	65.69	3,471.14
P-04	12/28/2005	61	2	3,513.5	51 - 61	2.27	3,515.77	3/26/2007	--	48.53	3,467.24
								6/18/2007	--	46.02	3,469.75
								9/17/2007	--	47.00	3,468.77
								12/10/2007	--	47.32	3,468.45
								3/10/2008	--	47.78	3,467.99
								9/15/2008	--	48.34	3,467.43
								3/9/2009	--	48.43	3,467.34
								7/13/2009	--	49.23	3,466.54

Table 1
Monitor Well Completion and Gauging Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Well Information								Groundwater Data			
Well ID	Date Drilled	Drilled Depth (bgs)	Well Dia. (inches)	Surface Elevation	Screen Interval (bgs)	Casing Stickup	TOC Elevation	Date Gauged	Depth to Fluid	Depth to Water	Corrected Water Elevation
P-05	12/28/2005	48	2	3,504.9	35 - 45	2.58	3,507.48	3/26/2007	--	37.60	3,469.88
								6/18/2007	--	36.43	3,471.05
								9/17/2007	--	37.19	3,470.29
								12/20/2007	--	37.29	3,470.19
								3/10/2008	--	37.29	3,470.19
								9/15/2008	--	37.25	3,470.23
								3/9/2009	--	37.68	3,469.80
								7/13/2009	--	38.51	3,468.97

Notes

All values are in feet, unless otherwise noted.

Survey datum based upon NAD 1927/NAVD 1929

bgs - below ground surface

TOC - top of casing

Wells drilled and installed by Alan Eades and Atkins Engineering. Schedule 40 threaded PVC casing and screen set.

* - Groundwater not encountered, NAPL observed for entire screened interval.

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
MW-02	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.0221	0.0397	0.00746	0.06627
	3/11/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	8.91	2.06	3.55	2.79
	3/10/2009	1.79	0.107	<0.1	<0.150
MW-02-02	3/27/2007	<0.002	<0.003	<0.007	<0.0009
	6/19/2007	0.00066	<0.0006	<0.0014	<0.0018
	9/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/11/2007	<0.002	<0.003	<0.007	<0.009
	3/11/2008	<0.0008	<0.002	<0.002	<0.003
	9/17/2008	<0.0008	<0.002	<0.002	<0.003
	3/11/2009	0.000979	<0.002	<0.002	<0.003
MW-02-03	3/29/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/20/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/18/2007	0.00055	<0.0003	<0.0007	0.00114
	12/11/2007	0.00283	0.00137	<0.0007	0.0028
	3/11/2008	<0.0008	<0.002	<0.002	<0.003
	9/17/2008	<0.0008	<0.002	<0.002	<0.003
	3/11/2009	0.0224	0.0035	<0.002	0.00595
MW-02-04	3/28/2007	<0.002	0.00041	<0.007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00021	<0.0003	<0.0007	0.00084
	3/11/2008	0.00685	0.00987	<0.002	0.0157
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
MW-02-05	3/27/2007	<0.002	<0.003	<0.007	<0.0009
	6/19/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/11/2007	<0.002	<0.003	<0.007	<0.0009
	3/11/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/11/2009	0.00115	<0.002	<0.002	<0.003

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
MW-02-06	3/28/2007	4.58	0.148	<0.035	0.222
	6/20/2007	4.89	0.421	0.243	0.8112
	9/18/2007	5.42	0.296	0.0467	0.3636
	12/11/2007	8.26	0.618	0.298	0.3636
	3/11/2008	6.59	1.04	0.443	1.95
	9/16/2008	5.36	1.18	<0.02	1.37
	3/10/2009	5.35	0.591	0.122	0.662
MW-02-07	3/28/2007	1.24	0.133	<0.007	0.276
	6/19/2007	1.25	0.12	<0.007	0.24
	9/18/2007	1.5	0.138	0.0013	0.311
	12/10/2007	1.75	0.124	<0.007	0.35
	3/11/2008	1.43	0.0901	<0.02	0.322
	9/17/2008	4.59	0.115	<0.04	0.325
	3/10/2009	5.85	0.108	<0.1	0.387
MW-02-15	3/29/2007	0.0193	<0.0003	<0.0007	0.00357
	6/20/2007	0.0268	<0.0003	<0.0007	<0.0009
	9/18/2007	0.041	0.00059	<0.0007	0.00419
	12/11/2007	0.0421	0.00104	<0.0007	0.00359
	3/11/2008	0.0208	<0.002	<0.002	0.00366
	9/17/2008	0.0294	0.00731	<0.002	0.0112
	3/10/2009	0.169	0.00639	<0.002	0.0135
MW-02-16	3/29/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/19/2007	0.00032	<0.0003	<0.0007	<0.0009
	9/18/2007	<0.001	<0.0015	<0.0035	<0.0045
	12/11/2007	<0.0002	<0.0003	<0.0007	<0.0009
	3/11/2008	0.0131	0.00247	<0.002	<0.003
	9/17/2008	<0.0008	<0.002	<0.002	<0.003
	3/11/2009	0.0055	<0.002	<0.002	<0.003
MW-02-18	3/28/2007	8.08	0.400	<0.035	0.188
	6/19/2007	6.63	0.405	<0.07	0.192
	9/18/2007	6.06	0.328	<0.0035	0.147
	12/11/2007	17.2	0.481	<0.007	0.251
	3/11/2008	11	0.25	<0.2	<0.3
	9/16/2008	15	0.362	<0.2	0.170
	3/10/2009	16.4	0.412	<0.4	<0.6

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
MW-03-01	3/28/2007	0.32	0.0788	<0.0035	0.22
	6/19/2007	0.0897	0.0149	<0.007	0.0598
	9/18/2007	0.28	0.0513	<0.0007	0.192
	12/11/2007	0.131	0.0149	<0.0007	0.111
	3/11/2008	0.156	0.141	<0.01	0.103
MW-03-02	3/29/2007	<0.0002	<0.0003	<0.0007	0.00077
	6/19/2007	<0.0002	0.00086	<0.0007	<0.0009
	12/11/2007	0.00233	0.00151	<0.0007	0.00331
MW-03-03	3/28/2007	1.02	0.346	<0.007	0.396
	6/17/2007	0.913	0.119	<0.007	0.187
	9/18/2007	0.983	0.110	<0.007	0.179
	3/11/2009	1.49	0.0569	<0.02	0.193
MW-05	3/29/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/19/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/18/2007	0.0008	<0.0003	<0.0007	0.0012
	12/11/2007	<0.0002	<0.0003	<0.0007	<0.0009
	3/11/2008	0.00668	<0.002	<0.002	<0.003
	9/17/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	0.106	0.0107	<0.002	0.0188
MW-07	3/28/2007	0.839	0.0211	<0.007	0.0178
	6/19/2007	0.791	0.0304	<0.007	0.0175
	9/18/2007	1.26	0.0369	<0.007	0.0291
	12/10/2007	1.36	0.0479	<0.007	0.043
	3/11/2008	0.657	<0.02	<0.02	<0.03
MW-08	3/28/2007	<0.0002	<0.0003	<0.0007	0.00075
	6/19/2007	0.00056	0.0005	<0.0007	<0.0009
	9/18/2007	0.00044	<0.0003	<0.0007	0.00113
	12/11/2007	0.00336	0.00196	<0.0007	0.00553
	3/11/2008	0.0311	0.00436	<0.002	<0.003
	9/17/2008	0.0254	0.00684	<0.002	0.00916
	3/11/2009	0.0174	0.00281	<0.002	0.0047
MW-12	3/11/2009	0.708	<0.02	<0.02	<0.03

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
MW-13	9/16/2008	0.767	<0.002	0.002	<0.003
	3/10/2009	0.00133	<0.002	0.002	<0.003
MW-15	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
MW-16	7/15/2009	<0.0008	<0.002	<0.002	<0.003
MW-17	7/15/2009	<0.0008	<0.002	<0.002	<0.003
MW-18	7/15/2009	0.013	0.0101	<0.002	0.00703
MW-20	7/15/2009	0.0176	0.0133	<0.002	0.0161
MW-22	7/15/2009	6.35	0.653	0.00458	0.466
MW-23	7/15/2009	2.26	0.164	<0.002	0.102
EB-01	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	<0.0002	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-02	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	<0.0002	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-03	3/27/2007	0.0115	0.00493	<0.0007	0.00473

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
EB-04	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00091	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-05	3/26/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00061	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-06	3/26/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	<0.0002	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-07	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00026	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
EB-08	3/27/2007	4.59	1.3	0.524	2.029
	6/18/2007	4.95	1.48	0.676	2.543
	9/17/2007	3.84	0.973	0.429	1.564
	12/10/2007	2.58	0.656	0.243	1.036
	3/10/2008	3.79	0.964	0.331	1.54
	9/16/2008	5.77	1.43	0.668	2.31
	3/10/2009	5.04	1.37	0.619	2.21

Table 2
Groundwater VOC Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethylbenzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
P-01	3/26/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00076	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	0.0127	<0.002	<0.002	<0.003
	3/10/2009	0.00148	<0.002	<0.002	<0.003
P-02	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/19/2007	<0.0002	0.45	<0.0007	0.206
	9/17/2007	0.00206	0.00309	<0.0007	0.0075
	12/10/2007	0.104	0.0932	0.0230	0.1506
	3/10/2008	0.016	0.0259	<0.01	0.0434
	9/16/2008	0.104	0.0901	0.0208	0.138
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
P-03	3/27/2007	0.00507	<0.0003	<0.0007	<0.0009
	6/18/2007	0.0057	<0.0003	<0.0007	<0.0009
	9/17/2007	0.0154	<0.0003	<0.0007	0.00154
	12/10/2007	0.00245	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	0.00115	<0.002	<0.002	<0.003
P-04	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	0.00041	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00026	<0.0003	<0.0007	<0.0009
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
P-05	3/27/2007	<0.0002	<0.0003	<0.0007	<0.0009
	6/18/2007	<0.0002	<0.0003	<0.0007	<0.0009
	9/17/2007	<0.0002	<0.0003	<0.0007	<0.0009
	12/10/2007	0.00033	<0.0003	<0.0007	0.00083
	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	<0.0008	<0.002	<0.002	<0.003
	3/10/2009	0.00322	<0.002	<0.002	<0.003

Notes

Volatiles analyzed via EPA SW846 Method 8021B by DHL Analytical, Inc.
All values reported in Milligrams per liter (mg/L, parts per million).
Blue indicates the compound exceeded NMWQCC standards.
< values - Indicate the value is less than Method Detection Limit MDL.

Table 2a
Groundwater VOC Quality Control Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Volatile Organic Compounds	Collection Date	Benzene	Ethyl benzene	Toluene	Total Xylenes
NMWQCC Standard (mg/L)		0.01	0.75	0.75	0.62
Duplicate-01 (P-02)	3/10/2008	0.0335	0.0401	0.00827	0.0697
Duplicate-01 (MW-13)	9/16/2008	0.760	<0.002	<0.002	<0.003
Duplicate-01 (MW-13)	3/10/2009	0.00148	<0.002	<0.002	<0.003
Duplicate-01 (MW-16)	7/15/2009	<0.0008	<0.002	<0.002	<0.003
Duplicate-02 (MW-02-16)	3/11/2008	0.0109	0.00228	<0.002	<0.003
Duplicate-02 (MW-02-07)	9/17/2008	4.42	0.116	0.0293	0.319
Duplicate-02 (MW-12)	3/11/2009	0.723	<0.02	<0.02	<0.03
Equipment Rinse	3/11/2008	<0.0008	<0.002	0.0104	<0.003
Equipment Rinse	3/10/2009	<0.0008	<0.002	0.00212	<0.003
Equipment Rinse	3/11/2009	<0.0008	<0.002	0.00204	<0.003
Field Blank	3/10/2008	<0.0008	<0.002	0.00961	<0.003
	9/17/2008	<0.0008	<0.002	0.00528	<0.003
	3/10/2009	<0.0008	<0.002	0.00204	<0.003
Trip Blank-01	3/10/2008	<0.0008	<0.002	<0.002	<0.003
	9/16/2008	0.00122	<0.002	<0.002	<0.003
	3/10/2009	<0.0008	<0.002	<0.002	<0.003
Trip Blank-02	3/11/2008	<0.0008	<0.002	<0.002	<0.003
	9/17/2008	<0.0008	<0.002	<0.002	<0.003
	3/11/2009	<0.0008	<0.002	<0.002	<0.003

Notes

Volatiles analyzed via EPA SW846 Method 8021B by DHL Analytical, Inc.

All values reported in Milligrams per liter (mg/L, parts per million).

Blue indicates the compound exceeded NMWQCC standards.

< values - Indicate the value is less than Method Detection Limit MDL.

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
MW-02	3/27/2007	0.0198	0.1550	<0.0003	555	0.00265	<0.0003	65.3	<0.00008	9.72	0.00926	<0.001	131
	6/18/2007	0.0159	0.0982	<0.0003	620	0.00228	<0.0003	77.6	<0.00008	8.25	0.01820	<0.001	113
	9/17/2007	0.00887	0.0677	<0.0003	536	<0.002	<0.0003	40.3	<0.00008	4.68	0.00686	<0.001	51.8
	12/10/2007	0.00991	0.0631	<0.0003	629	0.00427	<0.0003	74.4	<0.00008	9.59	0.00267	<0.001	124
	3/11/2008	0.0048	0.0350	<0.003	561	0.0027	<0.0003	43.6	<0.00008	5.55	0.00390	<0.001	59.2
	9/16/2008	0.127	0.0519	<0.0003	564	0.0105	<0.0003	54.9	<0.00008	8.06	<0.002	<0.001	77.2
	3/10/2009	0.0651	0.0593	<0.0003	656	0.0279	<0.0003	77.1	<0.00008	8.32	<0.002	<0.001	110
MW-02-02	3/27/2007	0.0485	<0.03	<0.003	256	<0.02	<0.003	49,500	<0.00008	1,840	<0.02	<0.01	53,600
	6/19/2007	<0.1	<0.15	<0.015	329	<0.2	<0.015	43,200	<0.00008	1,930	0.10500	<0.05	30,200
	9/18/2007	<0.02	<0.03	<0.003	263	<0.02	<0.006	39,400	<0.00008	1,910	<0.04	<0.01	25,700
	12/11/2007	<0.2	<0.3	<0.03	258	<0.2	<0.03	45,300	<0.00008	1,730	<0.2	<0.1	42,900
	3/11/2008	0.03950	<0.03	<0.003	223	<0.02	<0.003	53,100	<0.00008	1,720	<0.02	<0.01	58,400
	9/17/2008	0.0401	<0.015	0.00210	199	<0.01	<0.0015	45,200	<0.00008	1,500	0.0198	<0.005	50,700
	3/11/2009	0.0444	<0.03	<0.003	198	<0.01	<0.003	44,300	<0.00008	1,480	<0.01	<0.01	41,500
MW-02-03	3/29/2007	0.00369	0.0102	<0.0003	474	0.0484	<0.0003	120	<0.00008	5.02	0.00513	<0.001	55.6
	6/20/2007	0.00283	0.00972	<0.0003	567	0.0467	0.000334	126	<0.00008	4.88	0.00426	<0.001	69.0
	9/18/2007	<0.002	0.0081	<0.0003	561	0.0429	<0.0003	117	<0.00008	3.62	0.00758	<0.001	67.9
	12/11/2007	0.00213	0.00951	<0.0003	550	0.0510	<0.0003	115	<0.00008	4.16	0.00430	<0.001	45.7
	3/11/2008	0.00246	0.00995	<0.0003	561	0.0483	<0.0003	129	<0.00008	5.07	0.00363	<0.001	61.8
	9/17/2008	0.00240	0.01040	<0.0003	542	0.04560	<0.0003	127	<0.00008	4.66	0.00369	<0.001	60.4
	3/11/2009	0.0024	0.00943	<0.0003	510	0.0446	<0.0003	116	<0.00008	4.66	0.00335	<0.001	58.9
MW-02-04	3/28/2007	0.00339	0.0210	<0.0003	510	<0.002	<0.0003	116	<0.00008	13.2	<0.002	<0.001	69.9
	6/18/2007	<0.002	0.0204	<0.0003	612	<0.002	<0.0003	120	<0.00008	11.7	0.00377	<0.001	78.4
	9/17/2007	0.00393	0.0210	<0.0003	574	<0.002	<0.0003	121	<0.00008	10.4	0.00617	<0.001	75.0
	12/10/2007	<0.002	0.0189	<0.0003	616	<0.002	<0.0003	137	<0.00008	12.1	<0.002	<0.001	89.6
	3/11/2008	<0.002	0.0197	<0.0003	598	<0.002	<0.0003	138	<0.00008	12.9	<0.002	<0.001	80.2
	9/16/2008	<0.002	0.0216	<0.0003	506	<0.002	<0.0003	116	<0.00008	10.9	<0.002	<0.001	76.7
	3/10/2009	<0.002	0.0191	<0.0003	532	<0.002	<0.0003	120	<0.00008	11.4	<0.002	<0.001	69.3

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
MW-02-05	3/27/2007	0.0422	<0.03	<0.003	260	<0.02	<0.003	50,800	<0.0008	1,190	<0.02	<0.01	53,200
	6/19/2007	<0.1	<0.15	<0.015	325	<0.2	<0.015	43,600	<0.00008	1,180	<0.1	<0.05	28,900
	9/18/2007	<0.02	<0.03	<0.003	288	<0.02	<0.006	42,800	<0.00008	1,180	<0.002	<0.01	28,500
	12/11/2007	<0.2	<0.03	<0.03	295	<0.2	<0.03	49,700	<0.00008	1,280	<0.2	<0.1	42,100
	3/11/2008	0.0358	<0.03	<0.003	248	<0.02	<0.003	53,300	<0.0008	1,160	<0.02	<0.01	59,400
MW-02-06	9/17/2008	0.0350	<0.015	<0.0015	207	<0.01	<0.0015	46,400	<0.0008	955	0.0199	<0.005	53,200
	3/11/2009	0.0366	<0.03	<0.003	211	<0.01	<0.003	44,800	<0.00008	961	<0.01	<0.01	38,700
	3/28/2007	0.00783	0.0245	<0.0003	480	<0.002	<0.0003	206	<0.00008	8.52	<0.002	<0.001	58.4
	6/20/2007	0.00289	0.0243	<0.0003	604	<0.002	0.000413	140	<0.00008	8.08	<0.002	<0.001	31.8
	9/18/2007	0.00214	0.0225	<0.0003	596	0.00233	<0.0003	146	<0.00008	7.17	0.00615	<0.001	29.9
Mw-02-07	12/11/2007	0.00381	0.0271	<0.0003	580	<0.002	<0.0003	166	<0.00008	8.57	<0.002	<0.001	40.0
	3/11/2008	0.00316	0.0209	<0.0003	548	0.00286	0.00434	203	0.000317	7.49	<0.002	0.00128	52.9
	9/16/2008	0.00261	0.0221	<0.0003	565	<0.002	<0.0003	156	<0.00008	7.48	<0.002	<0.001	35.0
	3/10/2009	0.00368	0.0200	<0.0003	526	<0.002	<0.0003	183	0.000121	7.20	<0.002	<0.001	45.0
	3/28/2007	0.00354	0.0262	<0.0003	522	<0.002	<0.0003	71.8	<0.00008	8.85	<0.002	<0.001	114
MW-02-15	6/19/2007	0.00356	0.0267	<0.0003	545	0.00361	<0.0003	67.7	<0.00008	8.94	<0.002	<0.001	111
	9/18/2007	0.00247	0.0238	<0.0003	579	0.00449	<0.0003	64.2	<0.00008	7.28	0.00568	<0.001	112
	12/10/2007	0.00207	0.0265	<0.0003	587	0.00232	<0.0003	74.4	<0.00008	8.51	<0.002	<0.001	128
	3/11/2008	<0.002	0.0255	<0.0003	574	0.00222	<0.0003	80.0	<0.00008	9.23	<0.002	<0.001	136
	9/16/2008	0.00274	0.0259	<0.0003	603	0.00408	<0.0003	72.6	<0.00008	11.2	0.0494	<0.001	143
	3/10/2009	0.00327	0.0220	<0.0003	543	0.00246	<0.0003	70.3	<0.00008	8.41	<0.002	<0.001	139
	3/29/2007	0.0143	0.0188	<0.0003	564	<0.002	<0.0003	68.5	<0.00008	7.15	<0.002	<0.001	150
	6/20/2007	0.0147	0.016	<0.0003	626	<0.002	<0.0003	73.7	<0.00008	6.65	<0.002	<0.001	168
	9/18/2007	0.00978	0.0139	<0.0003	595	<0.002	<0.0003	64.5	<0.00008	5.88	0.00636	<0.001	153
	12/11/2007	0.0111	0.0182	<0.0003	608	<0.002	<0.0003	68.2	<0.00008	6.66	<0.002	<0.001	162
	3/11/2008	0.00948	0.0162	<0.0003	599	<0.002	<0.0003	71.6	<0.00008	7.74	<0.002	<0.001	176
	9/17/2008	0.0155	0.0175	<0.0003	596	<0.002	<0.0003	85.9	<0.00008	7.29	<0.002	<0.001	200
	3/10/2009	0.00963	0.0154	<0.0003	573	<0.002	<0.0003	64.8	<0.00008	6.67	<0.002	<0.001	177

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
MW-02-16	3/29/2007	0.014	0.01	<0.0003	490	<0.002	<0.0003	126	<0.00008	5.71	<0.002	<0.001	332
	6/19/2007	0.0089	0.01	<0.0003	584	<0.002	<0.0003	138	<0.00008	7.5	<0.002	<0.001	380
	9/18/2007	<0.002	0.0125	<0.0003	569	<0.002	<0.0003	136	<0.00008	5.02	0.00609	<0.001	345
	12/11/2007	0.00437	0.0136	<0.0003	528	<0.002	<0.0003	124	<0.00008	5.14	<0.002	<0.001	331
	3/11/2008	0.00287	0.0133	<0.0003	560	<0.002	<0.0003	134	<0.00008	6.07	<0.002	<0.001	380
MW-02-18	9/17/2008	0.00358	0.0137	<0.0003	565	<0.002	<0.0003	134	<0.00008	5.72	<0.002	<0.001	357
	3/11/2009	0.00274	0.0121	<0.0003	534	<0.002	<0.0003	128	<0.00008	5.24	<0.002	<0.001	342
	3/28/2007	0.00389	0.0182	0.000323	515	<0.002	<0.0003	262	<0.00008	2.76	<0.002	<0.001	115
	6/19/2007	<0.002	0.0193	<0.0003	557	<0.002	<0.0003	260	<0.00008	3.37	<0.002	<0.001	104
	9/18/2007	<0.002	0.0128	<0.0003	535	<0.002	<0.0003	227	<0.00008	2.49	0.00612	<0.001	88.3
MW-03-01	12/11/2007	<0.002	0.0224	<0.0003	610	<0.002	<0.0003	240	<0.00008	2.84	<0.002	<0.001	97.3
	3/11/2008	<0.002	0.0186	<0.0003	572	<0.002	<0.0003	279	<0.00008	3.45	<0.002	<0.001	103
	9/16/2008	0.00292	0.0216	<0.0003	604	<0.002	<0.0003	252	<0.00008	2.89	<0.002	<0.001	99.7
	3/10/2009	<0.002	0.0164	<0.0003	552	<0.002	<0.0003	239	<0.00008	2.70	<0.002	<0.001	96.1
	3/28/2007	0.0072	0.0247	<0.0003	571	<0.002	<0.0003	60.0	<0.00008	7.95	<0.002	<0.001	143
MW-03-02	6/19/2007	0.00677	0.0224	<0.0003	603	0.00201	<0.0003	68.4	<0.00008	7.75	<0.002	<0.001	156
	9/18/2007	0.00341	0.0199	<0.0003	570	<0.002	<0.0003	59.5	<0.00008	6.27	<0.002	<0.001	148
	12/11/2007	0.0043	0.0216	<0.0003	604	<0.002	<0.0003	65.5	<0.00008	7.30	<0.002	<0.001	166
	3/11/2008	<0.002	0.0209	<0.0003	597	<0.002	<0.0003	67.1	<0.00008	8.32	<0.002	<0.001	175
	3/29/2007	0.00259	0.0229	<0.0003	544	<0.002	<0.0003	104	<0.00008	6.46	<0.002	<0.001	276
MW-03-03	6/19/2007	0.00201	0.0181	<0.0003	539	<0.002	<0.0003	113	<0.00008	5.53	<0.002	<0.001	333
	12/11/2007	<0.002	0.0206	<0.0003	518	<0.002	<0.0003	104	<0.00008	4.98	<0.002	<0.001	304
	3/28/2007	0.00512	0.0254	<0.0003	405	<0.002	<0.0003	86.8	<0.00008	9.52	<0.002	<0.001	148
	6/19/2007	0.00328	0.0248	<0.0003	456	<0.002	<0.0003	94.8	<0.00008	8.47	<0.002	<0.001	178
	9/18/2007	0.00276	0.0229	<0.0003	425	<0.002	<0.0003	83.3	<0.00008	7.61	0.00649	<0.001	146
	3/11/2009	0.00419	0.0239	<0.0003	381	<0.002	<0.0003	78.7	<0.00008	7.96	<0.002	<0.001	120

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard	(mg/L)	0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
MW-05	3/29/2007	0.00233	0.0145	<0.0003	558	<0.002	<0.0003	136	<0.00008	5.69	<0.002	<0.001	199
	6/19/2007	0.00252	0.0124	<0.0003	555	<0.002	<0.0003	130	<0.00008	5.56	<0.002	<0.001	203
	9/18/2007	<0.002	0.0113	<0.0003	542	<0.002	0.00119	127	<0.00008	4.53	0.00418	<0.001	188
	12/11/2007	<0.002	0.0152	<0.0003	544	<0.002	<0.0003	123	<0.00008	5.23	<0.002	<0.001	194
	3/11/2008	<0.002	0.0127	<0.0003	570	<0.002	<0.0003	145	<0.00008	5.88	<0.002	<0.001	233
	9/17/2008	<0.002	0.0151	<0.0003	564	<0.002	<0.0003	134	<0.00008	5.9	<0.002	<0.001	209
MW-07	3/10/2009	<0.002	0.0132	<0.0003	527	<0.002	<0.0003	120	<0.00008	5.27	<0.002	<0.001	186
	3/28/2007	0.00245	0.016	<0.0003	491	0.0254	<0.0003	128	<0.00008	14.4	<0.002	<0.001	74.2
	6/19/2007	0.00238	0.0258	<0.0003	613	0.0247	<0.0003	33.3	<0.00008	8.94	<0.002	<0.001	74.2
	9/18/2007	<0.002	0.0221	<0.0003	622	0.0374	<0.0003	39.0	<0.00008	7.96	0.00589	<0.001	41.2
	12/10/2007	0.00213	0.0332	<0.0003	630	0.0356	<0.0003	48.8	<0.00008	10.1	<0.002	<0.001	99.1
	3/11/2008	<0.002	0.0187	<0.0003	618	0.0222	0.000721	67.0	<0.00008	13.6	<0.002	<0.001	81.2
MW-08	9/17/2008	<0.002	0.0151	<0.0003	564	<0.002	<0.0003	134	<0.00008	5.90	<0.002	<0.001	209
	3/28/2007	0.00726	0.0205	<0.0003	479	<0.002	<0.0003	122	<0.00008	6.85	<0.002	<0.001	286
	6/19/2007	0.00491	0.0189	<0.0003	496	<0.002	<0.0003	136	<0.00008	6.93	<0.002	<0.001	303
	9/18/2007	0.00436	0.0174	<0.0003	490	<0.002	<0.0003	127	<0.00008	5.39	0.00512	<0.001	288
	12/11/2007	0.00463	0.0221	<0.0003	479	<0.002	<0.0003	122	<0.00008	6.16	<0.002	<0.001	288
	3/11/2008	0.00548	0.0199	<0.0003	506	<0.002	<0.0003	135	<0.00008	7.4	<0.002	<0.001	320
MW-12	9/17/2008	0.00535	0.0194	<0.0003	486	<0.002	<0.0003	124	<0.00008	6.63	<0.002	<0.001	280
	3/11/2009	0.00583	0.0188	<0.0003	467	<0.002	<0.0003	121	<0.00008	6.55	<0.002	<0.001	280
MW-13	3/11/2009	<0.002	0.0141	<0.0003	535	<0.002	<0.0003	85.6	<0.00008	5.3	<0.002	<0.001	99.8
MW-15	9/16/2008	0.00853	0.0249	<0.0003	561	<0.002	<0.0003	36.0	<0.00008	5.92	<0.002	<0.001	77.4
	3/10/2009	0.00707	0.0246	<0.0003	546	<0.002	<0.0003	26.4	<0.00008	4.28	<0.002	<0.001	48.5
MW-16	9/16/2008	0.0174	0.0166	<0.0003	404	<0.002	<0.0003	3,560	<0.00008	116	0.00873	<0.001	4,190
	3/10/2009	0.0110	0.0180	<0.0015	424	<0.01	<0.0015	6,160	<0.00008	222	<0.01	<0.005	7,630
MW-17	7/15/2009	0.00683	0.0179	0.000498	513	0.00585	<0.0003	1,240	<0.00008	37.1	0.0104	<0.001	1,890
MW-17	7/15/2009	0.00814	0.0304	<0.0003	568	<0.002	<0.0003	111	<0.00008	5.58	<0.002	<0.001	132

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
MW-18	7/15/2009	0.00284	0.0320	<0.0003	623	<0.002	<0.0003	21.1	<0.00008	3.14	<0.002	<0.001	44.4
MW-20	7/15/2009	0.0821	0.0150	<0.0003	576	<0.002	<0.0003	117	<0.00008	8.33	<0.002	<0.001	306
MW-22	7/15/2009	0.00906	0.0255	<0.0003	664	<0.002	<0.0003	288	<0.00008	3.95	<0.002	<0.001	77.4
MW-23	7/15/2009	0.00259	0.0228	<0.0003	660	<0.002	<0.0003	145	<0.00008	6.72	<0.002	<0.001	245
EB-01	3/27/2007	0.00298	0.0122	<0.0003	508	<0.002	<0.0003	132	<0.00008	3.56	0.00663	<0.001	22.2
	6/18/2007	0.00232	0.0147	<0.0003	576	<0.002	<0.0003	135	<0.00008	4.39	0.00637	<0.001	94.3
	9/17/2007	0.00308	0.0156	<0.0003	524	<0.002	<0.0003	132	<0.00008	4.13	0.00901	<0.001	131
	12/10/2007	<0.002	0.0118	<0.0003	550	<0.002	<0.0003	124	<0.00008	3.19	0.00388	<0.001	24.9
	3/10/2008	<0.002	0.0119	0.000545	532	<0.002	<0.0003	123	<0.00008	3.50	0.00521	<0.001	22
	9/16/2008	0.00204	0.0105	<0.0003	496	<0.002	<0.0003	112	<0.00008	3.26	0.00507	<0.001	18.7
EB-02	3/10/2009	0.00214	0.0118	0.000331	545	<0.002	<0.0003	128	<0.00008	3.67	0.00488	<0.001	21.6
	3/27/2007	<0.002	0.0124	<0.0003	496	<0.002	<0.0003	198	<0.00008	10.1	0.00328	<0.001	152
	6/18/2007	<0.002	0.0156	<0.0003	531	<0.002	<0.0003	305	<0.00008	9.09	0.00485	<0.001	135
	9/17/2007	<0.002	0.0123	<0.0003	524	<0.002	<0.0003	228	<0.00008	8.77	0.00631	<0.001	152
	12/10/2007	<0.002	0.012	<0.0003	666	<0.002	<0.0003	192	<0.00008	9.13	<0.002	<0.001	164
	3/10/2008	<0.002	0.0107	<0.0003	514	<0.002	<0.0003	194	<0.00008	9.51	0.00203	<0.001	146
EB-03	9/16/2008	<0.002	0.0140	<0.0003	519	<0.002	<0.0003	165	<0.00008	9.50	<0.002	<0.001	149
	3/10/2009	<0.002	0.0128	<0.0003	512	<0.002	<0.0003	186	<0.00008	9.56	<0.002	<0.001	141
	3/27/2007	<0.002	0.0202	<0.0003	545	<0.002	<0.0003	30	<0.00008	3.93	<0.002	<0.001	56.5
	3/27/2007	0.00342	0.0163	<0.0003	591	0.0615	<0.0003	126	<0.00008	6.30	0.00242	<0.001	208
	6/18/2007	0.00277	0.0165	<0.0003	680	0.0718	<0.0003	138	<0.00008	6.07	<0.002	<0.001	232
	9/17/2007	0.00288	0.0164	<0.0003	636	0.0518	<0.0003	126	<0.00008	5.44	0.00606	<0.001	214
EB-04	12/10/2007	<0.002	0.0169	<0.0003	683	0.0515	<0.0003	135	<0.00008	5.60	<0.002	<0.001	235
	3/10/2008	0.00214	0.0165	<0.0003	689	0.0542	<0.0003	135	<0.00008	5.84	<0.002	<0.001	232
	9/16/2008	0.00245	0.174	<0.0003	625	0.0565	<0.0003	122	<0.00008	5.90	<0.002	<0.001	207
	3/10/2009	0.002	0.0165	<0.0003	609	0.0364	<0.0003	118	<0.00008	6.01	<0.002	<0.001	204

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
EB-05	3/26/2007	<0.002	0.0290	<0.0003	682	<0.002	<0.0003	12.4	<0.00008	3.16	3.16	<0.001	39.7
	6/18/2007	<0.002	0.0281	<0.0003	623	<0.002	<0.0003	14.3	<0.00008	3.27	3.27	<0.001	46.3
	9/17/2007	<0.002	0.0258	<0.0003	602	<0.002	<0.0003	18.8	<0.00008	3.33	3.33	<0.001	48.4
	12/10/2007	<0.002	0.0235	<0.0003	586	<0.002	<0.0003	13.5	<0.00008	2.51	2.51	<0.001	38.7
	3/10/2008	<0.002	0.0304	<0.0003	602	<0.002	<0.0003	11.2	<0.00008	2.73	<0.002	<0.001	32.1
EB-06	9/16/2008	<0.002	0.0403	<0.0003	556	<0.002	<0.0003	11.5	<0.00008	3.06	<0.002	<0.001	37.0
	3/10/2009	<0.002	0.0320	<0.0003	553	<0.002	<0.0003	11.0	<0.00008	3.05	<0.002	<0.001	35.3
	3/26/2007	0.00375	0.0155	0.000301	684	<0.002	<0.0003	142	<0.00008	4.74	0.00411	<0.001	41.6
	6/18/2007	<0.002	0.0174	<0.0003	600	<0.002	0.00474	127	<0.00008	4.85	0.00325	<0.001	39.8
	9/17/2007	<0.002	0.0151	0.000394	573	<0.002	0.00197	118	<0.00008	3.68	0.00676	<0.001	33.8
EB-07	12/10/2007	<0.002	0.0148	<0.0003	570	<0.002	<0.0003	117	<0.00008	3.73	0.0031	<0.001	40.1
	3/10/2008	<0.002	0.0158	0.000561	572	<0.002	<0.0003	122	<0.00008	3.86	0.00348	<0.001	47.5
	9/16/2008	<0.002	0.0155	0.000352	556	0.00217	<0.0003	117	<0.00008	4.27	0.00379	<0.001	34.4
	3/10/2009	<0.002	0.0142	0.000419	544	0.00607	<0.0003	112	<0.00008	4.33	0.00280	<0.001	33.9
	3/27/2007	0.02580	0.0158	<0.0003	562	<0.002	<0.0003	97.2	<0.00008	2.68	<0.002	<0.001	108
EB-08	6/18/2007	0.02730	0.0163	<0.0003	643	<0.002	<0.0003	107	<0.00008	2.98	<0.002	<0.001	117
	9/17/2007	0.0211	0.0164	0.000320	612	<0.002	<0.0003	99.6	<0.00008	2.65	<0.002	<0.001	109
	12/10/2007	0.0232	0.0152	<0.0003	614	<0.002	<0.0003	99.6	<0.00008	2.59	<0.002	<0.001	119
	3/10/2008	0.0301	0.0158	<0.0003	594	<0.002	<0.0003	91.4	<0.00008	2.94	<0.002	<0.001	106
	9/16/2008	0.0379	0.0173	<0.0003	589	<0.002	<0.0003	94.8	<0.00008	3.16	<0.002	<0.001	111
EB-08	3/10/2009	0.0416	0.0155	<0.0003	572	<0.002	<0.0003	86.6	<0.00008	3.48	<0.002	<0.001	102
	3/27/2007	0.00543	0.0259	<0.0003	646	<0.002	<0.0003	123	<0.00008	6.78	<0.002	<0.001	238
	6/18/2007	0.0036	0.0239	<0.0003	757	<0.002	<0.0003	130	<0.00008	7.04	0.0856	<0.001	262
	9/17/2007	0.00454	0.0209	<0.0003	689	<0.002	<0.0003	128	0.000354	5.61	0.00687	<0.001	223
	12/10/2007	<0.002	0.0198	<0.0003	676	<0.002	<0.0003	139	0.000354	5.19	<0.002	<0.001	177
EB-08	3/10/2008	0.00206	0.0209	<0.0003	723	<0.002	<0.0003	133	<0.00008	5.84	0.0799	<0.001	203
	9/16/2008	0.0048	0.0236	<0.0003	702	<0.002	<0.0003	120	<0.00008	6.47	<0.002	<0.001	215
	3/10/2009	0.00544	0.0232	<0.0003	704	0.00204	<0.0003	120	<0.00008	6.10	<0.002	<0.001	198

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
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Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWQCC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
P-01	3/26/2007	0.00327	0.0262	<0.0003	692	<0.002	<0.0003	17.9	<0.00008	3.20	<0.002	<0.001	42.6
	6/18/2007	0.00355	0.0246	<0.0003	610	<0.002	<0.0003	17.9	<0.00008	3.25	<0.002	<0.001	45.7
	9/17/2007	<0.002	0.0259	0.000644	604	<0.002	<0.0003	23.1	0.000172	3.21	<0.002	<0.001	56.5
	12/10/2007	<0.002	0.0270	<0.0003	584	<0.002	<0.0003	18.8	<0.00008	2.71	<0.002	<0.001	44.8
	3/10/2008	0.00505	0.022	<0.0003	608	<0.002	<0.0003	17.0	<0.00008	2.77	<0.002	<0.001	34.7
	9/16/2008	<0.002	0.051	<0.0003	583	<0.002	<0.0003	20.3	<0.00008	3.50	<0.002	<0.001	42.1
	3/10/2009	<0.002	0.0188	<0.0003	520	<0.002	<0.0003	34.9	<0.00008	3.25	<0.002	<0.001	58.3
P-02	3/27/2007	0.00256	0.0154	<0.0003	512	<0.002	<0.0003	201	<0.00008	4.14	<0.002	<0.001	48.5
	6/19/2007	0.00405	0.0167	<0.0003	564	<0.002	<0.0003	179	<0.00008	4.25	<0.002	<0.001	39.1
	9/17/2007	0.00206	0.0166	<0.0003	553	<0.002	<0.0003	175	<0.00008	3.59	<0.002	<0.001	37.9
	12/10/2007	<0.002	0.0162	<0.0003	601	<0.002	<0.0003	186	<0.00008	3.82	<0.002	<0.001	44.6
	3/10/2008	<0.002	0.0154	<0.0003	546	<0.002	<0.0003	177	<0.00008	3.84	0.00738	<0.001	43.7
	9/16/2008	<0.002	0.0163	<0.0003	529	<0.002	<0.0003	186	<0.00008	3.81	<0.002	<0.001	47.8
	3/10/2009	<0.002	0.0147	<0.0003	545	<0.002	<0.0003	200	<0.00008	3.84	<0.002	<0.001	44.2
P-03	3/27/2007	0.0326	0.0254	<0.0003	549	<0.002	<0.0003	238	<0.00008	4.77	<0.002	<0.001	106
	6/18/2007	0.0280	0.0246	<0.0003	664	<0.002	<0.0003	269	<0.00008	5.32	<0.002	<0.001	151
	9/17/2007	0.0248	0.0230	<0.0003	628	<0.002	<0.0003	256	<0.00008	4.50	0.00521	<0.001	162
	12/10/2007	0.0270	0.0226	<0.0003	623	<0.002	<0.0003	260	<0.00008	4.53	<0.002	<0.001	164
	3/10/2008	0.0319	0.022	<0.0003	603	<0.002	<0.0003	233	<0.00008	4.79	<0.002	<0.001	166
	9/16/2008	0.0390	0.0255	<0.0003	636	<0.002	<0.0003	251	<0.00008	5.13	<0.002	<0.001	207
	3/10/2009	0.0392	0.0233	<0.0003	608	<0.002	<0.0003	236	<0.00008	5.02	<0.002	<0.001	206
P-04	3/27/2007	0.0694	0.0243	<0.0003	592	<0.002	<0.0003	218	<0.00008	7.68	<0.002	<0.001	217
	6/18/2007	0.0496	0.0219	<0.0003	682	<0.002	<0.0003	212	<0.00008	7.84	<0.002	<0.001	225
	9/17/2007	0.0280	0.0198	<0.0003	611	<0.002	<0.0003	178	<0.00008	6.60	<0.002	<0.001	204
	12/10/2007	0.0306	0.0197	<0.0003	629	<0.002	<0.0003	187	<0.00008	6.40	<0.002	<0.001	219
	3/10/2008	0.0267	0.0188	<0.0003	674	<0.002	<0.0003	182	<0.00008	7.13	<0.002	<0.001	219
	9/16/2008	0.0591	0.0216	<0.0003	611	<0.002	<0.0003	206	<0.00008	6.94	<0.002	<0.001	210
	3/10/2009	0.0322	0.0199	<0.0003	592	<0.002	<0.0003	183	<0.00008	7.55	<0.002	<0.001	217

Table 3
Groundwater Metals Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
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Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMWWQC Standard (mg/L)		0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
P-05	3/27/2007	0.00579	0.0164	<0.0003	558	<0.002	<0.0003	52.0	<0.00008	3.52	<0.002	<0.001	73.7
	6/18/2007	0.00225	0.0134	<0.0003	603	<0.002	<0.0003	60.4	<0.00008	3.02	<0.002	<0.001	84.9
	9/17/2007	0.00241	0.0148	<0.0003	594	<0.002	<0.0003	51.0	<0.00008	2.83	<0.002	<0.001	71.2
	12/10/2007	<0.002	0.0161	<0.0003	623	<0.002	<0.0003	52.1	<0.00008	2.95	<0.002	<0.001	87.4
	3/10/2008	<0.002	0.0156	<0.0003	595	<0.002	<0.0003	50.7	<0.00008	3.2	<0.002	<0.001	81.3
	9/16/2008	<0.002	0.0161	<0.0003	573	<0.002	<0.0003	44.3	<0.00008	3.53	<0.002	<0.001	58.0
	3/10/2009	<0.002	0.0167	<0.0003	594	<0.002	<0.0003	40.9	<0.00008	3.58	<0.002	<0.001	55.3

Notes

Metals analyzed via EPA SW845 Method 6020 by DHL Analytical Inc., Round Rock, Texas
Mercury analyzed via EPA SW846 Method 7470A by DHL Analytical Inc., Round Rock, Texas
All values reported in Milligrams per liter (mg/L, parts per million).
< values - indicate the value is less than Method Detection Limit MDL.

Table 3a
Groundwater Metals Quality Control Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
MMWQCC Standard	(mg/L)	0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
Duplicate-01 (P-02)	3/10/2008	<0.002	0.0154	<0.0003	556	<0.002	<0.0003	194	<0.00008	3.63	0.00417	<0.001	49.8
Duplicate-01 (MW-13)	9/16/2008	0.00809	0.0227	<0.0003	560	<0.002	<0.0003	37.2	<0.00008	5.67	<0.002	<0.001	78.4
Duplicate-01 (MW-13)	3/10/2009	0.00752	0.0260	<0.0003	537	<0.002	<0.0003	27.2	<0.00008	4.38	<0.002	<0.001	50.0
Duplicate-01 (MW-16)	7/15/2009	0.00594	0.0176	<0.0003	542	0.005480	<0.0003	1,260	<0.00008	36.2	0.00884	<0.001	1,950
Duplicate-02 (MW-02-16)	3/11/2008	0.00260	0.0125	<0.0003	565	<0.002	<0.0003	135	<0.00008	6.21	<0.002	<0.001	377
Duplicate-02 (MW-02-07)	9/17/2008	0.00578	0.0281	<0.0003	594	0.00416	<0.0003	72.2	<0.00008	11.3	<0.002	<0.001	141
Duplicate-02 (MW-12)	3/11/2009	<0.002	0.0148	<0.0003	539	<0.002	<0.0003	87.4	<0.00008	5.42	<0.002	<0.001	103
Equipment Rinse	3/11/2008	<0.002	<0.003	<0.0003	0.396	<0.002	<0.0003	<0.1	<0.00008	<0.1	<0.002	<0.001	0.113
	3/10/2009	<0.002	<0.003	<0.0003	<0.1	<0.002	<0.0003	<0.1	<0.00008	<0.1	<0.002	<0.001	<0.1
	3/11/2009	<0.002	<0.003	<0.0003	<0.1	<0.002	<0.0003	<0.1	<0.00008	<0.1	<0.002	<0.001	<0.1

Table 3a
Groundwater Metals Quality Control Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Dissolved Metals	Collection Date	Arsenic	Barium	Cadmium	Calcium	Chromium	Lead	Magnesium	Mercury	Potassium	Selenium	Silver	Sodium
NMW/QCC Standard	(mg/L)	0.1	1	0.01	--	0.05	0.05	--	0.002	--	0.05	0.05	--
Field Blank	3/10/2008	<0.002	<0.003	<0.0003	0.487	<0.002	<0.0003	0.223	<0.00008	<0.1	0.00245	<0.001	<0.1
	9/17/2008	<0.002	<0.003	<0.0003	<0.1	<0.002	<0.0003	<0.1	<0.00008	<0.1	<0.002	<0.001	<0.1
	3/10/2009	<0.002	<0.003	<0.0003	<0.1	<0.002	<0.0003	<0.1	<0.00008	<0.1	<0.002	<0.001	<0.1

Notes

Metals analyzed via EPA SW846 Method 6020 by DHL Analytical Inc., Round Rock, Texas
Mercury analyzed via EPA SW846 Method 7470A by DHL Analytical Inc., Round Rock, Texas
All values reported in Milligrams per liter (mg/L, parts per million).
< values - Indicate the value is less than Method Detection Limit MDL.

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
MW-02	3/27/2007	163	<10	<10	163	151	7.19	1,650	3,030
	6/18/2007	298	<10	<10	298	139	3.42	1,750	3,170
	9/17/2007	218	<10	<10	218	61.2	3.31	1,350	2,500
	12/10/2007	272	<10	<10	272	131	0.408	1,890	3,080
	3/11/2008	186	<10	<10	186	72.5	2.85	1,720	2,650
	9/16/2008	490	<10	<10	490	95.0	<0.1	1,560	3,020
	3/10/2009	853	<10	<10	853	148	<0.1	1,470	3,340
MW-02-02	3/27/2007	5,350	736	<10	6,090	9,350	<10	392,000	554,000
	6/19/2007	9,390	<10	<10	9,390	16,300	<10	221,000	388,000
	9/18/2007	1,710	3,580	<10	5,280	11,500	<10	299,000	531,000
	12/11/2007	2,940	3,940	<10	6,880	13,300	<10	224,000	445,000
	3/11/2008	5,310	1,590	<10	6,900	11,600	<10	340,000	500,000
	9/17/2008	6,890	<10	<10	6,890	11,400	10.7	352,000	511,000
	3/11/2009	4,340	2,820	<10	7,170	9,460	12.8	294,000	510,000
MW-02-03	3/29/2007	137	<10	<10	137	51.7	5.56	1,960	2,990
	6/20/2007	158	<10	<10	158	60.1	4.39	1,840	3,100
	9/18/2007	154	<10	<10	154	57.4	5.38	1,870	3,040
	12/11/2007	120	<10	<10	120	50.3	5.97	1,840	2,960
	3/11/2008	145	<10	<10	145	58.7	4.65	1,930	3,030
	9/17/2008	305	<10	<10	305	52.2	5.73	1,970	3,030
	3/11/2009	151	<10	<10	151	52.2	4.86	1,820	3,120
MW-02-04	3/28/2007	279	<10	<10	279	82.3	0.129	1,750	3,150
	6/18/2007	294	<10	<10	294	96.0	<0.1	1,840	3,130
	9/18/2007	288	<10	<10	288	103	<0.1	1,800	3,250
	12/10/2007	292	<10	<10	292	105	<0.1	2,000	3,270
	3/11/2008	283	<10	<10	283	104	<0.1	1,910	3,260
	9/16/2008	360	<10	<10	360	99.2	<0.1	1,550	3,050
	3/10/2009	338	<10	<10	338	96.4	<0.1	1,750	3,150

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
MW-02-05	3/27/2007	4,720	2,320	<10	7,040	4,620	<10	394,000	569,000
	6/19/2007	8,900	3,720	<10	126,000	7,880	<10	244,000	387,000
	9/18/2007	1,320	4,510	<10	5,830	4,910	<10	317,000	553,000
	12/11/2007	2,350	5,220	<10	7,570	4,840	<10	216,000	435,000
	3/11/2008	4,690	2,970	<10	7,660	6,260	<10	352,000	506,000
	9/16/2008	7,750	<10	<10	7,750	5,490	<10	366,000	517,000
	3/11/2009	4270	4650	<10	8,920	5,440	14.7	297,000	498,000
MW-02-06	3/28/2007	687	<10	<10	687	30.3	0.177	1,730	3,560
	6/20/2007	480	<10	<10	480	23.3	0.289	1,690	3,230
	9/18/2007	547	<10	<10	547	25.4	0.111	1,790	3,270
	12/11/2007	598	<10	<10	598	26.8	<0.1	1,820	3,300
	3/11/2008	563	<10	<10	563	25.8	<0.1	2,060	3,410
	9/16/2008	556	<10	<10	556	28.3	2.90	1,800	3,320
	3/10/2009	700	<10	<10	700	30.2	0.238	1,540	3,370
MW-02-07	3/28/2007	631	<10	<10	631	109	<0.1	1,190	2,650
	6/19/2007	664	<10	<10	664	110	<0.1	1,280	2,740
	9/18/2007	643	<10	<10	643	126	<0.1	1,330	2,770
	12/10/2007	670	<10	<10	670	112	<0.1	1,320	2,810
	3/11/2008	640	<10	<10	640	130	<0.1	1,370	2,970
	9/17/2008	672	<10	<10	672	103	<0.1	1,420	3,010
	3/10/2009	656	<10	<10	656	163	<0.1	1,340	3,170
MW-02-15	3/29/2007	336	<10	<10	336	168	<0.1	1,800	3,090
	6/20/2007	346	<10	<10	346	167	<0.1	1,660	3,240
	9/18/2007	366	<10	<10	366	169	<0.1	1,670	3,180
	12/11/2007	366	<10	<10	366	185	<0.1	1,740	3,140
	3/11/2008	347	<10	<10	347	205	<0.1	1,700	3,200
	9/17/2008	359	<10	<10	359	244	<0.1	1,730	3,330
	3/10/2009	363	<10	<10	363	280	<0.1	1,520	3,430

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
MW-02-16	3/29/2007	818	<10	<10	818	181	<0.1	1,940	3,800
	6/19/2007	756	<10	<10	756	206	<0.1	1,810	3,900
	9/18/2007	802	<10	<10	802	175	<0.1	1,860	3,870
	12/11/2007	809	<10	<10	809	169	<0.1	1,850	3,790
	3/11/2008	780	<10	<10	780	193	<0.1	1,830	3,860
MW-02-18	9/17/2008	404	<10	<10	404	181	0.140	1,850	3,840
	3/11/2009	814	<10	<10	814	168	<0.1	1,730	3,840
	3/28/2007	747	<10	<10	747	148	<0.1	2,050	4,190
	6/19/2007	641	<10	<10	641	121	<0.1	1,970	3,820
	9/18/2007	675	<10	<10	675	121	<0.1	1,980	4,080
MW-03-01	12/11/2007	830	<10	<10	830	109	0.106	2,010	3,930
	3/11/2008	785	<10	<10	785	127	0.34	2,030	3,900
	9/16/2008	839	<10	<10	839	114	3.2	1,970	4,100
	3/10/2009	920	<10	<10	920	119	0.151	1,880	4,010
	3/28/2007	463	<10	<10	463	170	<0.1	1,420	3,000
MW-03-02	6/19/2007	455	<10	<10	455	192	<0.1	1,510	3,090
	9/18/2007	410	<10	<10	410	192	<0.1	1,440	2,870
	12/11/2007	361	<10	<10	361	200	<0.1	1,460	3,110
	3/11/2008	427	<10	<10	427	240	<0.1	1,570	3,240
	3/29/2007	637	<10	<10	637	204	<0.1	1,840	3,560
MW-03-03	6/19/2007	685	<10	<10	685	174	<0.1	1,600	3,420
	12/11/2007	656	<10	<10	656	178	<0.1	1,750	3,590
	3/28/2007	665	<10	<10	665	201	<0.1	964	2,420
	6/17/2007	660	<10	<10	660	231	<0.1	954	2,520
	9/18/2007	635	<10	<10	635	228	<0.1	963	2,480
	3/11/2009	684	<10	<10	684	147	<0.1	899	2,310

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMW/QCC Standard (mg/L)		--	--	--	--	250	10	600	1000
MW-05	3/29/2007	540	<10	<10	540	159	<0.1	1,910	3,440
	6/19/2007	514	<10	<10	514	146	<0.1	1,740	3,540
	9/18/2007	530	<10	<10	530	156	<0.1	1,810	3,450
	12/11/2007	535	<10	<10	535	160	<0.1	1,840	3,430
	3/11/2008	524	<10	<10	524	197	<0.1	1,840	3,400
	9/17/2008	1,080	<10	<10	1,080	172	<0.1	1,800	3,440
MW-07	3/10/2009	555	<10	<10	555	161	<0.1	1,650	3,460
	3/28/2007	435	<10	<10	435	31.1	<0.1	1,950	3,280
	6/19/2007	559	<10	<10	559	31.4	<0.1	1,580	2,880
	9/18/2007	651	<10	<10	651	23.7	<0.1	1,490	2,890
	12/10/2007	617	<10	<10	617	30.8	<0.1	1,660	2,980
MW-08	3/11/2008	531	<10	<10	531	46.2	<0.2	1,640	3,120
	3/28/2007	485	<10	<10	485	320	<0.1	1,650	3,500
	6/19/2007	464	<10	<10	464	344	<0.1	1,640	3,400
	9/18/2007	468	<10	<10	468	317	<0.1	1,550	3,420
	12/11/2007	472	<10	<10	472	302	<0.1	1,690	3,400
	3/11/2008	458	<10	<10	458	318	<0.1	1,730	3,470
MW-12	9/17/2008	444	<10	<10	444	333	<0.1	1,700	3,480
	3/11/2009	468	<10	<10	468	290	0.118	1,500	3,460
MW-12	3/11/2009	358	<10	<10	358	105	<0.1	1,540	3,100
MW-13	9/16/2008	222	<10	<10	222	76.3	<0.1	1,650	2,840
	3/10/2009	170	<10	<10	170	52.1	<0.1	1,560	2,560
MW-15	9/16/2008	503	<10	<10	503	1,430	5.30	23,500	37,200
	3/10/2009	1070	<10	<10	1070	3,170	7.33	47,900	73,200
MW-16	7/15/2009	232	<10	<10	232	1,500	4.95	7,560	13,900

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWWQC Standard (mg/L)		--	--	--	--	250	10	600	1000
MW-17	7/15/2009	197	<10	<10	197	96.6	<0.10	1,860	3,190
MW-18	7/15/2009	203	<10	<10	203	46.9	<0.10	1,400	2,570
MW-20	7/15/2009	481	<10	<10	481	135	<0.10	1,910	3,620
MW-22	7/15/2009	632	<10	<10	632	77.1	0.113	1,900	3,920
MW-23	7/15/2009	493	<10	<10	493	265	<0.10	1,710	3,730
EB-01	3/27/2007	101	<10	<10	101	30	7.37	1,790	2,890
	6/18/2007	118	<10	<10	118	130	7.05	2,000	3,250
	9/17/2007	112	<10	<10	112	122	7.64	1,870	3,250
	12/10/2007	103	<10	<10	103	32	6.72	1,990	2,910
	3/10/2008	103	<10	<10	103	32.4	7.72	1,870	2,990
	9/16/2008	102	<10	<10	102	29.9	7.11	1,750	3,010
EB-02	3/10/2009	103	<10	<10	103	33.2	7.75	1,880	2,940
	3/27/2007	318	<10	<10	318	106	3.91	2,260	3,730
	6/18/2007	339	<10	<10	339	111	2.93	2,090	3,610
	9/17/2007	307	<10	<10	307	110	4.05	2,360	3,740
	12/10/2007	330	<10	<10	330	111	3.11	2,190	3,630
	3/10/2008	319	<10	<10	319	118	3.79	2,210	3,820
EB-03	9/16/2008	365	<10	<10	365	113	2.41	2,150	3,640
	3/10/2009	350	<10	<10	350	112	2.49	2,220	3,720
	3/27/2007	293	<10	<10	293	65.1	<0.1	1,430	2,610

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
EB-04	3/27/2007	254	<10	<10	254	645	2.51	1,710	3,770
	6/18/2007	250	<10	<10	250	662	2.90	1,700	3,800
	9/17/2007	244	<10	<10	244	664	3.23	1,660	3,880
	12/10/2007	252	<10	<10	252	685	2.13	1,900	3,790
	3/10/2008	247	<10	<10	247	637	3.29	1,720	3,830
	9/16/2008	245	<10	<10	245	598	2.39	1,800	3,910
EB-05	3/10/2009	247	<10	<10	247	602	2.35	1,790	3,730
	3/26/2007	167	<10	<10	167	41	<0.1	1,400	2,420
	6/18/2007	183	<10	<10	183	52.5	<0.1	1,450	2,430
	9/17/2007	228	<10	<10	228	79.0	<0.1	1,560	2,550
	12/10/2007	173	<10	<10	173	43.7	<0.1	1,740	2,480
	3/10/2008	162	<10	<10	162	45.4	<0.1	1,420	2,470
EB-06	9/16/2008	172	<10	<10	172	47.0	<0.1	1,400	2,460
	3/10/2009	156	<10	<10	156	43.5	0.568	1,440	2,400
	3/26/2007	108	<10	<10	108	160	4.61	1,740	3,020
	6/18/2007	107	<10	<10	107	167	4.74	1,790	2,990
	9/17/2007	96.8	<10	<10	96.8	162	5.25	1,730	3,050
	12/10/2007	79.6	<10	<10	79.6	159	3.99	1,780	2,960
EB-07	3/10/2008	94.8	<10	<10	94.8	177	5.1	1,750	3,040
	9/16/2008	95.4	<10	<10	95.4	161	4.68	1,830	3,210
	3/10/2009	101	<10	<10	101	165	4.88	1,810	3,030
	3/27/2007	415	<10	<10	415	174	<0.1	1,610	3,230
	6/18/2007	414	<10	<10	414	187	<0.1	1,680	3,180
	9/17/2007	400	<10	<10	400	182	<0.1	1,800	3,200
	12/10/2007	422	<10	<10	422	171	<0.1	1,830	3,180
	3/10/2008	428	<10	<10	428	193	<0.1	1,670	3,300
	9/16/2008	438	<10	<10	438	158	<0.1	1,620	3,280
	3/10/2009	441	<10	<10	441	171	<0.1	1,910	3,190

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
EB-08	3/27/2007	947	<10	<10	947	504	<0.1	1,720	4,200
	6/18/2007	966	<10	<10	966	487	<0.1	1,610	4,130
	9/17/2007	764	<10	<10	764	418	<0.1	1,840	3,940
	12/10/2007	630	<10	<10	630	238	<0.1	1,770	3,650
	3/10/2008	717	<10	<10	717	381	0.599	1,750	3,900
P-01	9/16/2008	898	<10	<10	898	374	<0.1	1,620	4,020
	3/10/2009	902	<10	<10	902	358	<0.1	1,640	3,930
	3/26/2007	215	<10	<10	215	40.5	0.153	1,330	2,410
	6/18/2007	221	<10	<10	221	51.3	0.304	1,430	2,440
	9/17/2007	272	<10	<10	272	86.5	0.234	1,540	2,600
P-02	12/10/2007	233	<10	<10	233	50.7	0.215	1,410	2,410
	3/10/2008	238	<10	<10	238	47.6	0.954	1,350	2,480
	9/16/2008	266	<10	<10	266	51.0	0.146	1,410	2,600
	3/10/2009	234	<10	<10	234	71.9	0.232	1,430	2,630
	3/27/2007	333	<10	<10	333	63.1	<0.1	2,000	3,520
P-03	6/19/2007	441	<10	<10	441	55.8	<0.1	1,770	3,380
	9/17/2007	398	<10	<10	398	55.8	<0.1	1,840	3,370
	12/10/2007	391	<10	<10	391	52.0	<0.1	1,930	3,370
	3/10/2008	358	<10	<10	358	66.5	<0.1	1,990	3,530
	9/16/2008	362	<10	<10	362	58.2	<0.1	1,980	3,520
P-03	3/10/2009	351	<10	<10	351	61.6	<0.1	2,020	3,500
	3/27/2007	475	<10	<10	475	324	<0.1	1,990	4,020
	6/18/2007	479	<10	<10	479	445	<0.1	2,030	4,120
	9/17/2007	460	<10	<10	460	514	<0.1	2,180	4,150
	12/10/2007	462	<10	<10	462	489	<0.1	2,120	4,090
P-03	3/10/2008	303	<10	<10	303	529	3.65	1,410	3,360
	9/16/2008	467	<10	<10	467	659	<0.1	2,030	4,840
	3/10/2009	469	<10	<10	469	702	<0.1	2,090	4,540

Table 4
Groundwater Inorganics Other Than Metal Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWWCC Standard (mg/L)		--	--	--	--	250	10	600	1000
P-04	3/27/2007	553	<10	<10	553	618	<0.1	1,860	4,450
	6/18/2007	493	<10	<10	493	570	<0.1	1,900	4,150
	9/17/2007	408	<10	<10	408	516	<0.1	1,810	3,980
	12/10/2007	435	<10	<10	435	514	<0.1	2,060	3,960
	3/10/2008	414	<10	<10	414	452	0.215	1,840	3,880
	9/16/2008	521	<10	<10	521	508	0.144	1,920	4,530
	3/10/2009	461	<10	<10	461	575	0.538	2,000	4,110
P-05	3/27/2007	290	<10	<10	290	87.3	<0.1	1,520	2,840
	6/18/2007	270	<10	<10	270	103	<0.1	1,600	2,800
	9/17/2007	298	<10	<10	298	97.1	<0.1	1,520	2,800
	12/10/2007	304	<10	<10	304	104	<0.1	1,700	2,860
	3/10/2008	287	<10	<10	287	103	<0.1	1,580	2,870
	9/16/2008	294	<10	<10	294	73.9	<0.1	1,550	2,800
	3/10/2009	272	<10	<10	272	70.0	<0.1	1,510	2,740

Notes

Alkalinity analyzed via EPA Method 310.1 by DHL Analytical Inc., Round Rock, Texas
Anions analyzed via EPA Method 300 by DHL Analytical Inc., Round Rock, Texas
TDS analyzed via EPA Method 160.1 by DHL Analytical Inc., Round Rock, Texas
All values reported in Milligrams per liter (mg/L, parts per million).
< values - Indicate the value is less than Method Detection Limit MDL.

Table 4a
Groundwater Inorganics Other Than Metal Quality Control Summary
Frontier Field Services - Empire Abo Gas Plant (GW-022)
257 Empire Road
Artesia, New Mexico

Wet Chemistry	Collection Date	Alkalinity, Bicarbonate	Alkalinity, Carbonate	Alkalinity, Hydroxide	Alkalinity, Total	Chloride	Nitrate	Sulfate	Total Dissolved Solids
NMWQCC Standard (mg/L)		--	--	--	--	250	10	600	1000
Duplicate-01 (P-02)	3/10/2008	357	<10	<10	357	67.4	<0.1	2,020	3,520
Duplicate-01 (MW-13)	9/16/2008	215	<10	<10	215	77.4	<0.1	1,650	2,740
Duplicate-01 (MW-13)	3/10/2009	170	<10	<10	170	51.9	0.136	1,540	2,560
Duplicate-01 (MW-16)	7/15/2009	224	<10	<10	224	1,480	4.95	7,480	14,400
Duplicate-02 (MW-02-16)	3/11/2008	786	<10	<10	786	195	<0.1	1,920	3,870
Duplicate-02 (MW-02-07)	9/17/2008	670	<10	<10	670	108	<0.1	1,460	3,030
Duplicate-02 (MW-12)	3/11/2009	371	<10	<10	371	96.4	<0.1	1,640	3,140
Equipment Rinse	3/11/2008	<10	<10	<10	<10	<0.3	<0.1	<1	<10
	3/10/2009	<10	<10	<10	<10	0.349	<0.1	<1	48.0
	3/11/2009	<10	<10	<10	<10	<0.3	<0.1	<1	20.0
Field Blank	3/10/2008	<10	<10	<10	<10	<0.3	<0.1	<1	<10
	9/17/2008	<10	<10	<10	<10	<0.3	<0.1	<1	26.0
	3/10/2009	<10	<10	<10	<10	0.336	<0.1	<1	21.0

Notes

Alkalinity analyzed via EPA Method 310.1 by DHL Analytical Inc., Round Rock, Texas
Anions analyzed via EPA Method 300 by DHL Analytical Inc., Round Rock, Texas
TDS analyzed via EPA Method 160.1 by DHL Analytical Inc., Round Rock, Texas
All values reported in Milligrams per liter (mg/L, parts per million).
< values - indicate the value is less than Method Detection Limit MDL.

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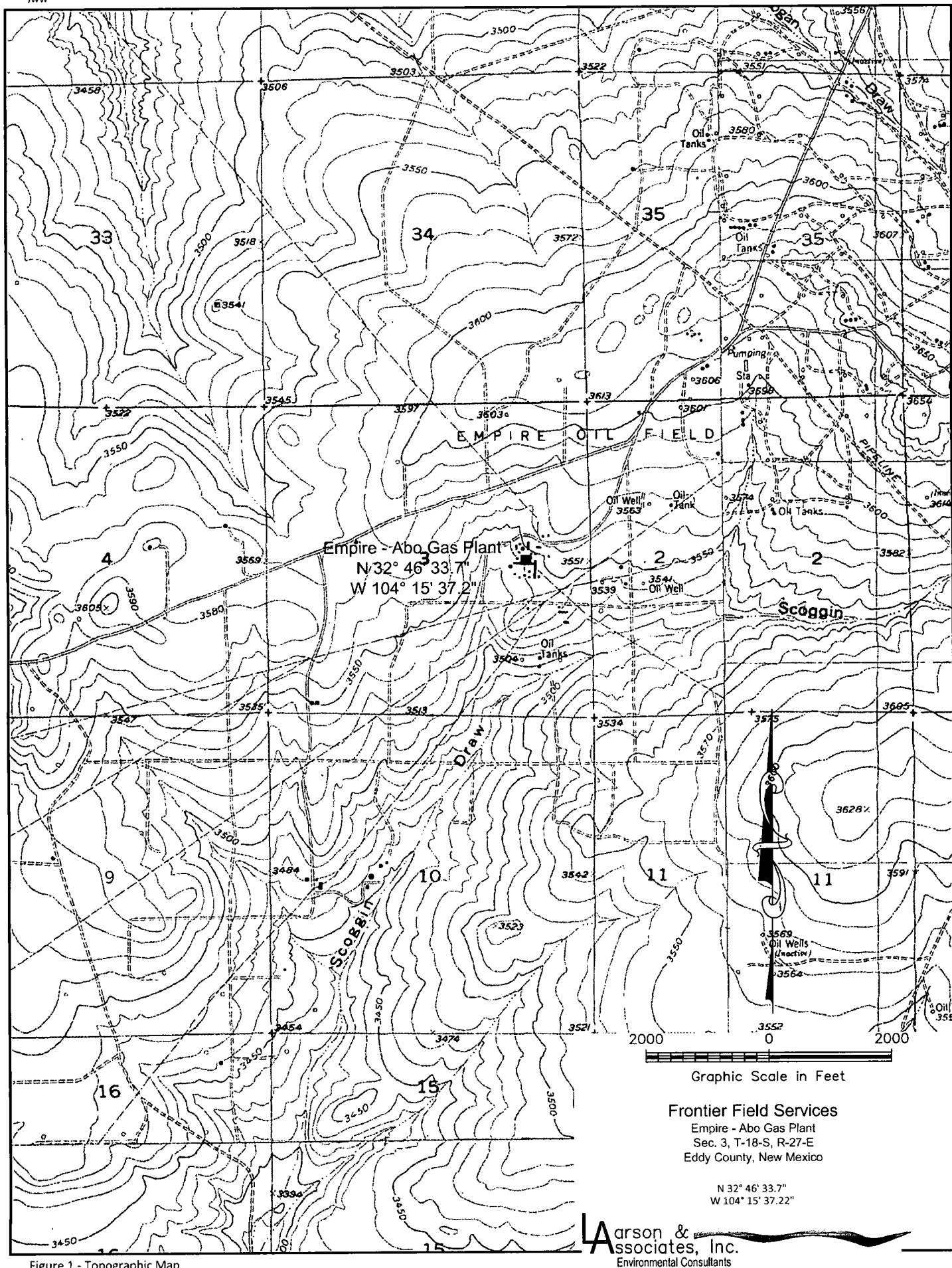
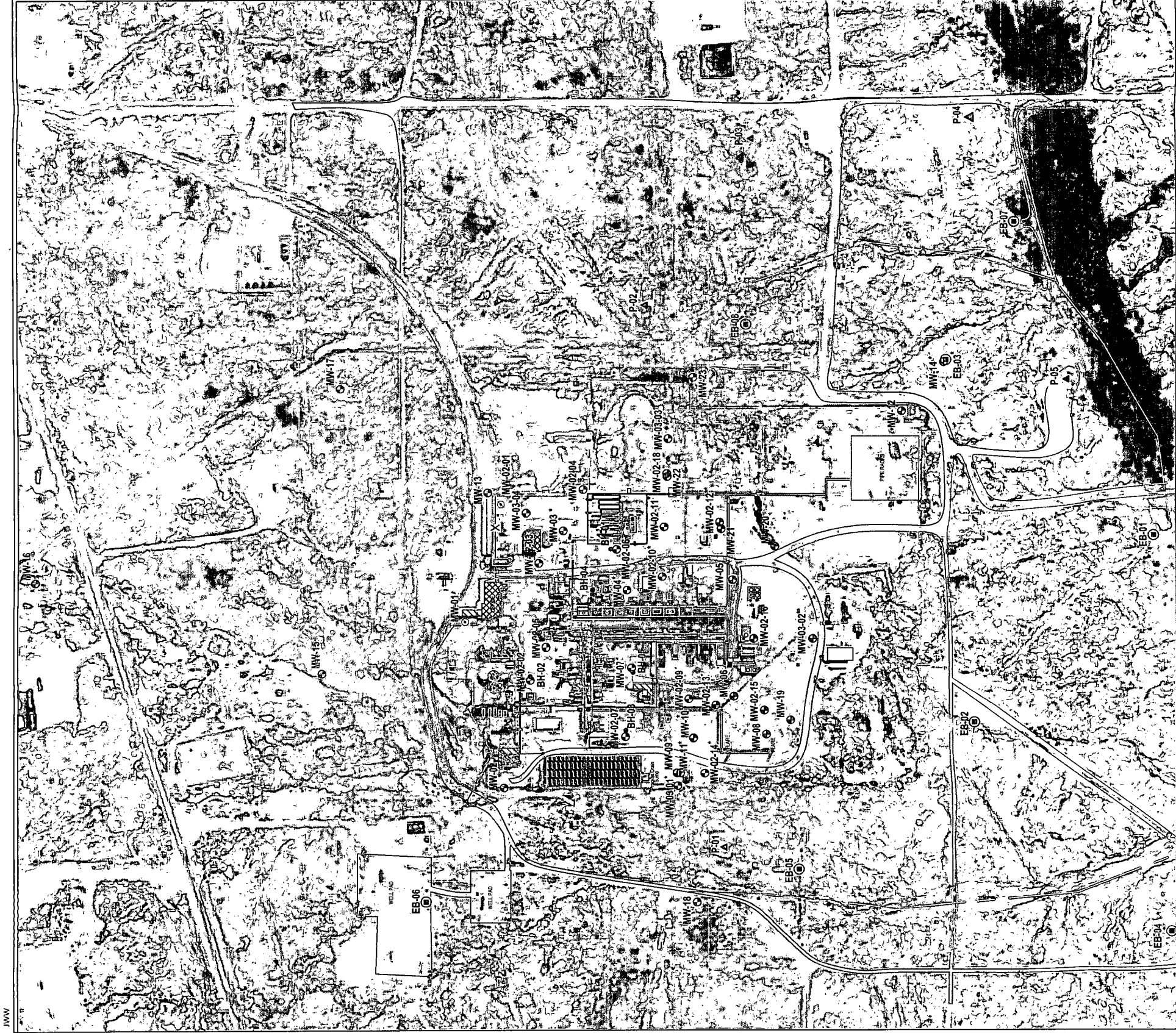


Figure 1 - Topographic Map



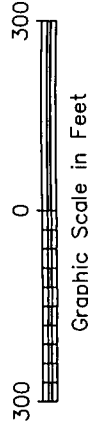
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Figure 2 - Aerial Map

LEGEND

- MW-01 - Plugged And Abandoned Monitoring Well Location
- MW-03 - Monitoring Well Location
- P-01 - Piezometer (Fluid Level) Location
- EB-03 - Monitoring Well Location
- * - Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity
- ** - Hydrocarbon Emulsion Present In Well
- X- - Fence
- - - - - Draw
- - - - - Roads
- - - - - Property Line

DESCRIPTION	NORTHINGS (N)	EASTING (E)	LATITUDE	LONGITUDE	ELEVATION TOP OF CONCRETE PAD	ELEVATION NATURAL GROUND
MW-02	646,317.1	522,066.1	32°46'36.47" N	104°15'41.54" W	3548.19	3545.52
MW-02-02	646,237.4	522,394.6	32°46'35.68" N	104°15'37.69" W	3552.26	3549.3
MW-02-03	646,211.5	522,753.7	32°46'35.42" N	104°15'33.49" W	3556.03	3553.37
MW-02-04	646,079.3	522,976.0	32°46'34.11" N	104°15'30.89" W	3553.79	3550.9
MW-02-05	646,90.4	522,497.2	32°46'35.21" N	104°15'36.49" W	3552.69	3550.14
MW-02-06	645,978.8	522,794.7	32°46'33.12" N	104°15'33.01" W	3550.82	3548.3
MW-02-07	645,954.0	522,221.8	32°46'32.87" N	104°15'39.72" W	3547.00	3544.28
MW-02-08	645,764.0	522,336.9	32°46'30.96" N	104°15'38.37" W	3546.52	3543.72
MW-02-10	645,842.8	522,711.8	32°46'31.77" N	104°15'33.98" W	3548.40	3545.4
MW-02-11	645,837.0	522,862.1	32°46'31.71" N	104°15'32.22" W	3544.12	3544.0
MW-02-12	645,870.8	522,876.3	32°46'30.07" N	104°15'32.06" W	3543.32	3540.96
MW-02-13	645,882.6	522,318.6	32°46'30.19" N	104°15'38.99" W	3545.99	3542.99
MW-02-14	645,16.2	522,110.4	32°46'30.52" N	104°15'41.03" W	3544.53	3541.3
MW-02-15	645,538.6	522,202.8	32°46'28.76" N	104°15'38.78" W	3543.28	3540.99
MW-02-16	645,567.8	522,524.6	32°46'29.05" N	104°15'38.18" W	3544.24	3541.36
MW-02-18	645,828.9	523,023.2	32°46'31.63" N	104°15'30.33" W	3545.70	3542.85
MW-03	646,138.4	522,851.3	32°46'34.70" N	104°15'32.35" W	3555.30	3552.66
MW-03-01	645,797.3	522,071.7	32°46'31.32" N	104°15'41.48" W	3542.56	3539.9
MW-03-02	645,392.6	522,921.5	32°46'27.32" N	104°15'36.21" W	3541.08	3538.68
MW-03-03	645,825.2	523,127.9	32°46'31.59" N	104°15'29.11" W	3544.72	3542.3
MW-03-04	645,248.7	522,905.0	32°46'35.80" N	104°15'31.72" W	3558.45	3556.02
MW-04	645,948.1	522,670.7	32°46'32.81" N	104°15'34.46" W	3550.98	3548.13
MW-05	645,633.0	522,701.7	32°46'29.69" N	104°15'34.10" W	3543.77	3540.79
MW-06	645,632.2	522,344.7	32°46'29.66" N	104°15'38.28" W	3544.50	3541.93
MW-07	645,934.3	522,433.1	32°46'32.68" N	104°15'37.25" W	3548.49	3546.26
MW-08	645,532.1	522,229.0	32°46'28.70" N	104°15'39.64" W	3543.73	3540.99
MW-09	645,799.3	522,110.7	32°46'31.34" N	104°15'41.02" W	3542.82	3540.21
MW-10	645,750.3	522,217.3	32°46'30.86" N	104°15'39.78" W	3544.44	3541.93
MW-11	645,789.1	522,110.0	32°46'31.24" N	104°15'41.03" W	3542.73	3540.40
MW-12	645,127.5	523,211.3	32°46'24.66" N	104°15'28.14" W	3525.26	3522.6
MW-13	645,584.9	522,965.9	32°46'36.94" N	104°15'31.00" W	3561.40	3558.71
MW-14	645,005.2	523,358.2	32°46'23.48" N	104°15'26.42" W	3520.32	3517.7
MW-15	646,860.1	522,416.5	32°46'41.84" N	104°15'37.43" W	3562.45	3559.91
MW-16	647,718.3	522,695.8	32°46'50.33" N	104°15'34.15" W	3585.46	3582.87
MW-17	646,804.7	523,280.9	32°46'41.29" N	104°15'27.31" W	3570.84	3568.0
MW-18	645,739.4	521,718.8	32°46'30.75" N	104°15'45.61" W	3532.63	3529.7
MW-19	645,460.3	522,272.4	32°46'27.99" N	104°15'39.13" W	3543.34	3540.6
MW-20	645,596.5	522,802.6	32°46'28.44" N	104°15'32.92" W	3541.47	3538.89
MW-21	645,668.8	522,886.0	32°46'30.05" N	104°15'32.18" W	3543.15	3540.82
MW-22	645,628.3	523,014.0	32°46'31.63" N	104°15'30.44" W	3545.87	3543.16
MW-23	645,750.5	523,314.0	32°46'30.85" N	104°15'26.93" W	3542.21	3539.2
P-01	645,660.5	521,884.9	32°46'29.97" N	104°15'43.67" W	3530.21	3528.08
P-02	645,895.5	523,533.0	32°46'32.29" N	104°15'24.36" W	3544.73	3542.47
P-03	645,977.5	524,036.9	32°46'29.14" N	104°15'18.46" W	3538.83	3534.4
P-04	644,922.9	524,101.6	32°46'22.66" N	104°15'17.71" W	3515.77	3513.5
P-05	644,637.8	523,307.2	32°46'19.84" N	104°15'27.02" W	3507.48	3504.9
EB-01	644,375.6	522,834.9	32°46'17.25" N	104°15'32.55" W	3492.15	3491.53
EB-02	644,910.9	522,265.5	32°46'22.59" N	104°15'39.22" W	3525.34	3522.65
EB-03	644,995.4	523,366.4	32°46'23.38" N	104°15'26.32" W	3521.05	3517.83
EB-04	644,322.3	521,630.7	32°46'16.73" N	104°15'46.66" W	3508.38	3505.64
EB-05	645,435.1	521,818.6	32°46'27.74" N	104°15'44.45" W	3526.61	3523.81
EB-06	646,550.9	521,720.8	32°46'38.78" N	104°15'45.58" W	3556.63	3555.6
EB-07	644,792.5	523,783.0	32°46'21.37" N	104°15'21.44" W	3503.97	3501.3
EB-08	645,591.3	523,474.8	32°46'29.28" N	104°15'25.05" W	3537.9	3533.8
EB-11	645,997.0	522,795.1	32°46'33.30" N	104°15'33.01" W	3537.07	3533.88
EB-12	646,238.3	522,402.3	32°46'35.69" N	104°15'37.60" W	3549.4	3546.8
EB-13	645,953.4	522,231.2	32°46'32.87" N	104°15'39.61" W	3544.3	3541.3
EB-14	646,051.7	522,672.3	32°46'33.84" N	104°15'34.44" W	3549.9	3546.0
EB-15	645,932.6	522,426.0	32°46'32.66" N	104°15'37.33" W	3543.9	3540.0
A-1	645,054.0	522,868.6	32°46'23.96" N	104°15'32.15" W	3523.9	3523.9
E-1	646,924.6	522,860.6	32°46'42.46" N	104°15'31.06" W	3547.6	3547.6
MW-16 Plant	646,418.1	522,053.3	32°46'37.47" N	104°15'41.67" W	3547.6	3547.6
MW-17 Plant	646,404.9	523,372.0	32°46'37.33" N	104°15'26.25" W	3557.7	3557.7
MW-18 Plant	644,798.8	523,396.3	32°46'21.44" N	104°15'25.97" W	3507.9	3507.9
SWC Plant	644,622.3	522,077.2	32°46'21.68" N	104°15'41.42" W	3517.5	3517.5



FRONTIER FIELD SERVICES, LLC

EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

Larson &
Associates, Inc.
Environmental Consultants



Figure 4 - Location Storage, Disposal, and Process Areas

MW-16

LEGEND

- Plugged And Abandoned Monitoring Well Location
- Monitoring Well Location and Groundwater Potentiometric Surface Elevation, Feet AMSL, September 15, 2008
- Piezometer (Fluid Level) Location and Groundwater Potentiometric Surface Elevation, Feet AMSL, September 15, 2008
- Monitoring Well Location and Groundwater Potentiometric Surface Elevation, Feet AMSL, September 15, 2008
- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity
- Hydrocarbon Emulsion Present In Well
- Contour of Groundwater Potentiometric Surface Elevation, Feet AMSL, September 15, 2008

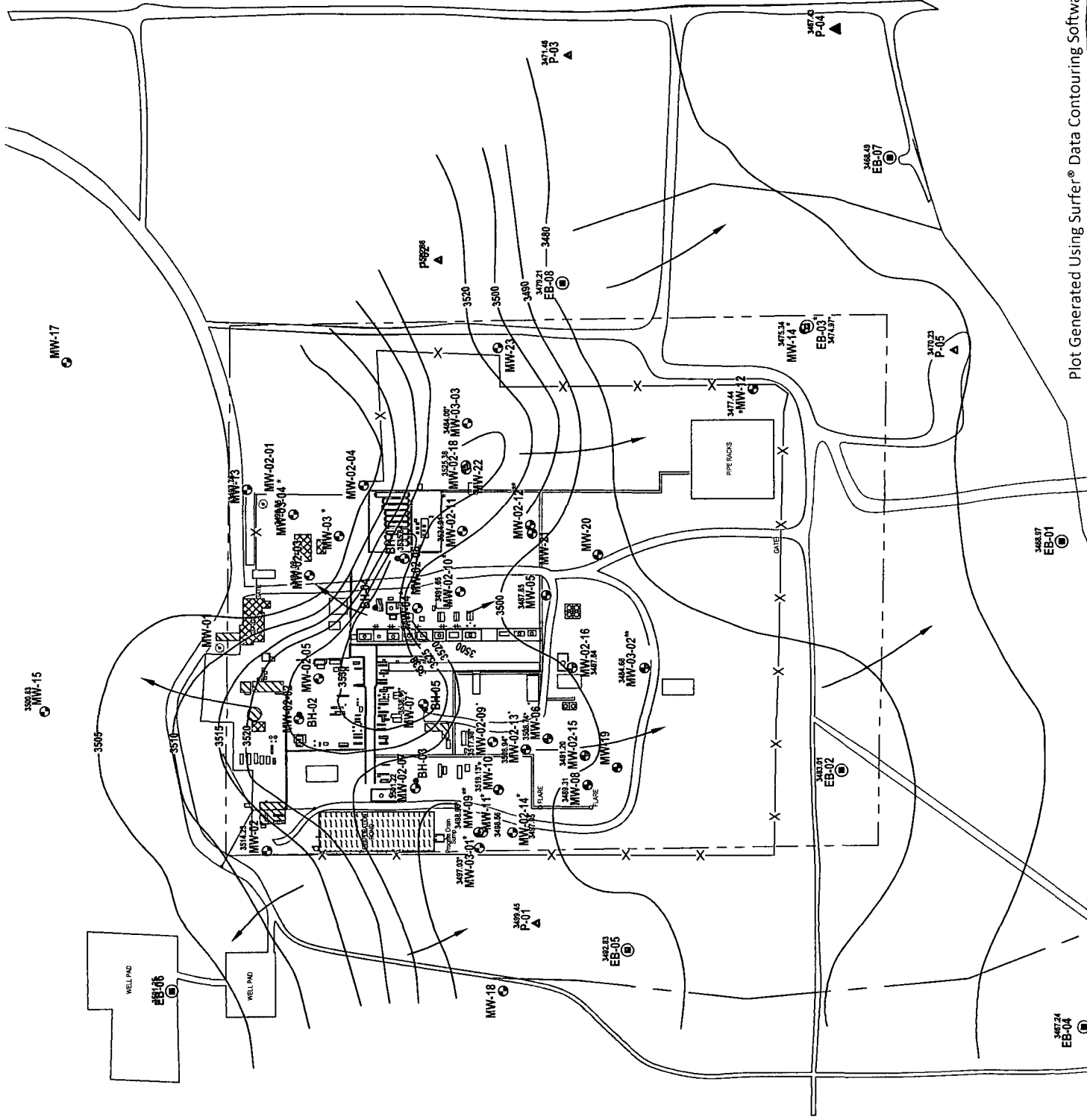
X ——— - Fence

————— - Draw

————— - Roads

————— - Property Line

————— - Groundwater Flow



DESCRIPTION	NORTHING (Y)	EASTING (X)	LATITUDE	LONGITUDE	ELEVATION TOP OF CONCRETE CASING	ELEVATION NATURAL PAD	ELEVATION GROUND
MW-02	646,317.1	522,086.1	32°46'36.47" N	104°15'41.54" W	3548.19'	3545.52'	3545.3'
MW-02-02	646,237.4	522,394.6	32°46'35.68" N	104°15'37.69" W	3552.26'	3549.56'	3549.3'
MW-02-03	646,211.5	522,753.7	32°46'35.42" N	104°15'33.49" W	3556.03'	3553.0'	3553.0'
MW-02-04	646,079.3	522,976.0	32°46'34.11" N	104°15'30.89" W	3553.78'	3551.26'	3550.9'
MW-02-05	646,190.4	522,487.2	32°46'35.21" N	104°15'36.49" W	3552.68'	3550.14'	3549.8'
MW-02-06	646,978.8	522,794.7	32°46'33.12" N	104°15'33.01" W	3550.82'	3548.53'	3548.3'
MW-02-07	645,954.0	522,221.8	32°46'32.87" N	104°15'39.72" W	3547.00'	3544.2'	3544.2'
MW-02-09	645,984.0	522,336.9	32°46'30.99" N	104°15'38.37" W	3543.72'	3543.72'	3543.5'
MW-02-10	645,942.8	522,711.8	32°46'31.77" N	104°15'33.98" W	3548.40'	3545.80'	3545.4'
MW-02-11	645,837.0	522,862.1	32°46'31.71" N	104°15'32.06" W	3546.79'	3544.12'	3544.0'
MW-02-12	645,670.8	522,876.3	32°46'30.07" N	104°15'32.06" W	3543.32'	3540.56'	3540.3'
MW-02-13	645,682.6	522,318.6	32°46'30.19" N	104°15'36.59" W	3545.59'	3542.99'	3542.7'
MW-02-14	645,716.2	522,110.4	32°46'30.52" N	104°15'41.03" W	3544.53'	3541.63'	3541.3'
MW-02-15	645,338.6	522,302.8	32°46'28.76" N	104°15'38.78" W	3543.28'	3540.58'	3540.2'
MW-02-16	645,367.8	522,524.6	32°46'29.05" N	104°15'36.18" W	3544.24'	3541.36'	3541.0'
MW-03	645,948.1	522,670.7	32°46'32.81" N	104°15'34.46" W	3550.99'	3548.13'	3547.8'
MW-03-01	645,397.3	522,071.7	32°46'31.32" N	104°15'41.48" W	3545.30'	3542.66'	3542.4'
MW-03-02	645,392.6	522,521.5	32°46'27.32" N	104°15'36.21" W	3544.85'	3542.85'	3542.6'
MW-03-03	645,825.2	523,127.9	32°46'31.59" N	104°15'29.11" W	3544.08'	3538.68'	3538.6'
MW-03-04	646,249.7	522,905.0	32°46'35.80" N	104°15'31.72" W	3558.45'	3556.02'	3555.7'
MW-04	645,948.1	522,670.7	32°46'32.81" N	104°15'34.46" W	3550.99'	3548.13'	3547.8'
MW-05	645,837.0	522,711.8	32°46'31.77" N	104°15'33.98" W	3548.40'	3545.80'	3545.4'
MW-06	645,828.2	522,344.7	32°46'29.66" N	104°15'38.28" W	3544.50'	3541.93'	3541.8'
MW-07	645,934.3	522,433.1	32°46'32.68" N	104°15'37.25" W	3546.49'	3546.26'	3546.0'
MW-08	645,532.1	522,229.0	32°46'28.70" N	104°15'39.84" W	3543.73'	3540.99'	3540.5'
MW-09	645,799.3	522,110.7	32°46'31.34" N	104°15'41.02" W	3542.82'	3540.21'	3540.4'
MW-10	645,789.1	522,217.3	32°46'30.86" N	104°15'39.78" W	3544.44'	3541.93'	3541.8'
MW-11	645,789.1	522,110.0	32°46'31.24" N	104°15'41.03" W	3540.40'	3540.40'	3540.2'
MW-12	645,127.5	523,211.3	32°46'24.69" N	104°15'28.14" W	3525.25'	3522.92'	3522.6'
MW-13	646,364.9	522,965.9	32°46'36.94" N	104°15'31.00" W	3561.40'	3558.71'	3558.5'
MW-14	645,085.2	523,398.2	32°46'23.48" N	104°15'26.42" W	3520.32'	3517.94'	3517.7'
MW-15	646,860.1	522,416.5	32°46'41.84" N	104°15'37.43" W	3562.45'	3559.91'	3559.7'
MW-16	647,718.3	522,695.8	32°46'50.33" N	104°15'34.15" W	3585.45'	3582.87'	3582.6'
MW-17	646,804.7	523,280.9	32°46'41.25" N	104°15'27.31" W	3570.84'	3568.18'	3568.0'
MW-18	645,739.4	521,718.8	32°46'30.75" N	104°15'45.51" W	3523.63'	3520.98'	3520.7'
MW-19	645,480.3	522,272.4	32°46'27.99" N	104°15'39.13" W	3543.34'	3540.6'	3540.6'
MW-20	645,868.8	522,802.6	32°46'28.44" N	104°15'32.92" W	3541.47'	3538.89'	3538.7'
MW-21	645,868.8	522,866.0	32°46'30.05" N	104°15'32.18" W	3543.15'	3540.52'	3540.2'
MW-22	645,828.3	523,014.0	32°46'31.63" N	104°15'30.44" W	3545.87'	3543.16'	3542.9'
MW-23	645,750.5	523,314.0	32°46'29.97" N	104°15'43.67" W	3530.21'	3528.08'	3527.9'
P-01	645,660.5	523,314.0	32°46'30.85" N	104°15'26.93" W	3530.21'	3528.08'	3527.9'
P-02	645,895.5	523,533.0	32°46'32.29" N	104°15'24.36" W	3544.73'	3542.47'	3542.3'
P-03	645,577.5	524,036.9	32°46'28.14" N	104°15'18.46" W	3536.83'	3534.67'	3534.4'
P-04	644,922.9	524,101.6	32°46'22.66" N	104°15'17.71" W	3515.77'	3513.78'	3513.5'
P-05	644,637.8	523,307.2	32°46'19.84" N	104°15'27.02" W	3507.48'	3505.25'	3504.9'
EB-01	644,375.6	522,834.9	32°46'17.25" N	104°15'32.55" W	3492.15'	3491.53'	3491.5'
EB-02	644,910.9	522,265.5	32°46'22.55" N	104°15'39.22" W	3525.34'	3522.65'	3522.6'
EB-03	644,995.4	523,366.4	32°46'23.38" N	104°15'26.32" W	3521.05'	3517.83'	3517.8'
EB-04	644,322.3	521,630.7	32°46'16.73" N	104°15'46.68" W	3508.38'	3505.64'	3505.3'
EB-05	645,435.1	521,818.6	32°46'27.74" N	104°15'44.45" W	3526.61'	3523.81'	3523.7'
EB-06	646,550.9	521,720.8	32°46'38.78" N	104°15'45.58" W	3556.63'	3553.92'	3553.6'
EB-07	644,792.5	523,783.0	32°46'21.37" N	104°15'21.44" W	3503.97'	3501.60'	3501.3'
BH-1	645,997.0	522,474.8	32°46'29.28" N	104°15'25.05" W	3537.07'	3533.88'	3533.8'
BH-2	646,238.3	522,231.2	32°46'35.69" N	104°15'37.60" W			
BH-3	645,953.4	522,231.2	32°46'32.87" N	104°15'39.61" W			
BH-4	646,051.7	522,672.3	32°46'33.84" N	104°15'34.44" W			
BH-5	645,932.6	522,426.0	32°46'32.66" N	104°15'37.33" W			
A-1	645,054.0	522,868.6	32°46'23.96" N	104°15'32.15" W			
E-1	646,923.6	522,960.6	32°46'42.46" N	104°15'31.06" W			
NWc Plant	646,418.1	522,055.3	32°46'37.47" N	104°15'41.67" W			
NEc Plant	646,404.9	523,372.0	32°46'37.33" N	104°15'26.25" W			
SEc Plant	644,798.8	523,396.3	32°46'21.44" N	104°15'25.97" W			
SWc Plant	644,822.3	522,077.2	32°46'21.68" N	104°15'41.42" W			

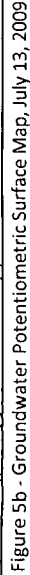
FRONTIER FIELD SERVICES, LLC

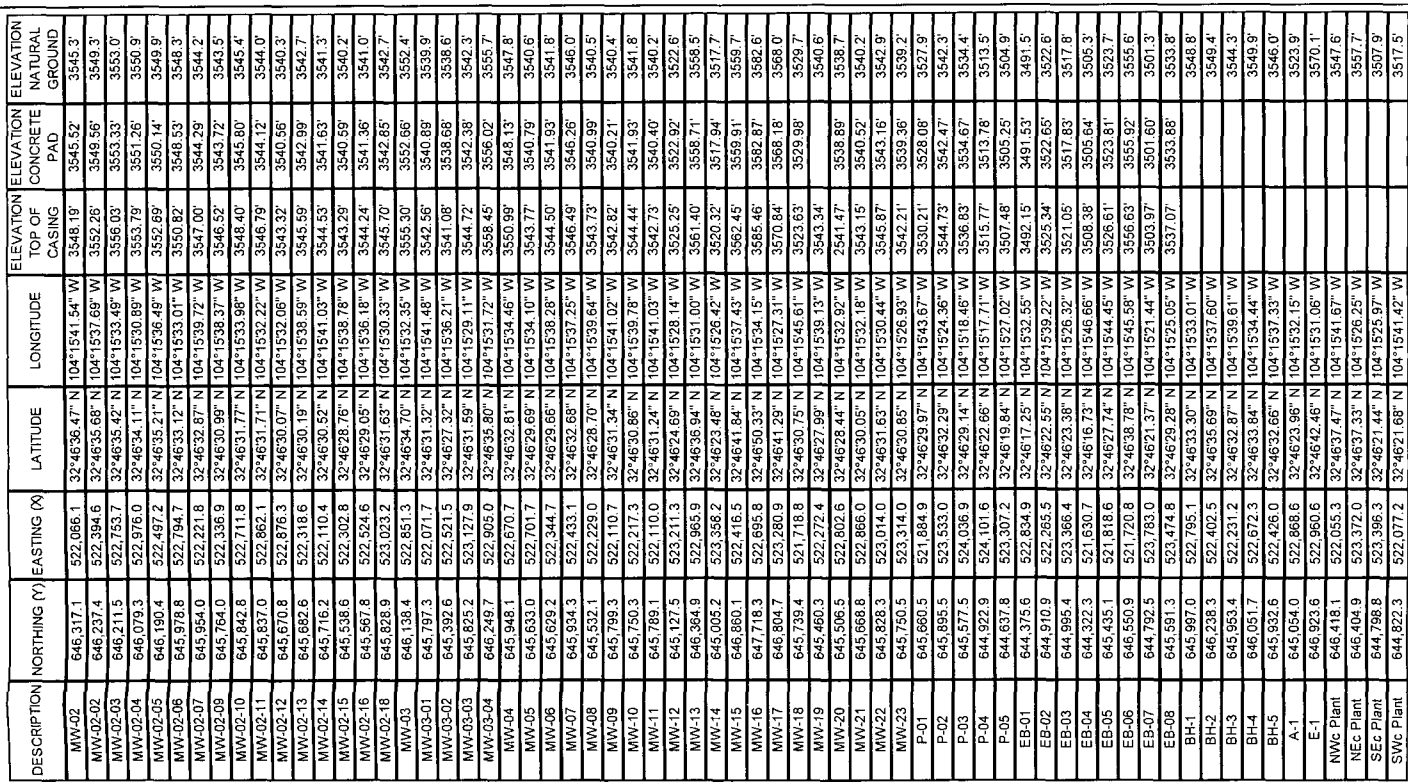
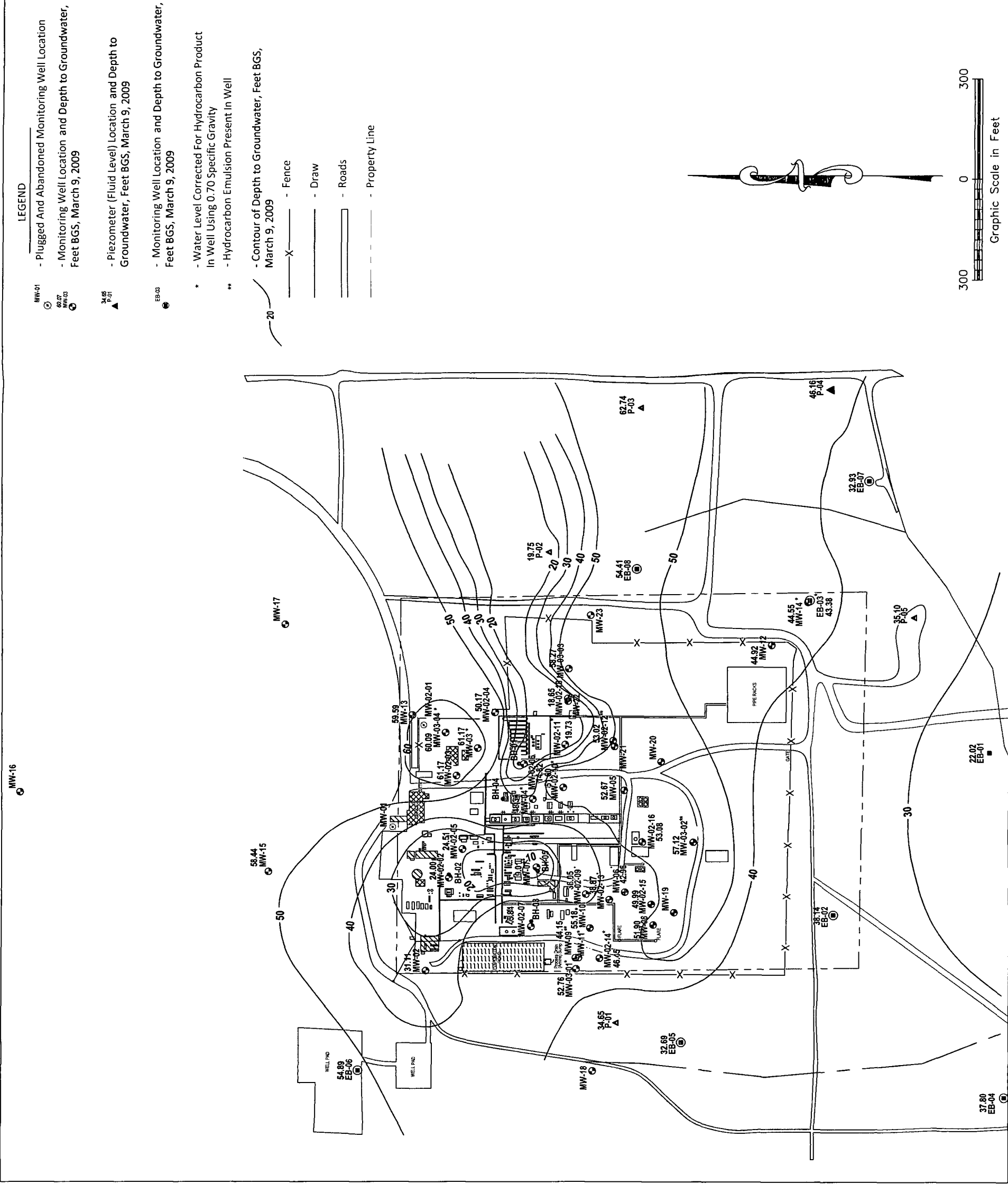
EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

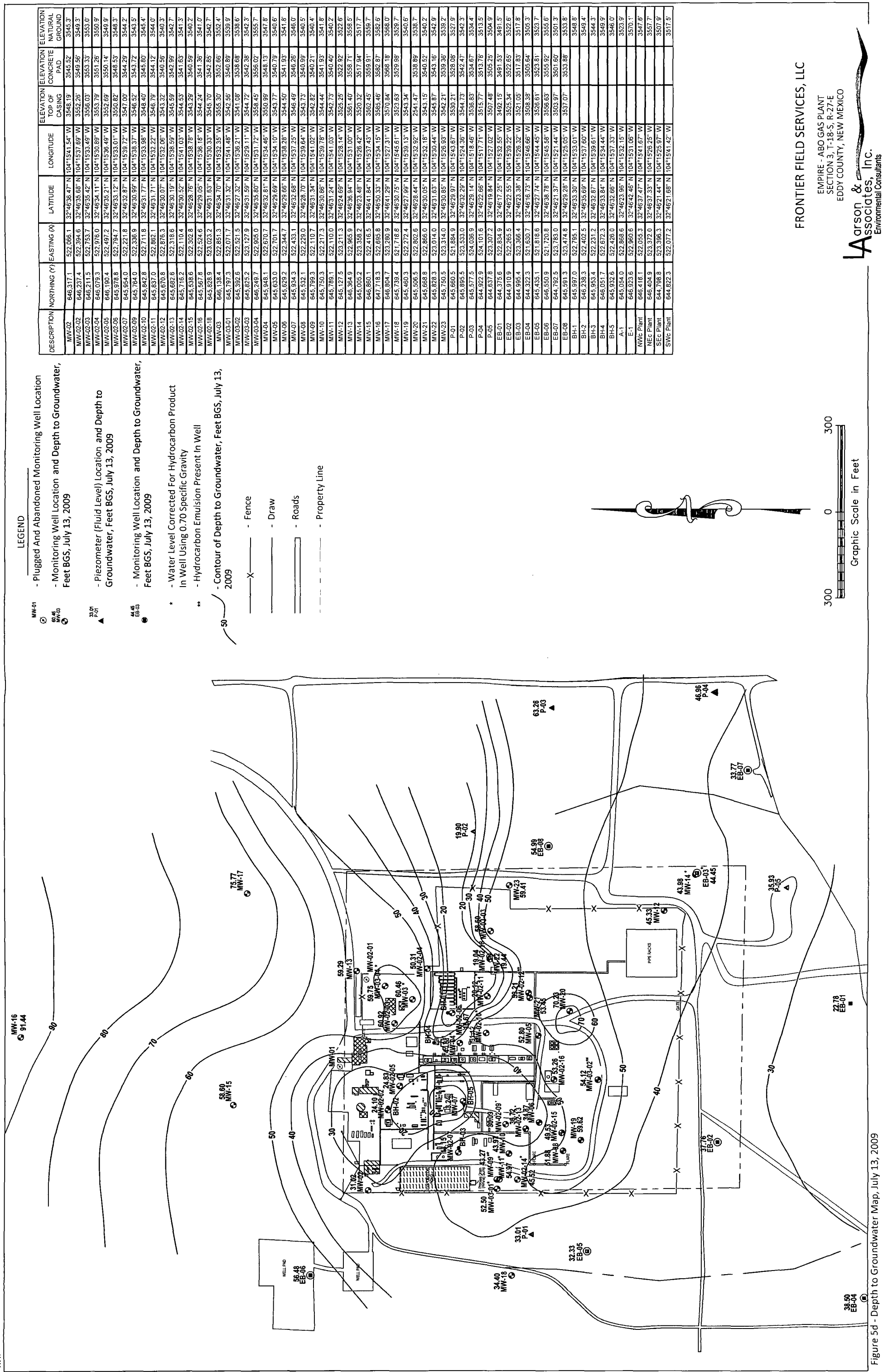
LA
Associates, Inc.
Environmental Consultants

Plot Generated Using Surfer® Data Contouring Software

Figure 5a - Groundwater Gradient Map September 15, 2008







- Plugged And Abandoned Monitoring Well Location

- Monitoring Well Location and Apparent PSH Thickness, Feet, September 15, 2008

- Piezometer (Fluid Level) Location

- Monitoring Well Location and Apparent PSH Thickness, Feet, September 15, 2008

- Water Level Corrected For Hydrocarbon Product
In Well Using 0.70 Specific Gravity

- ### - Hydrocarbon Emulsion Present In Well

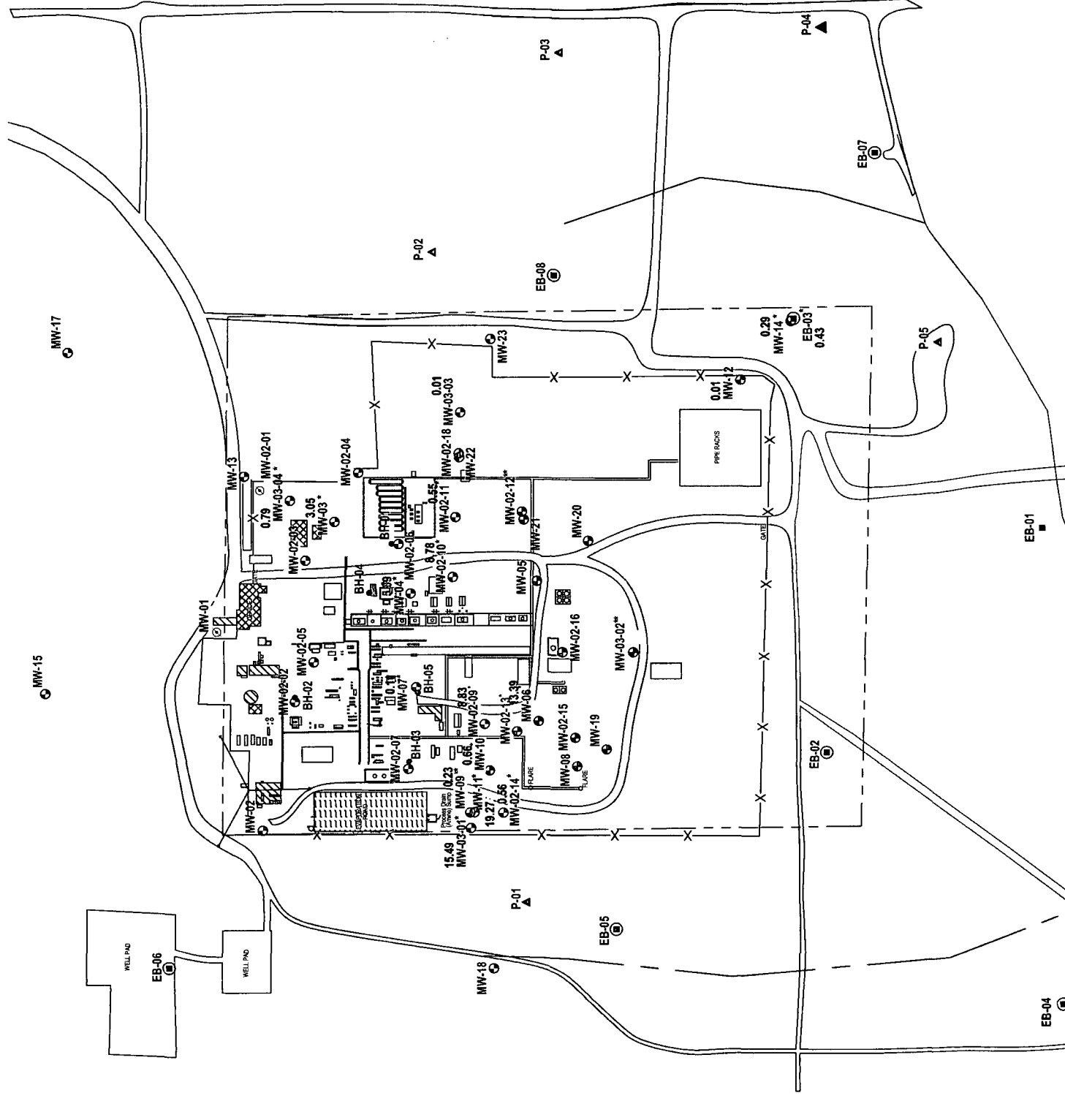
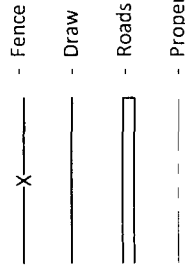
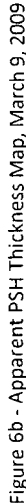


Figure 6a - Apparent PSH Thickness Map September 15, 2008

EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

LAarson &
Associates, Inc.
Environmental Consultants
EDDY COUNTY



- MW-01

MW-02
- P-01
- 1.67

EB-03
- *

- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity
- **

- Hydrocarbon Emulsion Present In Well

- Fence

- Draw

- Roads

- Property Line

LEGEND

- Plugged And Abandoned Monitoring Well Location
- Monitoring Well Location and Apparent PSH Thickness, Feet, July 13, 2009

- Piezometer (Fluid Level) Location

- Monitoring Well Location and Apparent PSH Thickness, Feet, July 13, 2009

- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity

- Hydrocarbon Emulsion Present In Well

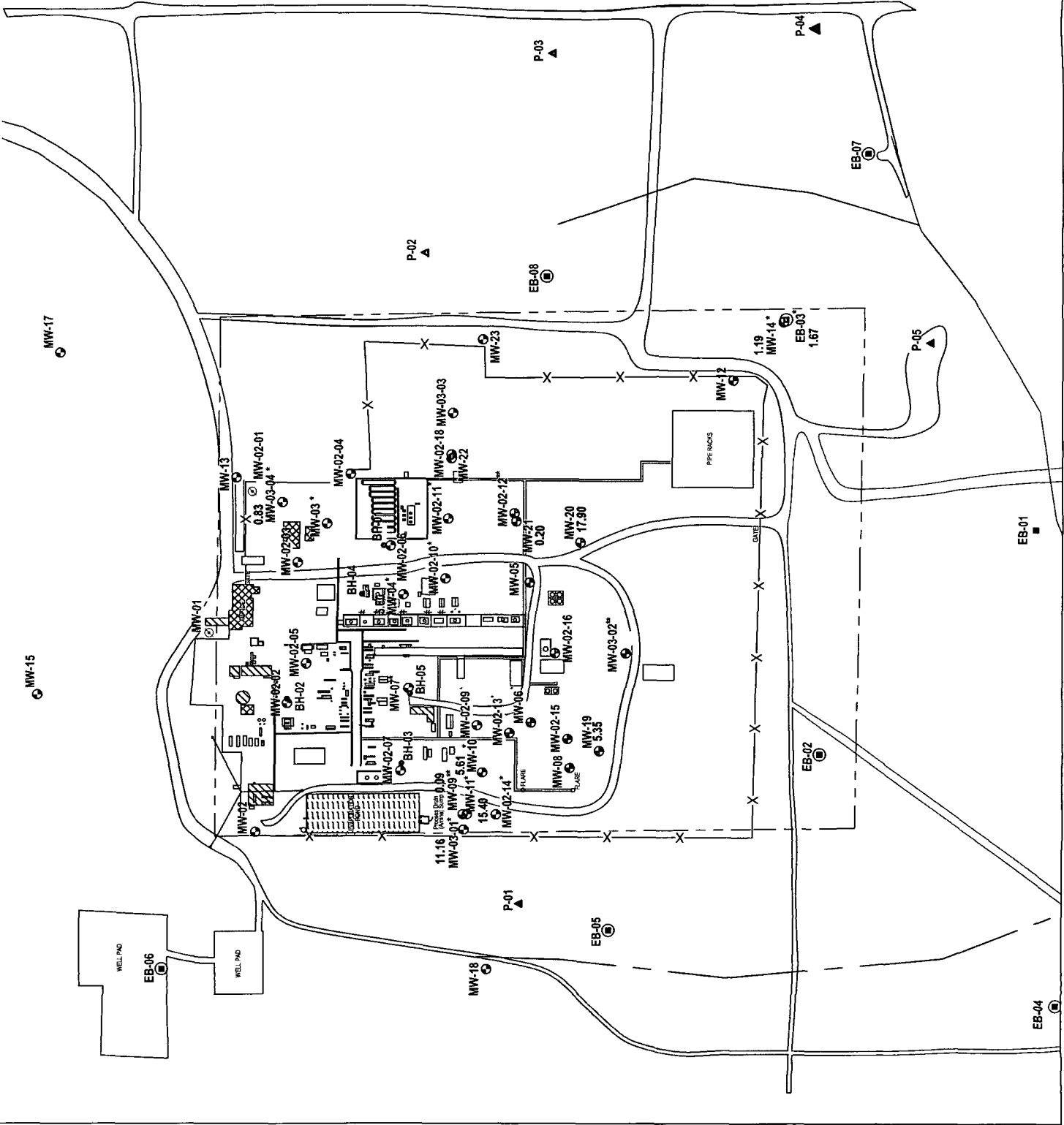


Figure 6c - Apparent PSH Thickness Map, July 13, 2009

DESCRIPTION	NORTHING (Y)	EASTING (X)	LATITUDE	LONGITUDE	ELEVATION TOP OF CASING	ELEVATION CONCRETE PAD	ELEVATION NATURAL GROUND
MW-02	646,317.1	522,066.1	32°46'36.47" N	104°1'541.54" W	3548.19	3545.52	3545.3
MW-02-02	646,237.4	522,394.6	32°46'35.66" N	104°1'537.69" W	3552.26	3549.56	3549.3
MW-02-03	646,211.5	522,753.7	32°46'35.42" N	104°1'533.49" W	3556.03	3553.33	3553.0
MW-02-04	646,079.3	522,978.0	32°46'34.11" N	104°1'530.89" W	3553.79	3551.26	3550.9
MW-02-05	646,190.4	522,487.2	32°46'35.21" N	104°1'536.49" W	3552.69	3550.14	3548.9
MW-02-06	645,978.8	522,794.7	32°46'33.12" N	104°1'533.01" W	3550.82	3548.53	3548.3
MW-02-07	645,954.0	522,221.8	32°46'32.87" N	104°1'539.72" W	3547.00	3544.29	3544.2
MW-02-09	645,764.0	522,336.9	32°46'30.99" N	104°1'538.37" W	3548.52	3543.72	3543.5
MW-02-10	645,842.8	522,711.8	32°46'31.77" N	104°1'533.98" W	3548.40	3545.80	3545.4
MW-02-11	645,637.0	522,862.1	32°46'31.71" N	104°1'532.22" W	3546.79	3544.12	3544.0
MW-02-12	645,670.8	522,876.3	32°46'30.07" N	104°1'532.06" W	3543.32	3540.56	3540.3
MW-02-13	645,682.6	522,318.6	32°46'30.19" N	104°1'538.59" W	3545.59	3542.99	3542.7
MW-02-14	645,716.2	522,110.4	32°46'30.52" N	104°1'541.03" W	3544.53	3541.63	3541.3
MW-02-15	645,538.6	522,302.8	32°46'28.76" N	104°1'538.78" W	3543.29	3540.59	3540.2
MW-02-16	645,567.6	522,524.6	32°46'29.05" N	104°1'536.18" W	3544.70	3541.36	3541.0
MW-02-18	645,828.9	523,023.2	32°46'31.63" N	104°1'530.33" W	3545.70	3542.85	3542.7
MW-03	646,138.4	522,861.3	32°46'34.70" N	104°1'532.35" W	3555.30	3552.66	3552.4
MW-03-01	645,797.3	522,071.7	32°46'31.32" N	104°1'541.48" W	3542.56	3540.89	3539.9
MW-03-02	645,392.6	522,521.5	32°46'27.32" N	104°1'536.21" W	3541.08	3538.68	3538.6
MW-03-03	645,825.2	523,127.9	32°46'31.58" N	104°1'529.11" W	3544.72	3542.38	3542.3
MW-03-04	646,249.7	522,905.0	32°46'35.80" N	104°1'531.72" W	3558.45	3556.02	3555.7
MW-04	645,948.1	522,670.7	32°46'32.81" N	104°1'534.46" W	3550.99	3548.13	3547.8
MW-05	645,633.0	522,701.7	32°46'29.69" N	104°1'534.10" W	3543.77	3540.73	3540.6
MW-06	645,629.2	522,344.7	32°46'29.66" N	104°1'538.28" W	3544.50	3541.93	3541.8
MW-07	645,934.3	522,433.1	32°46'32.68" N	104°1'537.25" W	3546.49	3546.26	3546.0
MW-08	645,532.1	522,229.0	32°46'28.70" N	104°1'539.64" W	3543.73	3540.99	3540.5
MW-09	645,993.3	522,110.7	32°46'31.34" N	104°1'541.02" W	3542.82	3540.21	3540.4
MW-10	645,750.3	522,217.3	32°46'30.86" N	104°1'539.78" W	3544.44	3541.93	3541.8
MW-11	645,789.1	522,110.0	32°46'31.24" N	104°1'541.03" W	3540.40	3540.73	3540.2
MW-12	645,127.5	523,211.3	32°46'24.69" N	104°1'528.14" W	3525.25	3522.92	3522.6
MW-13	646,364.9	522,965.9	32°46'36.94" N	104°1'531.00" W	3561.40	3558.71	3558.5
MW-14	645,005.2	523,358.2	32°46'23.48" N	104°1'526.42" W	3520.32	3517.94	3517.7
MW-15	646,860.1	522,416.5	32°46'41.84" N	104°1'537.43" W	3562.45	3559.91	3559.7
MW-16	647,718.3	522,895.8	32°46'50.33" N	104°1'534.15" W	3586.46	3582.87	3582.6
MW-17	646,804.7	523,280.9	32°46'41.29" N	104°1'527.31" W	3570.84	3568.18	3568.0
MW-18	645,739.4	521,718.8	32°46'30.75" N	104°1'545.61" W	3523.63	3523.98	3523.7
MW-19	645,460.3	522,272.4	32°46'27.99" N	104°1'539.13" W	3543.34	3540.6	3540.6
MW-20	645,506.5	522,802.6	32°46'28.44" N	104°1'532.92" W	2541.47	3538.89	3538.7
MW-21	645,668.8	522,866.0	32°46'30.05" N	104°1'532.18" W	3543.15	3540.52	3540.2
MW-22	645,928.3	523,014.0	32°46'31.63" N	104°1'530.44" W	3543.87	3543.16	3542.9
MW-23	645,750.5	523,314.0	32°46'30.85" N	104°1'526.93" W	3542.21	3539.36	3539.2
P-01	645,660.5	521,884.9	32°46'29.97" N	104°1'543.67" W	3530.21	3528.08	3527.9
P-02	645,895.5	523,533.0	32°46'32.29" N	104°1'524.36" W	3544.73	3542.47	3542.3
P-03	645,577.5	524,036.9	32°46'28.14" N	104°1'518.46" W	3538.83	3534.67	3534.4
P-04	644,922.9	524,101.6	32°46'22.66" N	104°1'517.71" W	3513.77	3513.78	3513.5
P-05	644,637.8	523,307.2	32°46'19.84" N	104°1'527.02" W	3507.48	3505.25	3504.9
EB-01	644,375.6	522,834.9	32°46'17.25" N	104°1'532.55" W	3492.15	3491.53	3491.5
EB-02	644,910.9	522,265.5	32°46'22.55" N	104°1'539.22" W	3525.34	3522.65	3522.6
EB-03	644,995.4	523,366.4	32°46'23.38" N	104°1'526.32" W	3521.05	3517.83	3517.8
EB-04	644,322.3	521,630.7	32°46'16.73" N	104°1'546.66" W	3508.38	3505.64	3505.3
EB-05	645,435.1	521,818.6	32°46'27.74" N	104°1'544.45" W	3528.81	3523.81	3523.7
EB-06	646,550.9	521,720.8	32°46'38.78" N	104°1'545.58" W	3556.63	3555.92	3555.6
EB-07	644,792.5	523,783.0	32°46'21.37" N	104°1'521.44" W	3503.97	3501.60	3501.3
EB-08	645,591.3	523,474.8	32°46'29.28" N	104°1'525.05" W	3556.63	3553.88	3553.8
BH-1	645,997.0	522,795.1	32°46'33.30" N	104°1'533.01" W	3548.4	3548.4	3548.4
BH-2	646,238.3	522,402.5	32°46'35.69" N	104°1'537.60" W	3548.4	3548.4	3548.4
BH-3	645,953.4	522,231.2	32°46'32.87" N	104°1'539.61" W	3544.3	3544.3	3544.3
BH-4	646,051.7	522,672.3	32°46'33.84" N	104°1'534.44" W	3549.9	3549.9	3549.9
BH-5	645,932.6	522,426.0	32°46'32.66" N	104°1'537.33" W	3546.0	3546.0	3546.0
A-1	645,054.0	522,868.6	32°46'23.96" N	104°1'532.15" W	3523.9	3523.9	3523.9
E-1	646,923.6	522,960.6	32°46'42.46" N	104°1'531.06" W	3570.1	3570.1	3570.1
NWc Plant	646,418.1	522,055.3	32°46'37.47" N	104°1'541.67" W	3547.6	3547.6	3547.6
NWc Plant	646,04.9	523,372.0	32°46'37.33" N	104°1'526.25" W	3557.7	3557.7	3557.7
SEC Plant	644,968.8	523,396.3	32°46'21.44" N	104°1'525.97" W	3507.9	3507.9	3507.9
SWc Plant	644,822.3	522,077.2	32°46'21.66" N	104°1'541.42" W	3517.5	3517.5	3517.5

MW-01

MW-03

0.0016
EB-01

<0.0008
EB-03

Legend

- Plugged And Abandoned Monitoring Well Location

- Monitoring Well Location and Benzene Concentration in Groundwater, mg/L, March 9, 2009 / July 15, 2009

- Piezometer (Fluid Level) Location and Benzene Concentration in Groundwater, mg/L, March 9, 2009 / July 15, 2009

- Monitoring Well Location and Benzene Concentration in Groundwater, mg/L, March 9, 2009 / July 15, 2009

- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity

- Hydrocarbon Emulsion Present In Well

- Less Than Method Detection Limit

- Fence

- Draw

- Roads

- Property Line

WOCC Human Health Standard: 0.01 mg/L

WOCC Human Health Standard: 0.01 mg/L

This figure is a Benzene Isocon Map showing the distribution of benzene concentrations in groundwater. The map includes several monitoring wells (MW-01 through MW-23) and piezometers (P-01 through P-05). Benzene concentrations are indicated by numerical values next to the well symbols, such as 0.0015 for MW-03 and 0.00115 for P-03. The map also shows property boundaries, roads, and other features like a well pad and a gate. A legend in the top left corner defines the symbols used for monitoring wells, piezometers, and benzene concentrations. A scale bar in the bottom right corner indicates distances in feet, ranging from 0 to 300. A north arrow is also present in the bottom right corner.

Figure 7b - Benzene Isocon Map, March and July 2009

FRONTIER FIELD SERVICES, LLC

EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S; R-27-E
EDDY COUNTY, NEW MEXICO

Larson &
Associates, Inc.
Environmental Consultants

MW-01 95.0 MW-03

- Plugged And Abandoned Monitoring Well Location
- Monitoring Well Location Chloride Concentration in Groundwater, mg/L, September 16, 2008

- Piezometer (Fluid Level) Location and Chloride Concentration in Groundwater, mg/L, September 16, 2008

- Monitoring Well Location Chloride Concentration in Groundwater, mg/L, September 16, 2008

- - Water Level Corrected For Hydrocarbon Product
In Well Using 0.70 Specific Gravity

- ### - Hydrocarbon Emulsion Present In Well

- Contour of Chloride Concentration in Groundwater, mg/L, September 16, 2008

- Fence
- Draw
- Roads
- Property Line

WQCC Domestic Water Quality Standard: 250 mg/L

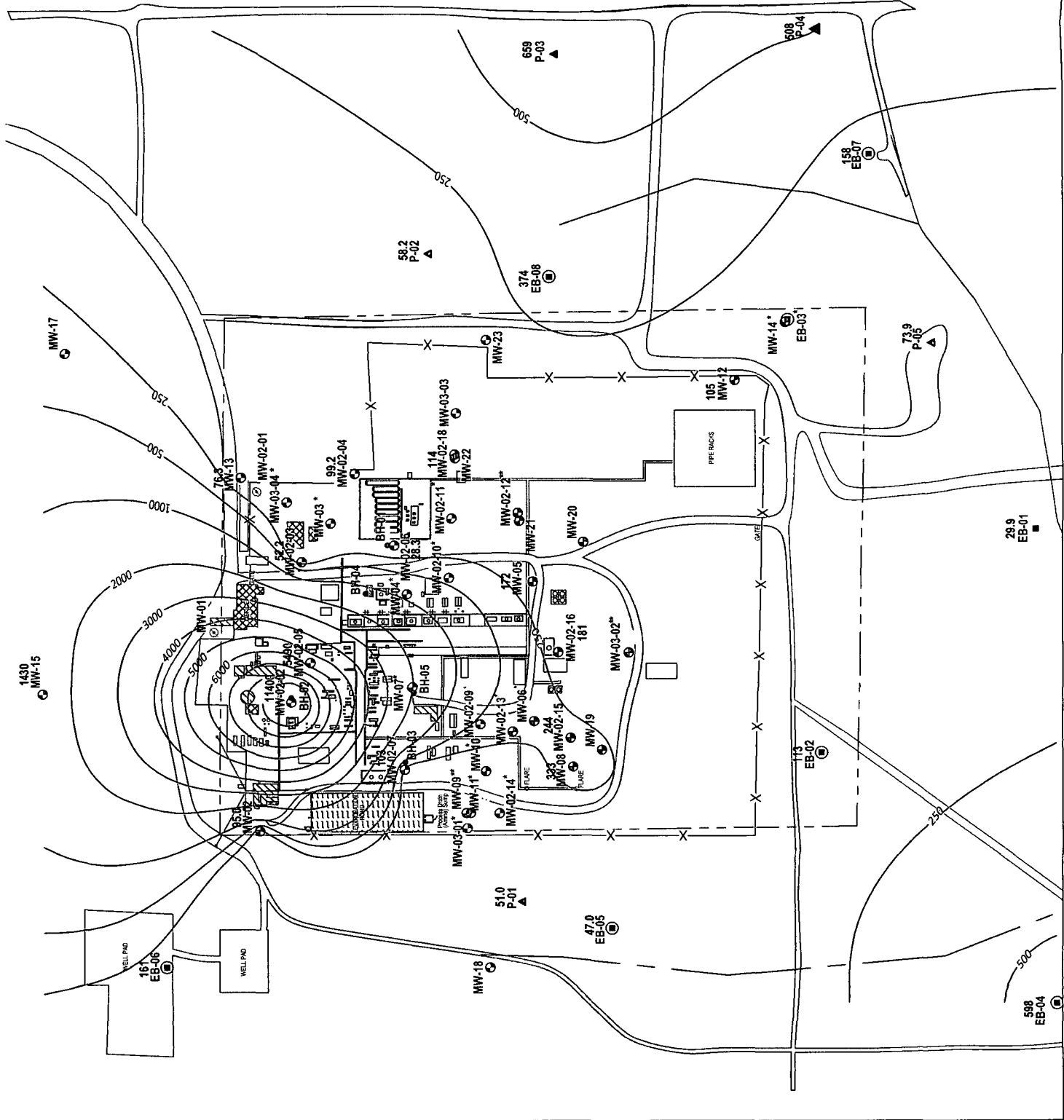


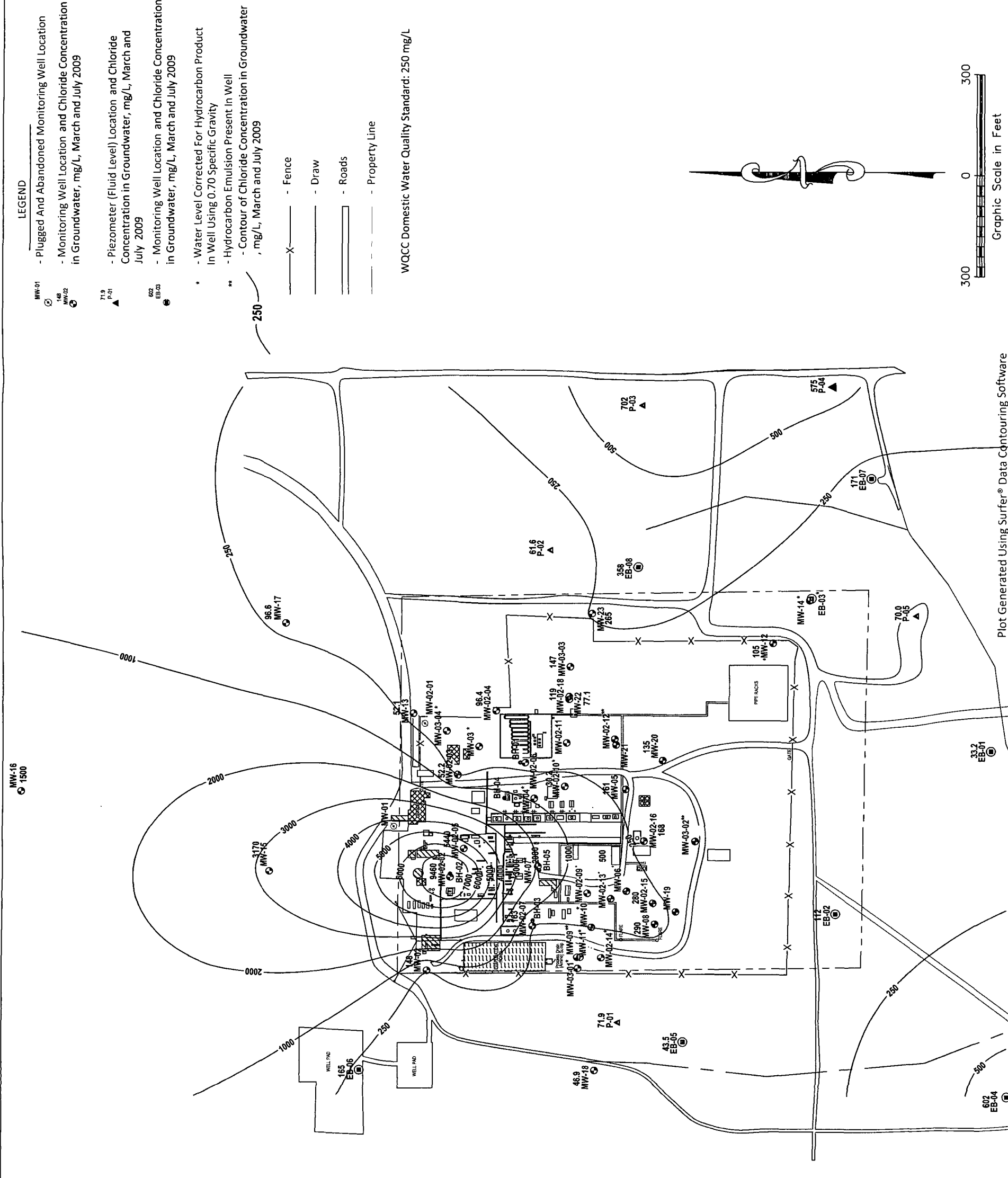
Figure 8a - Chloride Isocon Map September 2008

DESCRIPTION	NORTHING (Y)	EASTING (X)	LATITUDE	TOP OF CASING	ELEVATION CONCRETE PAD	ELEVATION NATURAL GROUND
MW-02	646.317.1	522.066.1	32°46'36.47" N	104°15'41.54" W	3548.19	3545.32
MW-02-02	646.237.4	522.394.6	32°46'35.68" N	104°15'37.69" W	3552.26	3549.56
MW-02-03	646.211.5	522.753.7	32°46'35.44" N	104°15'33.49" W	3556.03	3553.33
MW-02-04	646.079.3	522.976.0	32°46'35.11" N	104°15'30.89" W	3553.78	3550.9
MW-02-05	646.190.4	522.497.2	32°46'35.21" N	104°15'36.49" W	3552.89	3550.14
MW-02-06	645.978.8	522.784.7	32°46'32.18" N	104°15'33.01" W	3550.82	3548.53
MW-02-07	645.954.0	522.221.8	32°46'32.87" N	104°15'39.72" W	3547.07	3544.29
MW-02-09	645.764.0	522.336.9	32°46'30.99" N	104°15'38.37" W	3546.52	3543.72
MW-02-10	645.842.8	522.711.8	32°46'31.77" N	104°15'33.98" W	3548.40	3545.80
MW-02-11	645.837.0	522.862.1	32°46'31.71" N	104°15'32.22" W	3546.79	3544.12
MW-02-12	645.670.8	522.876.3	32°46'30.07" N	104°15'32.06" W	3545.39	3540.3
MW-02-13	645.682.6	522.318.6	32°46'30.19" N	104°15'38.59" W	3543.59	3542.96
MW-02-14	645.716.2	522.110.4	32°46'30.52" N	104°15'41.03" W	3544.53	3541.63
MW-02-15	645.567.8	522.302.8	32°46'29.76" N	104°15'38.78" W	3543.29	3540.2
MW-02-16	645.538.6	522.524.6	32°46'29.05" N	104°15'36.18" W	3544.24	3541.36
MW-02-18	645.828.9	523.023.2	32°46'31.63" N	104°15'30.33" W	3545.70	3542.85
MW-03	646.138.4	522.851.3	32°46'34.70" N	104°15'32.35" W	3555.30	3542.7
MW-03-01	645.797.3	522.071.7	32°46'34.32" N	104°15'41.48" W	3542.56	3539.9
MW-03-02	645.392.6	523.121.9	32°46'32.55" N	104°15'36.21" W	3544.18	3538.68
MW-03-03	645.825.2	523.127.9	32°46'31.59" N	104°15'29.11" W	3544.72	3542.38
MW-03-04	646.249.7	522.905.0	32°46'35.80" N	104°15'31.72" W	3558.45	3556.02
MW-04	645.948.1	522.670.7	32°46'32.89" N	104°15'34.48" W	3550.99	3548.13
MW-05	645.633.0	522.701.3	32°46'29.69" N	104°15'34.10" W	3543.77	3540.79
MW-06	645.629.2	522.344.7	32°46'29.66" N	104°15'38.28" W	3544.50	3541.93
MW-07	645.934.3	522.433.1	32°46'32.68" N	104°15'37.25" W	3546.49	3546.26
MW-08	645.532.1	522.229.0	32°46'28.78" N	104°15'39.64" W	3543.73	3540.99
MW-09	645.799.3	522.110.7	32°46'31.36" N	104°15'41.02" W	3544.42	3540.4
MW-10	645.750.3	522.217.3	32°46'30.86" N	104°15'39.78" W	3544.84	3541.93
MW-11	645.789.1	522.110.0	32°46'31.24" N	104°15'41.03" W	3542.73	3540.4
MW-12	645.127.5	523.211.3	32°46'24.69" N	104°15'28.14" W	3535.29	3522.6
MW-13	646.364.9	522.985.9	32°46'36.94" N	104°15'31.00" W	3551.40	3538.5
MW-14	645.005.2	523.358.2	32°46'23.48" N	104°15'26.42" W	3520.32	3517.94
MW-15	646.860.1	522.416.1	32°46'41.84" N	104°15'37.43" W	3552.45	3559.91
MW-16	647.718.3	522.685.8	32°46'50.33" N	104°15'34.15" W	3585.46	3582.87
MW-17	646.804.7	523.280.9	32°46'41.29" N	104°15'27.31" W	3570.84	3568.0
MW-18	645.739.4	521.718.8	32°46'30.65" N	104°15'45.61" W	3523.63	3529.98
MW-19	645.460.3	522.272.4	32°46'27.98" N	104°15'39.13" W	3543.34	3540.6
MW-20	645.506.5	522.802.6	32°46'28.44" N	104°15'32.92" W	3541.47	3538.89
MW-21	645.668.8	522.866.0	32°46'30.55" N	104°15'32.18" W	3543.15	3540.52
MW-22	645.728.3	523.014.0	32°46'31.63" N	104°15'30.43" W	3545.87	3543.16
MW-23	645.850.5	523.014.0	32°46'30.85" N	104°15'29.93" W	3542.21	3539.2
P-01	645.660.5	521.884.9	32°46'29.97" N	104°15'43.67" W	3530.21	3528.08
P-02	645.895.5	523.533.0	32°46'32.29" N	104°15'24.36" W	3544.73	3542.3
P-03	645.577.5	524.036.9	32°46'29.14" N	104°15'18.46" W	3536.83	3534.67
P-04	644.922.9	524.101.6	32°46'22.66" N	104°15'17.71" W	3515.77	3513.5
P-05	644.637.8	523.307.2	32°46'19.84" N	104°15'27.02" W	3507.48	3505.25
EB-01	644.375.6	522.834.9	32°46'17.25" N	104°15'32.55" W	3492.15	3491.53
EB-02	644.910.9	522.265.5	32°46'22.55" N	104°15'39.22" W	3525.34	3522.6
EB-03	644.995.4	523.366.4	32°46'23.38" N	104°15'26.32" W	3521.05	3517.83
EB-04	644.322.3	521.630.7	32°46'16.73" N	104°15'46.66" W	3508.38	3505.64
EB-05	645.435.1	521.818.6	32°46'27.74" N	104°15'44.45" W	3526.63	3523.81
EB-06	646.550.9	521.720.8	32°46'38.78" N	104°15'45.58" W	3556.63	3555.6
EB-07	644.792.5	523.783.0	32°46'21.37" N	104°15'21.44" W	3503.97	3501.60
EB-08	645.591.3	523.474.8	32°46'29.28" N	104°15'25.05" W	3537.07	3533.88
BH-1	645.997.0	522.795.1	32°46'33.30" N	104°15'03.01" W	3517.07	3514.8
BH-2	646.238.3	522.402.5	32°46'35.69" N	104°15'37.60" W	3549.4	3549.4
BH-3	645.953.4	522.231.2	32°46'32.87" N	104°15'39.61" W	3544.3	3544.3
BH-4	646.031.7	522.672.3	32°46'33.84" N	104°15'34.44" W	3549.9	3549.9
BH-5	645.932.6	522.426.0	32°46'32.66" N	104°15'37.33" W	3546.0	3546.0
A-1	645.054.0	522.868.6	32°46'23.96" N	104°15'32.15" W	3521.93	3523.9
E-1	646.918.1	522.980.6	32°46'42.35" N	104°15'31.06" W	3570.1	3570.1
NWC Plant	646.412.6	522.055.3	32°46'37.47" N	104°15'41.67" W	3547.6	3547.6
Nec Plant	646.404.9	523.372.0	32°46'37.33" N	104°15'26.25" W	3557.9	3557.9
Sec Plant	644.798.8	523.396.3	32°46'21.44" N	104°15'25.97" W	3507.9	3507.9
Swc Plant	644.822.3	522.077.2	32°46'21.66" N	104°15'41.42" W	3517.5	3517.5

FRONTIER FIELD SERVICES, LLC

EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

LAarson & Associates, Inc.
Environmental Consultants



LEGEND

- Plugged And Abandoned Monitoring Well Location
- Monitoring Well Location and Chloride Concentration in Groundwater, mg/L, March and July 2009
- Piezometer (Fluid Level) Location and Chloride Concentration in Groundwater, mg/L, March and July 2009
- Monitoring Well Location and Chloride Concentration in Groundwater, mg/L, March and July 2009
- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity
- Hydrocarbon Emulsion Present In Well
- Contour of Chloride Concentration in Groundwater , mg/L, March and July 2009
- Fence
- Draw
- Roads
- Property Line

WQCC Domestic Water Quality Standard: 250 mg/L

FRONTIER FIELD SERVICES, LLC

EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

Arson &
Associates, Inc.
Environmental Consultants

Plot Generated Using Surfer® Data Contouring Software

Figure 8b - Chloride Isocon Map March and July 2009

LEGEND

- Plugged And Abandoned Monitoring Well Location
- Monitoring Well Location and Sulfate Concentration in Groundwater, mg/L, September 15, 2008
- Piezometer (Fluid Level) Location and Sulfate Concentration in Groundwater, mg/L, September 15, 2008
- Monitoring Well Location and Sulfate Concentration in Groundwater, mg/L, September 15, 2008
- Water Level Corrected For Hydrocarbon Product In Well Using 0.70 Specific Gravity
- Hydrocarbon Emulsion Present In Well
- Contour of Sulfate Concentration in Groundwater Monitoring Well Location, mg/L, September 15, 2008

- Fence
- Draw
- Roads
- Property Line

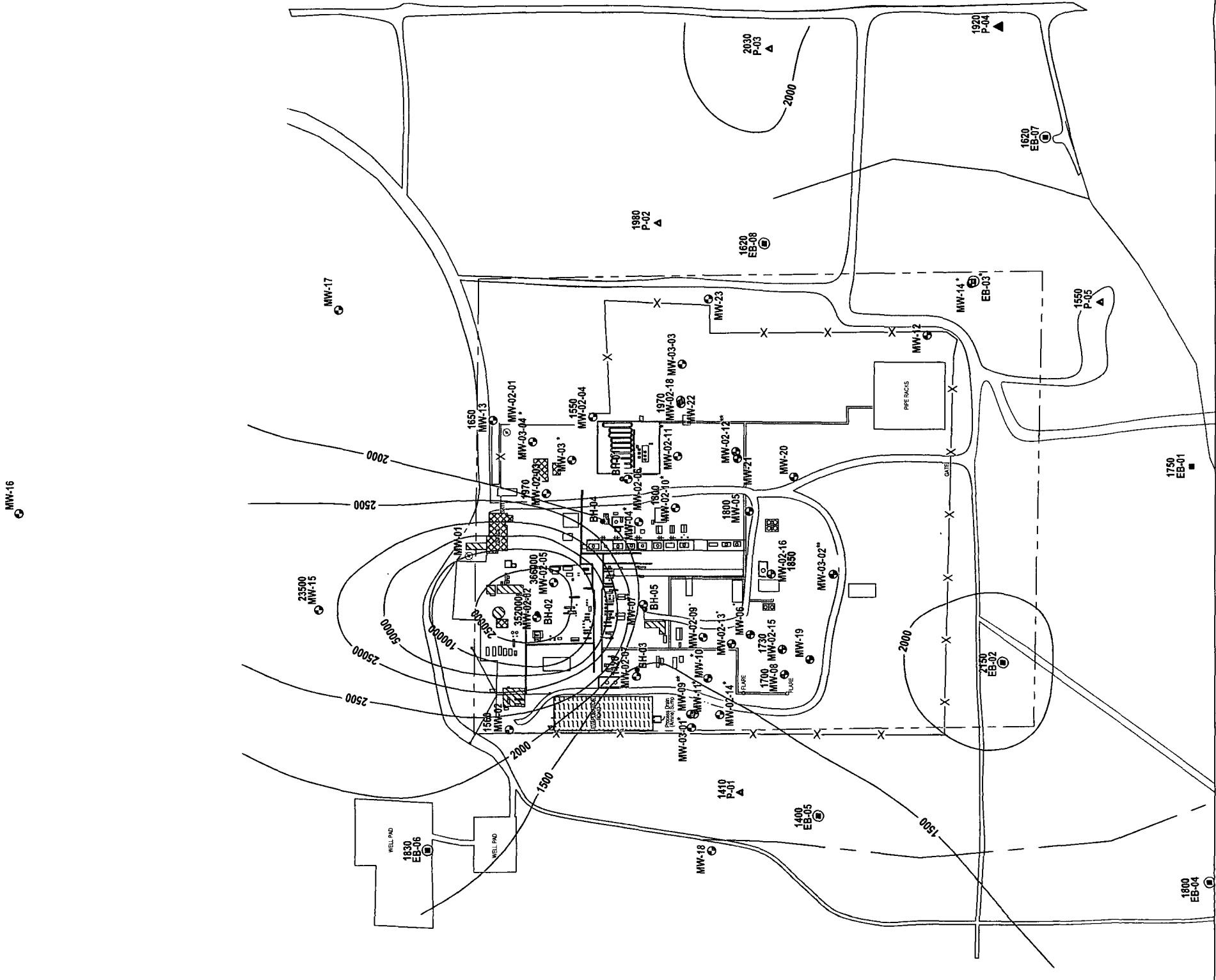
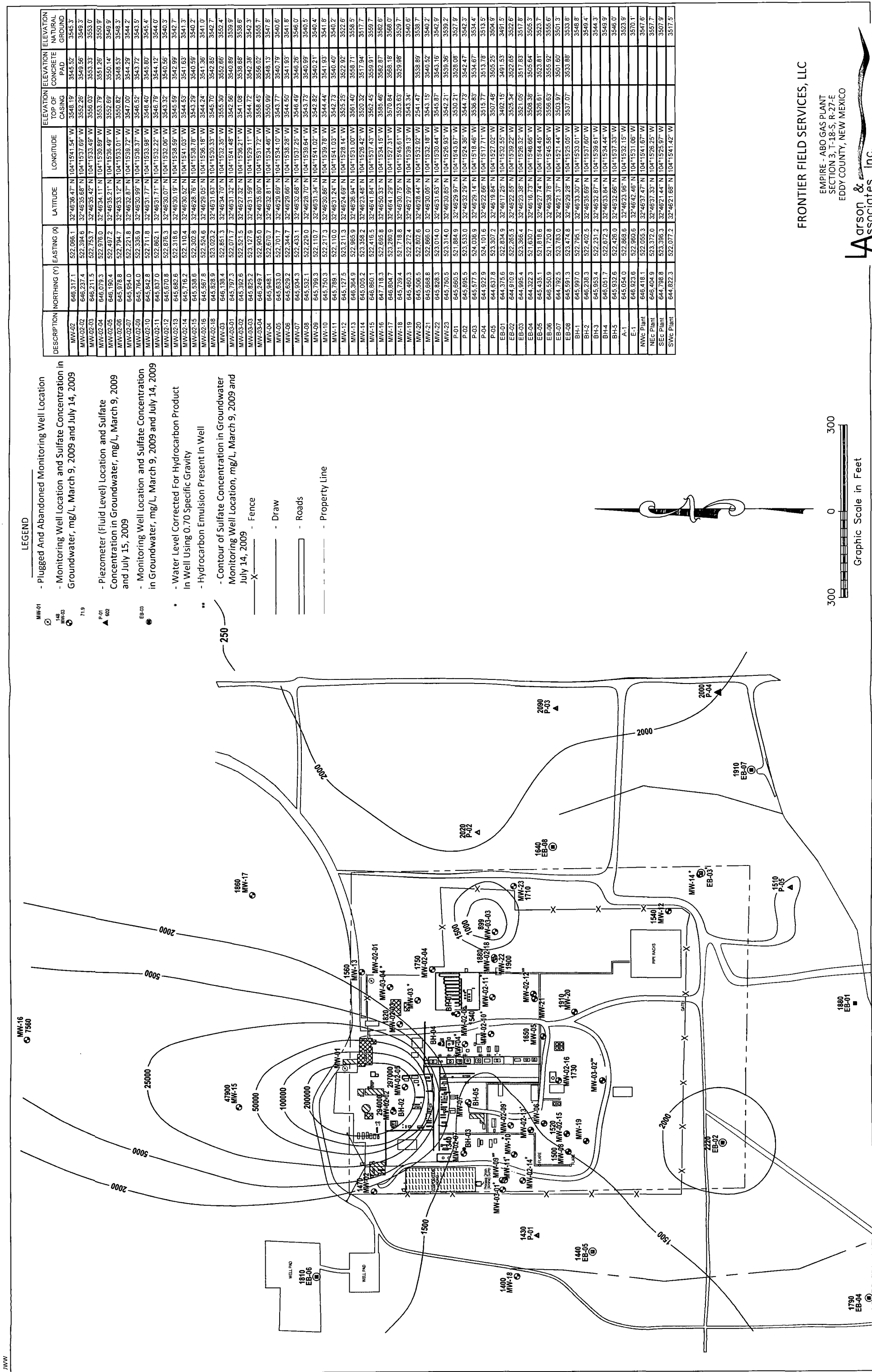
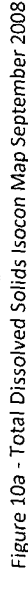



Figure 9a - Sulfate Isocon Map September 2008

DESCRIPTION	NORTHING (Y)	EASTING (X)	LATITUDE	LONGITUDE	ELEVATION TOP OF CASING	ELEVATION CONCRETE PAD	ELEVATION NATURAL GROUND
MW-02	646.317.1	522.066.1	32°46'36.47" N	104°15'41.54" W	3548.19'	3545.52'	3545.3'
MW-02-02	646.237.4	522.394.6	32°46'35.68" N	104°15'37.69" W	3552.26'	3549.36'	3549.3'
MW-02-03	646.211.5	522.753.7	32°46'35.42" N	104°15'33.49" W	3556.03'	3553.33'	3553.0'
MW-02-04	646.079.3	522.976.0	32°46'34.11" N	104°15'30.89" W	3553.79'	3551.26'	3550.9'
MW-02-05	646.190.4	522.497.2	32°46'35.21" N	104°15'36.49" W	3552.69'	3550.14'	3549.9'
MW-02-06	645.978.8	522.794.7	32°46'33.12" N	104°15'33.01" W	3550.82'	3548.53'	3548.3'
MW-02-07	645.954.0	522.221.8	32°46'32.87" N	104°15'39.72" W	3547.00'	3544.29'	3544.2'
MW-02-09	645.764.0	522.336.9	32°46'30.99" N	104°15'38.37" W	3546.52'	3543.72'	3543.5'
MW-02-10	645.842.8	522.711.8	32°46'31.77" N	104°15'33.98" W	3548.40'	3545.80'	3545.4'
MW-02-11	645.837.0	522.862.1	32°46'31.71" N	104°15'32.22" W	3546.79'	3544.12'	3544.0'
MW-02-12	645.670.8	522.876.3	32°46'30.07" N	104°15'32.06" W	3543.32'	3540.56'	3540.3'
MW-02-13	645.582.6	522.318.6	32°46'30.19" N	104°15'38.59" W	3545.69'	3542.93'	3542.7'
MW-02-14	645.776.2	522.110.4	32°46'30.52" N	104°15'41.03" W	3544.53'	3541.63'	3541.3'
MW-02-15	645.538.6	522.302.8	32°46'28.76" N	104°15'38.78" W	3543.29'	3540.59'	3540.2'
MW-02-16	645.567.8	522.524.6	32°46'29.05" N	104°15'36.18" W	3544.24'	3541.36'	3541.0'
MW-02-18	645.828.9	523.023.2	32°46'31.63" N	104°15'30.33" W	3545.70'	3542.85'	3542.7'
MW-03	646.138.4	522.851.3	32°46'34.70" N	104°15'32.35" W	3555.30'	3552.66'	3552.4'
MW-03-01	645.392.6	522.071.7	32°46'31.32" N	104°15'41.48" W	3542.56'	3540.89'	3539.9'
MW-03-02	645.825.2	523.127.9	32°46'31.59" N	104°15'29.11" W	3544.72'	3542.38'	3542.3'
MW-03-03	645.832.0	522.701.7	32°46'30.66" N	104°15'34.10" W	3543.77'	3540.79'	3540.6'
MW-03-04	646.249.7	522.905.0	32°46'35.80" N	104°15'31.72" W	3558.45'	3556.02'	3555.7'
MW-04	645.948.1	522.670.7	32°46'32.81" N	104°15'34.46" W	3550.99'	3548.13'	3547.8'
MW-05	645.633.0	522.344.7	32°46'29.69" N	104°15'34.10" W	3544.50'	3541.93'	3541.8'
MW-06	645.629.2	522.701.7	32°46'30.66" N	104°15'38.28" W	3544.50'	3541.93'	3541.8'
MW-07	645.934.3	522.433.1	32°46'32.68" N	104°15'37.25" W	3546.49'	3546.26'	3546.0'
MW-08	645.532.1	522.229.0	32°46'28.70" N	104°15'38.64" W	3543.73'	3540.99'	3540.5'
MW-09	645.799.3	522.110.7	32°46'31.34" N	104°15'41.02" W	3542.82'	3540.21'	3540.4'
MW-10	645.750.3	522.217.3	32°46'30.86" N	104°15'39.78" W	3544.44'	3541.93'	3541.8'
MW-11	645.789.1	522.110.0	32°46'31.24" N	104°15'41.03" W	3542.73'	3540.40'	3540.2'
MW-12	645.127.5	523.211.3	32°46'24.69" N	104°15'28.14" W	3523.25'	3522.92'	3522.6'
MW-13	646.364.9	522.965.9	32°46'36.94" N	104°15'31.00" W	3561.40'	3558.71'	3558.5'
MW-14	645.005.2	523.358.2	32°46'23.48" N	104°15'28.42" W	3520.32'	3517.94'	3517.7'
MW-15	646.860.1	522.416.5	32°46'41.84" N	104°15'37.43" W	3562.45'	3559.91'	3559.7'
MW-16	647.778.3	522.695.8	32°46'50.33" N	104°15'34.15" W	3585.46'	3582.87'	3582.6'
MW-17	646.804.7	523.280.9	32°46'41.29" N	104°15'27.31" W	3570.84'	3568.18'	3568.0'
MW-18	645.739.4	521.718.8	32°46'30.75" N	104°15'45.61" W	3523.63'	3529.98'	3529.7'
MW-19	645.460.3	522.272.4	32°46'27.99" N	104°15'39.13" W	3543.34'	3540.6'	3540.5'
MW-20	645.506.5	522.802.6	32°46'28.44" N	104°15'32.92" W	3541.47'	3538.89'	3538.7'
MW-21	645.668.8	522.866.0	32°46'30.05" N	104°15'32.18" W	3543.15'	3540.52'	3540.2'
MW-22	645.828.3	523.014.0	32°46'31.63" N	104°15'30.44" W	3545.87'	3543.16'	3542.9'
MW-23	645.750.5	523.314.0	32°46'30.85" N	104°15'28.93" W	3539.36'	3539.2'	3539.2'
P-01	645.660.5	521.884.9	32°46'29.97" N	104°15'43.67" W	3530.21'	3528.08'	3527.9'
P-02	645.895.5	523.533.0	32°46'32.29" N	104°15'24.36" W	3544.73'	3542.47'	3542.3'
P-03	645.577.5	524.036.9	32°46'29.14" N	104°15'18.46" W	3536.83'	3534.4'	3534.4'
P-04	644.922.9	524.101.6	32°46'22.66" N	104°15'17.71" W	3515.77'	3513.78'	3513.5'
P-05	644.637.8	523.307.2	32°46'19.84" N	104°15'27.02" W	3507.48'	3505.25'	3504.9'
EB-01	644.375.6	522.834.9	32°46'17.25" N	104°15'32.55" W	3492.15'	3491.53'	3491.5'
EB-02	644.910.9	522.265.5	32°46'22.55" N	104°15'39.22" W	3525.34'	3522.6'	3522.6'
EB-03	644.995.4	523.366.4	32°46'23.38" N	104°15'28.32" W	3521.05'	3517.83'	3517.8'
EB-04	644.322.3	521.630.7	32°46'16.73" N	104°15'46.66" W	3508.38'	3505.64'	3505.3'
EB-05	645.435.1	521.818.6	32°46'27.74" N	104°15'44.46" W	3526.61'	3523.81'	3523.7'
EB-06	646.550.9	521.720.8	32°46'38.78" N	104°15'45.58" W	3556.63'	3555.92'	3555.6'
EB-07	644.792.5	523.783.0	32°46'21.37" N	104°15'21.44" W	3503.97'	3501.60'	3501.3'
EB-08	645.591.3	523.474.8	32°46'29.28" N	104°15'25.05" W	3537.07'	3533.88'	3533.8'
BH-1	645.997.0	522.795.1	32°46'33.30" N	104°15'33.01" W			3548.8'
BH-2	646.238.3	522.402.5	32°46'35.69" N	104°15'37.60" W			3548.4'
BH-3	645.953.4	522.231.2	32°46'32.87" N	104°15'39.61" W			3544.3'
BH-4	646.051.7	522.672.3	32°46'33.84" N	104°15'34.44" W			3549.9'
BH-5	645.932.6	522.426.0	32°46'32.66" N	104°15'37.33" W			3546.0'
A-1	645.054.0	522.868.6	32°46'23.96" N	104°15'32.15" W			3523.9'
NWc Plant	646.418.1	522.955.3	32°46'37.47" N	104°15'41.67" W			3570.1'
SEC Plant	646.404.9	523.372.0	32°46'37.33" N	104°15'26.25" W			3547.6'
SWc Plant	644.798.8	523.396.3	32°46'21.44" N	104°15'25.97" W			3557.9'
	644.822.3	522.077.2	32°46'21.68" N	104°15'41.42" W			3517.5'





EMPIRE - ABO GAS PLANT
SECTION 3, T-18-S, R-27-E
EDDY COUNTY, NEW MEXICO

LA arson &  associates, Inc.
Environmental Consultants
EDDY COUNTY

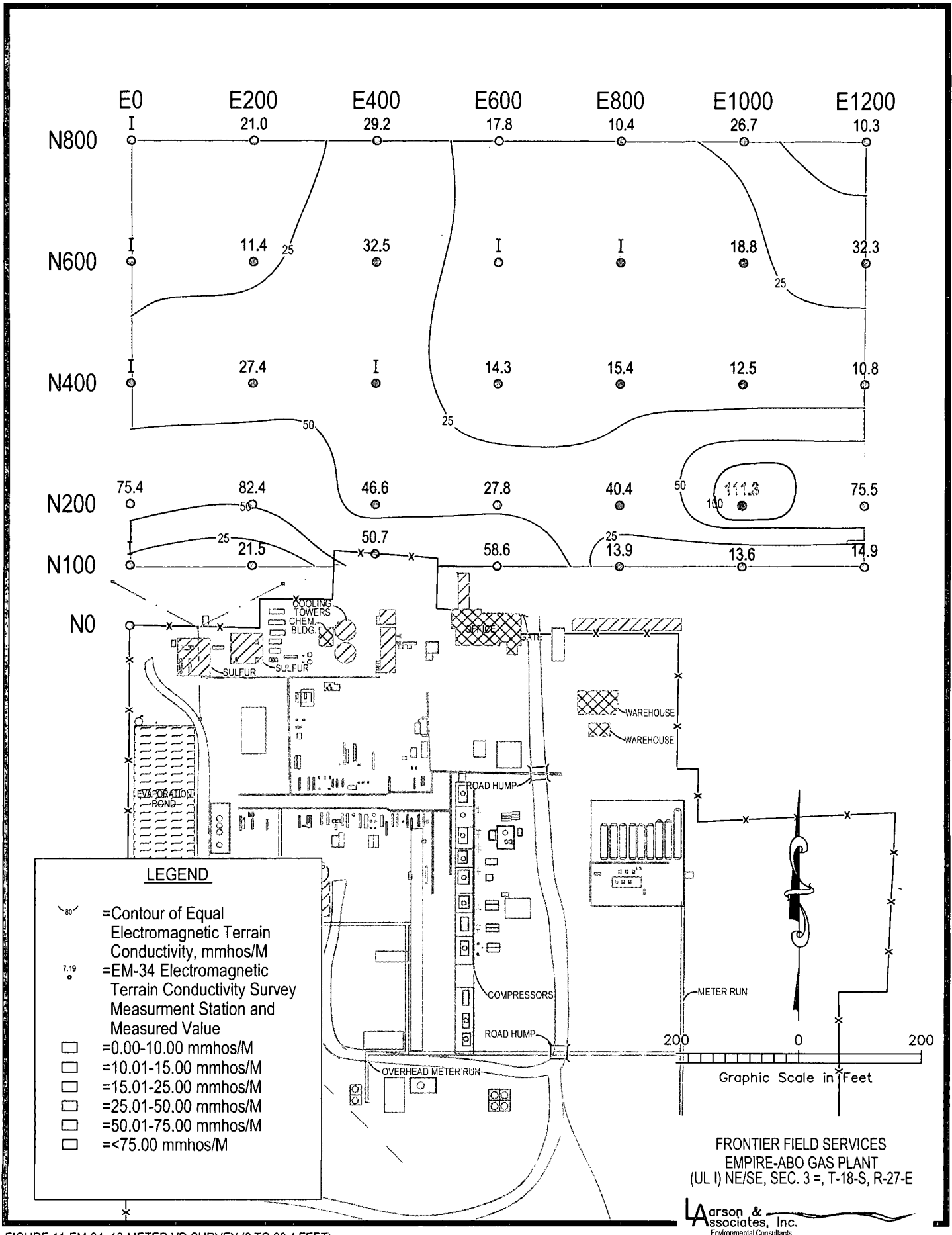
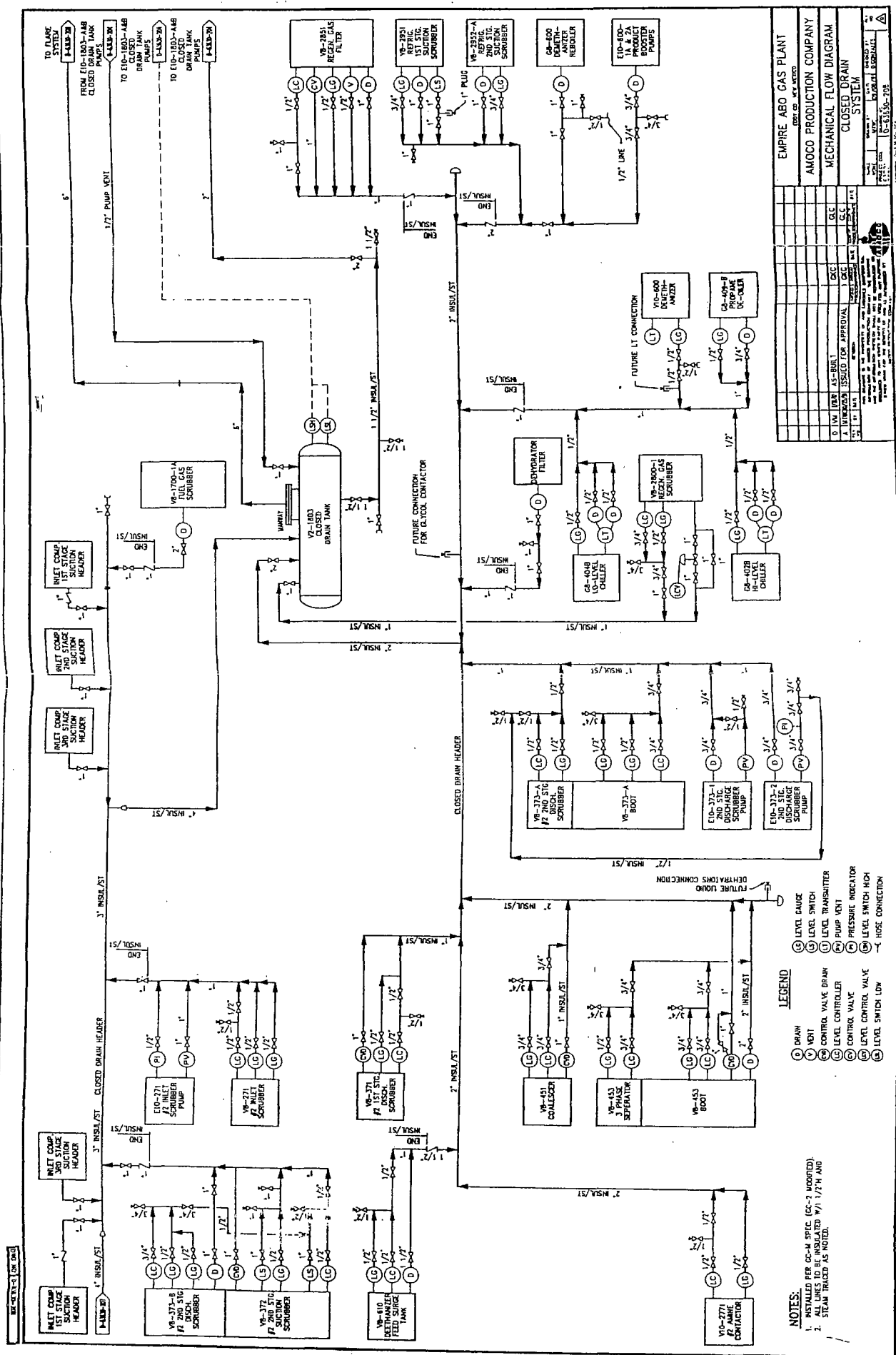
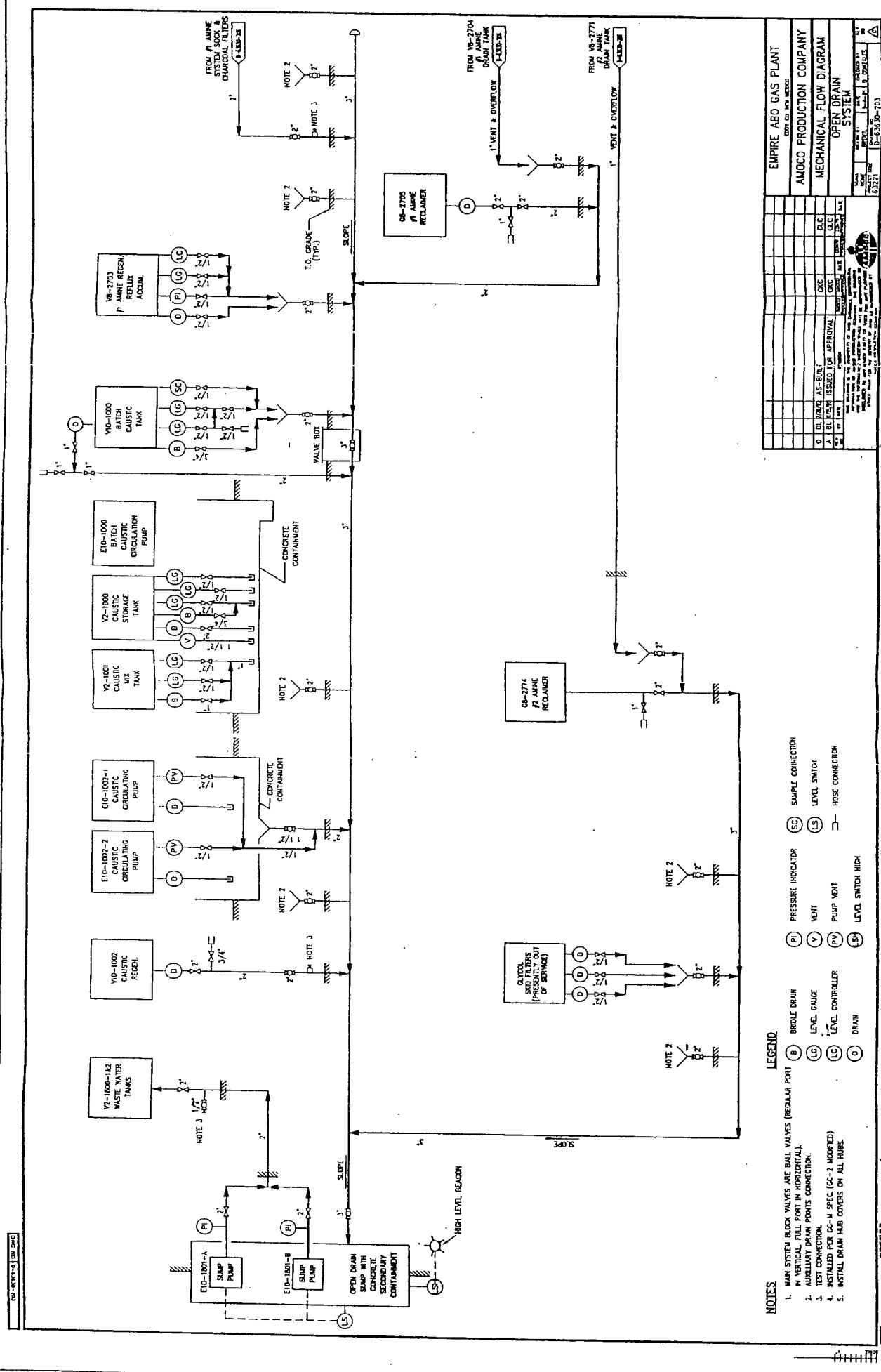


FIGURE 11-EM-34, 10-METER VD SURVEY (0 TO 98.4 FEET)



Fig. 94-3





EMPIRE ABO GAS PLANT	
AMOCO PRODUCTION COMPANY	
MECHANICAL FLOW DIAGRAM	
OPEN DRAIN SYSTEM	
DATE	12-1-68
BY	J. L. BROWN
CHECKED BY	J. L. BROWN
APPROVED BY	J. L. BROWN
PROJECT NO.	6-63850-103
FIG. NO.	94-4

- NOTES**
1. MAIN SYSTEM BLOCK VALVES ARE BALL VALVES (REGULAR PORT IN VERTICAL, FULL PORT IN HORIZONTAL).
 2. AUXILIARY DRAIN PORTS CONNECTION.
 3. TEST CONNECTION.
 4. INSTALLED PER CC-14 SPEC (CC-14 MODIFIED).
 5. INSTALL DRAIN HUB COVERS ON ALL HUBS.
- LEGEND**
- (B) BREAK DRAIN
 - (V) VENT
 - (LG) LEVEL GAUGE
 - (LC) LEVEL CONTROLLER
 - (D) DRAIN
 - (PI) PRESSURE INDICATOR
 - (PV) PUMP VENT
 - (S) LEVEL SWITCH HIGH
 - (SC) SAMPLE CONNECTION
 - (S) LEVEL SWITCH
 - (H) HOSE CONNECTION

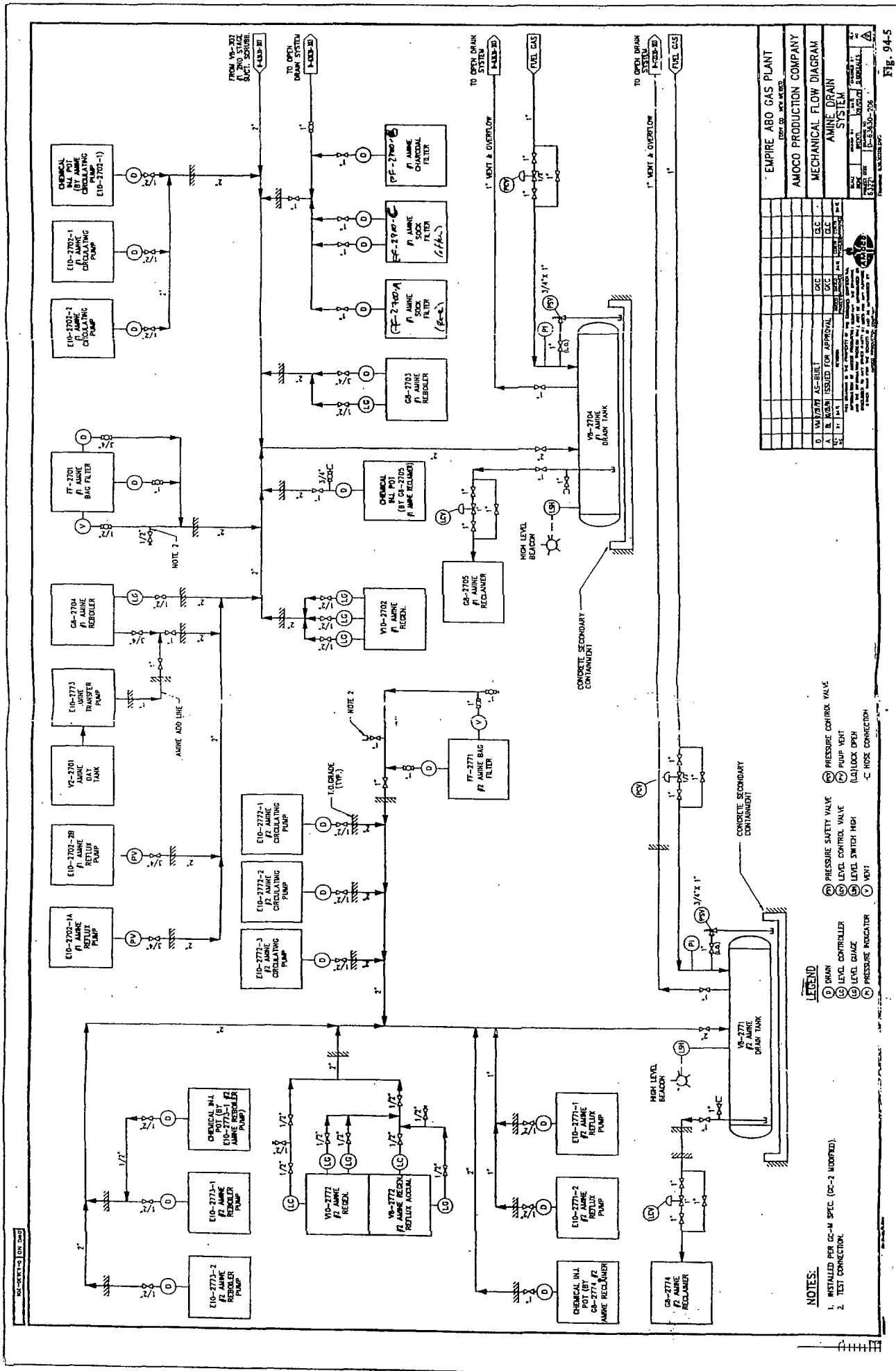
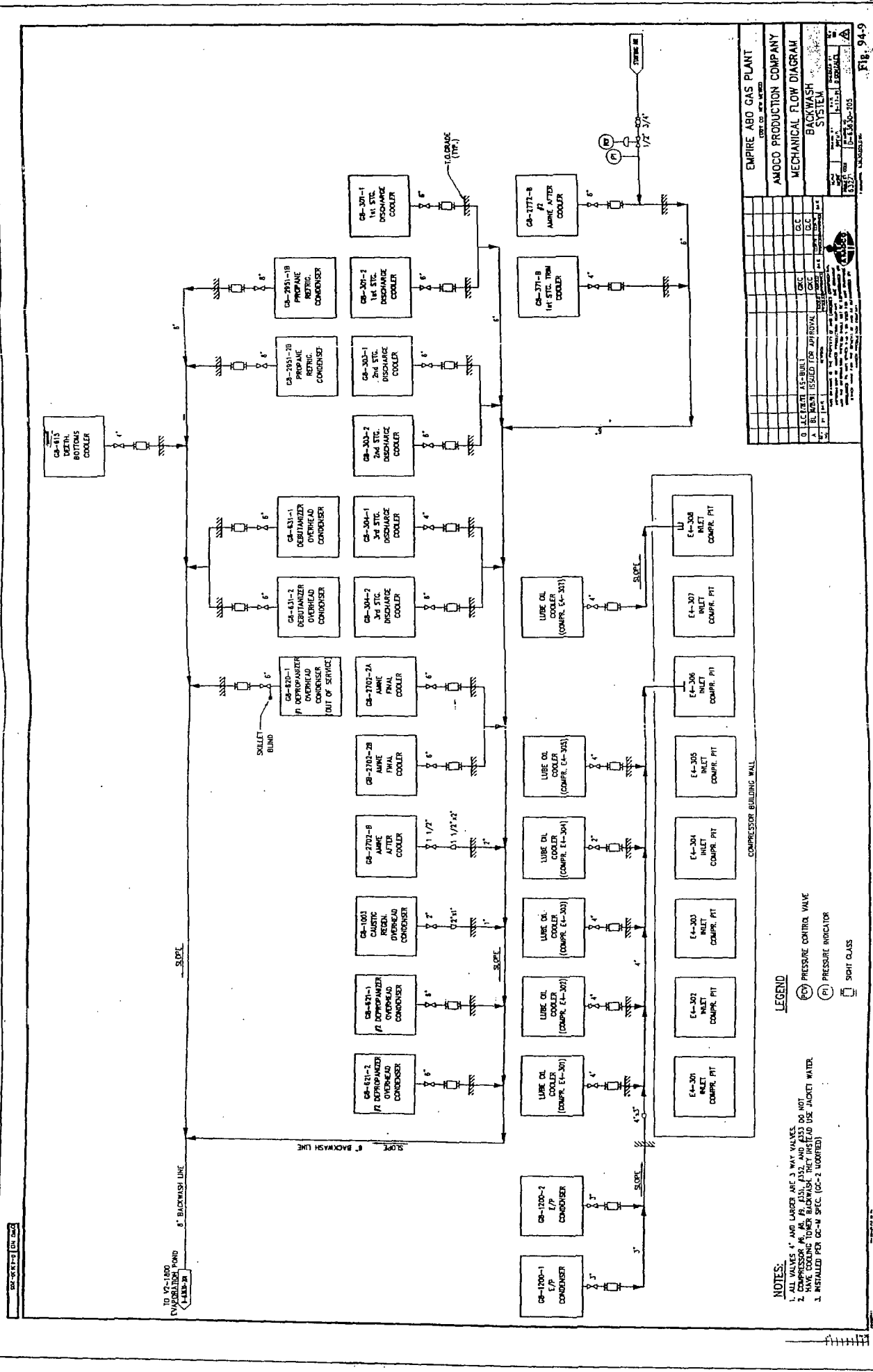


Fig. 94-5



Michelle Green

From: Mark Larson
Sent: Thursday, May 08, 2008 5:44 PM
To: dharris@frontierfieldservices.com
Cc: michelle@laenvironmental.com
Subject: FW: Discharge Permit GW-022 Groundwater Sampling Schedule Modification Approval
Attachments: image001.jpg

Dave,
Here's the OCD's approval for modifying the groundwater sampling schedule from quarterly to semi annually.

Mark J. Larson
Sr. Project Manager / President
507 N. Marienfeld St., Ste. 202
Midland, Texas 79701
(432) 687-0901 (office)
(432) 687-0456 (fax)
(432) 556-8656 (cell)
mark@laenvironmental.com



From: Price, Wayne, EMNRD [mailto:wayne.price@state.nm.us]
Sent: Thursday, May 08, 2008 5:28 PM
To: Mark Larson
Cc: VonGonten, Glenn, EMNRD
Subject: RE: Discharge Permit GW-022 Groundwater Sampling Schedule Modification Approval

Approved! Please make sure this approval is part of the submittal record.

Please be advised that OCD approval of this plan does not relieve the owner/operator of responsibility should their operations fail to adequately investigate and remediate contamination that pose a threat to ground water, surface water, human health or the environment. In addition, OCD approval does not relieve the owner/operator of responsibility for compliance with any other federal, state, or local laws and/or regulations.

From: Mark Larson [mailto:Mark@laenvironmental.com]
Sent: Thursday, May 08, 2008 1:48 PM
To: Price, Wayne, EMNRD
Cc: John Ferguson
Subject: Re: Discharge Permit GW-022 Groundwater Sampling Schedule Modification Approval

Dear Wayne,

This message is submitted to the New Mexico Oil Conservation Division (OCD) on behalf of Frontier Field Services, L.P. (Frontier) by Larson & Associates, inc., its consultant, to confirm verbal approval from the OCD for Frontier to modify the groundwater monitoring schedule for its Empire Abo Gas Plant (GW-022). Groundwater samples are currently obtained on a quarterly (4 times per year) schedule and a verbal request was approved by the OCD during a conversation today to allow Frontier to collect groundwater samples on a semi-annual (twice yearly) schedule beginning immediately. Thank you for your consideration of this request. Please do not hesitate to contact me if you have questions.

Mark J. Larson
Sr. Project Manager / President
507 N. Marienfeld St., Ste. 202
Midland, Texas 79701
(432) 687-0901 (office)
(432) 687-0456 (fax)
(432) 556-8656 (cell)
mark@laenvironmental.com



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5 YR. UNDERGROUND DRAIN TESTING

Task No.
Tenant
Assigned By STEVENSON
Assigned To STEVENSON
Scheduled Start Date
Scheduled Finish Date
Perform by Warranty No
Priority 3.00
Expense Class

Request Date 4/21/2005
Request Time 14:35:30
Originator STEVENSON
Telephone No. 505-677-5119
Extension 5119
WO Type ENV
Completion Date 5/9/05
Completion Time _____

CraftCrew SizeEstimated Labor Hours

Equipment No.	Equipment Description	Location	Sub-location 1	Sub-location 2	Sub-location 3
---------------	-----------------------	----------	----------------	----------------	----------------

1800	SYSTEM, SEWERAGE	EAGP	-	-	-
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Item No.	Equipment No.	Description	Qty Required	Date Used	Qty Used
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List extra parts and comments here

All Lines were Hydrotested. No Leaks were detected.

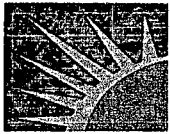
Employee Code	Equipment No.	Work Date	First Name	Last Name	Regular Hours	Overtime Hours
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Safety Notes

Equipment No. 1800

Ray Spencer - TRS Resources

Task Instructions



TRS Resources LLC

Global Industrial Solutions

SUMMARY REPORT

HYDROSTATIC PRESSURE TESTING OF UNDERGROUND DRAIN PIPING

Frontier
Field Services

EMPIRE ABO GAS PLANT



SUMMARY REPORT
HYDROSTATIC PRESSURE TESTING OF UNDERGROUND DRAIN PIPING
FRONTIER FIELD SERVICES
EMPIRE ABO GAS PLANT

INTRODUCTION

On 04/27/05, TRS Resources LLC began conducting hydrostatic pressure testing of the noted underground drain piping systems at the Empire ABO Gas Plant.

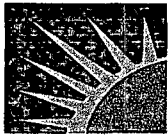
INSPECTION METHODOLOGY

Each piping circuit was isolated, filled with clean water ensuring that the air was removed and then connected to a water filled riser with a fill height of 83 ½ ". To ensure that a minimum of three (3) pounds per square inch was achieved a pressure gage was installed at the bottom of the riser to verify the minimum pressure). The system was considered acceptable when there was no change in the height of the water in the riser for a period of thirty (30) minutes.

INSPECTION

Drain line from	Drain line to	Line size/Length/Type	Test Date/Time	Results
Product storage containment sump	Dirty Slop Oil Tank	2&3"/35ft/CS	5/10/05 1235-1305	Acceptable
Compressor Building Sumps	Dirty Slop Oil Tank	3"/690ft/CS	5/10/05 1400-1430	Acceptable
Open Drain Sump Tank	Wastewater Process Tanks North & South	2"/216ft/CS	4/28/05 1110-1140	Acceptable
Sulfur Condensers	Evaporation Pond	2"/171ft/CS	4/27/05 1530-1600	Acceptable
Flare System	Flare Sump Tank	4"/335ft/CS	5/10/05 0800-0830	Acceptable
Glycol, Amine & Caustic Drain System	Open Drain Sump Tank	2"/283ft/CS 3"/284ft/CS 4"/18ft/CS	5/6/05 1530-1600	Acceptable
Flare Sump Tank	Clean Slop Oil Tank	3"/871ft/CS 1½ "/80ft/CS	5/10/05 1000-1030	Acceptable
Scrubber Coolers, Demethanizer System, Propane System, Debutanizer System, Amine System and Boiler Drains	Evaporation Pond	3"/16ft/CS 4"/332ft/CS 6"/1120ft/CS 8"/660ft/CS	4/27/05 1300-1330	Acceptable
EP Coolers, Lube Oil and Air Compressor Systems	Compressor Bldg Cellar	1"/40ft CS 3"/20ft/CS 4"/180ft/CS	5/10/05 1545-1615	Acceptable
Product Containment Sump	Dirty Slop Oil Tank	2"/27ft/CS	5/9/05 1115-1145	Acceptable
Compressor Skid	Fiberglass Tank	2"/93ft/CS	5/9/05 1400-1430	Acceptable

All line lengths are approximate per AGRA Measurements



TRS Resources LLC

Global Industrial Solutions

External Inspection:

All above ground piping was visually inspected for leaks after the test pressure had stabilized.


Note:

The Oil Conservation District was contacted and numerous messages were left notifying them about the line testing dates, No one from the OCD office returned any phone calls to the Frontier Field Services Representative Kyle Stevenson, or came to the plant to witness the line testing.

The above statements are indicative regarding the conditions observed at the time of the visits and the results of the documentation review conducted.

TRS Resources LLC does not warrant or specifically guarantee the continued serviceability of any item, and this report should not be construed or promulgated to indicate any implied guarantee of future integrity or serviceability.

Respectfully Submitted: _____

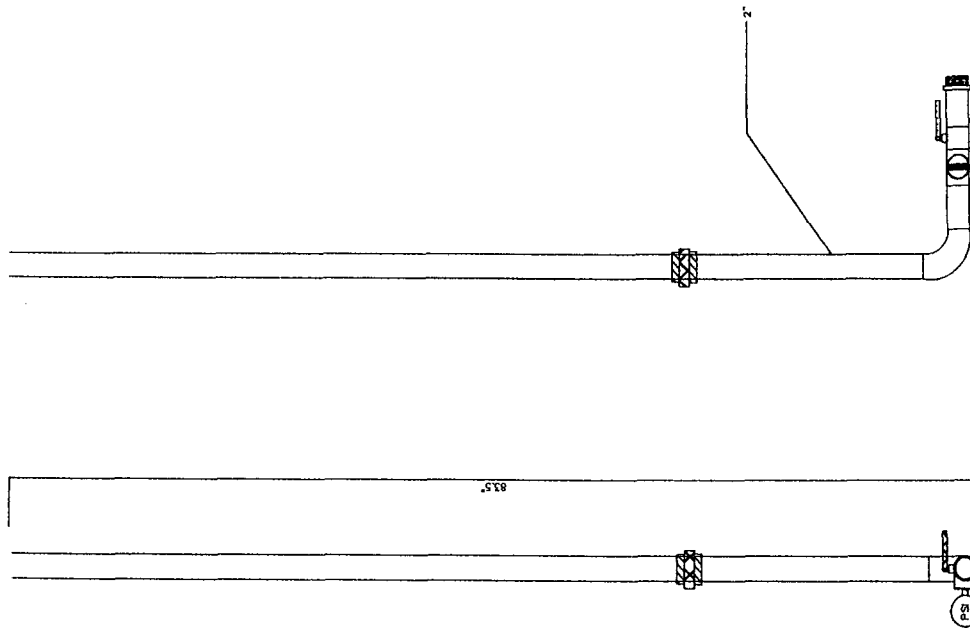

Ray Spencer
TRS Resources LLC
API-570 #7196

Date: 5/10/05

Enclosures: Mechanical Flow Diagrams

XC: File

100' 0.0000'



TRS Resources LLC
Global Industrial Solutions

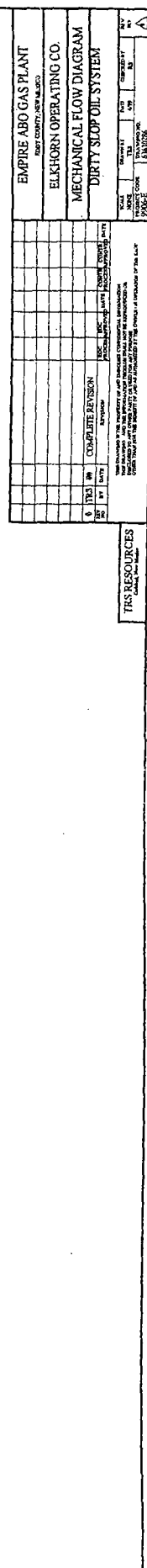
0 TRS 044B
BY: JAC

THIS DRAWING IS THE PROPERTY OF TRS RESOURCES LLC. IT IS TO BE USED ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED HEREON. IT IS NOT TO BE REPRODUCED, COPIED, OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT THE WRITTEN PERMISSION OF TRS RESOURCES LLC.

REVISION

PROJECT CODE				DATE			
PROJECT NAME				DATE			
PROJECT LOCATION				DATE			
PROJECT DESCRIPTION				DATE			
PROJECT STATUS				DATE			
PROJECT OWNER				DATE			
PROJECT CONTACT				DATE			
PROJECT PHONE				DATE			
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PROJECT EMAIL				DATE			
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PROJECT LANGUAGE				DATE			
PROJECT UNIT				DATE			
PROJECT MEASURE				DATE			
PROJECT SCALE				DATE			
PROJECT TOLERANCE				DATE			
PROJECT STANDARD				DATE			
PROJECT CODE				DATE			
PROJECT NAME				DATE			
PROJECT LOCATION				DATE			
PROJECT DESCRIPTION				DATE			
PROJECT STATUS				DATE			
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PROJECT LANGUAGE				DATE			
PROJECT UNIT				DATE			
PROJECT MEASURE				DATE			
PROJECT SCALE				DATE			
PROJECT TOLERANCE				DATE			
PROJECT STANDARD				DATE			

TRIS RESOURCES LLC
CORPORATION
Frontier Field Services
Drain Piping Test Riser
Drain Piping Test Riser

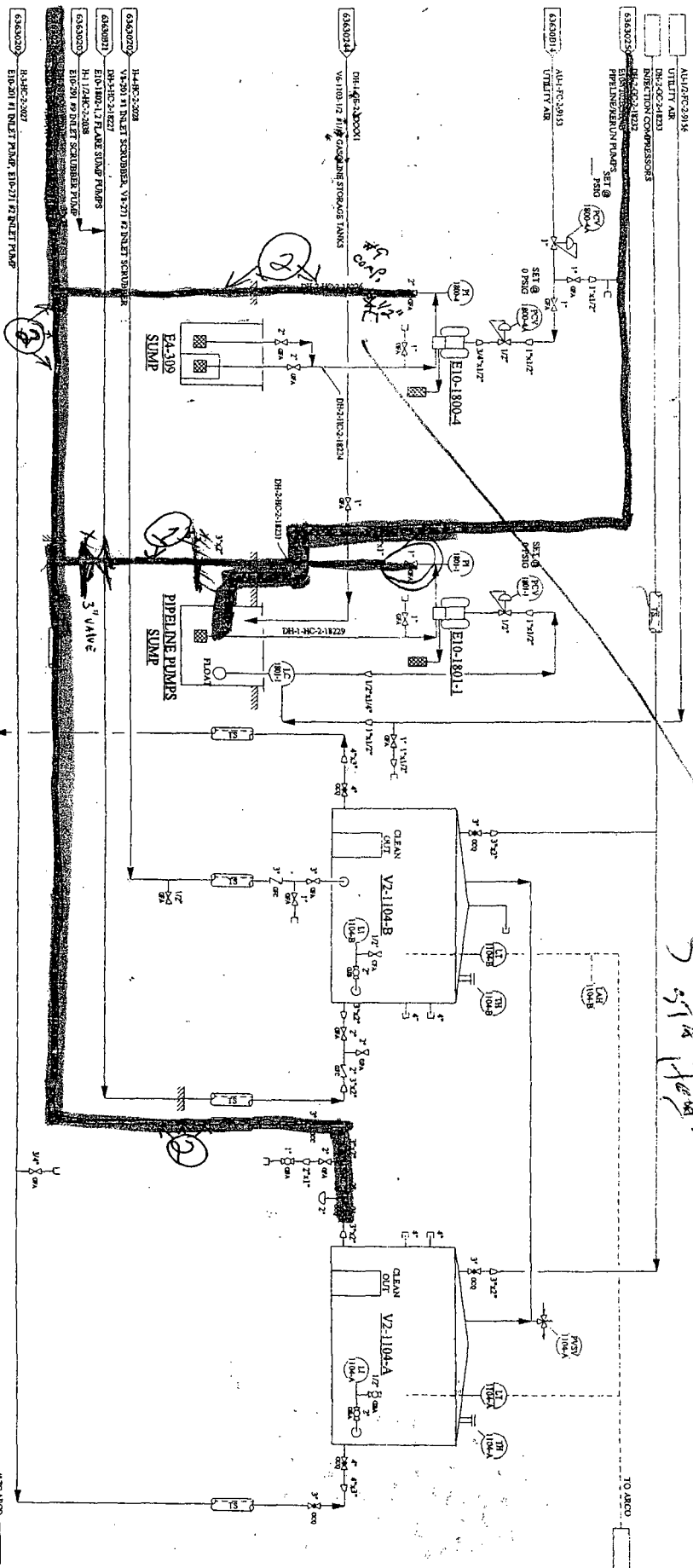
[illegible]

EIO-180-4
SLOP PUMP
12" CD, 2.20' x 2.5
371 BBL CAPACITY

EIO-180-1
PRODUCT CONTAINMENT DRAIN PUMP
12" CD, 2.20' x 2.5
371 BBL CAPACITY

V2-1104-B
SLOP OIL TANK (NORTH) CLEAN
12" CD, 2.20' x 2.5
371 BBL CAPACITY

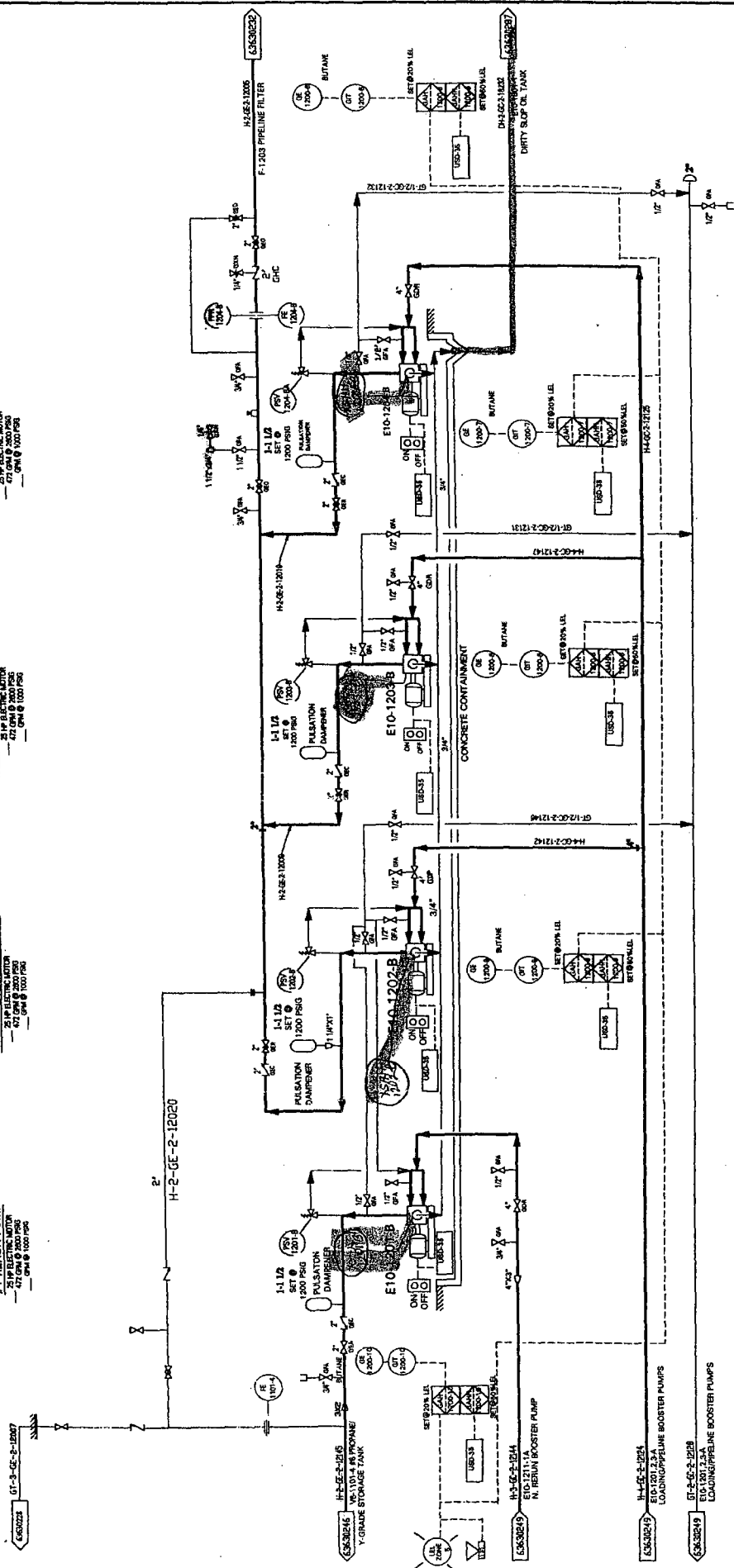
V2-1104-A
SLOP OIL TANK (SOUTH) DIRTY
12" CD, 2.20' x 2.5
371 BBL CAPACITY

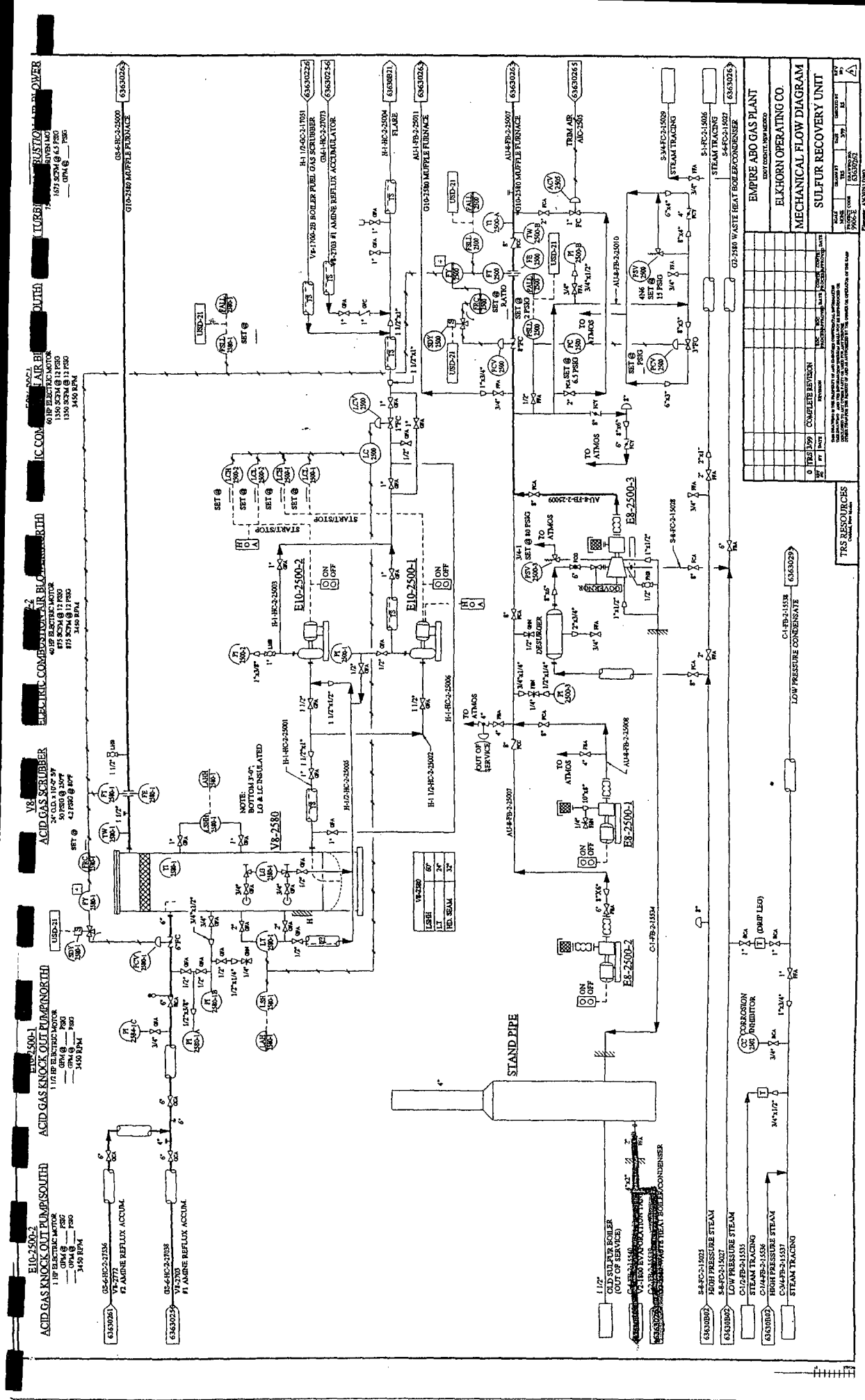


TMS RESOURCES

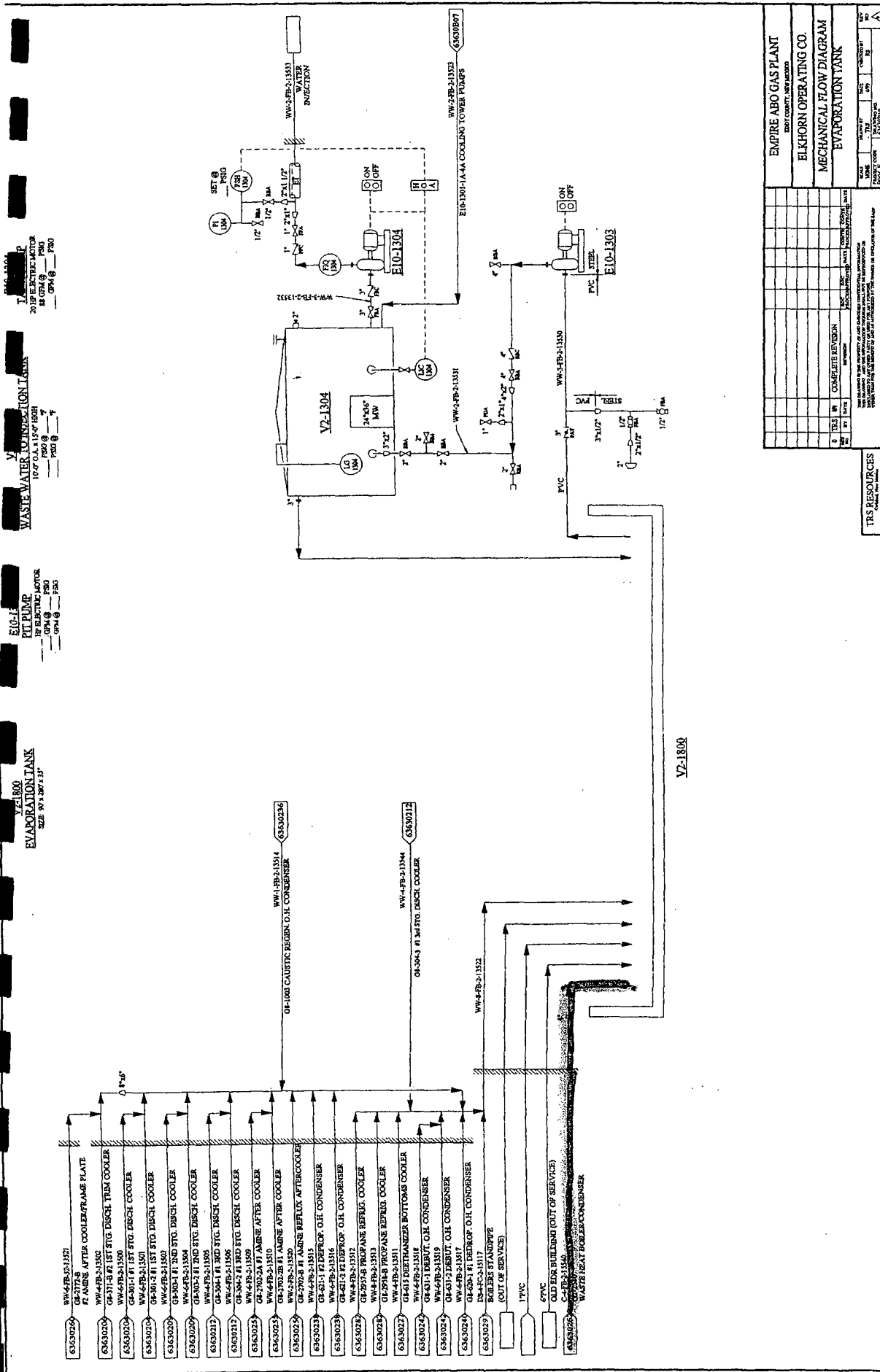
NO.	DATE	DESCRIPTION	BY	CHKD	DATE	REVISION
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EMPIRE ABO GAS PLANT
REPORT NUMBER: ABO-0001
ELKHORN OPERATING CO.
MECHANICAL FLOW DIAGRAM
DIRTY SLOP OIL SYSTEM

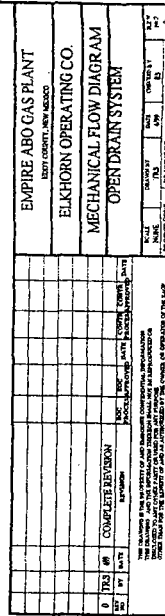
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Y7-1800
EVAPORATION TANK
SIZE: 90" x 280" x 35"

[illegible]

V2-1800-1-
WASTE WATER TANK(NORTH)



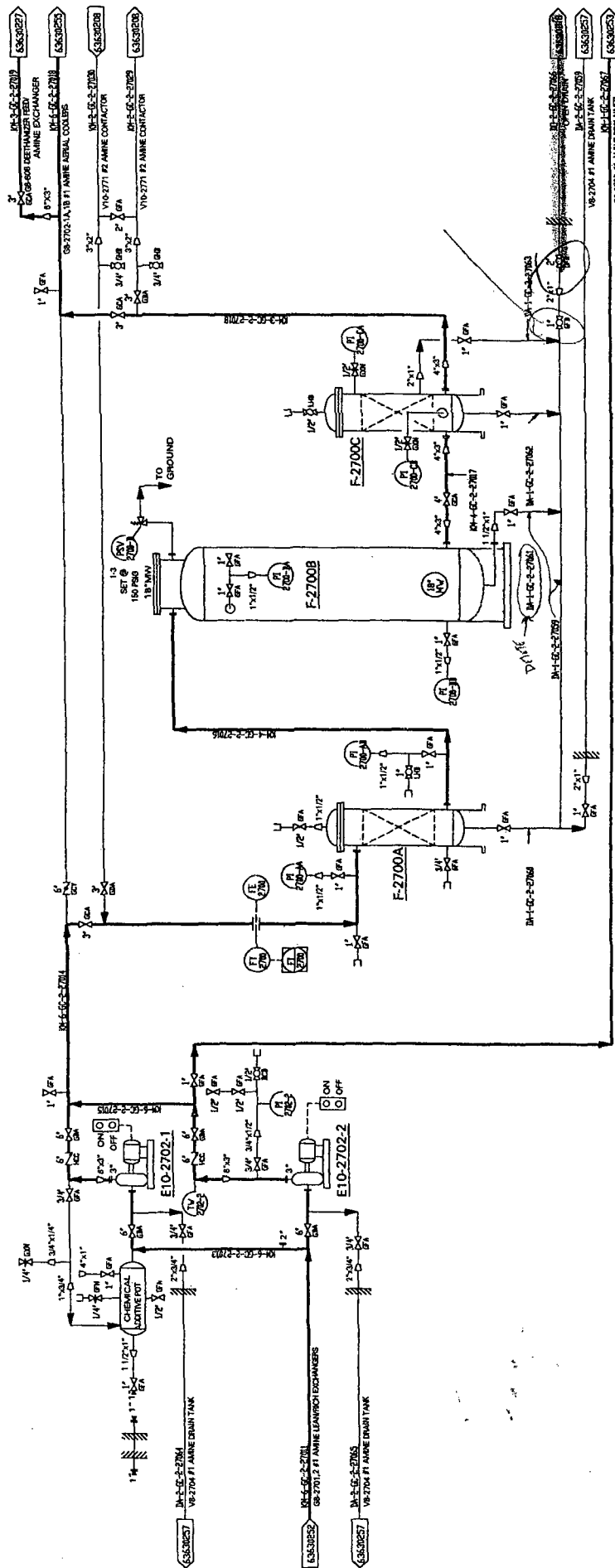
F-2
AFTER CHARCOAL FILTER

F-2
CHARCOAL FILTER

F-2
PRE CHARCOAL FILTER

E10-2
#1 AMINE CIRCULATION PUMP (WEST)

E10-2
#1 AMINE CIRCULATION PUMP (EAST)



EMPIRE ABO GAS PLANT
ELKHORN OPERATING CO.
MECHANICAL FLOW DIAGRAM
#1 AMINE SYSTEM

F-2700B	40"
V10-2701.1	40"

TIS RESOURCES

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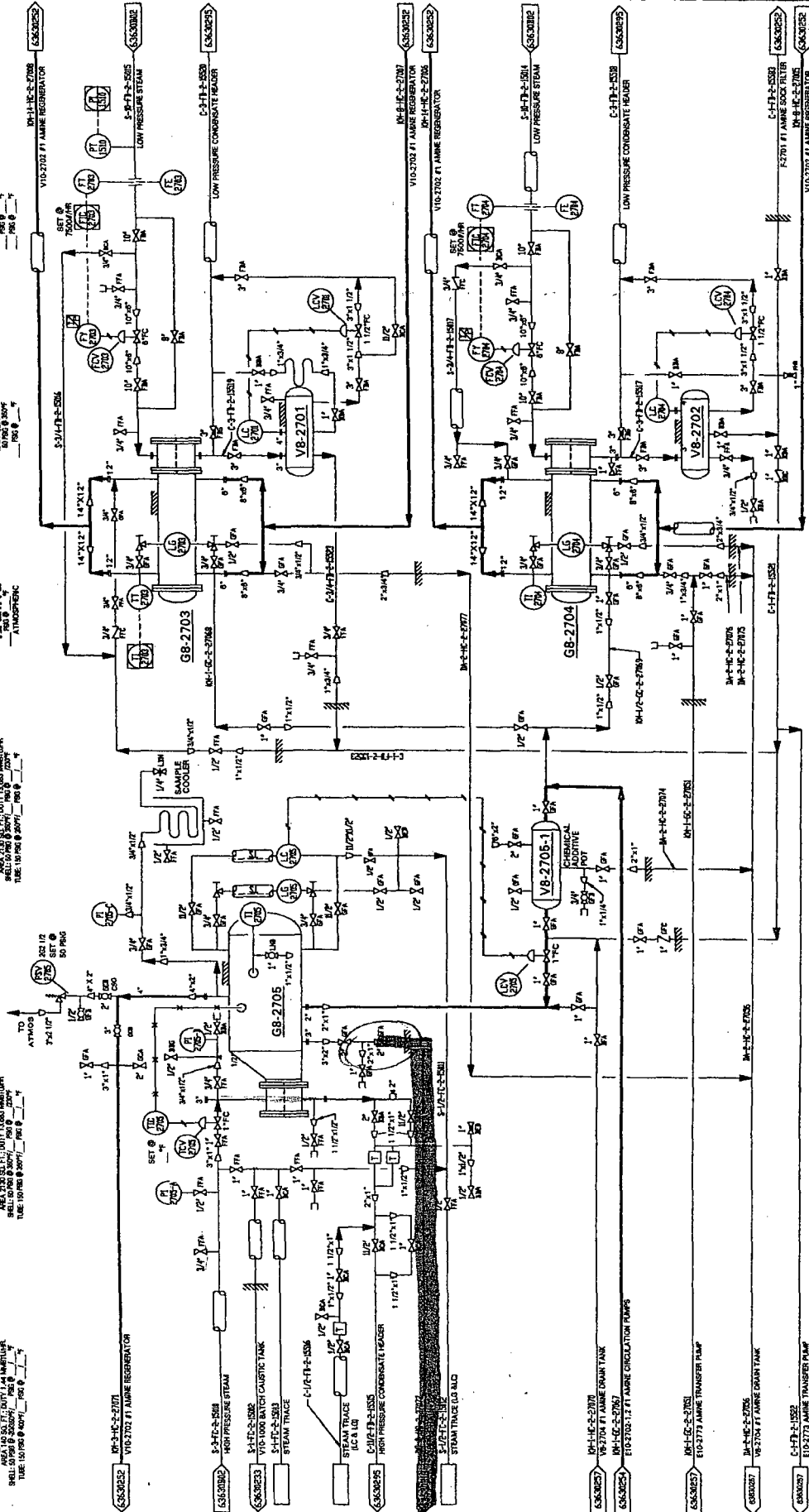
2705
#1 AMINE RECLAIMER
WATER TO 50 PSI, 100°F, 100 GPM
WATER TO 50 PSI, 100°F, 100 GPM
TUBE 100 PSI @ 50°F, 100 GPM

704
#1 AMINE REBOILER (WEST)
WATER TO 50 PSI, 100°F, 100 GPM
WATER TO 50 PSI, 100°F, 100 GPM
TUBE 100 PSI @ 50°F, 100 GPM

3
#1 AMINE REBOILER (EAST)
WATER TO 50 PSI, 100°F, 100 GPM
WATER TO 50 PSI, 100°F, 100 GPM
TUBE 100 PSI @ 50°F, 100 GPM

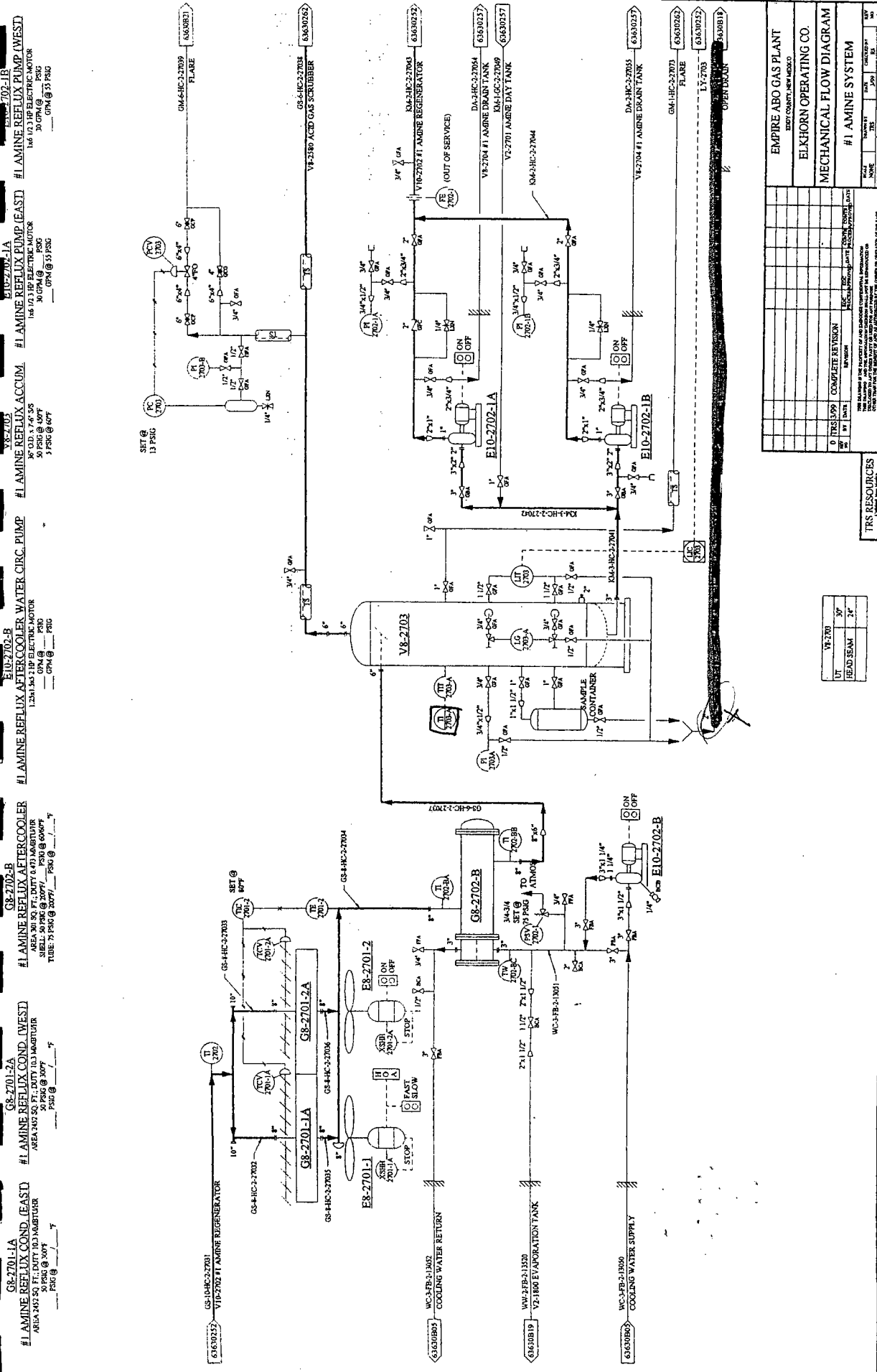
2701
#1 AMINE REBOILER (EAST)
WATER TO 50 PSI, 100°F, 100 GPM
WATER TO 50 PSI, 100°F, 100 GPM
TUBE 100 PSI @ 50°F, 100 GPM

2702
#1 AMINE REBOILER (WEST)
WATER TO 50 PSI, 100°F, 100 GPM
WATER TO 50 PSI, 100°F, 100 GPM
TUBE 100 PSI @ 50°F, 100 GPM

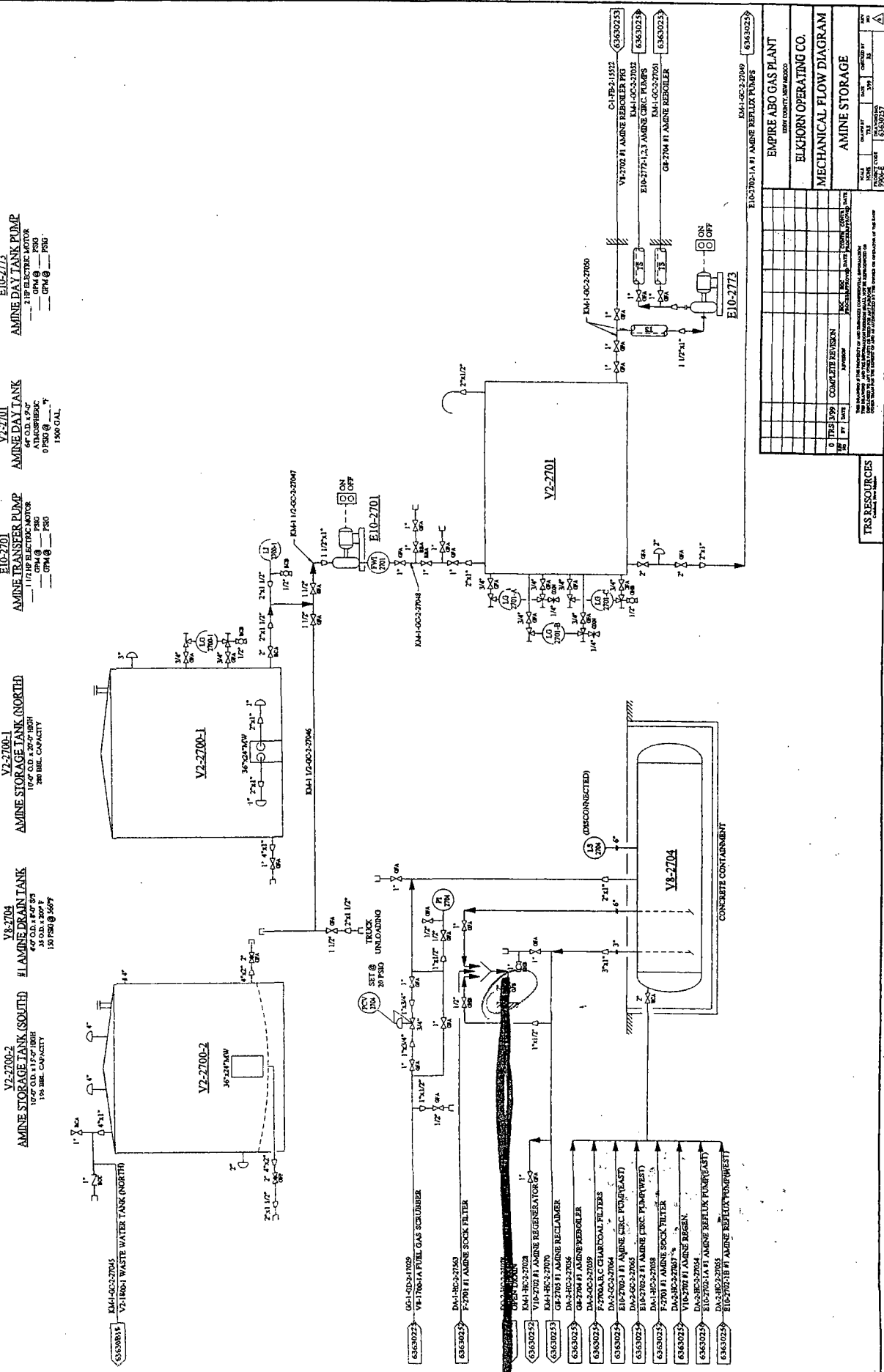


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EMPIRE ABO GAS PLANT
ELKHORN OPERATING CO.
MECHANICAL FLOW DIAGRAM
#1 AMINE SYSTEM
6500223



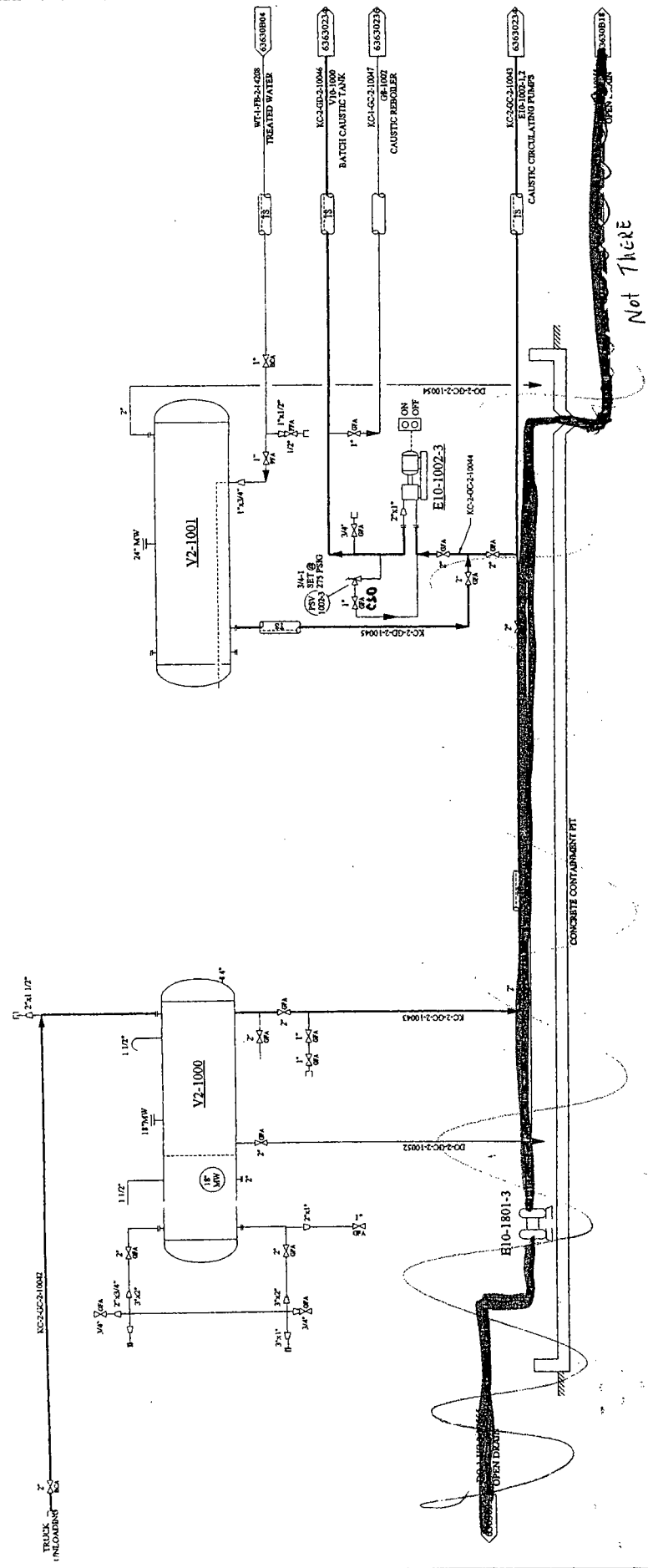
EMPIRE ABO GAS PLANT		ELKHORN OPERATING CO.		MECHANICAL FLOW DIAGRAM		#1 AMINE SYSTEM	
DATE	10/1/77	DESIGNED BY	W. J. BROWN	CHECKED BY	J. L. BROWN	APPROVED BY	J. L. BROWN
SCALE	AS SHOWN	PROJECT CODE	6360235	DATE	10/1/77	BY	J. L. BROWN
<p>THIS FLOW DIAGRAM IS THE PROPERTY OF ELKHORN OPERATING CO. AND IS NOT TO BE REPRODUCED OR COPIED IN ANY MANNER WITHOUT THE WRITTEN PERMISSION OF ELKHORN OPERATING CO.</p>							
<p>TRIS RESOURCES</p>							
<p>UT HEAD SEAM 24"</p>							



E10-1801-3
CAUSTIC CONTAINMENT DRAIN PUMP CAUSTIC STORAGE TANK
1" O.D. x 17'-4" S.S.
ATMOSP. PSIG @ 100°F
PSIG @ _____ °F

V2-1001
CAUSTIC MIX TANK
3" O.D. x 17'-4" S.S.
ATMOSP. PSIG @ 100°F
PSIG @ _____ °F

E10-1002-3
CAUSTIC CIRCULATING MIX PUMP (SPARE)
2 HP ELECTRIC MOTOR
11 CFM @ 250 PSIG
CFM @ _____ PSIG

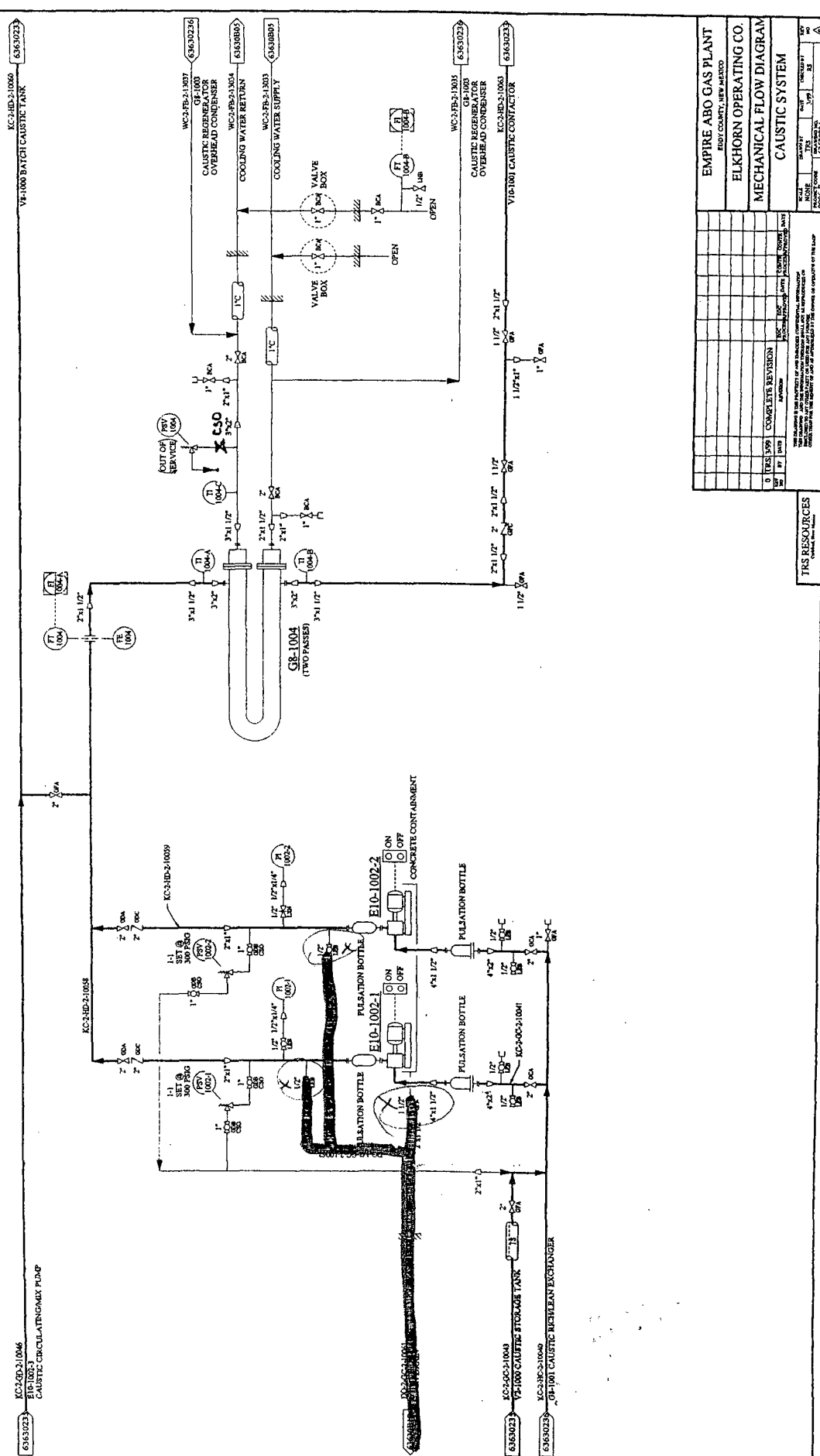


EMPIRE ABO GAS PLANT EAST COUNTY, NEW MEXICO	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
CAUSTIC SYSTEM	
DATE: 10/1/83	BY: J. L. HARRIS
PROJECT: 1000000000	REVISION: 1
TMS RESOURCES	

E10-1002-1
CAUSTIC CIRCULATION PUMP (EAST)
 1 1/4" 100 HP 3 PHASE ELECTRIC MOTOR
 11.0 GPM @ 250 PSIG

CR-1004
LEAN CAUSTIC COOLER
 AREA: 500 PSIG @ 650°F / 1201 LFT
 SHELL: 500 PSIG @ 650°F / 1201 LFT
 TUBE: 500 PSIG @ 650°F / 1201 LFT

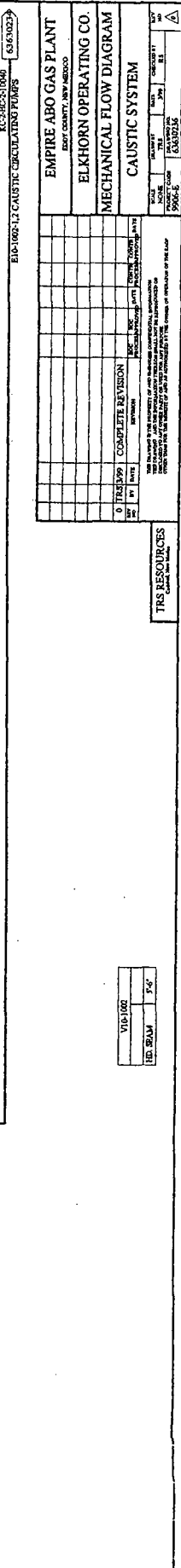
E10-1002-2
CAUSTIC CIRCULATION PUMP (WEST)
 1 1/4" 100 HP 3 PHASE ELECTRIC MOTOR
 11.0 GPM @ 250 PSIG



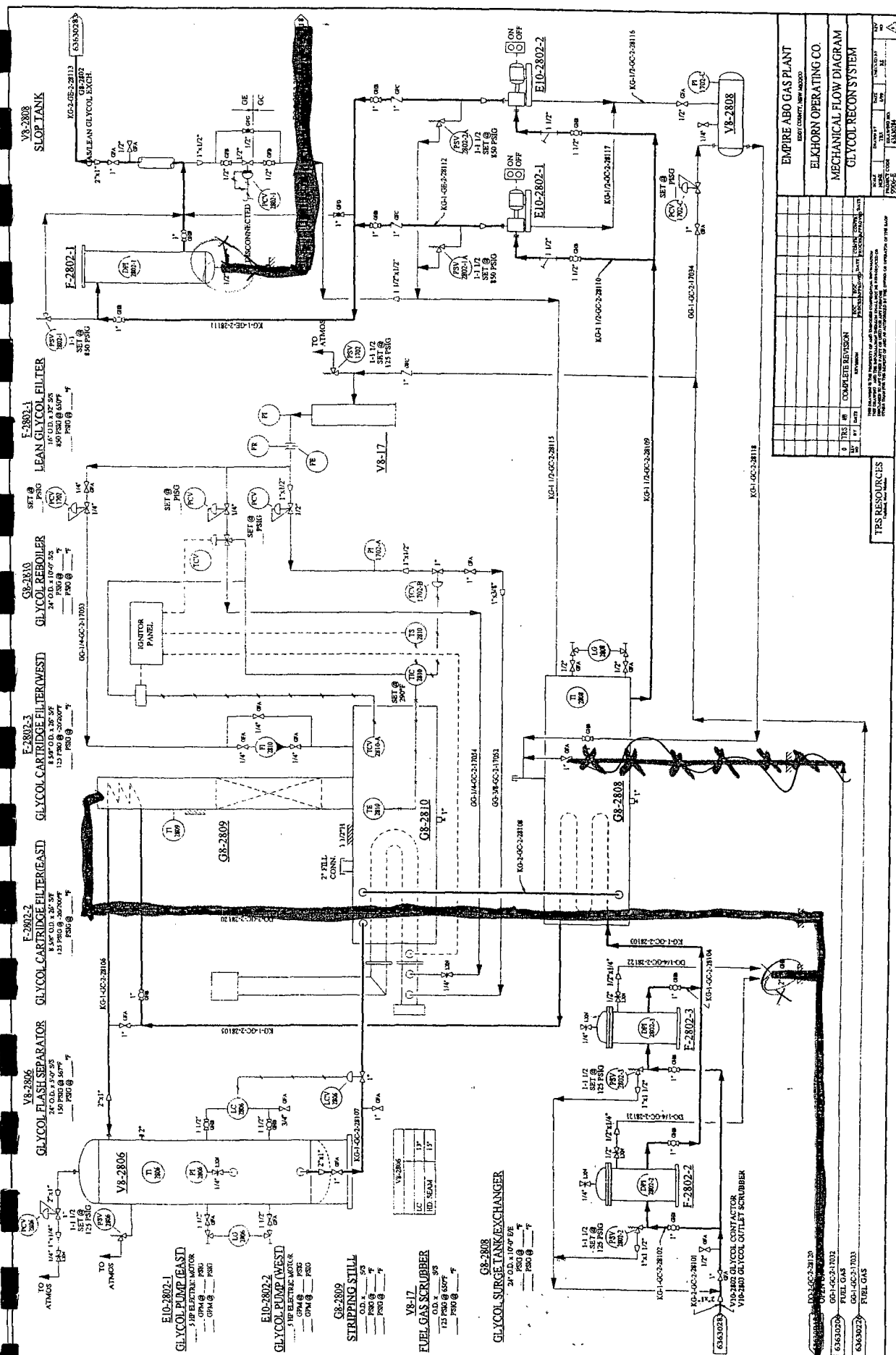
EMPIRE ABO GAS PLANT		E10-1002-1	
ELKHORN OPERATING CO.		E10-1002-2	
MECHANICAL FLOW DIAGRAM		E10-1002-3	
CAUSTIC SYSTEM		E10-1002-4	
TMS RESOURCES		E10-1002-5	
REVISIONS		E10-1002-6	
DATE		E10-1002-7	
BY		E10-1002-8	
CHECKED		E10-1002-9	
APPROVED		E10-1002-10	
SCALE		E10-1002-11	
SHEET NO.		E10-1002-12	
TOTAL SHEETS		E10-1002-13	
PROJECT NO.		E10-1002-14	
DRAWN BY		E10-1002-15	
CHECKED BY		E10-1002-16	
APPROVED BY		E10-1002-17	
DATE		E10-1002-18	
BY		E10-1002-19	
CHECKED		E10-1002-20	
APPROVED		E10-1002-21	
SCALE		E10-1002-22	
SHEET NO.		E10-1002-23	
TOTAL SHEETS		E10-1002-24	
PROJECT NO.		E10-1002-25	
DRAWN BY		E10-1002-26	
CHECKED BY		E10-1002-27	
APPROVED BY		E10-1002-28	
DATE		E10-1002-29	
BY		E10-1002-30	
CHECKED		E10-1002-31	
APPROVED		E10-1002-32	
SCALE		E10-1002-33	
SHEET NO.		E10-1002-34	
TOTAL SHEETS		E10-1002-35	
PROJECT NO.		E10-1002-36	
DRAWN BY		E10-1002-37	
CHECKED BY		E10-1002-38	
APPROVED BY		E10-1002-39	
DATE		E10-1002-40	
BY		E10-1002-41	
CHECKED		E10-1002-42	
APPROVED		E10-1002-43	
SCALE		E10-1002-44	
SHEET NO.		E10-1002-45	
TOTAL SHEETS		E10-1002-46	
PROJECT NO.		E10-1002-47	
DRAWN BY		E10-1002-48	
CHECKED BY		E10-1002-49	
APPROVED BY		E10-1002-50	
DATE		E10-1002-51	
BY		E10-1002-52	
CHECKED		E10-1002-53	
APPROVED		E10-1002-54	
SCALE		E10-1002-55	
SHEET NO.		E10-1002-56	
TOTAL SHEETS		E10-1002-57	
PROJECT NO.		E10-1002-58	
DRAWN BY		E10-1002-59	
CHECKED BY		E10-1002-60	
APPROVED BY		E10-1002-61	
DATE		E10-1002-62	
BY		E10-1002-63	
CHECKED		E10-1002-64	
APPROVED		E10-1002-65	
SCALE		E10-1002-66	
SHEET NO.		E10-1002-67	
TOTAL SHEETS		E10-1002-68	
PROJECT NO.		E10-1002-69	
DRAWN BY		E10-1002-70	
CHECKED BY		E10-1002-71	
APPROVED BY		E10-1002-72	
DATE		E10-1002-73	
BY		E10-1002-74	
CHECKED		E10-1002-75	
APPROVED		E10-1002-76	
SCALE		E10-1002-77	
SHEET NO.		E10-1002-78	
TOTAL SHEETS		E10-1002-79	
PROJECT NO.		E10-1002-80	
DRAWN BY		E10-1002-81	
CHECKED BY		E10-1002-82	
APPROVED BY		E10-1002-83	
DATE		E10-1002-84	
BY		E10-1002-85	
CHECKED		E10-1002-86	
APPROVED		E10-1002-87	
SCALE		E10-1002-88	
SHEET NO.		E10-1002-89	
TOTAL SHEETS		E10-1002-90	
PROJECT NO.		E10-1002-91	
DRAWN BY		E10-1002-92	
CHECKED BY		E10-1002-93	
APPROVED BY		E10-1002-94	
DATE		E10-1002-95	
BY		E10-1002-96	
CHECKED		E10-1002-97	
APPROVED		E10-1002-98	
SCALE		E10-1002-99	
SHEET NO.		E10-1002-100	

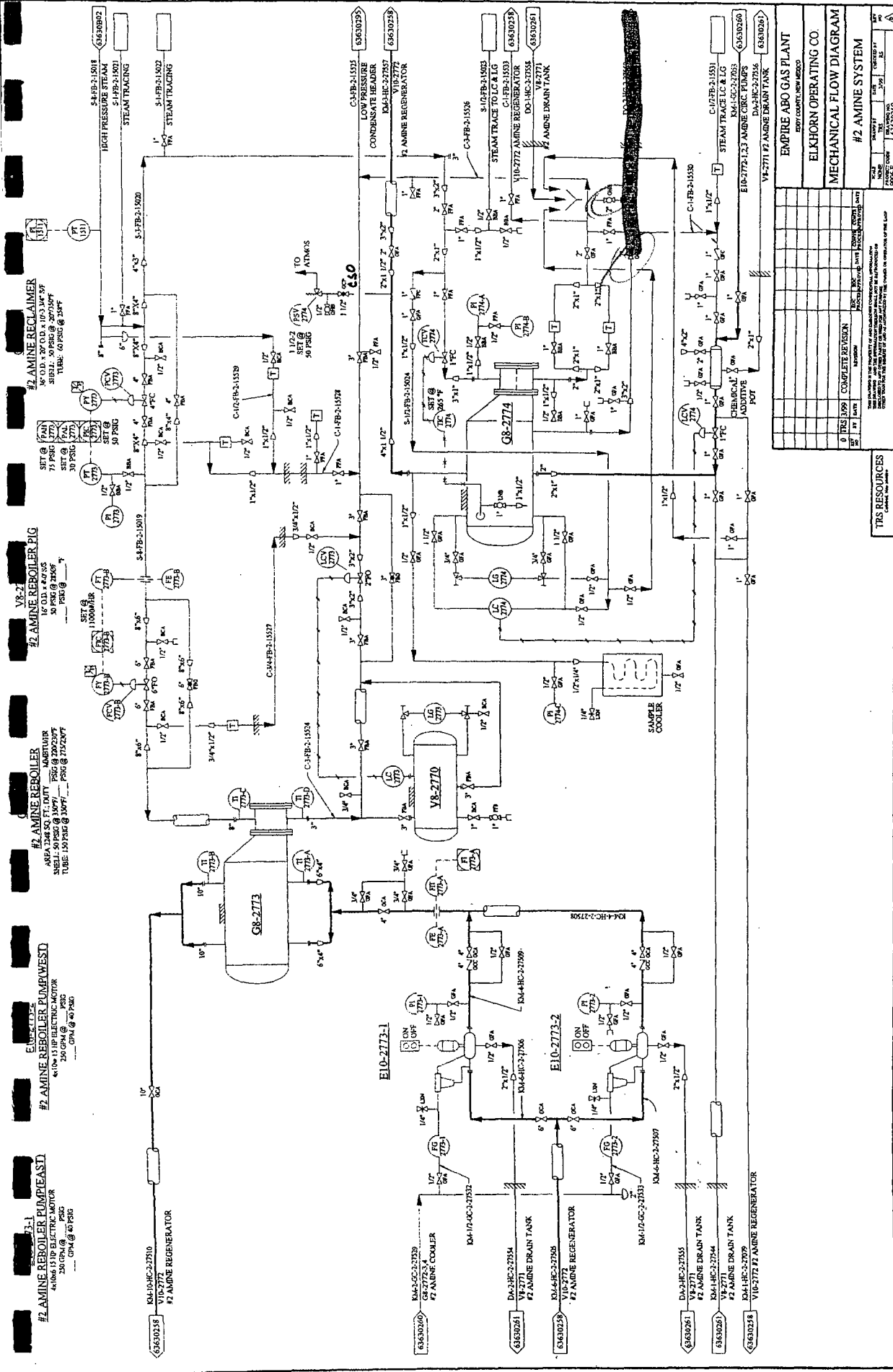
G8-1002
TIC REB
ET: NUTY?

Q6-100Z
TIC REP
FT.; DUTY 2
350°F/15 PSI
400°F/___ F



V10-1002	5'-6"
HD. SPAM	

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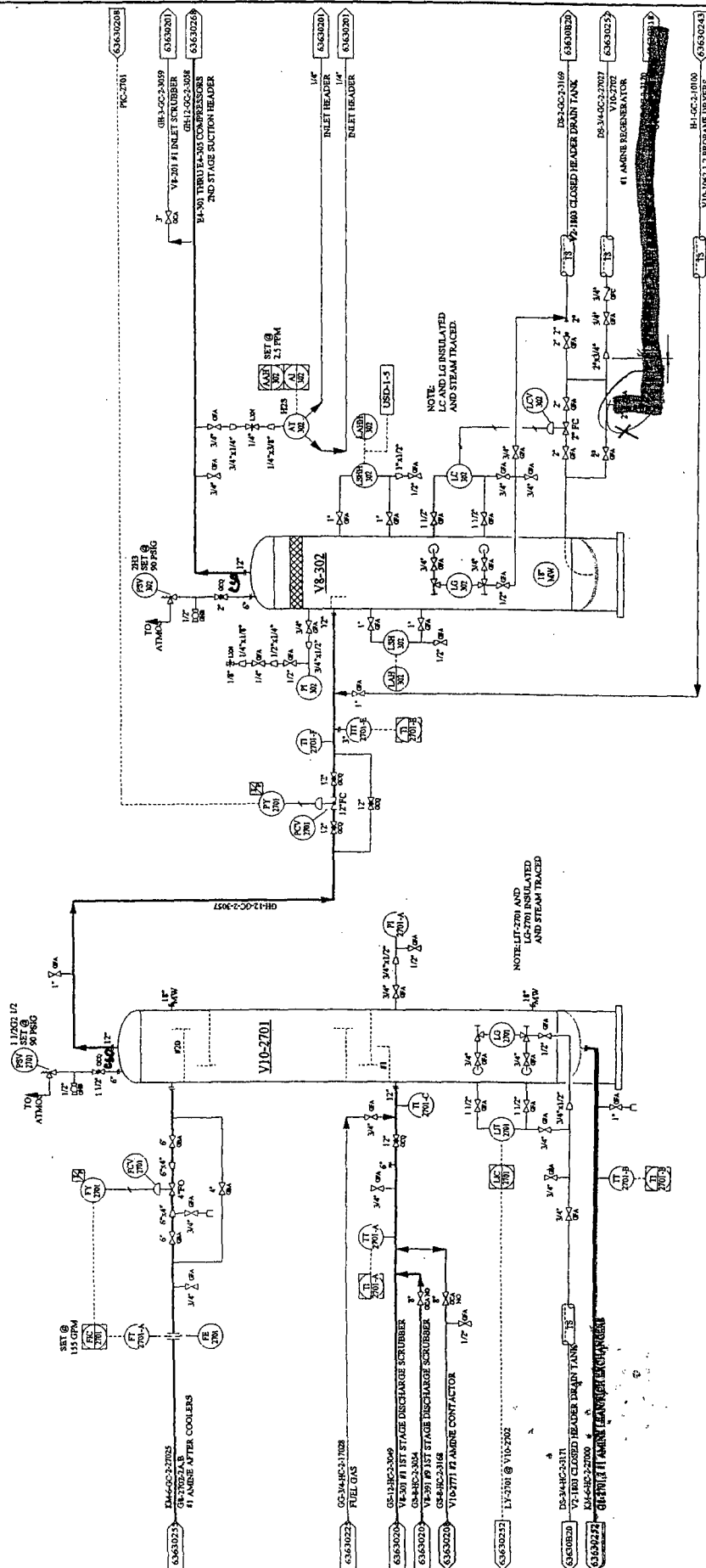


#2 AMINE REBOILER PUMPEAST		#2 AMINE REBOILER		#2 AMINE RECLAIMER	
4x106 15 HP ELECTRIC MOTOR 250 GPM @ 40 PSIG		4x106 15 HP ELECTRIC MOTOR 250 GPM @ 40 PSIG		10" O.D. x 20' L x 1/2" W 30 PSIG @ 2500' W TUBE: 1/2" O.D. x 10' L x 1/2" W 30 PSIG @ 2500' W	
E10-2773-1		E10-2773-2		E10-2773-3	
E10-2773-5		E10-2773-6		E10-2773-7	
E10-2773-9		E10-2773-10		E10-2773-11	
E10-2773-13		E10-2773-14		E10-2773-15	
E10-2773-17		E10-2773-18		E10-2773-19	
E10-2773-21		E10-2773-22		E10-2773-23	
E10-2773-25		E10-2773-26		E10-2773-27	
E10-2773-29		E10-2773-30		E10-2773-31	
E10-2773-33		E10-2773-34		E10-2773-35	
E10-2773-37		E10-2773-38		E10-2773-39	
E10-2773-41		E10-2773-42		E10-2773-43	
E10-2773-45		E10-2773-46		E10-2773-47	
E10-2773-49		E10-2773-50		E10-2773-51	
E10-2773-53		E10-2773-54		E10-2773-55	
E10-2773-57		E10-2773-58		E10-2773-59	
E10-2773-61		E10-2773-62		E10-2773-63	
E10-2773-65		E10-2773-66		E10-2773-67	
E10-2773-69		E10-2773-70		E10-2773-71	
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E10-2773-265		E10-2773-266		E10-2773-267	
E10-2773-269		E10-2773-270		E10-2773-271	
E10-2773					

V10-2701
 #1 AMINE CONTACTOR
 5'0" I.D. x 7'4" S.S.
 90 PSIG @ 140°F
 60 PSIG @ 100°F

V10-2701
 #1 AMINE CONTACTOR
 5'0" I.D. x 7'4" S.S.
 90 PSIG @ 140°F
 60 PSIG @ 100°F

V10-2701
 #1 AMINE CONTACTOR
 5'0" I.D. x 7'4" S.S.
 90 PSIG @ 140°F
 60 PSIG @ 100°F



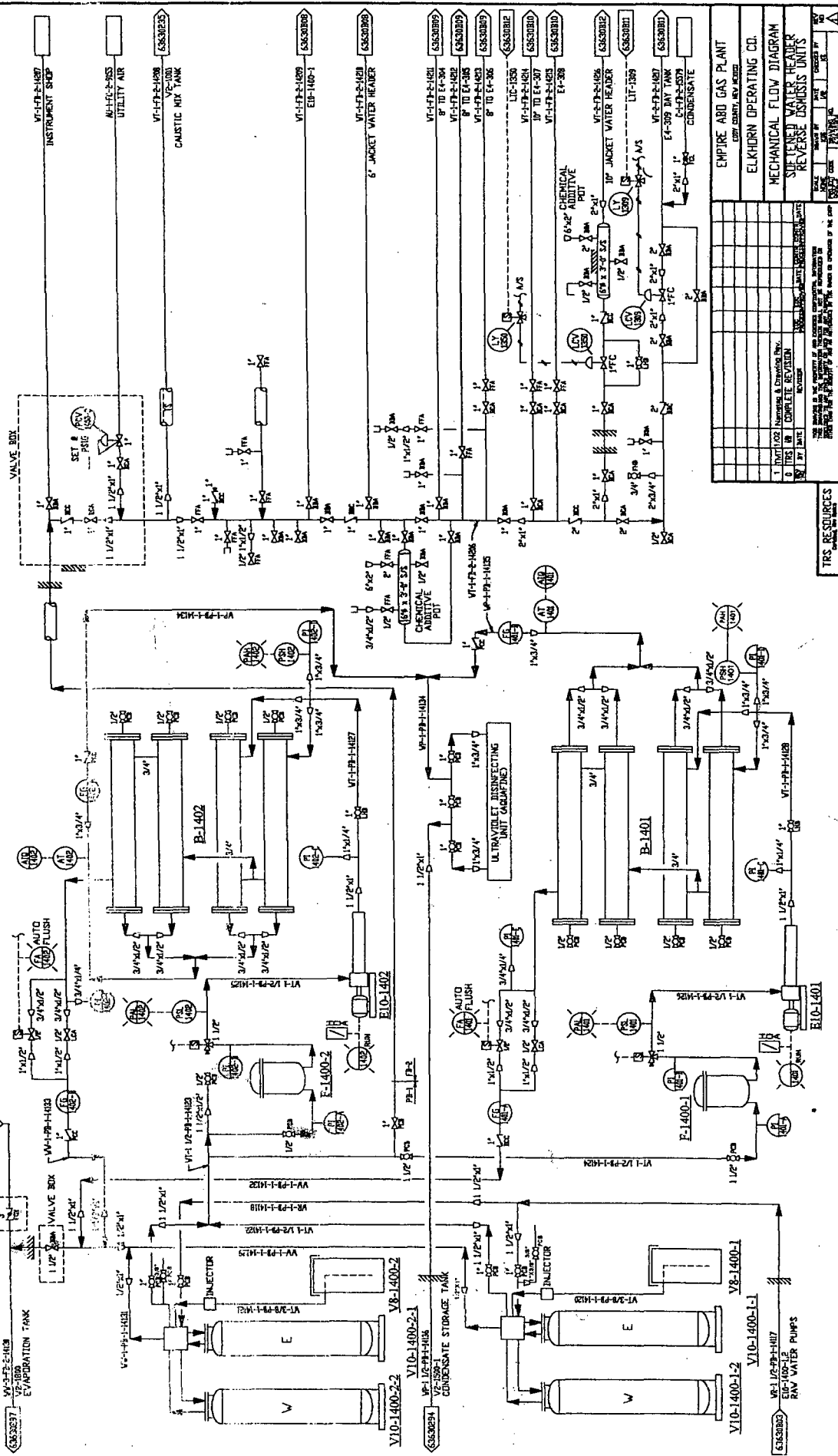
EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
#1 AMINE CONTACTOR	
2ND STAGE SCRUBBER	
SCALE	1" = 10'
DATE	11/1/77
BY	W. J. BROWN
CHECKED BY	W. J. BROWN
APPROVED BY	W. J. BROWN
DESIGNED BY	W. J. BROWN
REVISION	1
DATE	11/1/77
BY	W. J. BROWN
CHECKED BY	W. J. BROWN
APPROVED BY	W. J. BROWN
DESIGNED BY	W. J. BROWN

1" = 10'	1" = 10'
1" = 10'	1" = 10'
1" = 10'	1" = 10'

1" = 10'	1" = 10'
1" = 10'	1" = 10'
1" = 10'	1" = 10'

THESE RESOURCES

2/



TRS RESOURCES

7-9866

EMPIRE ABD GAS PLANT

EDISON COUNTY, NEW MEXICO

ELKHORN OPERATING CO.

MECHANICAL FLOW DIAGRAM

SUSTAINED WATER HEADER
NO. 8 PIPE CONCRETE LINING

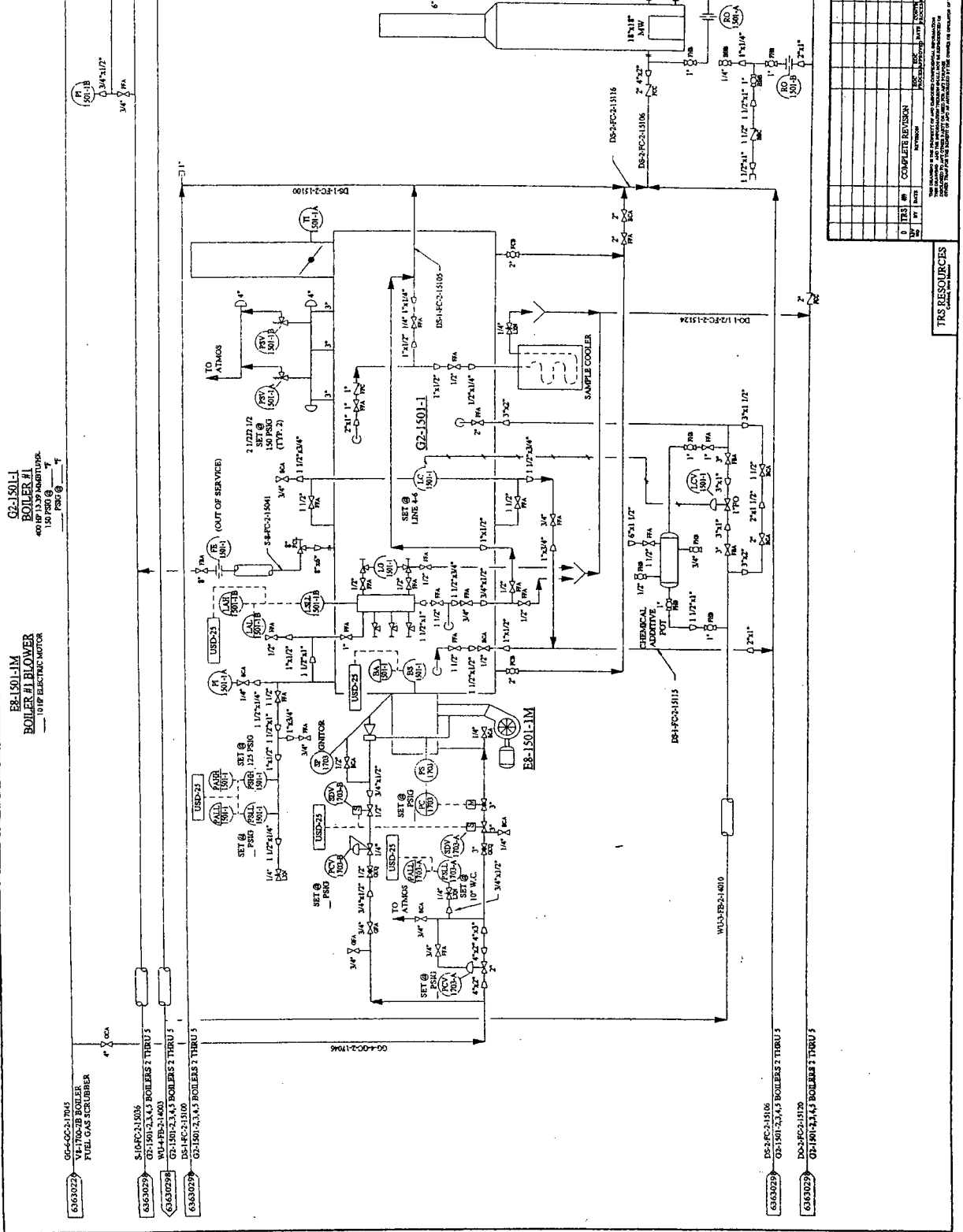
REVERSE ANALYSIS UNITS	ANALYSIS UNIT	ANALYSIS UNIT	ANALYSIS UNIT
1	2	3	4

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7 0076

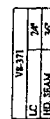
E8-150-1-M
BOILER #1 BLOWER
 10 HP ELECTRIC MOTOR

G2-150-1-M
 BOILER #1
 400 HP ELECTRIC MOTOR
 150 PSIG @ 175°F



EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
BOILER #1	
DATE	10/1/78
BY	W. J. B.
CHECKED BY	W. J. B.
APPROVED BY	W. J. B.
PROJECT NO.	6440178
REVISION	1
DESCRIPTION	COMPLETE DESIGN
SCALE	AS SHOWN
NOTES	SEE SPECIFICATIONS FOR MATERIALS AND DIMENSIONS. ALL DIMENSIONS ARE IN INCHES UNLESS OTHERWISE SPECIFIED.

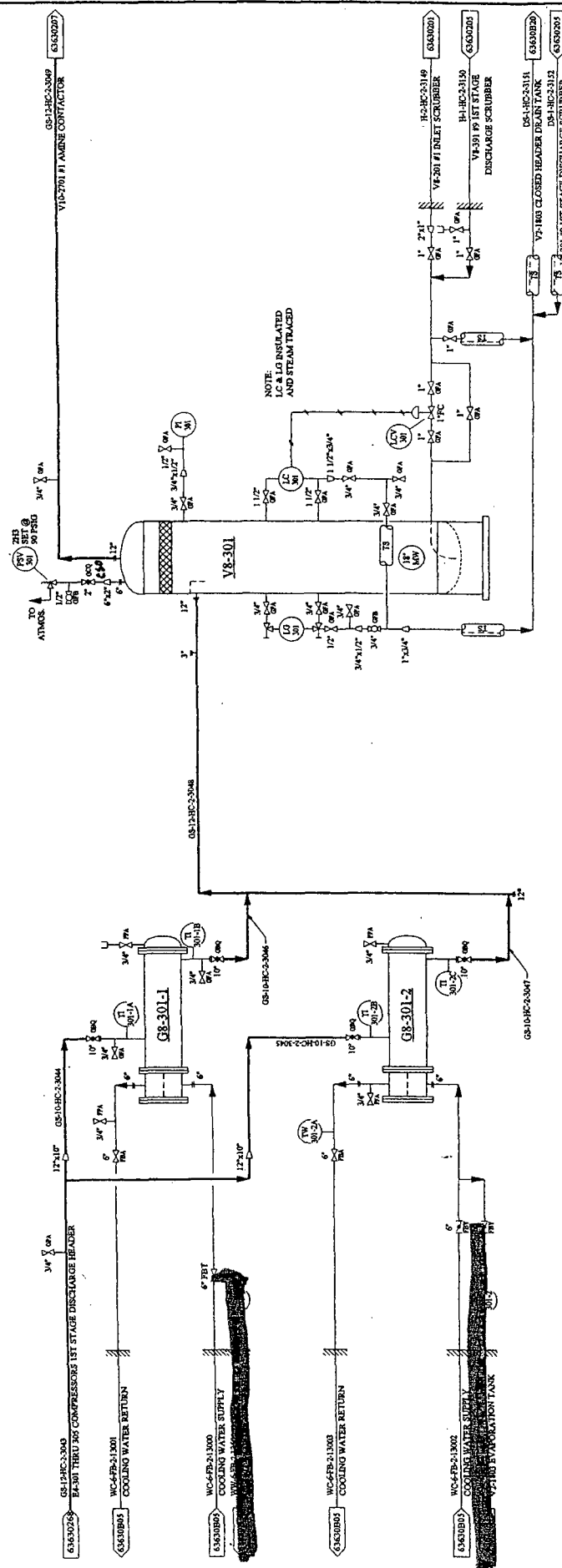
TRIS RESOURCES

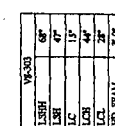
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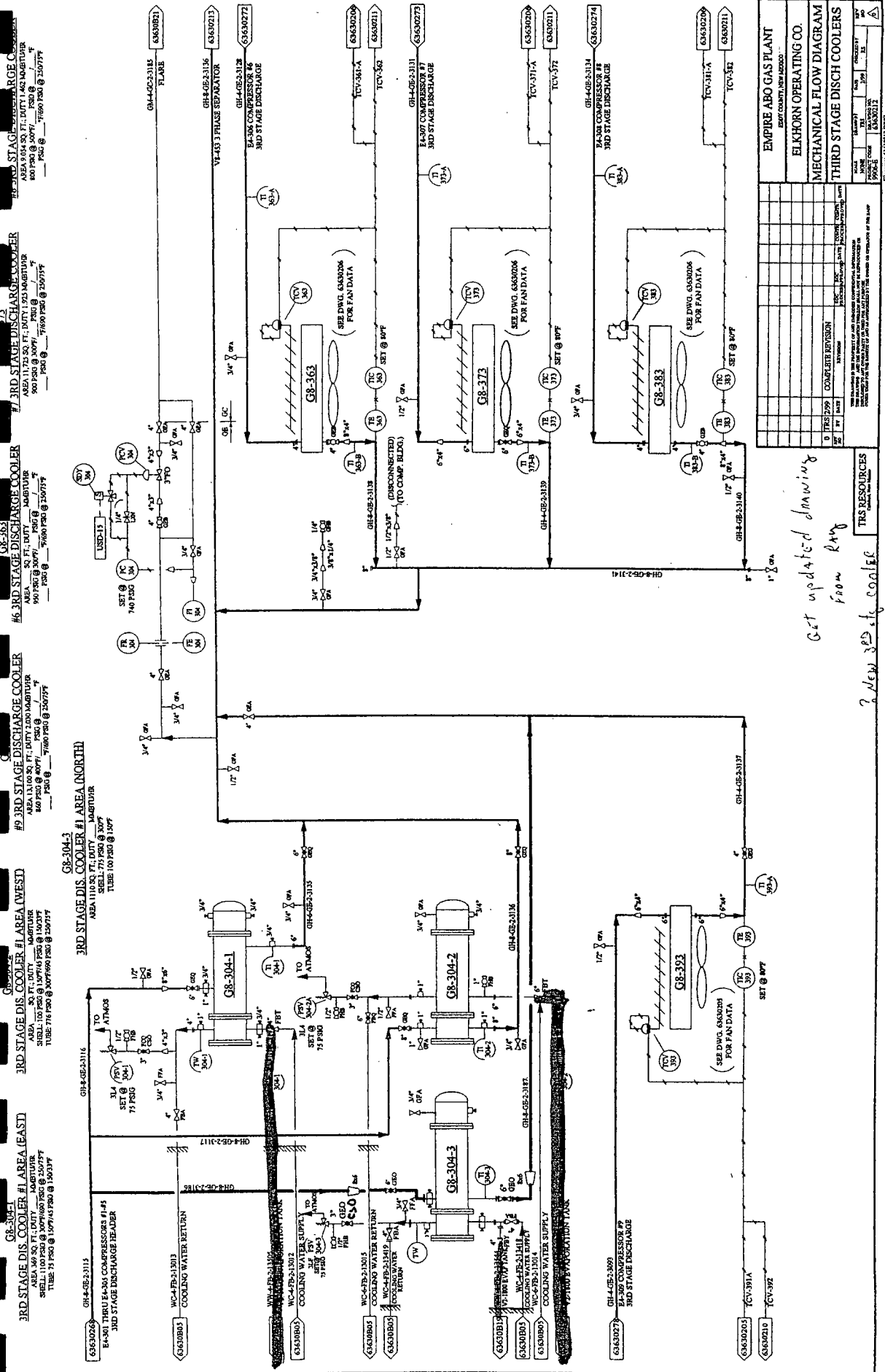
OK NO	ST RS	DATE TIME	TBL FRT	BOOK CODES E-9006-E 9006-E	ORIGIN NO. 6367006
----------	----------	--------------	------------	----------------------------------	-----------------------

GS-301-1
#1 1ST STAGE DISCHARGE COOLER (EAST)
 AREA 1721 SQ. FT. DUTY 1.869 ADJUSTER
 SHELL: 150 P530 @ 3007
 TUBE: 75 P530 @ 1507

GS-301-2
#1 1ST STAGE DISCHARGE COOLER (WEST)
 AREA 1721 SQ. FT. DUTY 1.869 ADJUSTER
 SHELL: 150 P530 @ 3007
 TUBE: 75 P530 @ 1507

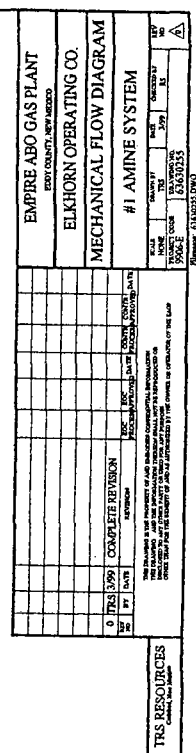
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EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
THIRD STAGE DISCH COOLERS	
DATE	10/1/77
BY	WJ
CHKD	WJ
APP'D	WJ
DESIGNED BY	WJ
PROJECT NO.	63630273
FIGURE NO.	1

Get updated drawing
from Ray
2 New 3rd stage cooler



1

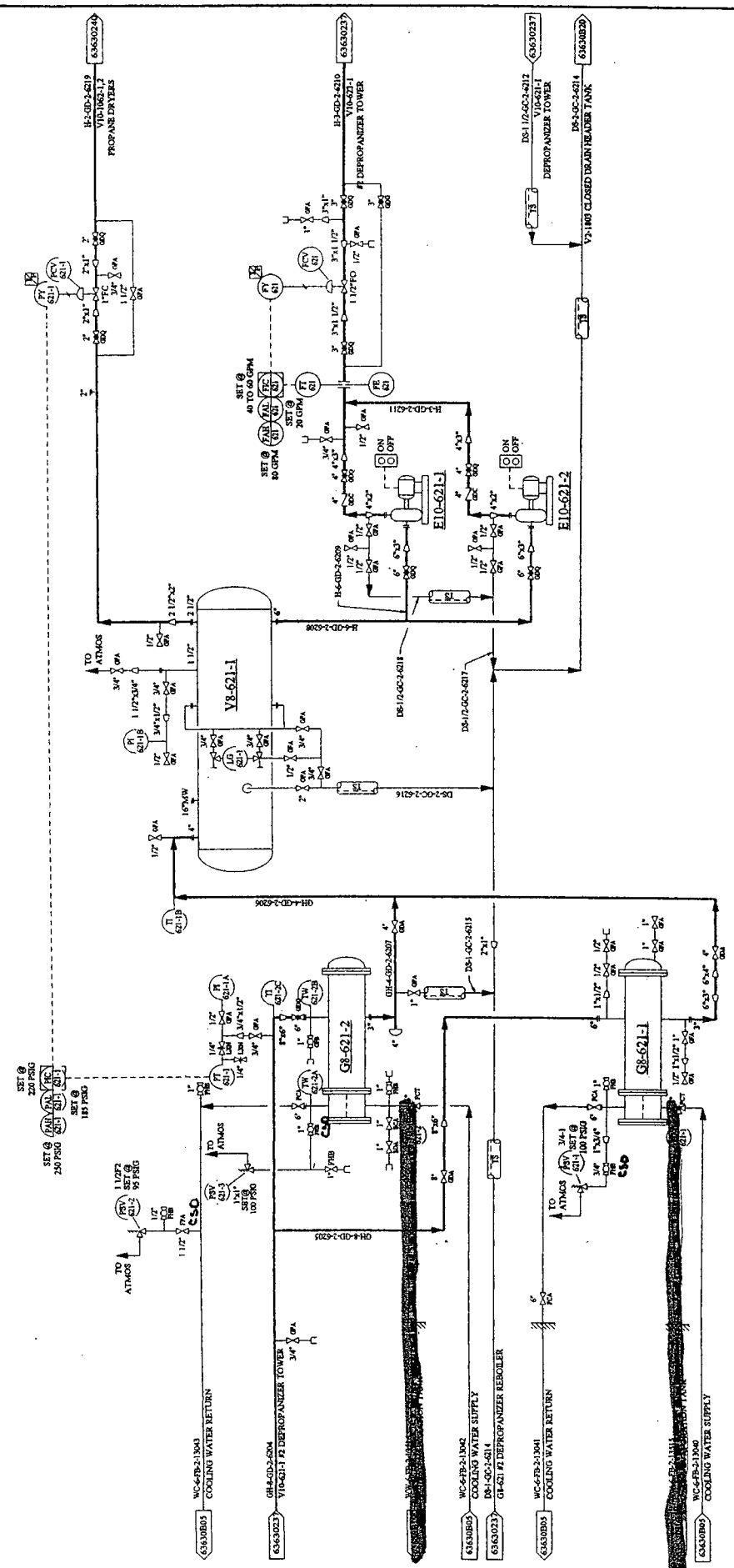
GR-621-1
#2 DEPROPANIZER OVERHEAD CONDENSER (EAST)
 AREA 250 SQ. FT. DUTY 4075 MMBTU/H
 SHELL 100 PSIG @ 200°F / 100 PSIG @ 100°F
 TUBE 100 PSIG @ 200°F / 100 PSIG @ 100°F
 SIZE 31-192

GR-621-2
#2 DEPROPANIZER OVERHEAD CONDENSER (WEST)
 AREA 250 SQ. FT. DUTY 4075 MMBTU/H
 SHELL 100 PSIG @ 200°F / 100 PSIG @ 100°F
 TUBE 100 PSIG @ 200°F / 100 PSIG @ 100°F
 SIZE 31-192

V8-621-1
#2 DEPROPANIZER REFLUX ACCUMULATOR
 AREA 250 SQ. FT. DUTY 4075 MMBTU/H
 SHELL 100 PSIG @ 200°F / 100 PSIG @ 100°F
 TUBE 100 PSIG @ 200°F / 100 PSIG @ 100°F
 SIZE 31-192

E10-621-1
#2 DEPROPANIZER REFLUX PUMP (EAST)
 15 HP ELECTRIC MOTOR
 210 GPM @ 750
 0.75 HP @ 750

E10-621-2
#2 DEPROPANIZER REFLUX PUMP (WEST)
 15 HP ELECTRIC MOTOR
 210 GPM @ 750
 0.75 HP @ 750



EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
PROPANE SYSTEM	
DATE	10/1/77
BY	W. J. BROWN
CHECKED BY	W. J. BROWN
APPROVED BY	W. J. BROWN
SCALE	AS SHOWN
PROJECT NO.	636023
REVISION	1

TSS RESOURCES

Y8-2953
PROANE REFRIGERANT ACCUMULATOR
4" O.D. x 20'-0" H
125 PSIG @ 150°F
1.50 PSIG @ 300°F

Q8-2951-A
1ST PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

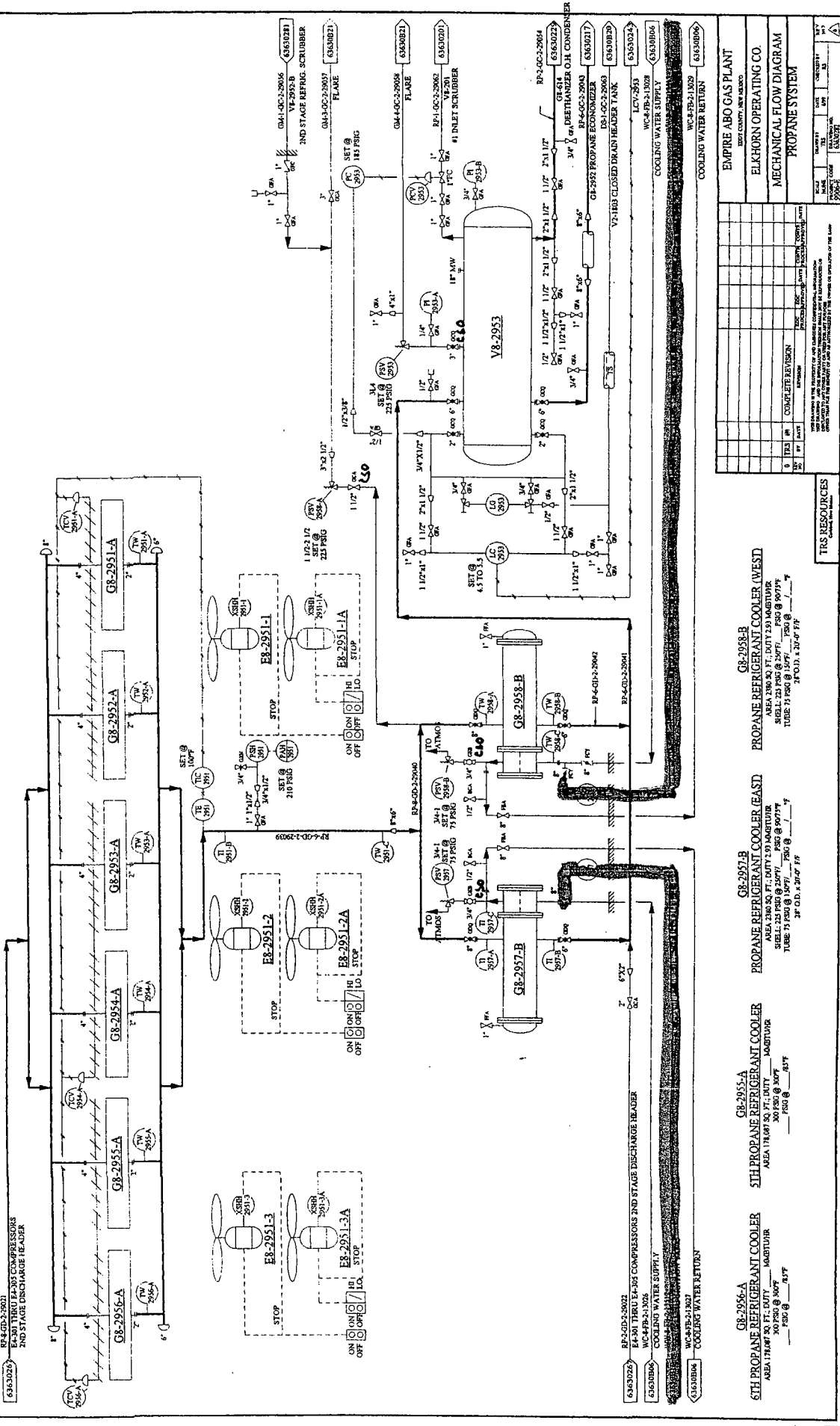
Q8-2952-A
2ND PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2953-A
3RD PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2954-A
4TH PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2955-A
5TH PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2956-A
6TH PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F



ITEM NO.	DESCRIPTION	QUANTITY	UNIT	REMARKS
1	PROANE REFRIGERANT ACCUMULATOR	1	EA	
2	PROANE REFRIGERANT COOLER	6	EA	
3	PROANE REFRIGERANT COMPRESSOR	6	EA	
4	COOLING WATER SUPPLY	1	IN	
5	COOLING WATER RETURN	1	IN	

ITEM NO.	DESCRIPTION	QUANTITY	UNIT	REMARKS
6	PROANE REFRIGERANT ACCUMULATOR	1	EA	
7	PROANE REFRIGERANT COOLER	6	EA	
8	PROANE REFRIGERANT COMPRESSOR	6	EA	
9	COOLING WATER SUPPLY	1	IN	
10	COOLING WATER RETURN	1	IN	

TDS RESOURCES
COURTESY OF THE LAR

Q8-2958-B
PROANE REFRIGERANT COOLER (WEST)
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2957-B
PROANE REFRIGERANT COOLER (EAST)
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2955-A
5TH PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2956-A
6TH PROANE REFRIGERANT COOLER
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-2953-B
PROANE REFRIGERANT COOLER (EAST)
AREA 17A.07 50 FT. DUTY
300 PSIG @ 300°F
1.50 PSIG @ 150°F

Q8-611 DEETHANIZER FEED EXCHANGER/CONDENSER

17' x 24" 81 3/4" I.D. DUTY: 2.31 MAGDTU
SHELL: 600 PSIG @ 240°F/500 PSIG @ 300°F/74
TUBE: 600 PSIG @ 300°F/500 PSIG @ 375°F/74

Q8-613 DEETHANIZER BOTTOMS COOLER

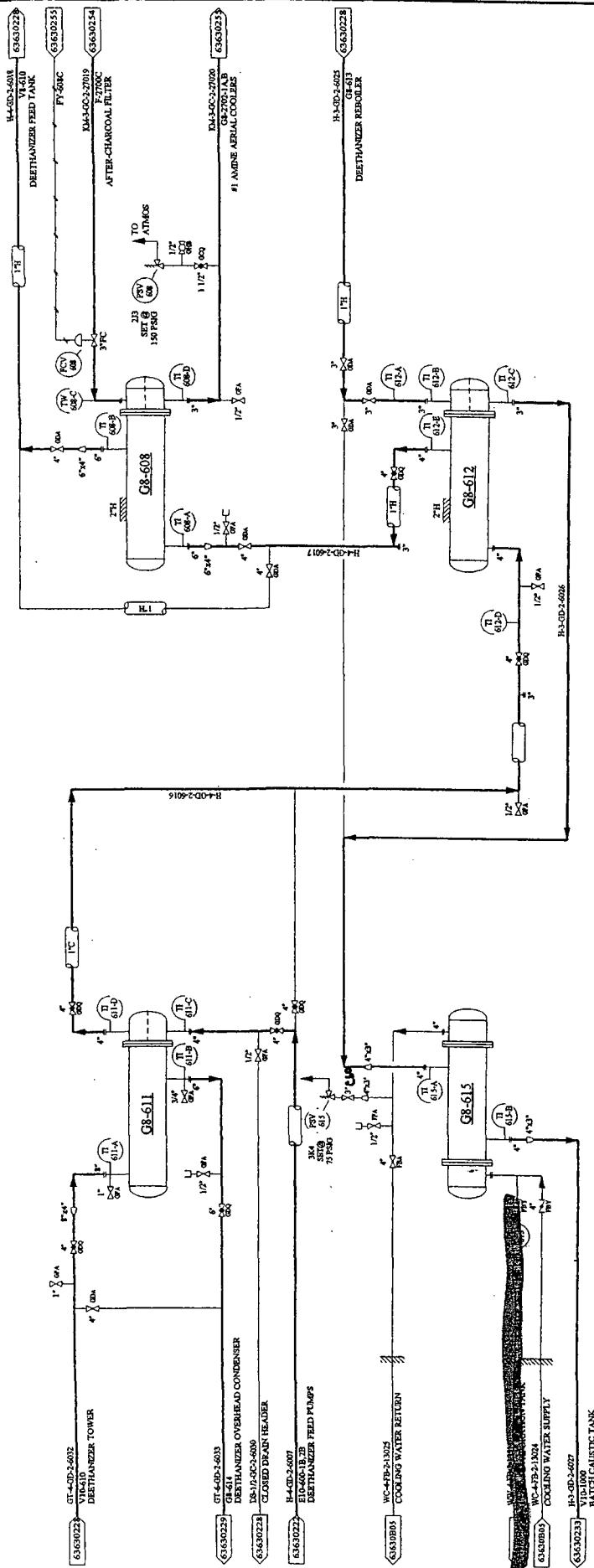
8' x 24" 33 1/2" I.D. DUTY: 1.33 MAGDTU
SHELL: 55 PSIG @ 240°F/500 PSIG @ 130°F/147
TUBE: 55 PSIG @ 147°F/500 PSIG @ 130°F/147

Q8-608 DEETHANIZER FEED/AMINE EXCHANGER

17' x 24" 24 3/4" I.D. DUTY: 2.31 MAGDTU
SHELL: 600 PSIG @ 240°F/500 PSIG @ 140°F/47
TUBE: 600 PSIG @ 240°F/500 PSIG @ 140°F/47

Q8-612 DEETHANIZER FEED HEATER

240 SQ. FT. DUTY: 1.63 MAGDTU
SHELL: 600 PSIG @ 240°F/500 PSIG @ 140°F/47
TUBE: 600 PSIG @ 240°F/500 PSIG @ 140°F/47



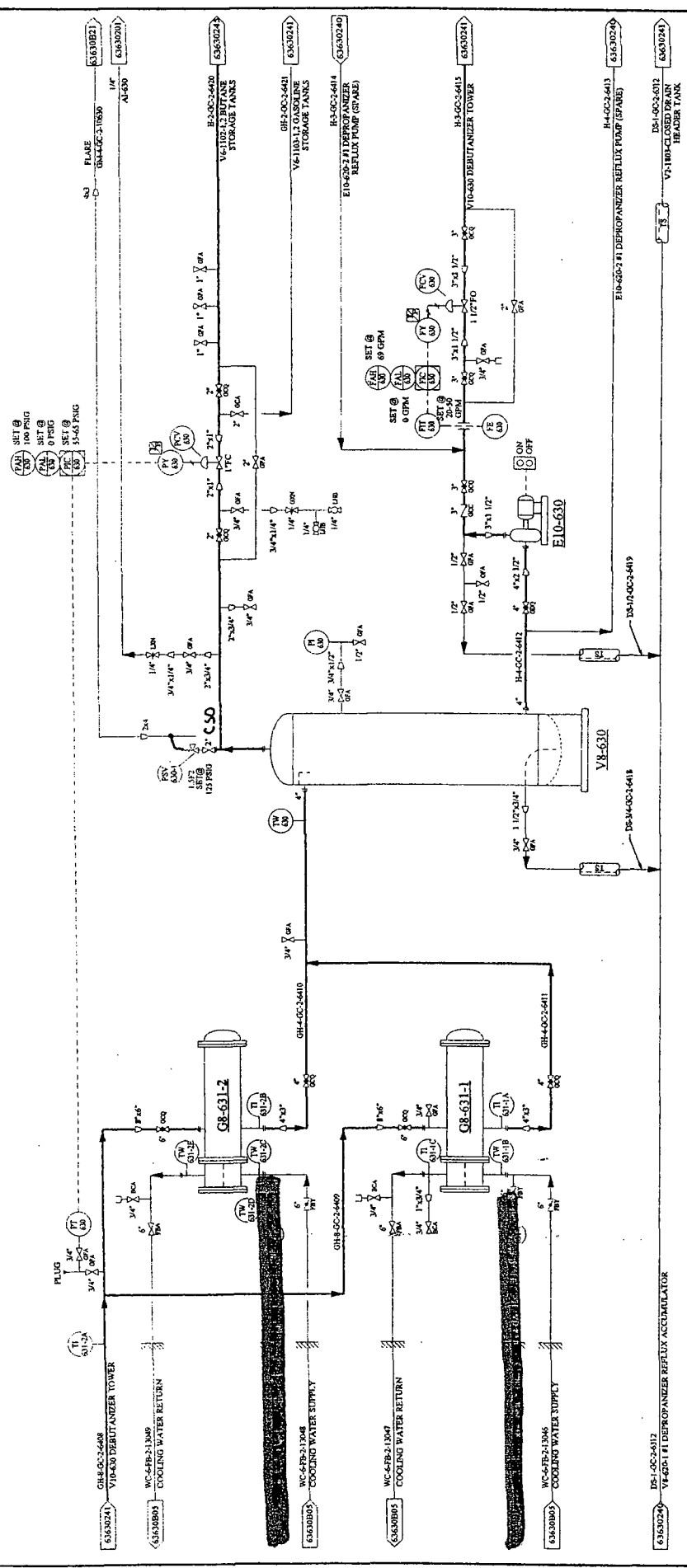
EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
DEETHANIZER EXCHANGERS	
TITUS RESOURCES 10000 10th Street, Suite 100 Denver, CO 80202 Phone: (303) 733-7777	
PROJECT NO. 10000 10th Street, Suite 100 Denver, CO 80202 Phone: (303) 733-7777	SHEET NO. 10000 10th Street, Suite 100 Denver, CO 80202 Phone: (303) 733-7777

G8-631-1
DEBUTANIZER OVERHEAD CONDENSER (EAST)
 AREA: 30 FT. DUTY
 SHELL: 150 PSIG @ 300°F
 TUBE: 100 PSIG @ 300°F

G8-631-2
DEBUTANIZER OVERHEAD CONDENSER (WEST)
 AREA: 30 FT. DUTY
 SHELL: 150 PSIG @ 300°F
 TUBE: 100 PSIG @ 300°F

V8-630
DEBUTANIZER REFLUX ACCUMULATOR
 AREA: 150 PSIG @ 300°F
 TUBE: 100 PSIG @ 300°F

E10-630
DEBUTANIZER REFLUX PUMP (MAIN)
 1/200 HP
 1/200 HP @ 300°F
 1/200 HP @ 300°F



EMPIRE ABO GAS PLANT
ELKHORN OPERATING CO.
MECHANICAL FLOW DIAGRAM
DEBUTANIZER SYSTEM
DATE: 10/1/60
BY: J. H. HARRIS
CHECKED: J. H. HARRIS
APPROVED: J. H. HARRIS
PROJECT: 630000
FIGURE: 630000-1

VR-630	2-0"
ID-630	2-0"

TR-630	2-0"
ID-630	2-0"

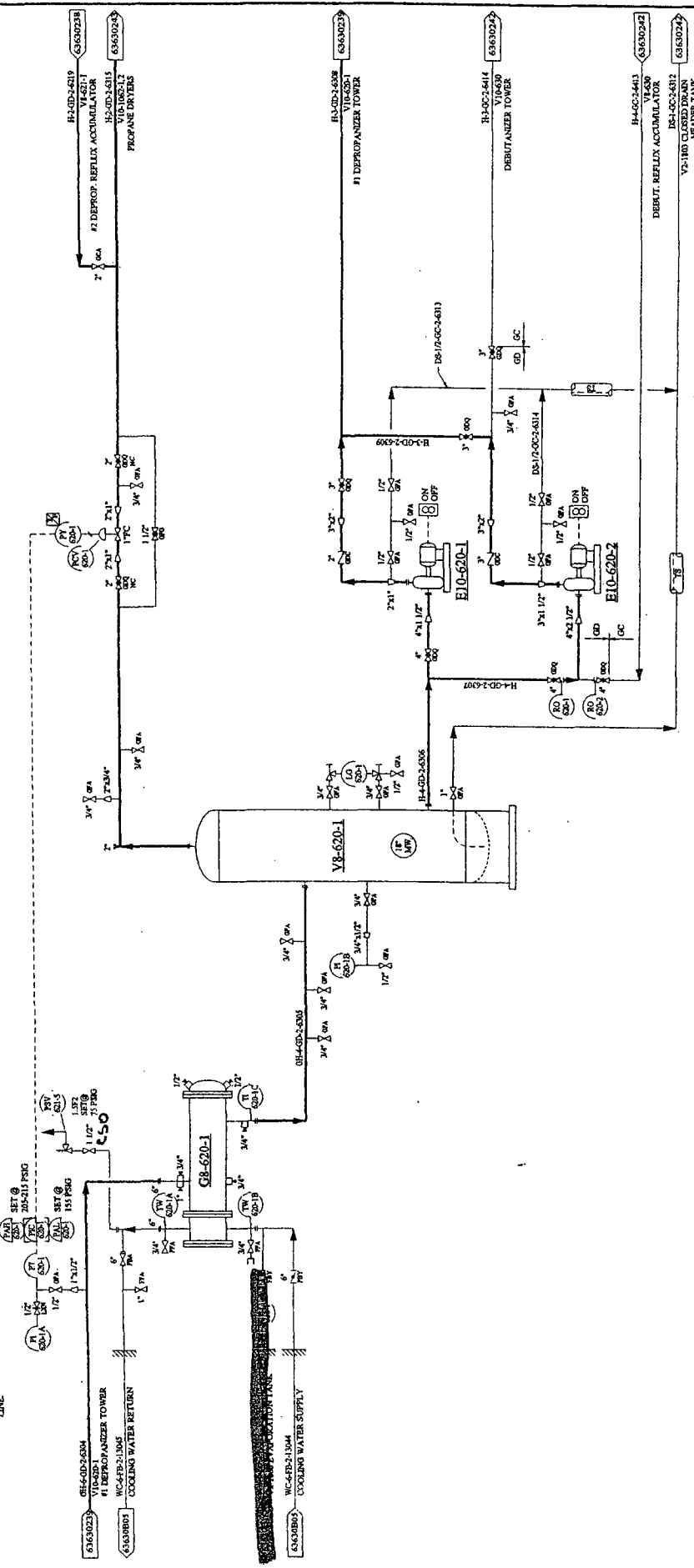
G8-620-1
#1 DEPROPANIZER OVERHEAD CONDENSER
 250 PSIG
 12" DIA. 10' LONG
 SHEET PILE
 TUBES 71.500 @ 1.571" PSIG
 SIZE: 19-4-240

VR-620-1
#1 DEPROPANIZER REFLUX ACCUMULATOR
 1.074" DIA. 2.5 HP ELECTRIC MOTOR
 300 PSIG @ 200°F
 750 @ 75°F

E10-620-1
#1 DEPROPANIZER REFLUX PUMP (MAIN)
 1.074" DIA. 2.5 HP ELECTRIC MOTOR
 300 PSIG @ 200°F
 750 @ 75°F

E10-620-2
#1 DEPROPANIZER REFLUX PUMP (SPARE)
 1.074" DIA. 2.5 HP ELECTRIC MOTOR
 300 PSIG @ 200°F
 750 @ 75°F

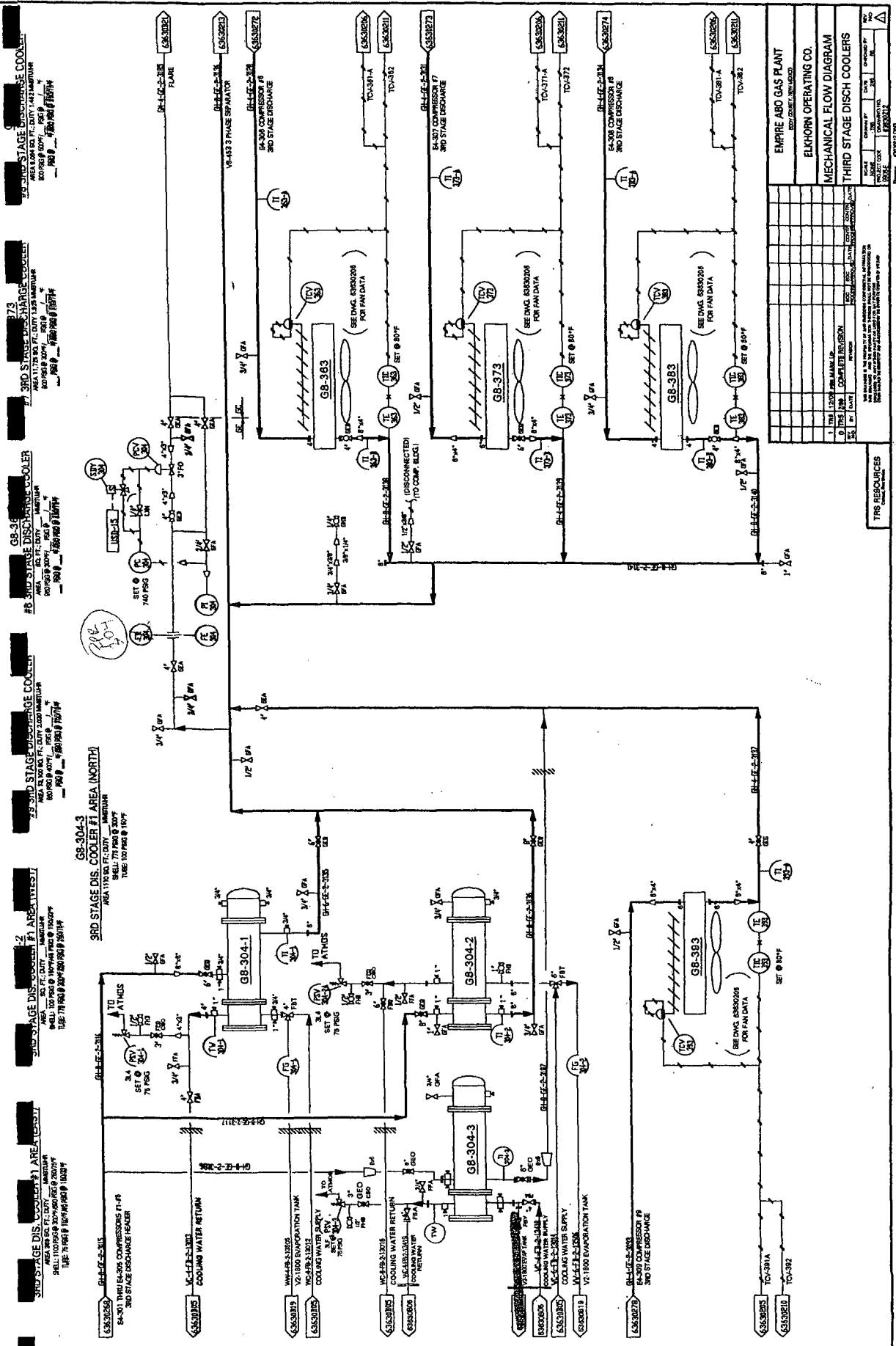
NOTE: PFC-620-1 IS HEAT
 TRACED AT THE IMPULSE
 LINE.



EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
#1 DEPROPANIZER SYSTEM	
DATE	10/20/80
BY	W. J. B.
CHECKED BY	W. J. B.
APPROVED BY	W. J. B.
PROJECT NO.	63630242
FIGURE NO.	9502-B
REVISION	

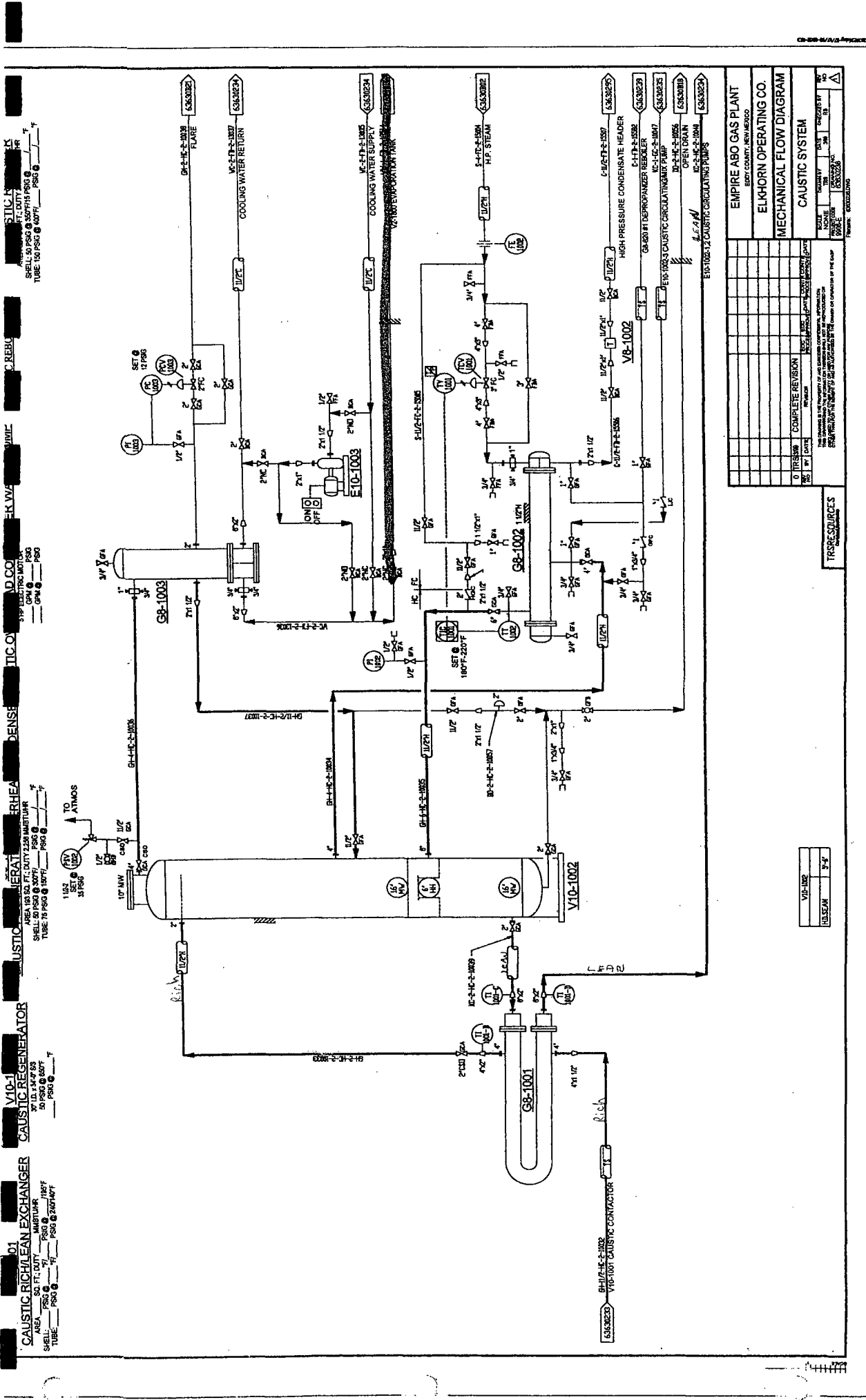
VR-620-1
HD. SEAL
7.0"

TRC RESOURCES



EQUIPMENT		QTY	UNIT	DATE	BY
GS-304-1	3RD STAGE DISCHARGE COOLER	1	EA	10/1/88	WJH
GS-304-2	3RD STAGE DISCHARGE COOLER	1	EA	10/1/88	WJH
GS-304-3	3RD STAGE DISCHARGE COOLER	1	EA	10/1/88	WJH
GS-303-1	3RD STAGE COMPRESSOR	1	EA	10/1/88	WJH
GS-303-2	3RD STAGE COMPRESSOR	1	EA	10/1/88	WJH
GS-303-3	3RD STAGE COMPRESSOR	1	EA	10/1/88	WJH
GS-302-1	3RD STAGE DISCHARGE SEPARATOR	1	EA	10/1/88	WJH
GS-302-2	3RD STAGE DISCHARGE SEPARATOR	1	EA	10/1/88	WJH
GS-302-3	3RD STAGE DISCHARGE SEPARATOR	1	EA	10/1/88	WJH

RESOURCES		DATE	BY
WJH	WJH	10/1/88	WJH
WJH	WJH	10/1/88	WJH
WJH	WJH	10/1/88	WJH



CAUSTIC RICHLEAN EXCHANGER
AREA: 50 FT. DUTY
SHELL: 50 PSIG @ 1180F
TUBE: 75 PSIG @ 240/40F

CAUSTIC REGENERATOR
AREA: 50 FT. DUTY
SHELL: 50 PSIG @ 207F
TUBE: 75 PSIG @ 197F

CAUSTIC SYSTEM
AREA: 50 FT. DUTY
SHELL: 50 PSIG @ 207F
TUBE: 75 PSIG @ 197F

CAUSTIC SYSTEM
AREA: 50 FT. DUTY
SHELL: 50 PSIG @ 207F
TUBE: 75 PSIG @ 197F

EMPIRE ABO GAS PLANT
EAST COUNTY, NEW MEXICO
ELKHORN OPERATING CO.
MECHANICAL FLOW DIAGRAM
CAUSTIC SYSTEM

DATE: 10/1/68
BY: J. E. A. M.
CHECKED: J. E. A. M.
APPROVED: J. E. A. M.

NO.	DATE	REVISION	BY	CHKD.	APPD.
1	10/1/68	COMPLETE REVISION	J. E. A. M.	J. E. A. M.	J. E. A. M.

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TRIP SOURCES
V10-1002
HULSAM

[illegible]

TRS RESOURCES
Contact Your Trainer

10

10

UNION REPUBLIC OF CAMBODIA

COMBUSTION AIR SCRUBBER O.T. TANK

COMBUSTION AIR COOLER

#2 SULLAIR COMBUSTION AIR COMPRESSOR (NORTH MIDDLE)

COMBUSTION AIR SCRUBBER O.T. TANK

COMBUSTION AIR COOLER

#3 SULLAIR COMBUSTION AIR COMPRESSOR NORTHWEST

COMBUSTION AIR SCRUBBER O.T. TANK

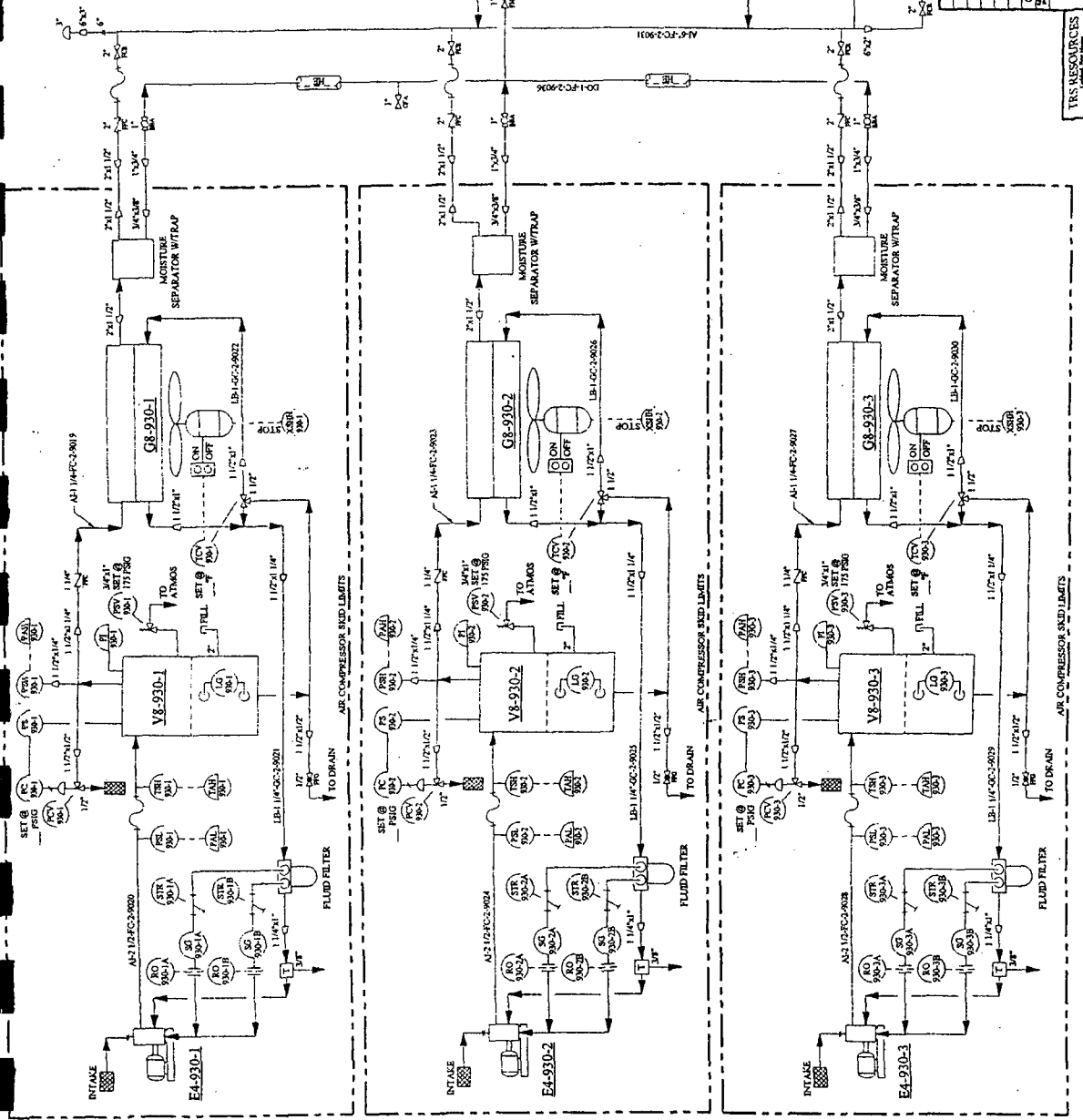
COMBUSTION AIR COOLER

EMPIRE ABO GAS PLANT

ELKHORN OPERATING CO.

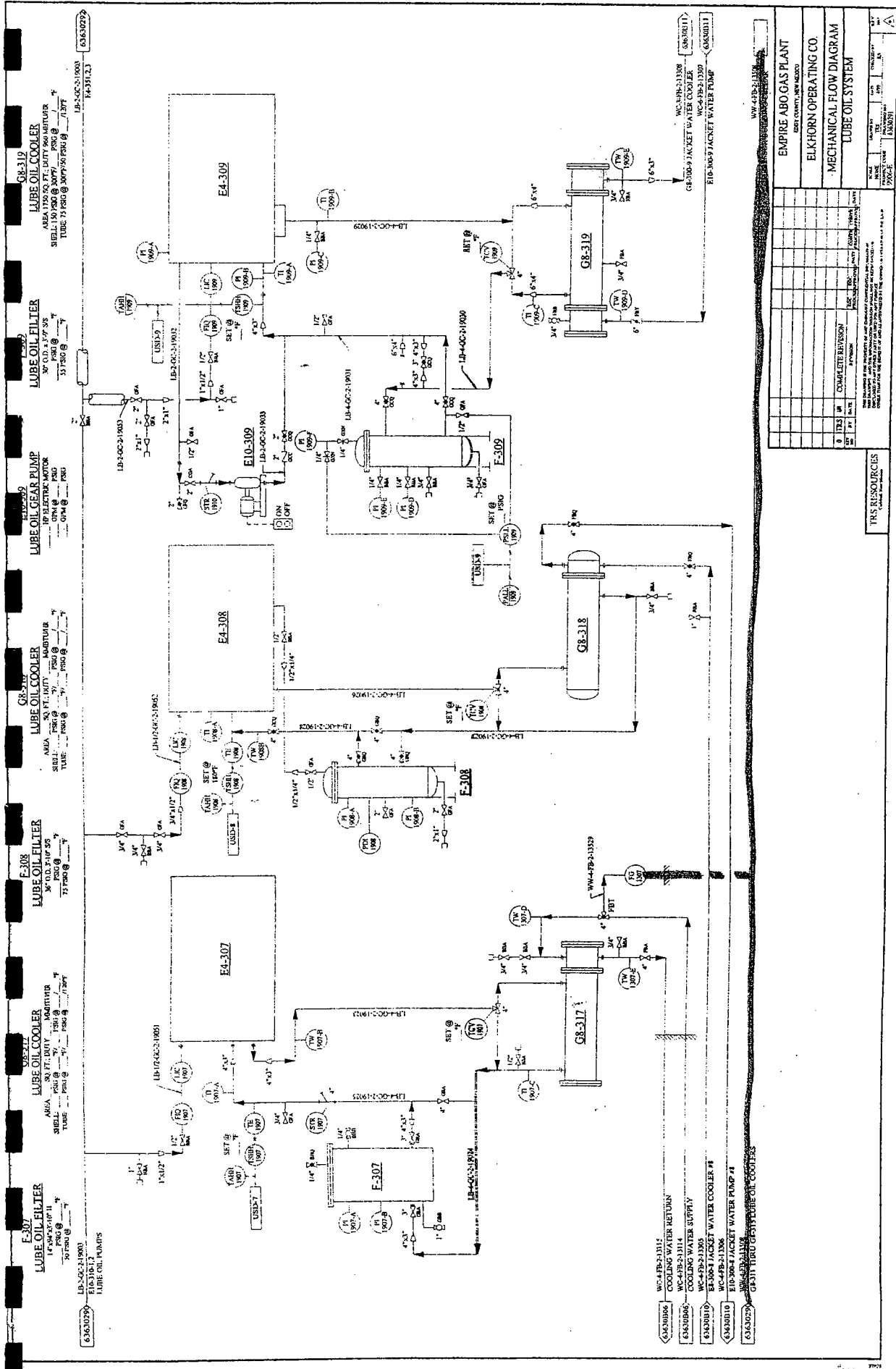
MECHANICAL FLOW DIAGRAM

INSTRUMENT AIR



TRC RESOURCES

NO.	DATE	BY	REVISION	DESCRIPTION
1	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
2	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
3	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
4	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
5	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
6	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
7	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
8	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
9	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
10	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
11	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
12	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
13	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
14	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
15	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
16	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
17	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
18	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
19	10/1/80	TRC	COMPLETE	INSTRUMENT AIR
20	10/1/80	TRC	COMPLETE	INSTRUMENT AIR



EMPIRE ABO GAS PLANT	
ELKHORN OPERATING CO.	
MECHANICAL FLOW DIAGRAM	
LUBE OIL SYSTEM	
DATE	10/1/77
BY	W. J. HARRIS
CHKD	W. J. HARRIS
APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

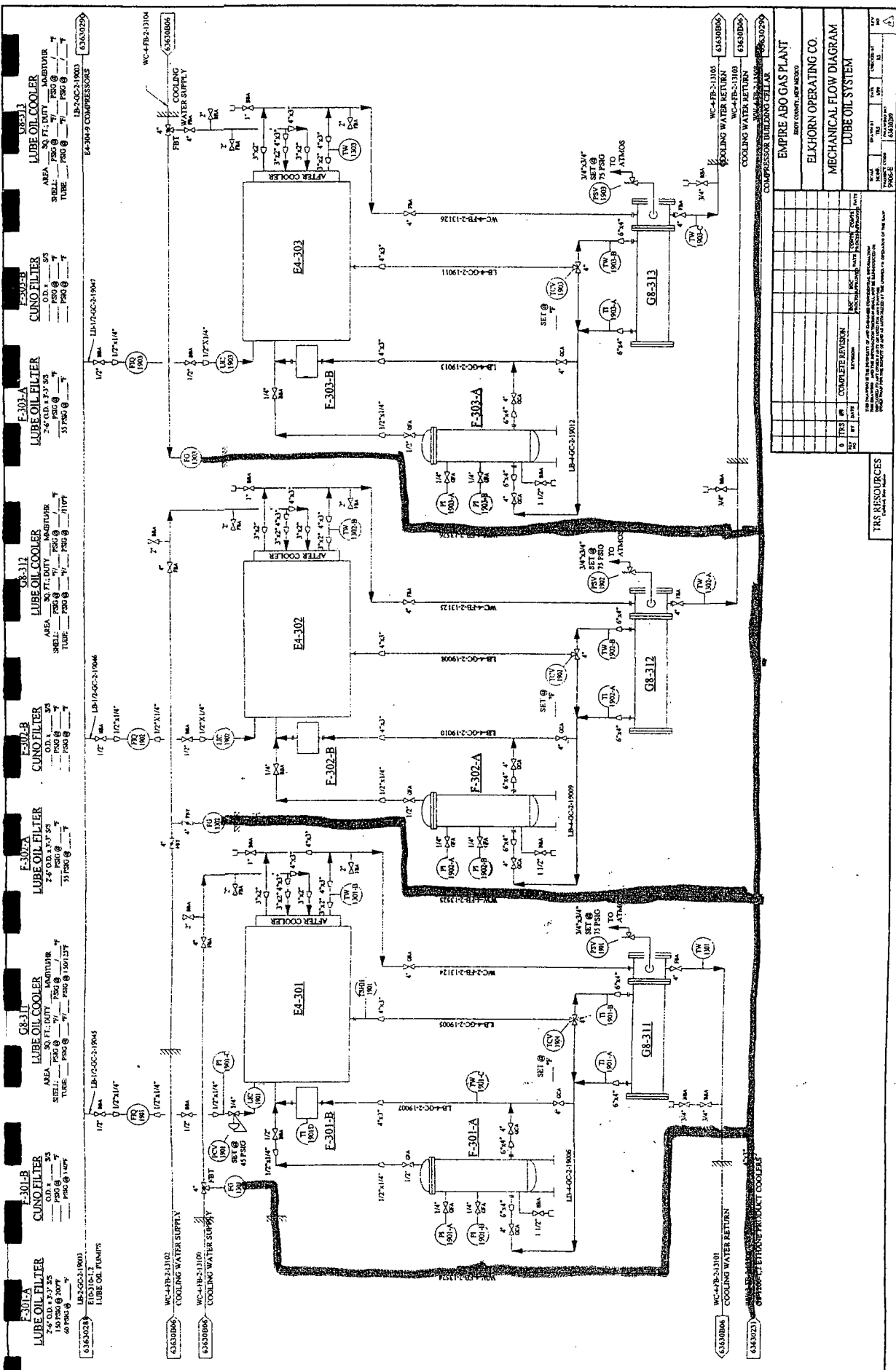
TMS RESOURCES	
NO.	1721
DATE	10/1/77
BY	W. J. HARRIS
CHKD	W. J. HARRIS
APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

COMPLETE REVISION	
NO.	1
DATE	10/1/77
BY	W. J. HARRIS
CHKD	W. J. HARRIS
APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

TMS RESOURCES	
NO.	1721
DATE	10/1/77
BY	W. J. HARRIS
CHKD	W. J. HARRIS
APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

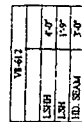
TMS RESOURCES	
NO.	1721
DATE	10/1/77
BY	W. J. HARRIS
CHKD	W. J. HARRIS
APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

TMS RESOURCES	
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DATE	10/1/77
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APPROVED	W. J. HARRIS
PROJECT	63630272
SCALE	AS SHOWN

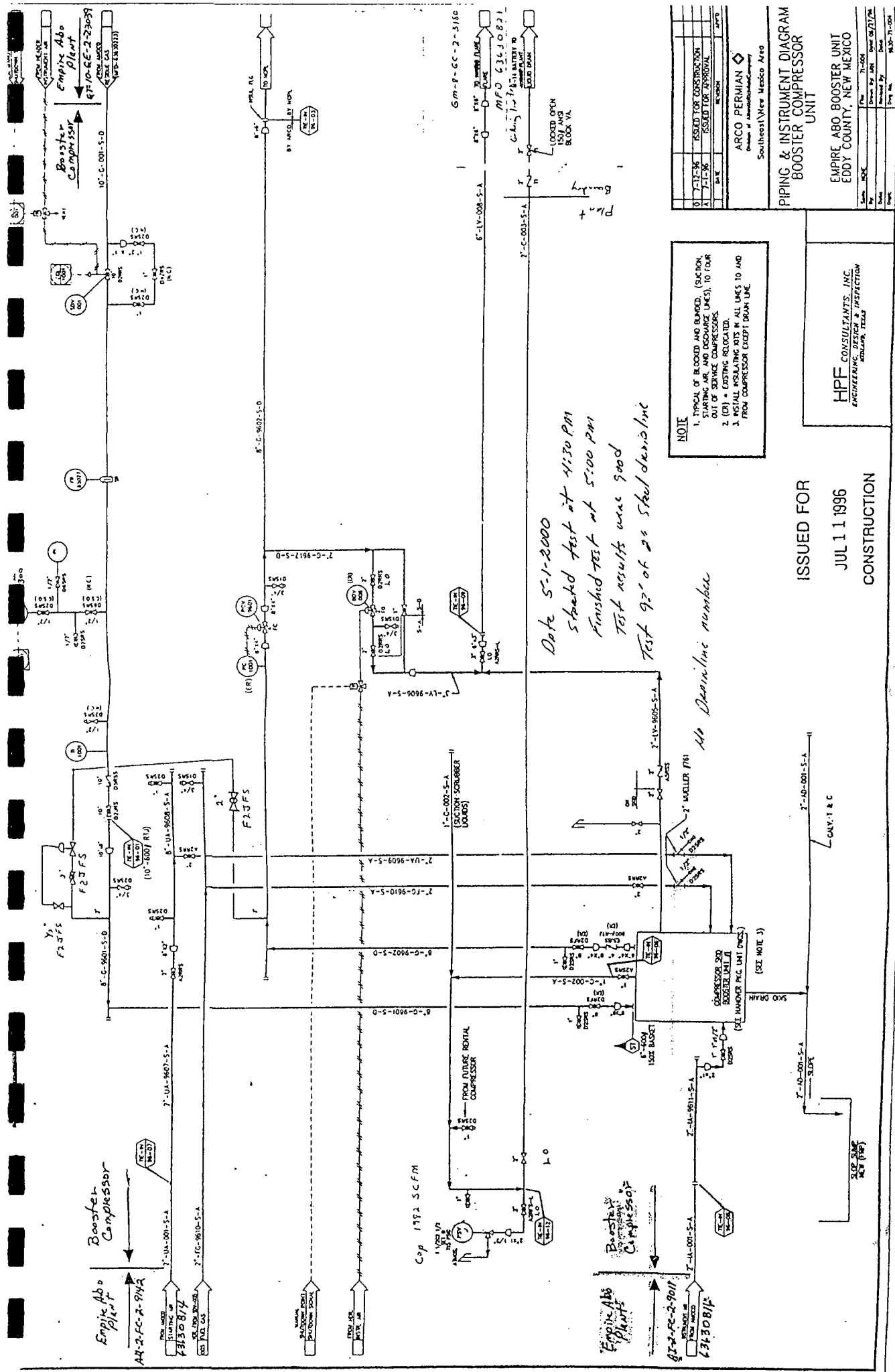


ETHANE PRODUCT COOLER (SOUTH)

AREA 440 SQ. FT.; DUTY 2.45 MEGATONNES
SIDE L: 300 PSIG @ 650°F / ____ PSIG @ ____ / 75°F
TUBE: 1700 PSIG @ 400°F / 1050 PSIG @ ____ / 85°F

[illegible]

156698	ON ORDER	DATE & TIME	BY
56	56	56	56
15 JUL 1968	15 JUL 1968	15 JUL 1968	15 JUL 1968



NOTE

1. TYPICAL OF BLOCKED AND BANGED. (SUCROX, STARTING AIR, AND COMPRESSOR, 10 FOUR OUT OF SERVICE COMPRESSOR.
2. (10) = EXISTING RELOCATED.
3. INSTALL INSULATING RITS IN ALL LINES TO AND FROM COMPRESSOR EXCEPT DRAIN LINE.

ISSUED FOR
JUL 11 1996
CONSTRUCTION

HPF CONSULTANTS, INC.
ENGINEERING DESIGN & INSPECTION
HOUSTON, TEXAS

PIPING & INSTRUMENT DIAGRAM
BOOSTER COMPRESSOR
UNIT

Rev	7-001	Date	06/27/96
By	HPF	Drawn By	HPF
Check	HPF	Checked By	HPF
Scale	AS SHOWN	Sheet No.	96-02-71-001

ARCO PERMIAN
Southwest New Mexico Area

Date 5-1-2000
Started test at 4:30 PM
Finished test at 5:00 PM
Test results were good
Test 92' of 21 Steel densiline

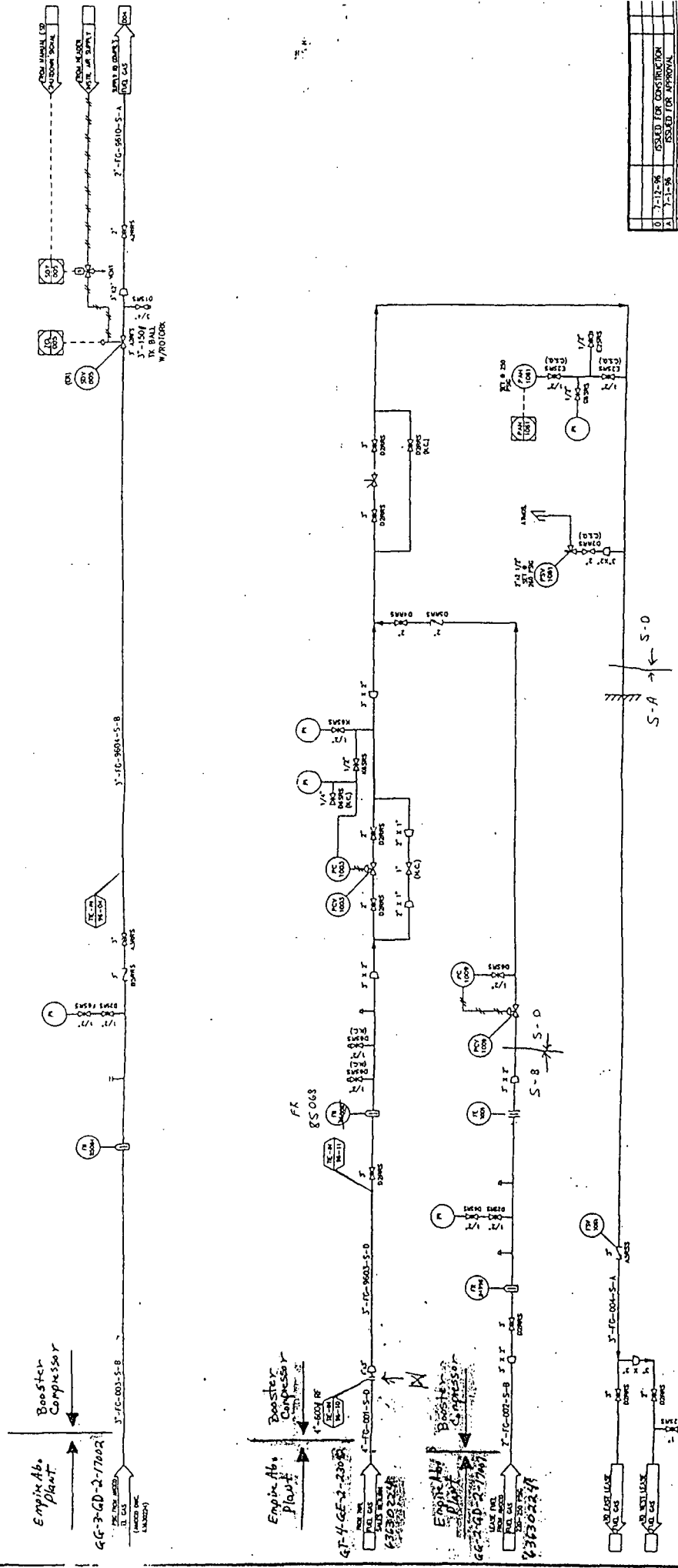
No Densiline number

Cap 1752 SCFM

Empire Abo
Booster
Compressor

41-2-FC-2-9011
NEW MEXICO
63430811

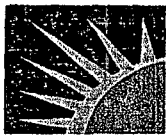
SLOP SUMP
NEW MEXICO



ARCO PERMIAN Division of American Petroleum Company Southeast New Mexico Area	
DATE	REVISION
0 7-12-96	ISSUED FOR CONSTRUCTION
1 7-11-96	ISSUED FOR APPROVAL
PIPING & INSTRUMENT DIAGRAM BOOSTER COMPRESSOR UNIT	
EMPIRE ABO BOOSTER UNIT EDDY COUNTY, NEW MEXICO	
Drawn	7-1-96
Checked	7-1-96
Reviewed	7-1-96
Approved	7-1-96

ISSUED FOR
JUL 11 1996
CONSTRUCTION

HPF CONSULTANTS, INC.
ENGINEERING, DESIGN & INSPECTION
DENVER, COLORADO



TRS Resources LLC

Global Industrial Solutions

Thank You for Your Business

SPILL PREVENTION, CONTROL, AND COUNTERMEASURE PLAN

EMPIRE ABO GAS PLANT

**Eddy County, New Mexico
257 Empire Road, Artesia, NM 88211 -0070**

**Operated by:
Frontier Field Services, LLC**

**Owned by:
Frontier Field Services, LLC
4200 Skelly Drive, Suite 700
Tulsa, Oklahoma 74135**

**Updated by:
Flatrock Engineering and Environmental, Ltd
2000 S.E. 15th Street, Bldg 150-D
Edmond, OK 73013**

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LOG OF PLAN REVIEW AND AMENDMENTS

NON TECHNICAL AMENDMENTS

- Non-technical amendments are not certified by a Professional Engineer.
- Examples of changes include, but are not limited to, phone numbers, name changes, or any non-technical text change(s).

TECHNICAL AMENDMENTS

- Technical amendments are certified by a Professional Engineer (§112.5(c)).
- Examples of changes include, but are not limited to, commissioning or decommissioning containers; replacement, reconstruction, or movement of containers; reconstruction, replacements, or installation of piping systems; construction or demolition that might alter secondary containment structures; changes of product or service; or addition/deletion of standard operation or maintenance procedures related to discharge prevention measures. It is the responsibility of the facility to determine, and confirm with the regulatory authority as necessary, what constitutes a technical amendment. The preamble of the rule states that an amendment is required only "when there is a change that materially affects the facility's potential to discharge oil" (67 FR 47091).
- An amendment made under this section will be prepared within six (6) months of the change and implemented as soon as possible but not later than six (6) months following preparation of the amendment.
- Technical Amendments affecting various pages within the plan can be P.E. certified on those pages, certifying those amendments only, and will be documented on the log form below.

MANAGEMENT REVIEW

- Management will review this SPCC Plan at least each five (5) years and document the review on the form below (§112.5(b)).

Review/ Amend Date	Signature* (Specify)	Amend Plan (will/will not)	Description of Review Amendment	Affected Page(s)	P.E. Certification (Y/N)

* Typically signed by Manager, Professional Engineer or plan reviewer.

Spill Prevention, Control, and Countermeasure Plan

ONSHORE FACILITY - REGULATORY CROSS-REFERENCE		
Citation	Description	Section
§112.3(d)(1)	Professional Engineer Certification	1.2
§112.5(b)	Management of Five Year Review	Foreword
§112.7	General requirements for SPCC Plans for all facilities and all oil types	-----
§112.7(a)	General requirements: discussion of facility's conformance with rule requirements; deviations from Plan requirements; facility characteristics that must be described in the Plan; spill reporting information in the Plan; emergency procedures	1, 2, App. A-D
§112.7(b)	Fault analysis	2A.1
§112.7(c)	Secondary containment	2A.1, 2A.3.1
§112.7(d)	Contingency planning	App. D
§112.7(e)	Inspections, tests, and records	2A.5.3, 2A.7, App. B
§112.7(f)	Employee training and discharge prevention procedures	1.6, App. A, App. B
§112.7(g)	Security (excluding oil production facilities)	2A.4.2, 2A.6
§112.7(h)	Loading/unloading (excluding offshore facilities)	2A.5
§112.7(i)	Brittle fracture evaluation requirements	2A.7
§112.7(j)	Conformance with State requirements	1.11
§112.8	Requirements for onshore facilities (excluding production facilities)	-----
§112.8(a)	General and specific requirements	2A.1 - 2A.4, 2A.7
§112.8(b)	Facility drainage	2A.3
§112.8(c)	Bulk storage containers	2A.1, 2A.2, 2A.7
§112.8(d)	Facility transfer operations, pumping, and facility process	2A.4, 2A.7
§112.9	Requirements for onshore production facilities	N/A
§112.9(a)	General and specific requirements	N/A
§112.9(b)	Oil production facility drainage	N/A
§112.9(c)	Oil production facility bulk storage containers	N/A
§112.9(d)	Facility transfer operations, oil production facility	N/A
§112.10	Requirements for onshore oil drilling and workover facilities	N/A
§112.10(a)	General and specific requirements	N/A
§112.10(b)	Mobile facilities	N/A
§112.10(c)	Secondary containment - catchment basins or diversion structures	N/A
§112.10(d)	Blowout prevention (BOP)	N/A
§112.11	Requirements for offshore oil drilling, production, or workover facilities	N/A
§112.11(a)	General and specific procedures	N/A
§112.11(b)	Facility drainage	N/A
§112.11(c)	Sump systems	N/A
§112.11(d)	Discharge prevention systems for separators and treaters	N/A
§112.11(e)	Atmospheric storage or surge containers; alarms	N/A
§112.11(f)	Pressure containers; alarm systems	N/A
§112.11(g)	Corrosion protection	N/A
§112.11(h)	Pollution prevention system procedures	N/A
§112.11(i)	Pollution prevention systems; testing and inspection	N/A
§112.11(j)	Surface and subsurface well shut-in valves and devices	N/A
§112.11(k)	Blowout prevention	N/A
§112.11(l)	Manifolds	N/A
§112.11(m)	Flowlines, pressure sensing devices	N/A
§112.11(n)	Piping; corrosion protection	N/A
§112.11(o)	Sub-marine piping; environmental stresses	N/A
§112.11(p)	Inspections of sub-marine piping	N/A

SECTION ONE

General Information

1.0 General Information

1.1 Management Approval and Review

Management Approval	
● Operator responsible for Facility:	<u>Frontier Field Services, LLC</u>
Facility Name and Location:	<u>Empire Abo Gasoline Plant</u> <u>257 Empire Road, Artesia NM 88211</u>
● Owner of the Facility:	<u>Frontier Field Services, LLC</u>
Address:	<u>4200 Skelly Drive, Suite 700., Tulsa, OK 74135</u>
● This SPCC Plan will be implemented as herein described.	
Signature: _____	Designated person accountable for oil spill prevention at the facility:
Name: <u>Chad Cagle</u>	Name: <u>David Harris</u>
Date: _____	Title: <u>Plant Manager</u>
Title: <u>Director of Operations</u>	
● This SPCC Plan will be implemented as herein described.	
Signature: _____	Designated person accountable for oil spill prevention at the facility:
Name: _____	Name: _____
Date: _____	Title: _____
Title: _____	

1.2 Professional Engineer Certification

Professional Engineer Certification

By means of this Professional Engineer Certification, I hereby attest to the following:

- I am familiar with the requirements of 40 CFR Part 112 and have verified that this Plan has been prepared in accordance with the requirements of this Part.
- I or my agent have visited and examined the facility(s).
- I have verified that this Plan has been prepared in accordance with good engineering practice, including consideration of applicable industry standards.
- I have verified that the required inspection and testing procedures have been established as described in Section 2.
- I have verified that the Plan is adequate for the facility.

Mark Martelli

Printed Name of Registered Professional Engineer

(Seal)

Signature of Registered Professional Engineer

Date: _____

Registration No.: 77679

State: Texas

1.3 Substantial Harm Certification (excerpt from 40 CFR Part 112 - Attachment CII)

CERTIFICATION OF THE APPLICABILITY OF THE SUBSTANTIAL HARM CRITERIA

FACILITY NAME: Empire Abo Gasoline Plant

FACILITY ADDRESS: 257 Empire Road

Artesia NM 88211

1. Does the facility transfer oil over water to or from vessels **and** does the facility have a total oil storage capacity greater than or equal to 42,000 gallons?

☐

YES

☒

NO

2. Does the facility have a total oil storage capacity greater than or equal to 1 million gallons **and** does the facility lack secondary containment that is sufficiently large to contain the capacity of the largest aboveground oil storage tank plus sufficient freeboard to allow for precipitation within any aboveground oil storage tank area?

☐

YES

☒

NO

3. Does the facility have a total oil storage capacity greater than or equal to 1 million gallons **and** is the facility located at a distance (as calculated using the appropriate formula in Attachment C-III to this appendix or a comparable formula¹) such that a discharge from the facility could cause injury to fish and wildlife and sensitive environments, see Appendices I, II, and III to DOC/NOAA's "Guidance for Facility and Vessel Response Plans: Fish and Wildlife and Sensitive Environments" (59 FR 14713, March 29, 1994) and the applicable Area Contingency Plan.

☐

YES

☒

NO

4. Does the facility have a total oil storage capacity greater than or equal to 1 million gallons **and** is the facility located at a distance (as calculated using the appropriate formula in Attachment C-III to this appendix or a comparable formula¹) such that a discharge from the facility would shut down a public drinking water intake²?

☐

YES

☒

NO

5. Does the facility have a total oil storage capacity greater than or equal to 1 million gallons **and** has the facility experienced a reportable oil spill in an amount greater than or equal to 10,000 gallons within the last 5 years?

☐

YES

☒

NO

CERTIFICATION

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document, and that based on my inquiry of those individuals responsible for obtaining this information, I believe that the submitted information is true, accurate, and complete.

Signature

Chad Cagle

Name (please type or print)

Director of Operations

Title

Date

¹ If a comparable formula is used, documentation of the reliability and analytical soundness of the comparable formula must be attached to this form.

² For the purposes of 40 CFR part 112, public drinking water intakes are analogous to public water systems as described at 40 CFR 143.2(c).

1.4 Contact List and Phone Numbers

The contact list and phone number reference for the facility is provided in Appendix A. Also, please refer to the "Emergency Action Plan" kept at the plant, for any updated telephone numbers.

1.5 Notification Data Sheet

A Notification Data Sheet is provided in Appendix A.

1.6 Personnel, Training, and Discharge Prevention Procedures

Training

- The Facility provides the following minimum training to oil-handling personnel prior to assignment of job responsibilities:
 - Operation and maintenance of equipment to prevent oil discharges;
 - Oil Spill Contingency Plan;
 - Applicable oil spill prevention (State & Federal) laws, rules, and regulations;
 - General facility operations; and,
 - The contents of the facility SPCC Plan and applicable pollution control laws, rules, and regulations.

Briefings

The facility conducts prevention briefings for oil-handling personnel at least once a year to assure adequate understanding of the SPCC Plan for the facility. These briefings include discussion of potential discharges or component failures and precautionary measures. Also included are any known discharges, failures, malfunctioning components and any new precautionary measures.

Documentation

Documentation of these Personnel, Training, and Discharge Prevention Briefing programs is maintained for a minimum period of three (3) years. The training company issues wallet cards to each employee undergoing the training so that each employee can document that he/she has been trained/ briefed on an annual basis. Additionally, the plant clerk in the main office keeps annual training/ briefing logs.

1.7 Facility Layout and Diagram

1.7.1 Facility Layout

Diagrams of the facility are located in Appendix C. More detailed drawings can be found in the plant office. The first set of diagrams shows the general layout and placement of tanks and other equipment. The second diagram shows the locations of fences, dikes and other items relevant to this plant.

The physical layout of the facility is described as follows:

The facility is laid out in a north-south and east-west grid pattern. At the northern top side of the plant is the main office and control room. Important areas for the storage of hydrocarbons and potential sources of spills would include:

1. The LPG and NGL storage facility located south easterly of the office. This area contains nine different horizontal "bullet" tanks ranging in size from 1000 Bbl to 1285 Bbl. Only refrigeration grade propane is stored in this area at this time.
2. Lubricating oils and solvents are stored in an area between the office and the LPG and NGL storage facility. The storage area has two 322 Bbl lubricating oil tanks, one 1000 gallon vehicle gasoline storage tank and one 500 gallon vehicle gasoline storage tank.
3. Used lubricating oils and process water are stored in the slop oil storage area located near the south border of the facility. Three 400 Bbl tanks and one 400 Bbl gunbarrel are used to store a mixture of water, produced oils and used lubricating oil.
4. Materials from the process drain system are stored in two tanks located in the process drain storage area. The process drain storage area is located in a southwesterly direction from the main office just east of the evaporation pond. The diked area contains four tanks. The 500 Bbl tank is used by for holding materials from the process drain system. A second 210 Bbl tank may be used if required. The tanks receive wastewater, hydrocarbons and amine from the process drain system.

Spill Prevention, Control, and Countermeasure Plan

5. The loading and unloading racks are located just to the northeast of the LPG and NGL storage facility. Several truck racks are located in this area to load gasoline, butane, propane or a mixture of petroleum liquids. LPG and NGL are no longer loaded into trucks. Only refrigeration grade propane is unloaded.

• Further details are provided in Section 2 - Container and Potential Spills Table and also in Appendix "E" which shows the storage tanks and containment areas.

1.7.2 Facility and Containment diagrams are attached (Appendix C and E) with the following detail and location information (as applicable):

- Process equipment, operating equipment, electrical equipment.
- Loading/Unloading racks.
- Fixed aboveground storage tanks.
- Transfer Stations and connecting lines.
- Drum and portable container storage areas.
- The contents of all containers.

1.8 Prevention, Response and Cleanup

Prevention

- The facility discharge prevention measures, including procedures for routine handling of products (loading, unloading, facility transfers, etc.), are described as follows:

The facility has developed operating procedures to assure the safe operation of the plant and also to prevent spills. Procedures include truck loading and unloading, bleeding of vessels, pumping of liquids and other items.

The facility has also been designed to collect any drainage from areas having lines containing gasoline or other liquid hydrocarbons. Storm water levees are located on the south and west sides of the plant. These levees are in place to act as containment for storm water and as tertiary containment for oil, other hydrocarbon liquids, or chemicals. Oil will be collected if accumulations occur in this area as described above for diked containment areas.

The removal of oil fluid from the diked containment areas will be through the use of vacuum trucks and/or portable pumps with disposal at approved facilities or the fluid may be placed in the production stream for reconditioning.

Vacuum trucks may be used, if necessary, during large storm events to remove rainwater from diked areas. The rainwater is disposed of in an approved manner. The water may be disposed of in an approved disposal well in accordance with the Discharge Plan. Clean rainwater may also be discharged immediately outside of the diked area if the water has no visible sheen and the discharge is logged on the Tank Drainage Form found on page B-4 of this plan.

Countermeasures

- The facility discharge discovery, response and cleanup capabilities are described as follows:

Spill Prevention, Control, and Countermeasure Plan

On the operator's routine rounds, the operator will look for signs of oil. Operators will look for signs of leaking equipment (tanks, flanges, piping etc.), oil sheens in water, and stained soil near known underground pipelines.

The Oil Spill Contingency Plan found in Appendix D is used if an oil spill is observed. If oil is observed, the Plant Manager will be notified. Liquid spilled product will be recovered by pumps and/or vacuum trucks and handled in approved methods (disposal or recycled). Any contaminated soil or clean-up debris will be collected and either remediated or disposed of in an approved manner.

The plant has personnel, hand tools and other equipment available for cleaning up any minor oil spill on a 24-hour basis. Outside contractors will be brought in to assist in the event that the spill is too large to be cleaned up by plant personnel.

- The resources available to the facility for discharge cleanup are provided in the "Emergency Action Plan" that may be found in the Safety office. This plan is kept up to date and can be used to address many other emergencies, besides oil cleanup activities.

1.8 Prevention, Response and Cleanup (Cont'd)

Disposal

The facility has established the following methods of disposal for recovered materials in accordance with applicable legal requirements:

If the substance spilled is a hazardous chemical, prior to taking any action, refer to the chemical's Material Safety Data Sheet (MSDS).

1. Removal:

Once the release is contained, an attempt shall be made to remove the spilled material in a manner, which minimizes damage to the environment. The Frontier Plant Manager for the facility should be contacted for site-specific guidelines. Possible removal methods may include:

- A. Natural biodegradation/enhanced bioremediation
- B. Soil removal
- C. Application of sorbent materials
- D. Evaporation and/or in situ burning (requires regulatory approvals)
- E. Skimmers
- F. Chemical treatment (e.g. Dispersants, which require regulatory approvals)

2. Disposal:

Contaminated soil, sorbent materials, and all other forms of oil or hazardous wastes resulting from spill and cleanup efforts will be disposed in accordance with applicable regulations. Consideration should be given to all onsite options before shipping offsite.

Spill Prevention, Control, and Countermeasure Plan

Those materials that cannot be disposed of onsite must go to an approved offsite waste disposal or recycling location. The Frontier Plant Manager maintains a list of approved waste disposal. If needed, contact the Frontier Plant Manager for assistance in selecting the appropriate disposal option.

3. Restoration:

Restoration will be performed as necessary to minimize ecological damages. The Frontier Plant Manager should be consulted for guidance specific to each spill location. All temporary containment devices such as dikes, trenches, etc., will be removed. The topography should resemble the appearance present prior to the spill. If any soil was removed, it shall be replaced with compatible material. If vegetation is destroyed, it may be necessary to replant and revitalize the landscape.

In any event, the Frontier Plant Manager should be consulted, for assistance in developing site-specific plans for spill cleanup and remediation.

If not, the following provides a description of the impracticability. _____

[illegible]

• **If not** practicable, ☐ an oil spill contingency plan is attached (provided in Appendix D) or ☐ is addressed by the Facility Response Plan.

- ④ A written commitment of manpower, equipment and materials required to expeditiously control and remove any quantity of oil discharged is provided in ☐ Appendix D or in the ☐ Facility Response Plan.
- ⑤ If containment and/or diversionary structures are impracticable for bulk storage containers, then periodic integrity testing of the container(s) and integrity and leak testing of the valves and piping is required.
- ⑥ *Reference supporting documentation maintained separately, as appropriate:* _____

[Additional pages may be attached as necessary.]

1.10 Deviations to Rule

- ## 1.11 Improvements

The facility may from time-to-time install additional measures or implement new procedures to improve spill prevention, control or countermeasures. The following area allows the SPCC plan user to list any additional improvements after the plan was enacted.

[illegible]

1.12 Conformance with other Requirements

Describe conformance with other applicable requirements and effective discharge prevention and containment procedures in-place at the facility. Include a description of compliance with more stringent State rules, regulations, and guidelines, if any:

The facility is in conformance with the New Mexico Oil Conservation Division (OCD) "Discharge Plan" requirements. Pertinent requirements quoted from the "Discharge Plan" include:

Attachment 10: Inspection, Maintenance and Reporting

Inspection and maintenance of the facility occurs on a daily basis (See SPCCP, Appendix E). Below ground and non-pressurized process and wastewater lines are tested every 5 years (See Drain Line Testing Report, Appendix D).

Groundwater Monitoring

All wastewater is stored in tanks with secondary containment or the lined evaporation pond. All wastewater is transported from the point of generation to the storage units via pipelines with documented mechanical integrity. Therefore, ground water monitoring is not necessary. Ground water monitoring is addressed separately in the Stage I/II Abatement Plan.

Precipitation Runoff Control

The plant has levees around its southern, and western sides to contain storm water runoff. These act as a tertiary containment for other spills at the plant. Any oil liquid that accumulates in this area is recovered with vacuum trucks and portable pumps. This is disposed at an approved offsite facility or added to the production stream.

SECTION 2A

Onshore Facility Information

Spill Prevention, Control, and Countermeasure Plan

2A.1 Container and Potential Spills Table

- The potential spills sources at the facility are summarized in the following table:

Oil Source	Associated Substance (Contents) (Oil)	Source Capacity (Bbls)	Potential Failure	Rate of Flow (Bbls/hr)	Direction of Flow	Containment System(s)*
Aboveground Fixed Containers						
NGL Storage Area	Ref grade propane only	4285	Leak	4285	South	Yes – Bermed area
Process Drain Storage Area	Water, Oil, Amine	500, 210	Leak	500	South	Yes – Bermed area
Amine Tank	Water, amine	280	Leak	280	South	Yes – Bermed area
Amine Tank	Water, Amine	195	Leak	195	South	Yes – Bermed area
Amine Day Tank	Amine	26	Leak	26	South	Yes – Bermed area
Methanol Tank	Methanol	24	Leak	24	South	Yes – Bermed area
Lube Oil Storage Area	2 lube oil storage tanks	322, 322	Leak	322	South	Yes – Bermed area
Lube Oil Storage Area	Gasoline storage tank	12	Leak	12	South	Yes – Bermed area
Lube Oil Storage Area	Gasoline storage tank	24	Leak	24	South	Yes – Bermed area
Solvent Storage Area	Solvent Storage Tank	12	Leak	12	South	Yes – Fiberglas containment
Lube Oil Storage Area – Not used	Propane Fuel Storage tank	24	Leak	24	South	Yes – Bermed area
Diesel Tank	Diesel Tank	12.5	Leak	12.5	South	Yes – Bermed area
1 Ethyl Mercaptan tank – to be removed	Ethyl Mercaptan	15	Leak	15	South	Yes – Bermed area
Slop Oil Storage	Water, Oil	387, 380, 380, 380	Leak	387	South	Yes – Bermed area
Completely or Partially Buried Tanks						
Mobile and Portable Containers						
Oil Drum	Lube Oil	1.3	Leak	1.3	South	Yes – Bermed Area

Spill Prevention, Control, and Countermeasure Plan

Oil Source	Associated Substance (Contents) (Oil)	Source Capacity (Bbls)	Potential Failure	Rate of Flow (Bbls/hr)	Direction of Flow	Containment System(s)*
Operational Equipment (Transformers, Manufacturing Equipment, Process Vessels, etc.)						
Truck or Rail Loading/Unloading Rack						
LPG Loading Rack – Not used	Propane, Butane	1000 Bbl	Rupture	100	Evaporates	No
NGL Loading Rack	Ref grade propane unloading only	1000 Bbl	Rupture	100	South	Yes – Bermed area (proposed)
Other Potential Spill Sources (Piping, Surface Impoundments, etc.)						
Gasoline Piping – Not used	Gasoline	100 Bbl	Rupture	100	South	Yes – Flows into southern bermed area

- The material and construction of bulk storage containers are compatible with the material stored and conditions of storage such as pressure and temperature.
- All bulk storage container installations are constructed so that a means of secondary containment is provided for the entire capacity of the largest single container and sufficient freeboard to contain precipitation.
- Diked areas are sufficiently impervious to contain discharged oil. (See Appendix E)
- Visible discharges, which result in a loss of product from containers, will be promptly corrected and any accumulations of oil in the diked area(s) will be promptly removed.

* See Sec. 2A.3.1 for further details.

2A.2 Bulk Storage Containers

2A.2.1 Completely and Partially Buried Tanks

- The facility has several buried tanks. Each of the tanks has secondary containment or a leak detection system installed. A list of the tanks is as follows:
 - Process Drain Tank (Metal tank inside of a concrete enclosure with inspection ports.)
 - Molten Sulfur Tank (Metal tank built to provide for leak detection through inspection ports.)
 - Amine Drain Tank (Metal tank inside of a concrete enclosure with inspection ports.)
 - Flare Sump (Metal tank inside of a concrete enclosure with inspection ports.)
- Protective coatings provide corrosion protection and the tanks are placed inside of concrete cellars that are kept dry.

2A.2.2 Mobile or Portable Oil Storage Containers

- Mobile or portable oil storage containers are located at the facility. Drums are used for lubricating oils and miscellaneous chemicals.
- Secondary containment is **provided** which is adequately sized to contain the largest container plus sufficient freeboard for precipitation. See Sec. 2A.3.1 for details. Secondary containment includes:
 - A concrete containment area is provided under the barrel storage area. See Appendix E for details.
 - Drum "coffins" being of either fiberglass or metal are used whenever chemicals are used in the plant.

2A.2.3 Internal Heating Coils

- The facility does utilize internal heating coils in the sulfur storage tank. Internal heating coil leakage is controlled by monitoring the vents off of the molten sulfur storage tank. The steam return line is in a closed system and does not discharge into an open water course.

2A.2.4 Fail Safe Precautions

The plant is manned 24 hours a day to assure that alarms are properly responded to.

Spill Prevention, Control, and Countermeasure Plan

- The following precautions are used to assure that tanks are not overfilled:
 - Slop Oil Tanks: Has a Level Safety High (LSH) sensor and alarm to alert the operators if a high level condition exists. A light is turned on at the tank by the sensor (local alarm).
 - South Process Drain Tank: Has a Level Safety High (LSH) sensor and alarm to alert the operators if a high level condition exists. A light is turned on at the tank by the sensor (local alarm).

2A.3.2 Facility Drainage to Surface Waters without Facility Treatment System

- Water is removed only by vacuum truck from the inside of secondary containment areas. The water is disposed of in an approved manner in accordance with the water discharge plan.
- Storm water flows in a southerly direction where it is contained by dikes. The water evaporates or percolates into the ground.

2A.3.3 Water Treatment System

- A water treatment system for discharges is not applicable at this facility. Water discharges are made in accordance with the water discharge plan obtained from the State of New Mexico.

2A.3.4 Effluent Treatment Facilities

The facility does not treat water prior to discharge off site.

2A.3.5 Facility Undiked Drainage to Surface Waters

- The facility may have the potential to discharge into undiked areas.

The facility un-diked areas flow to diked catchment basins located at the western and southern sides of the plant.

2A.4 Facility Transfer Operations, Pumping and Facility Process

2A.4.1 Facility Piping

- The facility does have buried piping. Corrosion protection for all new and replaced buried piping is provided as follows
 - Wrapping and Coating
- When a pipe section is exposed, it is examined and corrective action taken as necessary.
- Cathodic protection is not used, as the plant is located in an arid region where historical records show that use of cathodic corrosion devices have not increased protection.
- Describe the facility piping systems (aboveground and buried): Most all of the piping is above ground at the plant. The pipe is generally installed on elevated or ground level pipe racks. Leaks are very evident to the operators and maintenance personnel. The drain system piping is buried. The drain system piping is leak tested every five years in accordance with the water discharge plan.

2A.4.2 Out of Service Piping

Out of service piping terminal connections are capped or blank-flanged and marked when the piping is not in service or in standby service for extended periods.

2A.4.3 Pipe Supports

Pipe supports are designed to minimize abrasion and corrosion and allow for expansion and contraction.

2A.4.4 Vehicle Warnings

Vehicles are warned orally, by signs, fencing and with bumper guards, to be sure that no vehicle will endanger aboveground piping or other oil transfer operations. The entire plant is fenced with only maintenance vehicles allowed inside of the fenced areas. Inside the plant, there are numerous guards placed to prevent maintenance vehicles from hitting the piping. The loading racks have guards in place to assure that vehicles do not endanger any of the loading connections.

2A.5. Facility Tank Truck Loading/Unloading Rack

- Tank truck unloading of refrigerant grade propane does occur at the facility.
- Tank car (rail) loading/unloading does not occur at the facility.

2A.5.1 Tank Truck Containment Systems for Loading/Unloading Rack

- Loading/unloading area drainage has modifications to allow spills to flow into a catchment basin designed to handle discharges. Unloading of refrigerant grade propane only occurs at the loading/unloading rack.

The containment system holds the maximum capacity of any single compartment of a tank truck loaded or unloaded at the facility.

The containment system consists of concrete walls to direct the flow of any spilled materials into a catchment pond.

Spill Prevention, Control, and Countermeasure Plan

- Refer to the Container and Potential Spills Table in Section 2A.1 for additional details.

2A.5.2 Prevention of Premature Vehicular Departure

- The methods, procedures, and/or equipment used to prevent premature vehicular departure include:

- | | |
|--|--|
| <input type="checkbox"/> <i>Interlocked warning lights,</i> | <input checked="" type="checkbox"/> <i>Physical barrier systems,</i> |
| <input checked="" type="checkbox"/> <i>Warning signs,</i> | <input checked="" type="checkbox"/> <i>Wheel chocks,</i> |
| <input type="checkbox"/> <i>Vehicle brake interlock systems,</i> | <input type="checkbox"/> <i>Company personnel supervising</i> |
| | <i>loading operation – refrigeration grade</i> |
| | <i>propane only</i> |

- Describe these and other premature vehicular departure prevention measures: Warning signs have been posted to alert the drivers about premature vehicular departure. Trucks are required to have wheel chocks in place to assure that the truck does not move during loading operations. A physical barrier (warning cone) is placed in front of the vehicle during loading operations. It is noted that a fixed non-moveable barrier is in place at the rear of the truck, as the truck must back into the loading area.

2A.5.3 Drain And Outlet Inspection

Drains and outlets on tank trucks are checked for leakage before unloading or departure and, if necessary, are tightened, adjusted or replaced by the drivers. Concrete pads are installed under the truck loading areas to assist the drivers in identifying any leaks or drips that may have occurred during loading operations.

2A.6 Security

Visitors and contractors must first sign in at the front office of the facility. Each individual must view the orientation program where plant safety systems and spills are discussed. Each individual must pass a written test to work in the plant.

Spill Prevention, Control, and Countermeasure Plan

The facility is fully fenced except for the truck loading area. A six-foot high chain link fence is installed around the northern perimeter, and next to the truck loading area on the west side of the plant. Barbwire fencing is used in the remote areas on the southern and western side of the plant.

The main entrance gate is locked and under the control admin/operations department located on the north side of the plant near the main office complex. The facility is attended twenty-four hours a day. Other gates are locked and may be opened by the operations staff.

Any valves, which permit direct outflow of a container's contents, have adequate security measures so that they remain closed when in non-operating or standby status. All valves are located within the plant boundaries.

Starter controls on all oil pumps in non-operating or standby status are locked in the off position in accordance with the energy isolation (lock out tag out) program. All pump switches and switchgear is located inside of the fenced plant boundaries and accessible only to authorized personnel.

Facility lighting is commensurate with the operation and the type and location of the facility to assist in the discovery of discharges and to prevent discharges occurring through acts of vandalism.

2A.7 Inspections, Tests and Records

Container Testing and Inspections

- Below is the facility aboveground bulk storage container integrity testing and inspection program including inspection frequency, records of inspections and any equivalent environmental protection:
 - Visual exterior inspections are made once a month and are documented
 - The plant follows API 653 for tank inspections. API 653 includes Calculations of Minimum Thickness for Existing Tank Shell, Maximum Period of Operation, Minimum Thickness for Tank Bottom Plate, Maximum Fill Height (Hydrostatic Testing), and Corrosion Rates and Inspection Intervals; Reinforcement of Openings, Nondestructive Testing and Welding Requirements, as well as Cathodic Protection.

Spill Prevention, Control, and Countermeasure Plan

- For pressurized vessels, the plant follows API 510. This includes Calculations of Heads, Reinforcement, Impact Testing, Cylindrical Components under Internal and External Pressure, and Pressure Testing Requirements; Nondestructive Testing and Welding Requirements; as well as Repairs and Alterations.
- The Plant Manager makes an annual review of the plant, which is documented.
- Daily checks (undocumented) are made by plant personnel.
- In the event that a field-constructed aboveground container undergoes a repair, alteration, reconstruction, or a change in service, the container will be evaluated for the risk of discharge or failure due to brittle fracture or other catastrophe.
- The facility leak testing program for completely buried tanks includes weekly inspections of the concrete cellars around the steel tanks, or visual inspections through inspection ports to determine if a leak has been initiated.
- Liquid level sensing devices are checked on an annual basis

Buried Piping Integrity and Leak Testing

- Buried piping is present.
- Integrity and leak testing of buried piping is performed at the time of ☒ installation, ☒ modification, ☒ construction, ☒ relocation, or ☒ replacement.

Aboveground Piping Examination

- All aboveground valves and piping (including flange joints, valve glands and bodies, catch pans, pipe supports, locking of valves, and metal surfaces) are regularly examined.
- The facility also uses API 570 for the inspection of above ground piping. API 570 includes Calculations of Corrosion Rate and Remaining Life Determination, Maximum Allowable Working Pressure, Minimum Required Thickness, Evaluation of Locally Thinned Areas, and Pressure Testing Requirements; Nondestructive Testing and Welding Requirements, Repairs and Alterations as well as Recommended Inspection Practices.

Dike Integrity and Drainage Inspections

- Dikes are inspected for integrity weekly in accordance with preventive maintenance procedures (PM). All PM inspections are recorded. Undocumented inspections are made on a daily basis and particularly after major storms. A work order is generated if equipment or dikes are found to be in need of repair.
- The diked area is inspected on the basis of daily observations and weekly PM and particularly after major storms for any oil stains on soil, sheen on standing water or drip from equipment. A work order is generated if equipment needs to be repaired.
- Drainage of rainwater from secondary containment into a storm drain or an open watercourse is not allowed. (However, rainwater may be drained onto the ground as stated in Section 1.8.) All rainwater is usually removed from diked areas by a vacuum truck and disposed of in accordance with the discharge plan.

Other Applicable Inspections

- A test is conducted every five years in accordance with the discharge plan to test all buried drain piping.

Documentation:

- Inspection and test records are provided in Appendix B.
- Other documentation concerning inspections, and repairs may be found in the operator's logbook, in the environmental files (located in the main office) or in the automated work order system.

APPENDIX A

NOTIFICATION

- Contact List and Phone Numbers
- Notification Data Sheet
- Procedures for Reporting Spills and Upsets
- BLM "Report of Undesirable Event" (Form NM 3162-1)
- Oil Conservation Division Form "Release Notification and Corrective Action" Form (C-141)
- Frontier Field Services, Growth Fund Policy Spill Reporting Form
- Submittal of Information to Regional Administrator for Qualified Discharge(s)

Spill Prevention, Control, and Countermeasure Plan

Contact List and Phone Numbers

The following is a contact list and phone number reference for the Facility:

REFERENCE THE "EMERGENCY ACTION PLAN" FOR ADDITIONAL AND THE MOST UPDATED NUMBERS

Contact	Primary	Alternate
<i>Designated Person Accountable For Oil Spill Prevention and/or Facility Response Coordinator</i>		
<i>Name/Title: <u>David Harris/ Plant Manager</u></i>	505-677-5117	505-703-0891
<i>Name/Title: <u>Glen Parrish/ Maintenance Supt.</u></i>	505-677-5102	505-513-0408
<u>National Response Center</u>	800-424-8802	202-267-2675
<u>Bureau of Land Management</u>	505-887-6544	
State Agency for Oil Spill Response <u>New Mexico Oil Conservation Division (24 hr)</u>	505-748-1283	
<i>Cleanup Contractors (as necessary):</i>		
Vacuum Trucks – I&W Trucking, Loco Hills	505-677-2111	
Vacuum Trucks – Rowland Trucking, Hobbs	505-393-4994	
Contract Labor – Stevenson Roach, Artesia	505-746-3222	
Contract Labor – E.D. Walton	800-616-3633	
Earth Moving Equipment – Sweatt Construction, Artesia	505-748-1238	
Earth Moving Equipment – E.D. Walton	800-616-3633	
HazMat Response – _____		
HazMat Response – Safety & Env Solutions, Hobbs	505-397-0510	
<i>Other Federal, State and local agencies (as necessary):</i>		

Spill Prevention, Control, and Countermeasure Plan

Notification Data Sheet

The Facility will utilize the following form to relate information in the event of a discharge:

Date: _____ Time: _____

INCIDENT DESCRIPTION

Reporter's Full Name: _____ Position: _____
Day Phone Number: _____ Evening Phone Number: _____
Company: _____ Organization Type: _____
Facility Address: _____ Owner's Address: _____

Facility Latitude: _____ Facility Longitude: _____

Spill Location: _____
(if not at Facility) _____

Responsible Party's Name: _____ Phone Number: _____

Responsible Party's Address: _____

Source and/or cause of discharge: _____

Nearest City: _____

County: _____ State: _____ Zip code: _____

Section: _____ Township: _____ Range: _____ County: _____

Distance from City: _____ Direction from City: _____

Container Type: _____ Container Storage Capacity: _____

Facility Oil Storage Capacity: _____

Material: _____

Total Quantity Released	Water Impact (YES or NO)	Quantity into Water

RESPONSE ACTION(S)

Action(s) taken to Correct, Control, or Mitigate Incident: _____

Number of Injuries: _____ Number of Deaths: _____

Evacuation(s): _____ Number Evacuated: _____

Damage Estimate: _____

More information about impacted medium: _____

CALLER NOTIFICATIONS

National Response Center (NRC): 1-800-424-8802

Additional Notifications (Circle all applicable): State Other

ADDITIONAL INFORMATION

Any information about the incident not recorded elsewhere in this report: _____

NOTE: DO NOT DELAY NOTIFICATION PENDING COLLECTION OF ALL INFORMATION.

Spill Prevention, Control, and Countermeasure Plan

Procedures for Reporting Spills and Upsets

1. PROCEDURES FOR REPORTING SPILLS AND UPSETS

Empire Abo Gasoline Plant

This is to be used to know what type of spills or upsets are "reportable" and the reporting procedures to follow, as required by Frontier Field Services and the agencies of jurisdiction for the gas plant. These reporting procedures are consistent with and should be used in conjunction with any facility comprehensive spill contingency plans. Both the New Mexico Oil Conservation Division and the Bureau of Land Management combine the volume of produced water and oil to determine reportable volume.

For spills that do not create a sheen on water or allow oil into a dry draw, the following procedures should be followed.

2. REPORTABLE SPILLS

Releases to be reported by the Plant Manager or delegated person:

a. OIL AND PRODUCED WATER

Spill Conditions		NMOCD		Required Reports		NRC ¹	BP*
Location	Amount (bbl)	Phone ²	Write ³	BLM	BLM	Phone	Phone
Federal	<5	No	No	No	No	No	Yes
Federal	>5, <10	No	Yes	No	No	No	Yes
Federal	>10, <25	No	Yes	No	Yes	No	Yes
Federal	>25, <100	Yes	Yes	No	Yes	No	Yes
Federal	>100	Yes	Yes	Yes	Yes	No	Yes
Fee, State	<5	No	No	No	No	No	Yes
Fee, State	>5, <25	No	Yes	No	No	No	Yes
Fee, State	>25	Yes	Yes	No	No	No	Yes
In Water - BLM ⁴	Any	Yes	Yes	Yes	Yes	Yes	Yes
In Water - State ⁴	Any	Yes	Yes	Yes	Yes	Yes	Yes

*All oil spills greater than 1 barrel must be reported to the Plant Manager.

Notes:

- 1 National Response Center (1-800-424-8802) for any spills in water
- 2 Phone - telephone call made within 24 hours of the spill
- 3 Write - written report as described below, within 10 days
- 4 See "Oil Spill Contingency Plan" located in Appendix D.

Report to

- Frontier Plant Manager
- Chad Cagle - Tulsa
- New Mexico Oil Conservation Division
- If on BLM land, the BLM District Office
- If spill enters water or water course - National Response Center (1-800-424-8802).

Reporting Method:

- As required, phone in report within 24 hours
See note on telephone reporting

Spill Prevention, Control, and Countermeasure Plan

- For all spills, written report within 10 days
- Use Release Notification and Corrective Action Form (C-141) to report to OCD
- Use BLM form NM 3162-1 to report to the BLM
- Use Frontier Field Services, Growth Fund Policy Spill Reporting Form (see attached).

b. CHEMICAL SPILLS

Reportable Spill: Spills of caustics, acids, or chemicals endangering persons, wildlife, or property

Methanol

5000 lbs. or 16 bbls.

CERCLA

For other chemicals, contact the Frontier Plant Manager.

Reporting Method:

- First, report immediately any chemical spill to the Frontier Plant Manager before reporting further, unless people or wildlife are immediately endangered.
- Spills that could potentially harm the public or cause significant damage to the environment should be reported to the New Mexico Oil Conservation Division and the Bureau of Land Management (if applicable) district office.
- If communications with Frontier Plant Manager confirm the existence of a "reportable quantity" spill, additional reports must be made to the National Response Center, the SERC, LEPC, and OCD.

MSDS sheets and other available resources should be used in obtaining data on chemicals used in your facility.

c. GASEOUS RELEASE

Reportable Release:

- On BLM land, any event releasing 500 MCF or more of gas (use BLM form NM 3162-1)
- Any event that releases more than 500 MCF requires immediate notification of the NMOCD district office
- Any event that releases more than 5000 MCF requires written notification of the NMOCD district office
- Any event that places life or property in danger requires NMOCD verbal and written report

Reporting Method:

- First, report immediately any gaseous release to the Frontier Plant Manager, unless people or wildlife are immediately endangered.
- Releases that could potentially harm the public or cause significant damage to the environment should be reported to the New Mexico Oil Conservation Division and the Bureau of Land Management district office.

3. NOTES ON REPORTING

a. TELEPHONE REPORTS

- Reports should be made as soon as possible, at least within 24 hours. It is recommended to discuss spill with Randy McCollum, Manager of Compliance, before reporting to other entities.
- For telephone reports, use the Frontier Field Services, Growth Fund Policy Form as a guide to indicate what information needs to be given. A copy of this form is attached to the plan.
- Document in facility records, all attempts to telephone reports to agencies successfully or unsuccessfully.
- Document spills of less than reportable amounts in facility files.

b. WRITTEN REPORTS

- Use the Frontier Field Services, Growth Fund Policy Spill Report Forms for reporting all spills and releases.
- Use Release Notification and Corrective Action Form (C-141) to report to OCD.
- Use BLM form NM 3162-1 to report to the BLM

Spill Prevention, Control, and Countermeasure Plan

- Reports should be submitted within 10 days of spill.

Spill Prevention, Control, and Countermeasure Plan

c. ADDRESSES AND PHONE NUMBERS

- **Empire Abo Plant**
Production: David Harris (505) 677-5177 (W) (505) 703-0891 (Cell)
Environmental: Randy McCollum (505) 676-3505 (W) (505) 361-0128 (Cell)
- **For the State of New Mexico**
New Mexico Oil Conservation Division
New Mexico Environment Department
District II
811 S. First Street
Artesia, NM 88210
(505) 748-1283
Ground Water Quality Bureau
P.O. Box 1778
Santa Fe, NM 87502
(505) 827-2918
- **Bureau of Land Management**
BLM - Carlsbad Resource Area
P.O. Box 1778
Carlsbad, NM 87820
(505) 887-6544
BLM - New Mexico State Office
P.O. Box 1449
Santa Fe, NM 87504
(505) 438-7400
- **National Response Center:** 1-800-424-8802
- **For SARA and CERCLA reportable spills (chemical spills):**
 - a.) **SERC:**
Max Johnson, ERC Coordinator
Department of Public Safety
Title III Bureau
P.O. Box 1628
Santa Fe, NM 87504-1628
(505) 827-9224
 - b.) **Local Emergency Planning Committee**
Eddy County LEPC
Attn: Mr. Joel Arnwine
101 West Greene St.
Carlsbad, NM 88220
(505) 887-9511
 - c.) **Fire Department**
Artesia Fire Department
309 N. 7th
Artesia, NM 88210
(505) 746-2701
Loco Hills Volunteer Fire Department
P.O. Box 9
Loco Hills, NM 88255
(505) 677-3266

Spill Prevention, Control, and Countermeasure Plan

Form NM 3162-1
(July 1991)

UNITED STATES DEPARTMENT OF THE INTERIOR
Bureau of Land Management
New Mexico State Office

REPORT OF UNDESIRABLE EVENT

DATE OF OCCURRENCE/DISCOVERY: _____ TIME OF OCCURRENCE: _____

DATE REPORTED TO BLM: _____ TIME REPORTED: _____

BLM OFFICE REPORTED TO: (RESOURCE AREA/DISTRICT/OTHER): _____

LOCATION: (1/4 1/4) _____ SECTION _____ T. _____ R. _____ MERIDIAN _____

COUNTY: _____ STATE: _____ WELL NAME: _____

OPERATOR: COMPANY NAME _____ PHONE NO. _____

CONTACT PERSON'S NAME _____

SURFACE OWNER: _____ MINERAL OWNER: _____
(FEDERAL/INDIAN/FEE/STATE)

LEASE NO.: _____ RIGHT-OF-WAY NO.: _____

UNIT NAME / COMMUNITIZATION AGREEMENT No.: _____

TYPE OF EVENT, CIRCLE APPROPRIATE ITEM(S):

BLOWOUT, FIRE, FATALITY, INJURY, PROPERTY DAMAGE, OIL SPILL, SALTWATER SPILL, OIL AND
SALTWATER SPILL, TOXIC FLUID SPILL, HAZARDOUS MATERIAL SPILL, UNCONTROLLED FLOW OF
WELLBORE FLUIDS, OTHER (SPECIFY):

CAUSE OF EVENT: _____

HazMat Notified: (for spills) _____

Law Enforcement Notified: (for thefts) _____

CAUSE AND EXTENT OF PERSONAL INJURIES/CAUSE OF DEATH(S):

Safety Officer Notified: _____

EFFECTS OF EVENT: _____

ACTION TAKEN TO CONTROL EVENT: _____

LENGTH OF TIME TO CONTROL BLOWOUT OR FIRE: _____

Facility: Empire Abo Gas Plant

A-8

Date: November 2006

Spill Prevention, Control, and Countermeasure Plan

VOLUMES DISCHARGED: OIL _____ WATER _____ GAS _____

OTHER AGENCIES NOTIFIED: _____

ACTION TAKEN OR TO BE TAKEN TO PREVENT RECURRENCE: _____

FINAL INVESTIGATION:

TEAM NAME(S) _____

FIELD INSPECTION DATE _____

SUMMARY OF RESULTS OF INSPECTION _____

RESOURCE LOSS WAS (CIRCLE ITEM): AVOIDABLE UNAVOIDABLE

DATE OF MEMO NOTIFYING MINERALS MANAGEMENT SERVICE THAT LOSS WAS AVOIDABLE: _____

DATE/TIME/PERSON NOTIFIED:

DISTRICT OFFICE _____

STATE OFFICE _____

WASHINGTON OFFICE _____

SUMMARY OF RESULTS OF RECLAMATION/CORRECTIVE ACTION:

REMARKS: _____

Spill Prevention, Control, and Countermeasure Plan

SIGNATURE OF AUTHORIZED OFFICER: _____

DATE: _____ TITLE: _____

Spill Prevention, Control, and Countermeasure Plan

District I
1615 N. French Dr., Hobbs, NM 88240
District II
1301 W. Grand Avenue, Artesia, NM 88210
District III
1000 Rio Brazos Road, Aztec, NM 87410
District IV
1220 S. St. Francis Dr., Santa Fe, NM 87505

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
1220 South St. Francis Dr.
Santa Fe, NM 87505

Form C-141
Revised October 10, 2003

Submit 2 Copies to appropriate
District Office in accordance
with Rule 116 on back
side of form

Release Notification and Corrective Action

OPERATOR

☐ Initial Report ☐ Final Report

Name of Company	Contact
Address	Telephone No.
Facility Name	Facility Type
Surface Owner	Mineral Owner
Lease No.	

LOCATION OF RELEASE

Unit Letter	Section	Township	Range	Feet from the	North/South Line	Feet from the	East/West Line	County
-------------	---------	----------	-------	---------------	------------------	---------------	----------------	--------

Latitude _____ Longitude _____

NATURE OF RELEASE

Type of Release	Volume of Release	Volume Recovered
Source of Release	Date and Hour of Occurrence	Date and Hour of Discovery
Was Immediate Notice Given? <input type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Not Required	If YES, To Whom?	
By Whom?	Date and Hour	
Was a Watercourse Reached? <input type="checkbox"/> Yes <input type="checkbox"/> No	If YES, Volume Impacting the Watercourse.	

If a Watercourse was Impacted, Describe Fully.*

Describe Cause of Problem and Remedial Action Taken.*

Describe Area Affected and Cleanup Action Taken.*

I hereby certify that the information given above is true and complete to the best of my knowledge and understand that pursuant to NMOCD rules and regulations all operators are required to report and/or file certain release notifications and perform corrective actions for releases which may endanger public health or the environment. The acceptance of a C-141 report by the NMOCD marked as "Final Report" does not relieve the operator of liability should their operations have failed to adequately investigate and remediate contamination that pose a threat to ground water, surface water, human health or the environment. In addition, NMOCD acceptance of a C-141 report does not relieve the operator of responsibility for compliance with any other federal, state, or local laws and/or regulations.

OIL CONSERVATION DIVISION

Signature:	Approved by District Supervisor:	
Printed Name:	Approval Date:	Expiration Date:
Title:	Conditions of Approval:	Attached <input type="checkbox"/>
E-mail Address:	Date:	Phone:

* Attach Additional Sheets If Necessary

Spill Prevention, Control, and Countermeasure Plan

Southern Ute Growth Fund Spill/Release Report

Forward to the Growth Fund Safety & Environmental Compliance Management Group at Fax 870-247-1178

Report Date _____ Time: _____ am/pm or (military time)

Spill Date _____ Spill Time: _____ am/pm or (military time)

Company Name: _____ Phone Number: _____

Reported By: _____ Title: _____

Facility Name: _____

Location: 1/4 _____ Section: _____ Township: _____ Range: _____

Type of Spill (Circle One): Produced Water, Oil, Gas, Other: _____

Estimate spilled: _____ barrels Estimate recovered: _____ Hazardous: Y / N

Is the Spill Contained: Y / N If No, is it within the property "footprint": Y / N

Extent of spill (area) _____ ft² Surrounding Land Use _____

Damages/Injuries? _____ Evacuation Needed?: Y / N

Ground Water impacted: Y ___ N ___ Surface Water impacted: Y ___ N ___

IF LESS THAN A MILE, report distance IN FEET to the nearest _____

Surface water: _____ Wetlands: _____ Water wells: _____ Dry arroyo: _____ Residence: _____

Cause Of Spill: _____

Describe immediate response: _____

Does this facility require an SPCC plan: Yes / No If yes, is there one in place: Yes / No

Is there a remediation plan in place for clean up: Yes / No

Follow-up Report Being Sent: Yes / No Due By the Following Date: _____, 20____

Closure Report Being Sent: Yes / No Due By the Following Date: _____, 20____

OTHER NOTIFICATIONS

Date	Agency	Contact Person	Type of notification	Comments:
			Written / Verbal / Both	
			Written / Verbal / Both	
			Written / Verbal / Both	
			Written / Verbal / Both	

For Office Use Only (if initial report was by voice):

Report Completed By: _____ Title: _____

Facility: Empire Abo Gas Plant

A-12

Date: November 2006

Spill Prevention, Control, and Countermeasure Plan

Note: This form is only used if the facility has spills (see below), which require submission of the plan to the EPA.

Sample - Submittal of Information to Regional Administrator for Qualified Discharge(s)

In the event of a qualified discharge or discharges, this page can be utilized to provide official notification to the Regional Administrator. If the Facility has had a discharge or discharges, which meet one of the following two criteria, then this report must be submitted to the Regional Administrator within 60 days. (Check as appropriate)

- ☐ This Facility has experienced a reportable spill as referenced in 40 CFR Part 112.1(b) of 1,000 gallons or more.
- ☐ This Facility has experienced two (2) reportable spills (as referenced in 40 CFR Part 112.1(b) of greater than 42 gallons each within a 12-month period.

Facility Name and Location: _____

Facility Contact Person (Name, address/phone number): _____

Facility maximum storage or handling capacity: _____

Facility normal daily throughput: _____

Describe the corrective action and countermeasures taken (include description of equipment repairs and replacements): _____

Describe the Facility (maps, flow diagrams and topographical maps attached as necessary): _____

Describe the cause of discharge (as referenced in 40 CFR Part 112.1(b)) including failure analysis of the system is: _____

Describe the preventative measures taken or contemplated to be taken to minimize the possibility of recurrence: _____

Other pertinent information: _____

- A copy of this report is also to be sent to the appropriate state agency in charge of oil pollution control activities.

APPENDIX B

LOGS

- SPCC Inspection Checklist
- Onshore Facility Bulk Storage Tank Drainage System

Spill Prevention, Control, and Countermeasure Plan

SPCC INSPECTION CHECKLIST

At least once annually, the Plant Manager in charge of the facility will visually inspect the facility for leaks and potential problems. This visual examination will review the condition of foundation and supports of tanks, possible corrosion of tanks, overflow equalizing lines, thief hatches (vacuum protection), back pressure vent valves, drain valves and lines, fill and shipping lines, oil transfer facilities, alarm systems, and overall condition of complete installation and secondary containment. Additionally, the Plant Manager will inspect and document the conditions of diked areas.

Production Facility: _____ Reviewer: _____
Review Date: _____

Berms around Storage Tanks:

- ___ Can they hold the capacity of storage tanks?
- ___ Are they in good shape (No low spots in berm)?
- ___ Do they have proper drainage?
- ___ Is there any contaminated soil inside or outside berms?
- ___ Is rainwater inspected prior to drainage?
- ___ Are drains properly closed and sealed after water drainage?
- ___ Are adequate records kept after water drainage?
- ___ Are accumulations of oil in traps, drips, sumps, etc. properly removed?

Comments: _____

Storage Tanks:

- ___ Are tanks leaking anywhere (pinholes, manways, etc.)?
- ___ Are tanks free of rust?
- ___ Are they visually examined on a routine basis?
- ___ Are they fail-safe engineered to prevent spills?
- ___ Adequate capacity ___ Over flow equalizing lines
- ___ Vacuum protection ___ High level shut down

Comments: _____

Truck Loading Racks:

- ___ Are truck drivers receiving their annual training on proper loading of trucks?
- ___ Are premature departure methods in place (chocks, signs, physical barriers [cones])?
- ___ Are trucks checked for leaking valves and fittings prior to departure?
- ___ Is the containment area in good condition and able to contain the full volume of one truck?

Comments: _____

Spill Prevention, Control, and Countermeasure Plan

Facility Inspection Procedures:

- ☐ Are weekly PM checks on berms documented?
- ☐ Are API 510 recommended practices for inspecting pressurized vessels being used?
- ☐ Are API 570 recommended practices for above ground piping inspections being used?
- ☐ Are API 653 recommended practices for inspecting tanks being used?

Comments: _____

General Comments: _____

**ONSHORE FACILITY BULK STORAGE
TANKS DRAINAGE SYSTEM**

Record of drainage, bypassing, inspection and oil removal from secondary containment:

Date of Drainage	Date of Bypassing		Date of Inspection	Oil Removal	Supervisor's or Inspector's Signature
	Open	Closed			

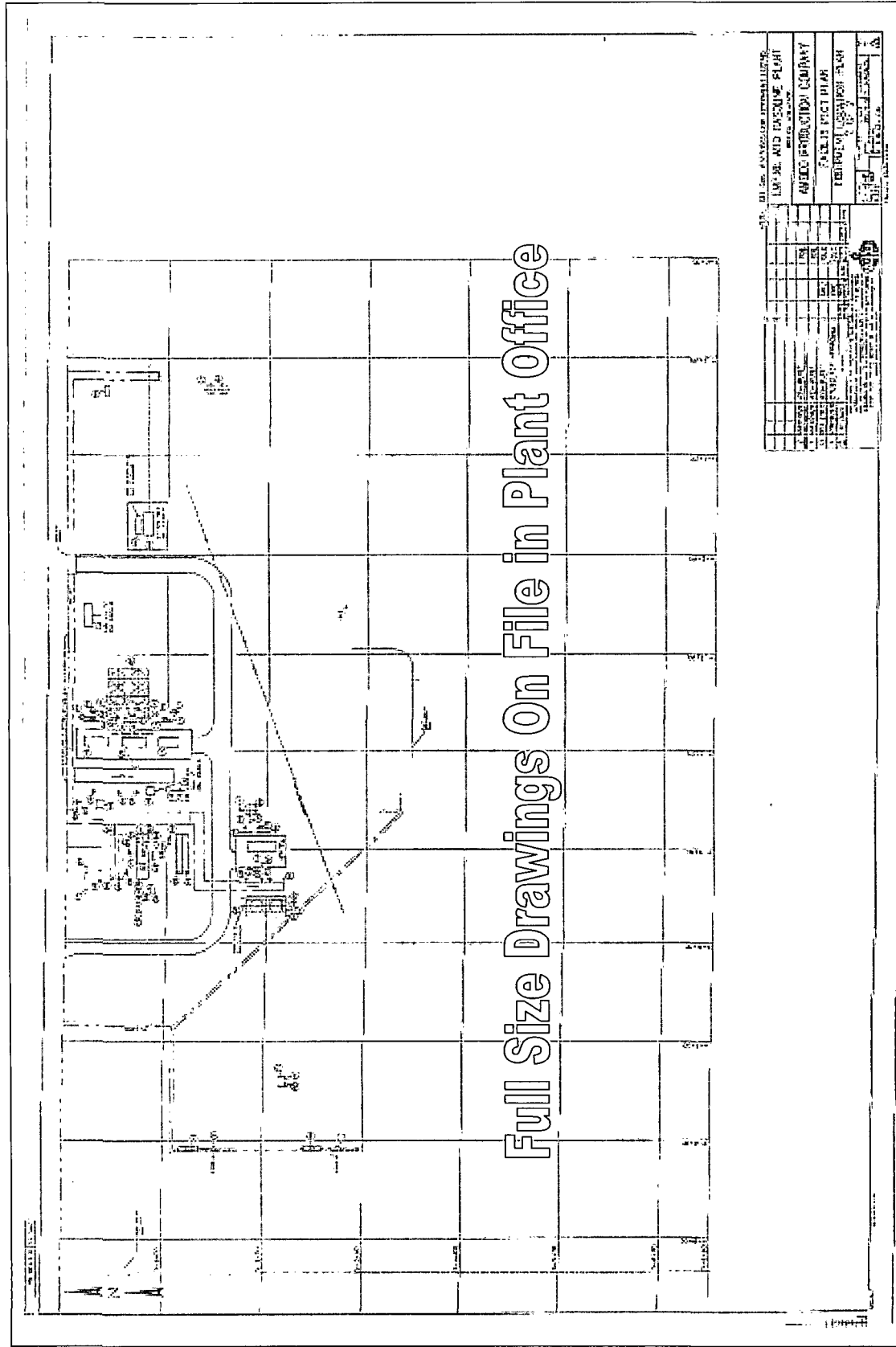
APPENDIX C

Facility Diagrams

- Equipment Layout (Page 1 and Page 2)
- Tanks and containment structures
- Topographical Map (1975)
- Aerial Photograph (October 1997)

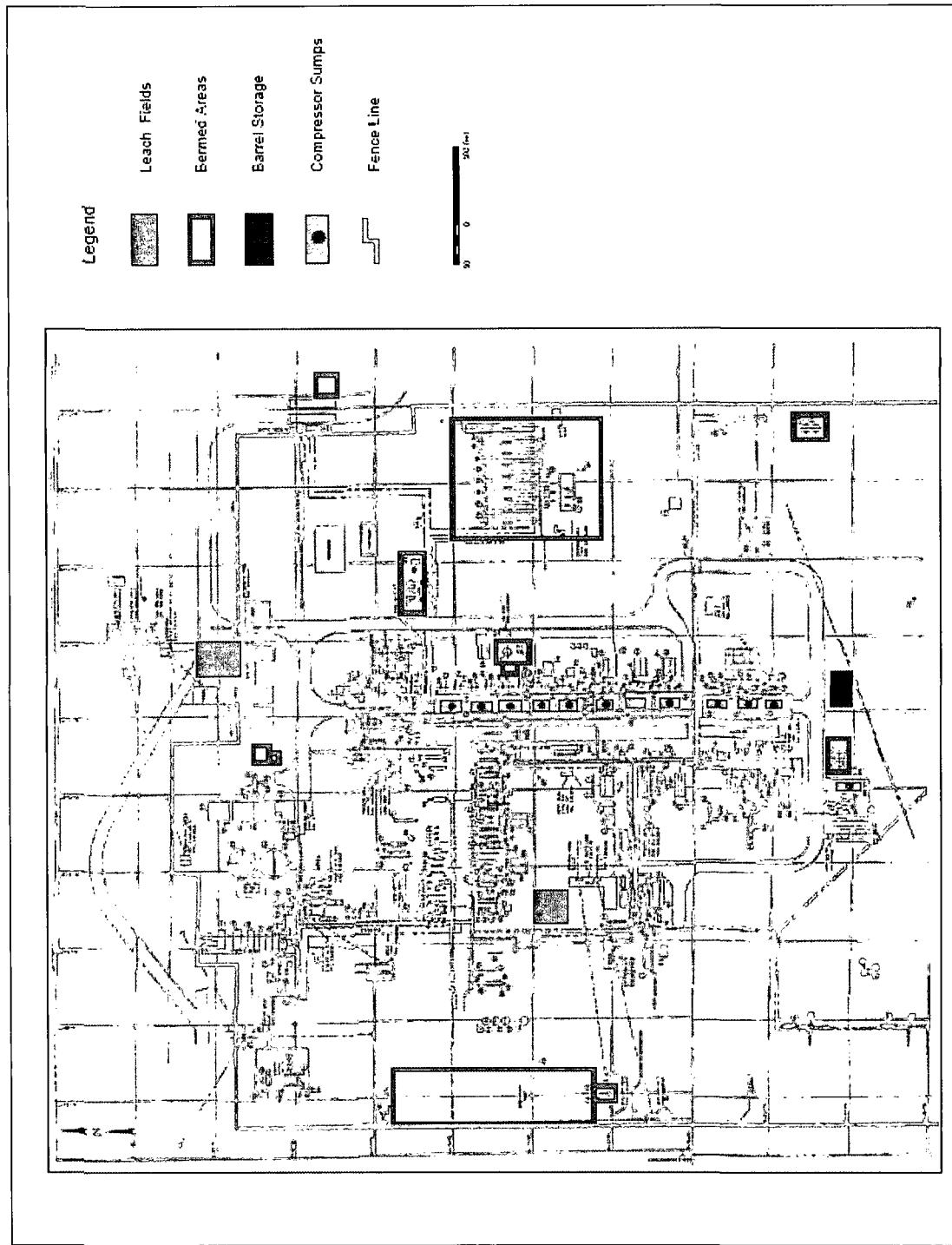
Full Size Drawings On File in Plant Office

Spill Prevention, Control, and Countermeasure Plan

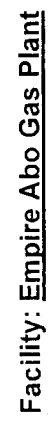


Spill Prevention, Control, and Countermeasure Plan

Tanks and Containment Structures

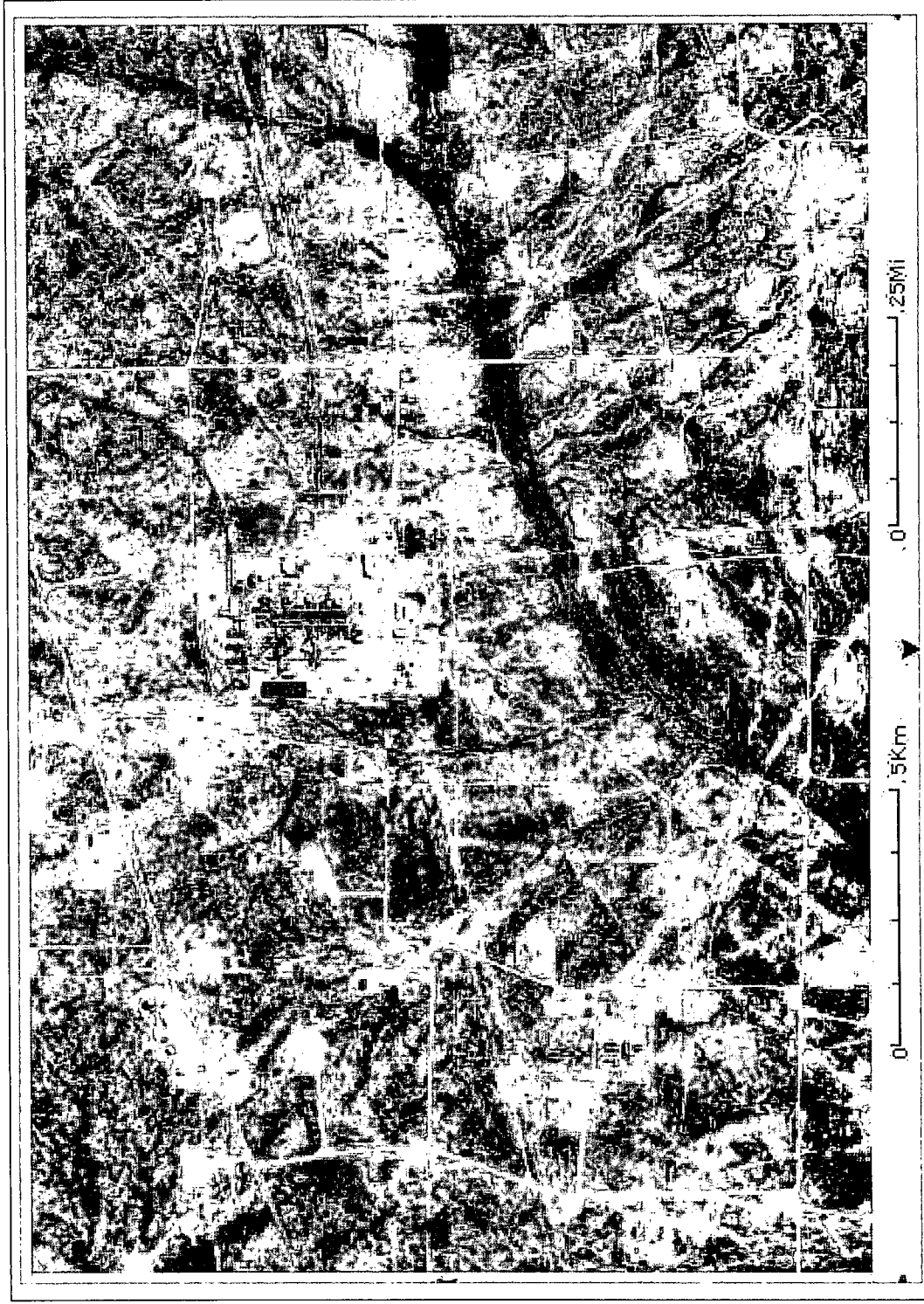


Topographical Map (1975)



Spill Prevention, Control, and Countermeasure Plan

Aerial Photograph (October 1997)



Facility: Empire Abo Gas Plant

C-6

Date: November 2006

APPENDIX D

Oil Spill Contingency Plan

Spill Prevention, Control, and Countermeasure Plan

A. INITIAL ACTION AT THE SITE OF A SPILL

The responsible Frontier Field Services, LLC employee at the scene of the operation who first learns about an oil spill or pollution shall take the following action:

1. **Notify Appropriate Supervisor** - Immediately contact supervisor, giving an assessment of the situation. The Supervisor on duty shall notify the Plant Manager or his designate. (David Harris: Home (505) 736-1846, Cell (505) 703-0891)
2. **Alleviate danger** - If any human life or property is in danger, take prompt action to alleviate such danger.
3. **Contain spill** - If the spill can be stopped or brought under control, take prompt action to do so. If possible, contain the spread of the spill using equipment available on-site.
4. **Determine if spill reached "navigable water."** "Navigable water" includes a variety of different sources, including lakes, creeks, and dry draws. A spill into navigable water is reportable if it is enough to create a sheen. Even if the draw is dry at the time of the spill, if oil gets into it, the spill is reportable to the National Response Center (NRC). If the spill did not get into "navigable water" respond according to the "Procedures for Reporting Spills and Upsets" found in Appendix A. If the spill did get into "navigable water", the Plant Manager or his designee will call the NRC and one of the following, beginning with the Plant Engineer:

- | | | |
|--|------|----------------------------------|
| 1) David Harris
Plant Engineer | Cell | (505) 677-5117
(505) 703-0891 |
| 2) Randy McCollum
Manager of Compliance | Cell | (505) 676-3505
(505) 361-0128 |
| 3) Chad Cagle
Director of Operations | Cell | (918) 388-8442
(918) 808-4863 |

Your supervisor will contact the Plant Manager and one of Frontier personnel and apprise them of the situation.

B. ACTIVATION OF SPCC PLAN:

After being notified, the Plant Manager or other responsible official shall promptly accomplish three actions:

1. **Notify Management** - He shall apprise Frontier of the situation as appropriate.
2. **Notify Agencies** - If the spill reaches navigable water, verify that the National Response Center, the New Mexico Oil Conservation Division (OCD), the Bureau of Land Management (as necessary), and the Frontier Plant Manager have been notified. To notify Federal and State agencies, call the following numbers:

Federal Agencies:	National Response Center (USCG)	(800) 424-8802
	Bureau of Land Management	(505) 877-6544
State Agencies	NM Oil Conservation Commission	(505) 748-1283

When a spill is outside the responsibility of the SPCC plan (i.e. it still does not reach navigable water) it may still need to be reported to a federal or local agency depending on area, amount, and type of spill. The "Procedure for Reporting Spills and Upsets" found in Appendix A contains reporting procedures.

3. **Initiate Cleanup** - The Plant Manager is responsible for determining the degree and speed of containment and cleanup measures required as outlined in the Oil Spill Clean Up Plan in C below. Decisions as to how to clean up the spill are based on

Spill Prevention, Control, and Countermeasure Plan

- Substance spilled
- Size of spill
- Sensitivity of location to people and environment
- If spill entered water
- Type of watercourse entered
- Requirements of agency

Do not talk to media - During an oil or condensate spill situation, the following matters should not be discussed with anyone other than Frontier Field Services, LLC personnel unless prior clearances have been obtained:

- a. Cause, liability, legal consequences of the spill
- b. Estimates of damage to property or ecology
- c. Length and scope of cleanup operations
- d. Opinions concerning county, state, federal or other government agencies' response to the spill

C. OIL SPILL CLEAN UP PLAN

1. The Plant Manager shall:

- a. Ensure the spill is contained or stabilized to the extent conditions allow.
- b. Ensure that the spill has been reported to the proper agencies.
- c. Initiate cleanup operations.
- d. Supervise and direct the cleanup operation subject to the approval of BP Management.
- e. Determine the needs of equipment and personnel involved in the cleanup operations.
- f. Keep the Frontier Plant Manager informed of progress.

2. The facility's Plant Manager shall clean up the spill as follows:

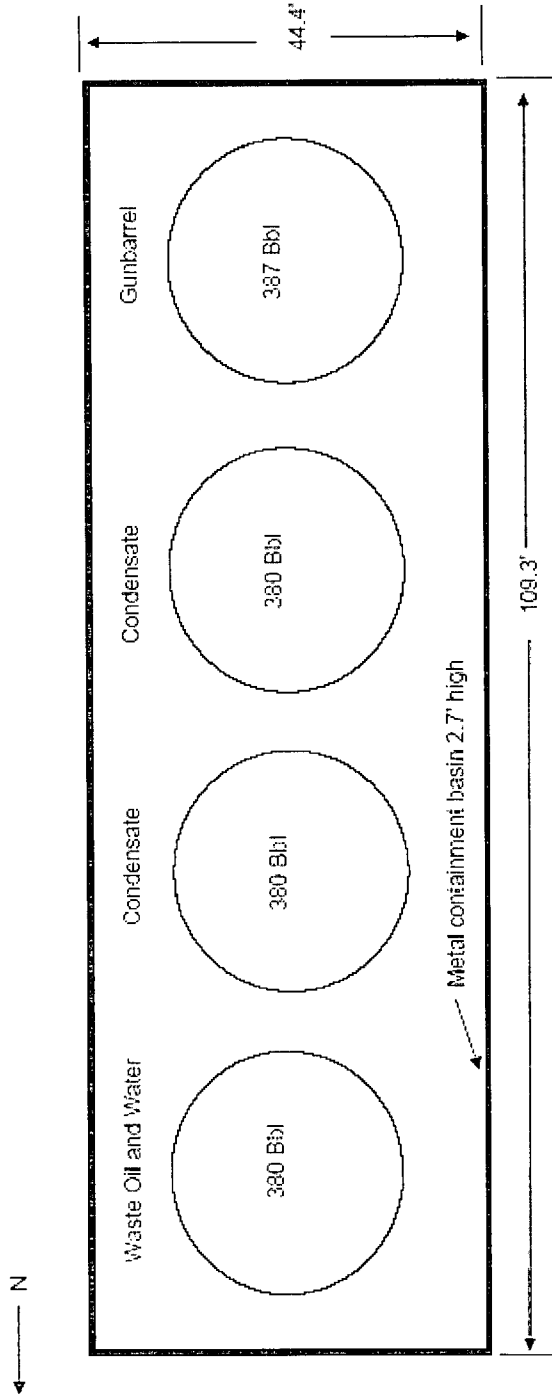
- a. Establish a plan of action for cleanup. This plan should be discussed with the Frontier Plant Manager and the responsible agency before implementing.
- b. Procure bulldozers and/or backhoe to build additional containment such as dikes, dams, etc., to better contain the oil spill.
- c. Procure vacuum trucks to reclaim the effluents spilled.
- d. Restore the area of the spill, as nearly as possible, to the same condition as before the spill.
- e. The Frontier Plant Manager will advise on appropriate action if the spill reaches waters of the United States.
- f. Record any reportable SPCC spill and maintain records in local files.
- g. If the spill enters the waters of the U.S. and is greater than 1000 gallons, or if two reportable spills occur within 12 consecutive months, a report must be submitted to the EPA within 60 days. This report will contain the entire SPCC plan along with details of the spill event(s).

APPENDIX E

CONTAINMENT DRAWINGS

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT SLOP OIL TANKS



Containment Capacity Calculations				
1. Capacity of Diked Area:	1729	4. Largest Tank Volume:	387	
2. Applicable Tank Disp.:	81	5. Excess Capacity:	1117	
3. Precipitation Allowance*:	144	All units in Barrels		

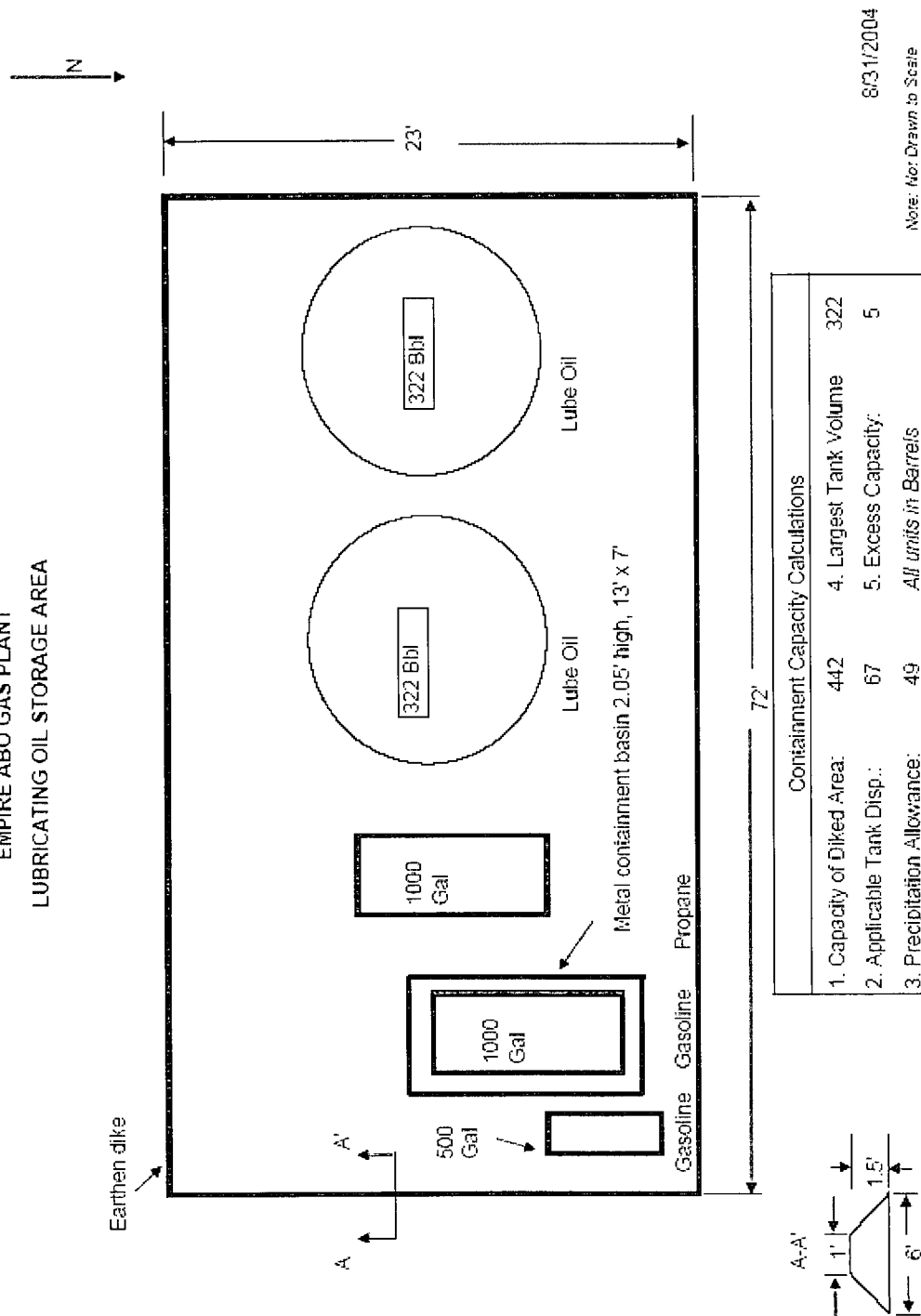
*Precipitation allowance of 2"

Note: Not Drawn to Scale

11/10/2006

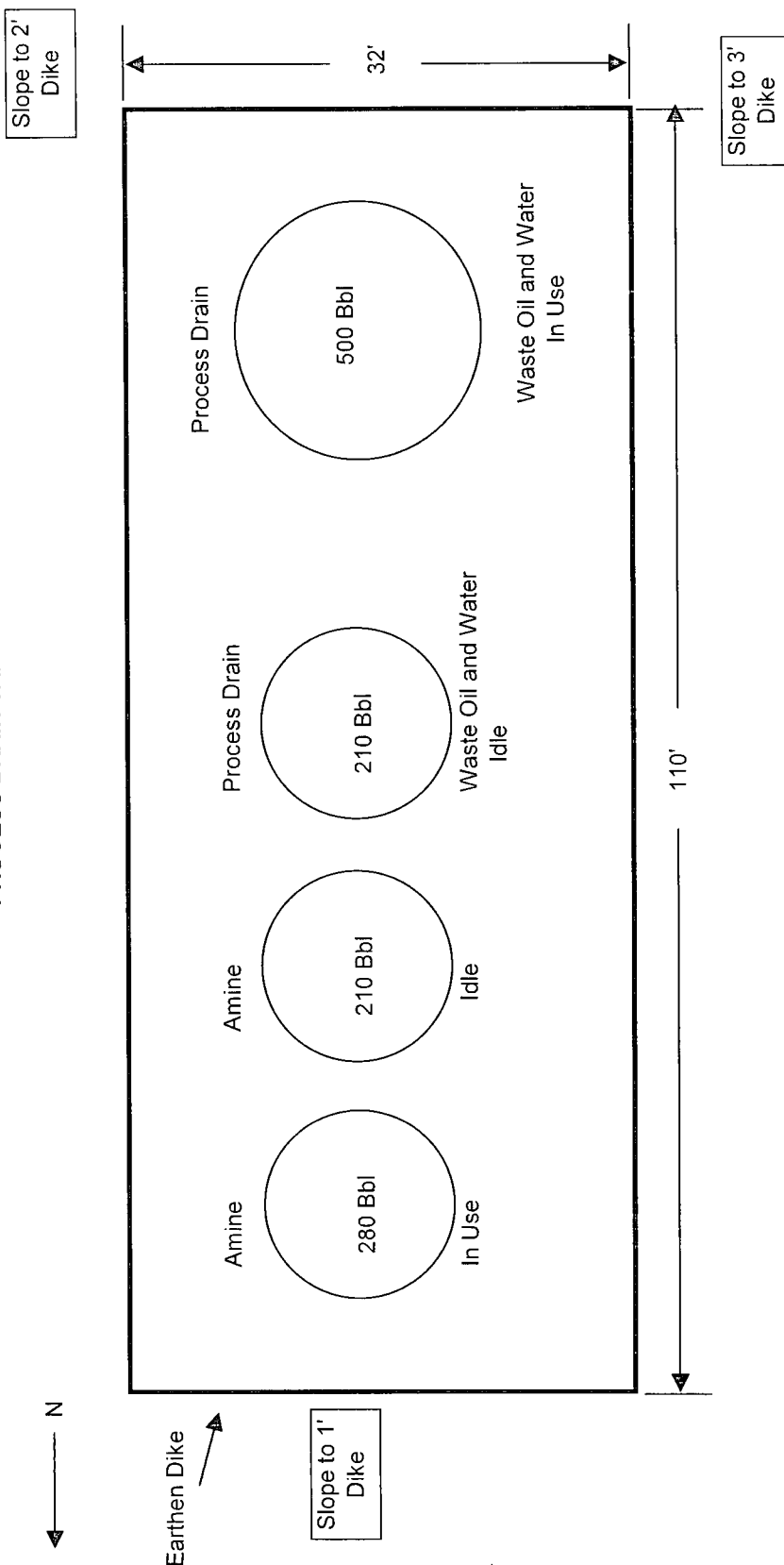
Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT LUBRICATING OIL STORAGE AREA



Spill Prevention, Control, and Countermeasure Plan

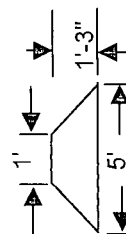
EMPIRE ABO GAS PLANT PROCESS DRAIN TANK AREA



Containment Capacity Calculations			
1. Capacity of Diked Area:	784	4. Largest Tank Volume:	500
2. Applicable Tank Disp.:	120	5. Excess Capacity:	114
3. Precipitation Allowance*:	49	All units in Barrels	

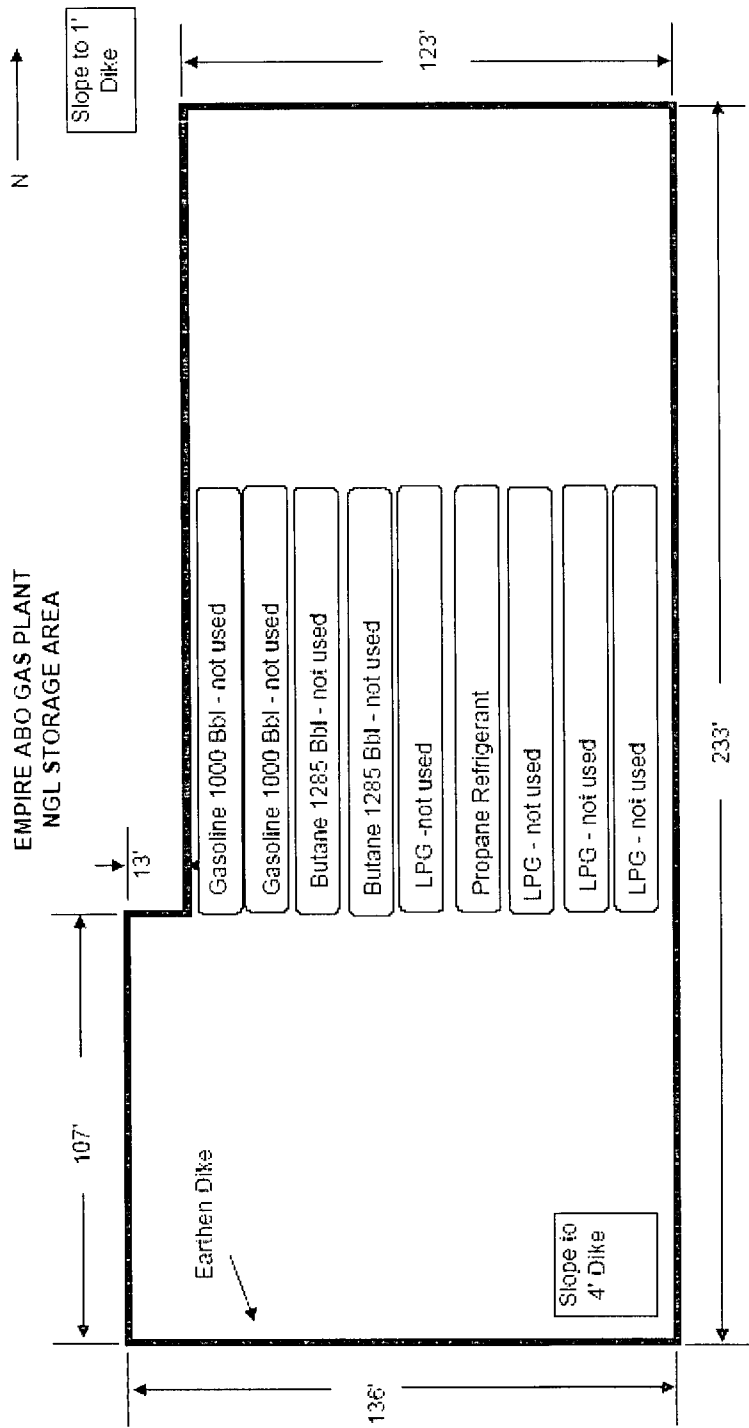
*Precipitation allowance of 2"

Minimum Dike Dimensions



Note: Not Drawn to Scale 8/31/2004

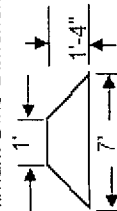
Spill Prevention, Control, and Countermeasure Plan



Containment Capacity Calculations			
1. Capacity of Diked Area:	7118	4. Largest Tank Volume:	1000
2. Applicable Tank Disp.: Elevated	5226	5. Excess Capacity:	5226
3. Precipitation Allowance*: 892	All units in Barrels		

*Precipitation allowance of 2"

Minimum Dike Dimensions

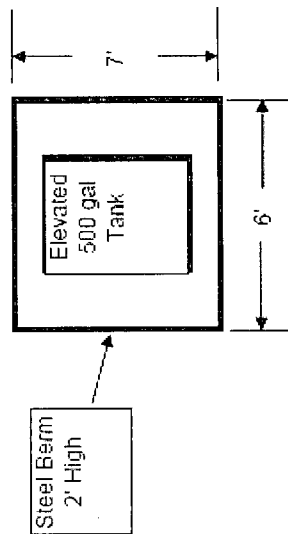


Note: Not Drawn to Scale 8/31/2004

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT MISCELLANEOUS STORAGE SITES

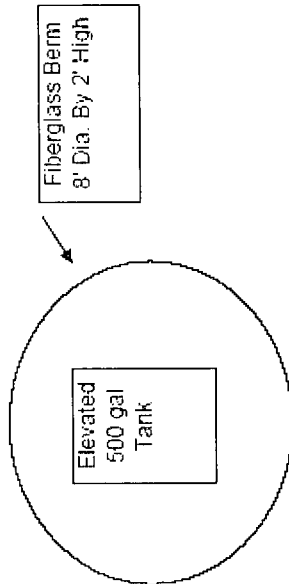
500 Gallon Luhe Oil Tank at Rental Compressor - TO BE REMOVED



Containment Capacity Calculations				
1. Capacity of Diked Area:	15	4. Largest Tank Volume:	11.9	
2. Applicable Tank Disp.:	0	5. Excess Capacity:	2	
3. Precipitation Allowance*:	1	<i>All units in Barrels</i>		

*Precipitation allowance of 2"

500 Gallon Diesel Storage Tank Near Chemical Storage Area



Containment Capacity Calculations				
1. Capacity of Diked Area:	18	4. Largest Tank Volume:	11.9	
2. Applicable Tank Disp.:	0	5. Excess Capacity:	4	
3. Precipitation Allowance*:	1	<i>All units in Barrels</i>		

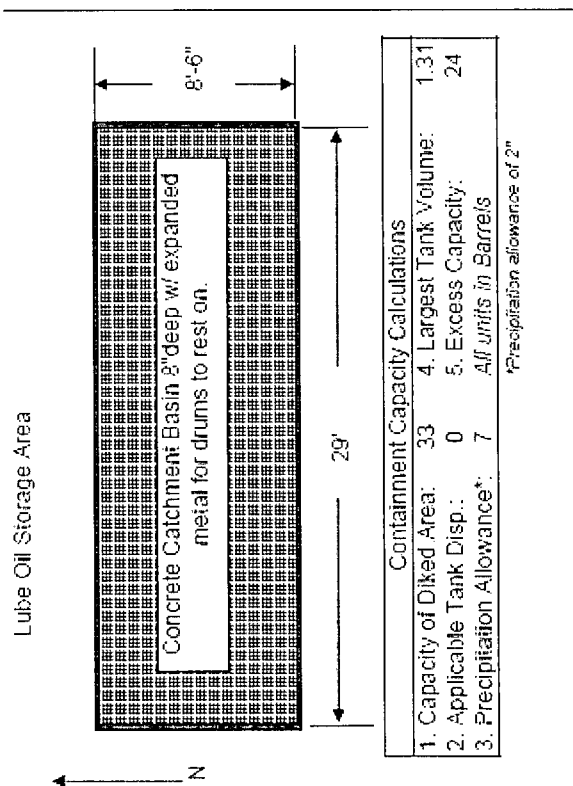
*Precipitation allowance of 2"

Note: Not Drawn to Scale

8/31/2004

Spill Prevention, Control, and Countermeasure Plan

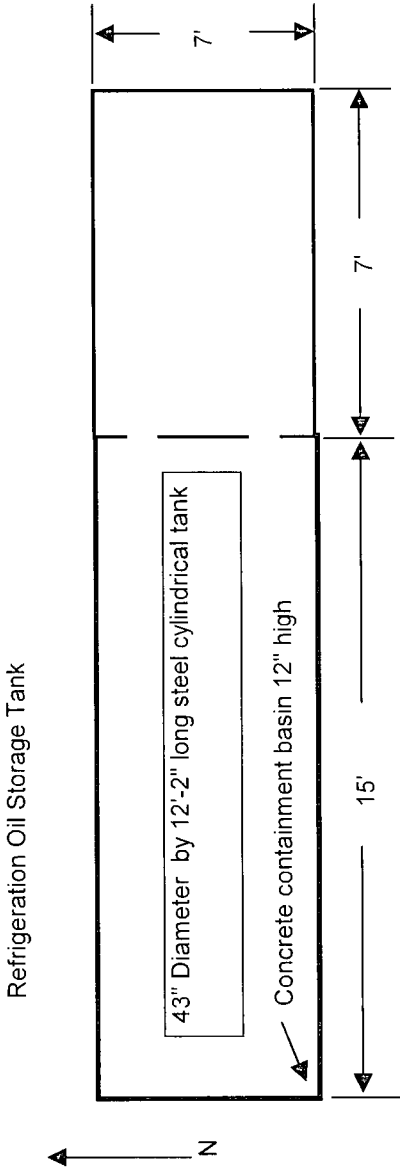
EMPIRE ABO GAS PLANT MISCELLANEOUS STORAGE SITES



Note: Not Drawn to Scale 8/31/2004

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT
MISCELLANEOUS STORAGE SITES



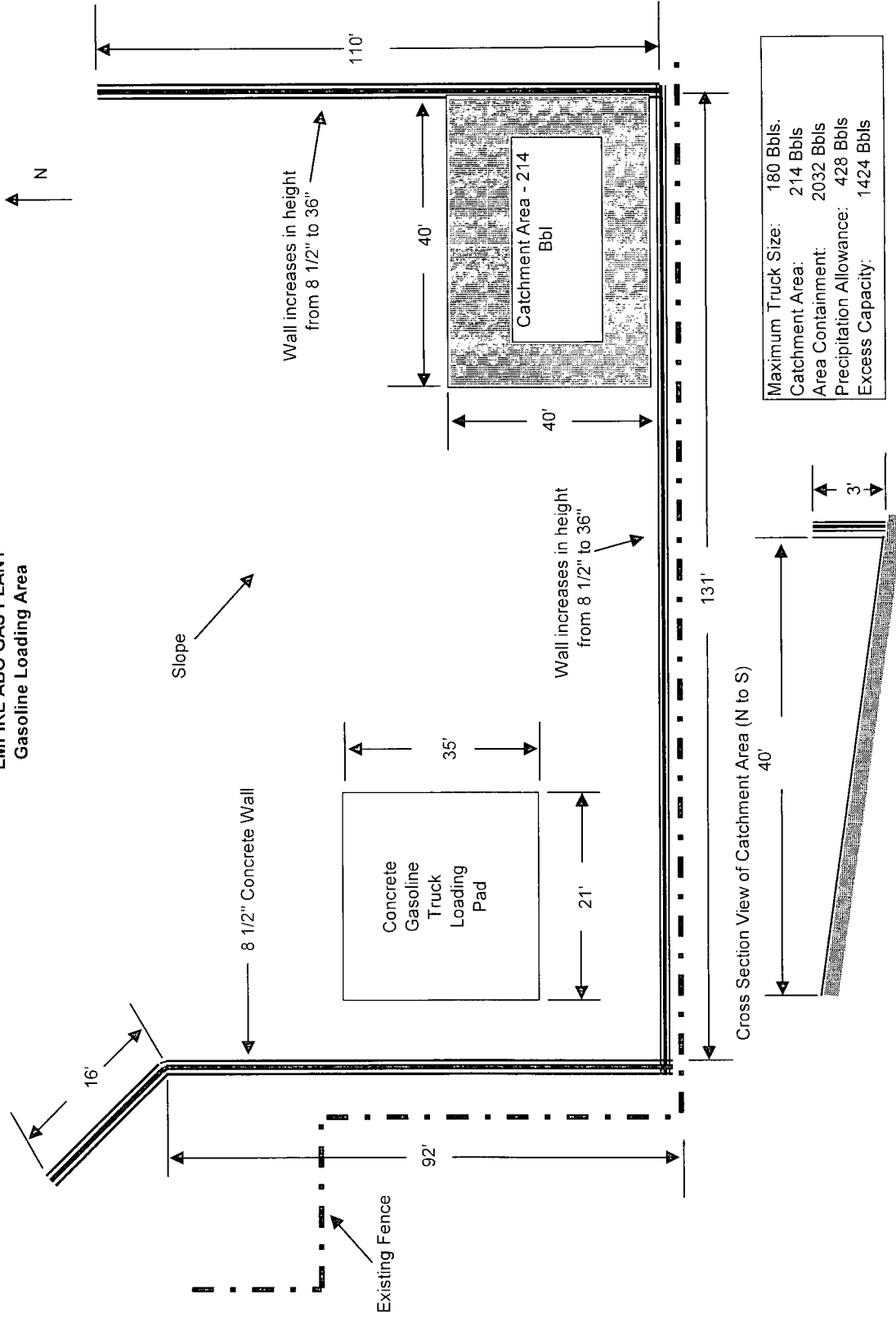
Containment Capacity Calculations				
1. Capacity of Diked Area:	27	4. Largest Tank Volume:	21.8	
2. Applicable Tank Disp.:	0	5. Excess Capacity:	1	
3. Precipitation Allowance*:	5	All units in Barrels		

*Precipitation allowance of 2"

Note: Not Drawn to Scale 12/13/2004

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT Gasoline Loading Area

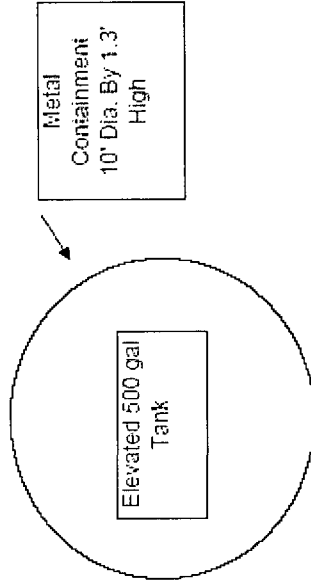


Note: Not Drawn to Scale 12/13/2004

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT MISCELLANEOUS STORAGE SITES

500 Gallon MR Solvent Storage Tank Due
East of Diesel Fuel Area



Containment Capacity Calculations				
1. Capacity of Diked Area:	18	4. Largest Tank Volume:	11.9	
2. Applicable Tank Disp.:	0	5. Excess Capacity:	4	
3. Precipitation Allowance*:	2	All units in Barrels		

*Precipitation allowance of 2"

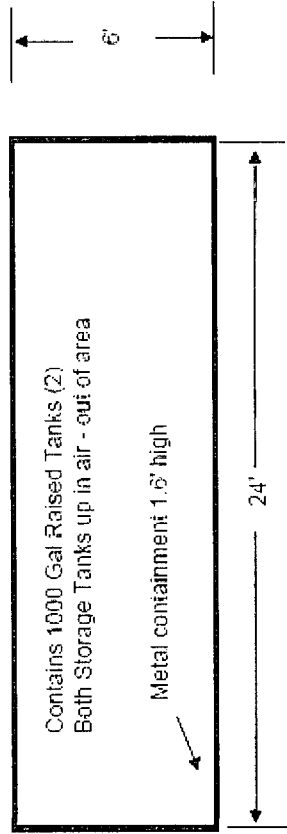
Note: Not Drawn to Scale

11/10/2006

Spill Prevention, Control, and Countermeasure Plan

EMPIRE ABO GAS PLANT MISCELLANEOUS STORAGE SITES

Monitor Well Groundwater - by evaporation pond - Temporary



Containment Capacity Calculations				
1. Capacity of Diked Area:	41	4. Largest Tank Volume:	23.8	
2. Applicable Tank Disp.:	0	5. Excess Capacity:	13	
3. Precipitation Allowance*:	4	All units in Barrels		

*Precipitation allowance of 2"

Note: Not Drawn to Scale

11/10/2006

ARTESIA 6 S, NEW MEXICO (290600)

Period of Record Monthly Climate Summary

Period of Record : 1/ 1/1914 to 3/31/2004

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
Average Max. Temperature (F)	56.8	62.1	69.1	78.3	86.4	94.0	94.8	93.2	86.9	77.9	65.8	57.9	76.9
Average Min. Temperature (F)	23.4	27.7	34.0	42.6	52.3	61.2	65.1	63.5	55.9	44.0	31.8	23.9	43.8
Average Total Precipitation (in.)	0.40	0.41	0.45	0.57	1.25	1.47	1.59	1.75	1.78	1.20	0.47	0.47	11.83
Average Total SnowFall (in.)	1.7	1.2	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.8	1.7	6.2
Average Snow Depth (in.)	0	0	0	0	0	0	0	0	0	0	0	0	0

Percent of possible observations for period of record.

Max. Temp.: 64.4% Min. Temp.: 64.4% Precipitation: 98.5% Snowfall: 60% Snow Depth: 58.5%

Check Station Metadata or Metadata graphics for more detail about data completeness.

Western Regional Climate Center, wrcc@dri.edu

Note: 2" of precipitation was used as a maximum storm event based on the above table. The 2" is in excess of the total monthly average for any given month over the past 90 years.



New Mexico Office of the State Engineer

Point of Diversion by Location

(with Owner Information)

(acre ft per annum)				(quarters are 1=NW 2=NE 3=SW 4=SE)				(quarters are smallest to largest)				(NAD83 UTM in meters)			
Nbr	Sub	basin	Use	Diversion	Owner	County	POD Number	Grant	Source	q	q	q	X	Y	Distance
5		DOM	3	PATON BROTHERS		ED	RA 02996		2	3	1	02	569808	3627025*	1117
7		PRO	0	PAN AMERICAN PETROLEUM CORP.		LE	RA 03917		Artesian	4	1	2	569019	3625660*	1154

Count: 2

MNAD83 Radius Search (in meters):

Easting (X): 568719 Northing (Y): 3626775 Radius: 2500

Sorted by: Distance

Information was derived from PLSS - see Help

This information is furnished by the NMOSE/ISC and is accepted by the recipient with the expressed understanding that the OSE/ISC make no warranties, expressed or implied, concerning the accuracy, completeness, usability, or suitability for any particular purpose of the data.

1:00 AM

Page 1 of 1

POINT OF DIVERSION BY LOCATION



New Mexico Office of the State Engineer

Water Right Summary

WR File Number: RA 02996

Primary Purpose: DOM 72-12-1 DOMESTIC ONE HOUSEHOLD

Primary Status: PMT PERMIT

Total Acres:

Total Diversion: 3

Owner: PATON BROTHERS

Documents on File

Doc	File/Act	Status			Transaction Desc.	From/To	Acres	Diversion	Consumptive
		1	2	3					
72121	1953-01-06	PMT	APR	ABS	RA 02996	T		3	

Point of Diversion

Pod Number	Source	Q Q Q			X	Y	Other Location Desc	
		64	16	4				
RA 02996		2	3	1	02 18S 27E	569808	3627025*	

An () after northing value indicates UTM location was derived from PLSS - see Help

The data is furnished by the NMOSE/ISC and is accepted by the recipient with the expressed understanding that the OSE/ISC make no warranties, expressed or implied, concerning the accuracy, completeness, reliability, usability, or suitability for any particular purpose of the data.

WATER RIGHT SUMMARY: 1 pg

8/6/09 11:02 AM



New Mexico Office of the State Engineer Transaction Summary

72121 All Applications Under Statute 72-12-1

Transaction Number: 283630

Transaction Desc: RA 02996

File Date: 12/22/1952

Primary Status: PMT Permit

Secondary Status: APR Approved

Person Assigned: *****

Applicant: PATON BROTHERS

Events

Date	Type	Description	Comment	Processed By
12/22/1952	APP	Application Received		*****
01/06/1953	FIN	Final Action on application		*****
01/06/1953	WAP	General Approval Letter		*****
09/09/2003	RUB	Re-Update the WR Database		*****

Change To:

WR File Nbr	Acres	Diversion	Consumptive	Purpose of Use
RA 02996		3		DOM 72-12-1 DOMESTIC ONE HOUSEHOLD

**Point of Diversion

RA 02996	569808	3627025*
----------	--------	----------

An () after northing value indicates UTM location was derived from PLSS - see Help

Remarks

THIS WELL IS A PLUGGED AND ABANDONED OIL WELL. WE ANTICIPATE REOPENING THE WELL AND CLEANING IT OUT TO AN APPROXIMATE DEPTH OF 300'. UNABLE TO LOCATE WELL LOG.

Conditions

- 10 Total diversion from all wells under this permit number shall not exceed 3 acre-feet per annum.
- B The well shall be drilled by a driller licensed in the State of New Mexico in accordance with Section 72-12-12 New Mexico Statutes Annotated. A licensed driller shall not be required for the construction of a driven well; provided, that the casing shall not exceed two and three-eighths (2 3/8) inches outside diameter (Section 72-12-12).
- D The casing shall not exceed 7 inches outside diameter except under specific conditions in which reasons satisfactory to the State Engineer are shown.

Action of the State Engineer

Approval Code: A - Approved

Action Date: 01/06/1953

Log Due Date: 01/06/1954

State Engineer:



New Mexico Office of the State Engineer

Water Right Summary

WR File Number: RA 03917

Primary Purpose: PRO 72-12-1 PROSPECTING OR DEVELOPMENT OF NATURAL RESOURCE

Primary Status: PMT PERMIT

Total Acres:

Total Diversion: 0

Owner: PAN AMERICAN PETROLEUM CORP.

Documents on File

Doc	File/Act	Status			Transaction Desc.	From/To	Acres	Diversion Consumptive
		1	2	3				
72121	1958-08-06	PMT	APR	ABS	RA 03917	T		3

Point of Diversion

Pod Number	Source	Q Q Q			X	Y	Other Location Desc
		64	16	4			
RA 03917	Artesian	4	1	2	10 18S 27E	569019	3625660*

An () after northing value indicates UTM location was derived from PLSS - see Help

The data is furnished by the NMOSE/ISC and is accepted by the recipient with the expressed understanding that the OSE/ISC make no warranties, expressed or implied, concerning the accuracy, completeness, reliability, usability, or suitability for any particular purpose of the data.

WATER RIGHT SUMMARY: 1 pg

8/6/09 11:07 AM



New Mexico Office of the State Engineer

Point of Diversion Summary

(quarters are 1=NW 2=NE 3=SW 4=SE)

(quarters are smallest to largest)

(NAD83 UTM in meters)

POD Number

Q64 Q16 Q4 Sec Tws Rng

X

Y

RA 03917

4 1 2 10 18S 27E

569019 3625660*

Driller License: BURKE, EDWARD B.

Driller Name:

Source: Artesian

Drill Start Date: 07/31/1958

Drill Finish Date: 07/31/1958

Log File Date: 08/06/1958

PCW Received Date:

Pump Type:

Pipe Discharge Size:

Casing Size:

Estimated Yield:

Depth Well: 130 feet

Depth Water: 50 feet

*UTM location was derived from PLSS - see Help

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8/6/09 11:00 AM

Page 1 of 1

POINT OF DIVERSION SUMMARY



New Mexico Office of the State Engineer

Transaction Summary

72121 All Applications Under Statute 72-12-1

Transaction Number: 255920

Transaction Desc: RA 03917

File Date: 08/06/1958

Primary Status: PMT Permit

Secondary Status: APR Approved

Person Assigned: *****

Applicant: PAN AMERICAN PETROLEUM CORP.

Events

Date	Type	Description	Comment	Processed By
08/06/1958	APP	Application Received		*****
08/06/1958	FIN	Final Action on application		*****
08/06/1958	WAP	General Approval Letter		*****

Change To:

WR File Nbr	Acres	Diversion	Consumptive	Purpose of Use
RA 03917		3		PRO 72-12-1 PROSPECTING OR DEVELOPMENT OF NATURAL RESOURCE
**Point of Diversion				
RA 03917		569019	3625660*	

An () after northing value indicates UTM location was derived from PLSS - see Help

Remarks

Malco "D" lease, Eddy Co.

Conditions

- 1A Depth of the well shall not exceed the thickness of the valley fill.
- 4 Use shall be limited to household, non-commercial trees, lawn and garden not to exceed one acre and/or stock use.

Action of the State Engineer

Approval Code: A - Approved

Action Date: 08/06/1958

Log Due Date: 08/06/1959

State Engineer:

The data is furnished by the NMOSE/ISC and is accepted by the recipient with the expressed understanding that the OSE/ISC make no warranties, expressed or implied, concerning the accuracy, completeness, reliability, usability, or suitability for any particular purpose of the data.

TRANSACTION SUMMARY: 1 pg

8/6/09 11:10 AM



United States
Department of
Agriculture



NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for **Eddy Area, New Mexico**

Empire Abo Gas Plant



August 6, 2009

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://soils.usda.gov/sqi/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<http://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://soils.usda.gov/contact/state_offices/).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Soil Data Mart Web site or the NRCS Web Soil Survey. The Soil Data Mart is the data storage site for the official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil scientists classified and named the soils in the survey area, they compared the

Custom Soil Resource Report

individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

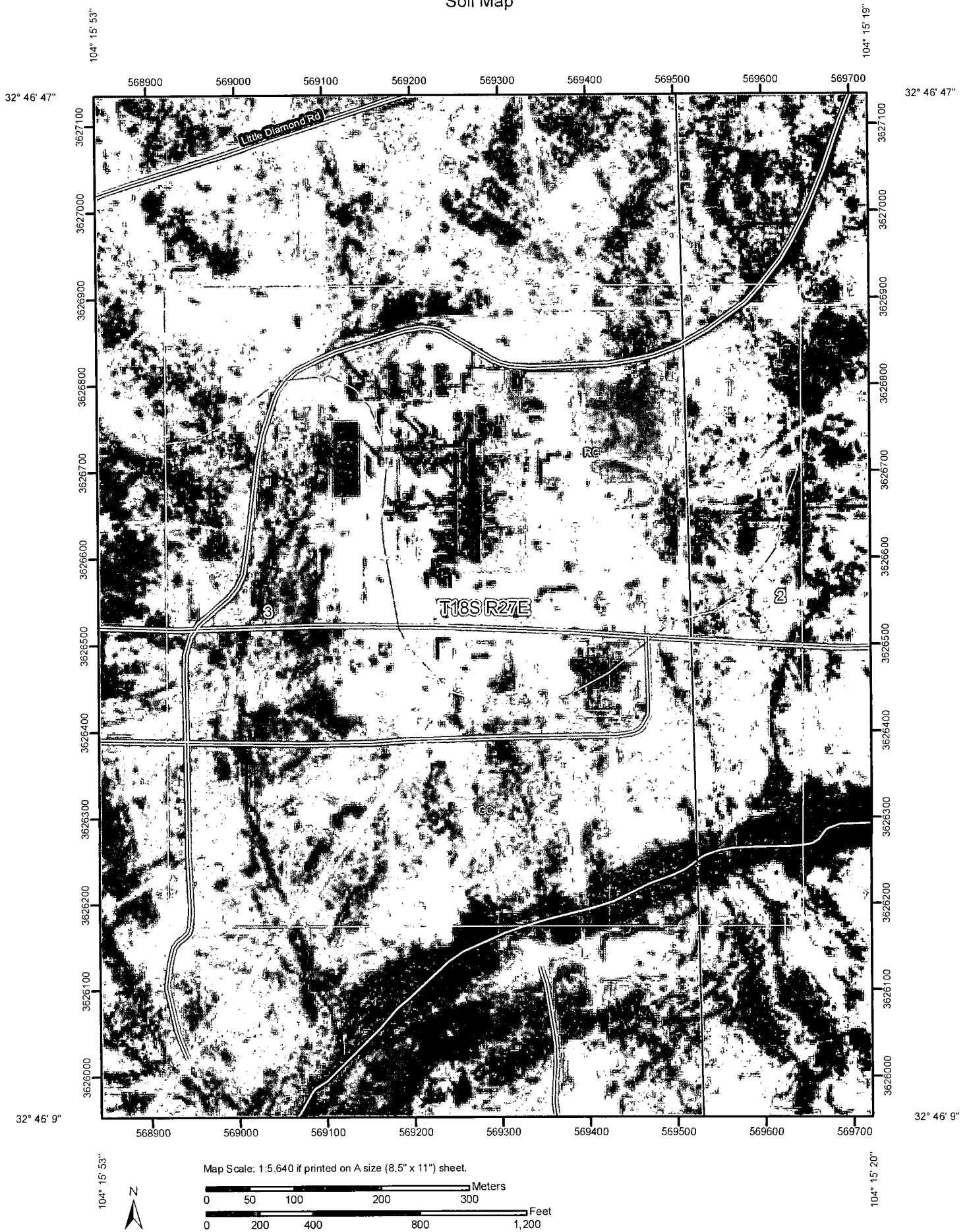
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map


The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report
Soil Map



MAP LEGEND

MAP INFORMATION

Area of Interest (AOI)
 Area of Interest (AOI)

Soils


Soil Map Units

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip




Sodic Spot





Spoil Area



Stony Spot

 Very Stony Spot

 Wet Spot

 Other

Special Line Features



Gully



Short Steep Slope



Other

Political Features



Cities



PLSS Township and Range



PLSS Section

Federal Land



Bureau of Land Management

Water Features



Oceans



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Map Scale: 1:5,640 if printed on A size (8.5" x 11") sheet.

The soil surveys that comprise your AOI were mapped at 1:20,000.

Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
 Coordinate System: UTM Zone 13N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Eddy Area, New Mexico
 Survey Area Data: Version 9, Feb 20, 2009

Date(s) aerial images were photographed: 10/19/1997

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Eddy Area, New Mexico (NM614)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
GC	Gypsum land-Cottonwood complex, 0 to 3 percent slopes	75.5	56.9%
RG	Reeves-Gypsum land complex, 0 to 3 percent slopes	57.2	43.1%
Totals for Area of Interest		132.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If

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intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Eddy Area, New Mexico

GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes

Map Unit Setting

Elevation: 3,000 to 5,000 feet
Mean annual precipitation: 10 to 14 inches
Mean annual air temperature: 60 to 64 degrees F
Frost-free period: 190 to 220 days

Map Unit Composition

Gypsum land: 60 percent
Cottonwood and similar soils: 30 percent

Description of Gypsum Land

Setting

Landform: Hills, plains, ridges
Landform position (two-dimensional): Shoulder, toeslope, backslope, footslope
Landform position (three-dimensional): Crest, nose slope, side slope, head slope
Down-slope shape: Convex
Across-slope shape: Linear
Parent material: Residuum weathered from gypsum

Interpretive groups

Land capability (nonirrigated): 8s

Description of Cottonwood

Setting

Landform: Hills, ridges
Landform position (two-dimensional): Shoulder, toeslope, backslope, footslope
Landform position (three-dimensional): Head slope, crest, nose slope, side slope
Down-slope shape: Convex
Across-slope shape: Linear
Parent material: Residuum weathered from gypsum

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: 3 to 12 inches to paralithic bedrock
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.20 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Gypsum, maximum content: 5 percent
Maximum salinity: Nonsaline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 1.0
Available water capacity: Very low (about 1.2 inches)

Interpretive groups

Land capability (nonirrigated): 6s
Ecological site: Gyp Upland (R042XC006NM)

Typical profile

0 to 8 inches: Loam

8 to 60 inches: Bedrock

RG—Reeves-Gypsum land complex, 0 to 3 percent slopes

Map Unit Setting

Elevation: 3,000 to 5,000 feet

Mean annual precipitation: 10 to 14 inches

Mean annual air temperature: 60 to 64 degrees F

Frost-free period: 190 to 220 days

Map Unit Composition

Reeves and similar soils: 55 percent

Gypsum land: 30 percent

Description of Reeves

Setting

Landform: Hills, plains, ridges

Landform position (two-dimensional): Toeslope, backslope, footslope, shoulder

Landform position (three-dimensional): Side slope, head slope, crest, nose slope

Down-slope shape: Convex

Across-slope shape: Linear

Parent material: Residuum weathered from gypsum

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 25 percent

Gypsum, maximum content: 80 percent

Maximum salinity: Nonsaline to slightly saline (2.0 to 8.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water capacity: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): 3s

Land capability (nonirrigated): 7s

Ecological site: Loamy (R042XC007NM)

Typical profile

0 to 8 inches: Loam

8 to 32 inches: Clay loam

32 to 60 inches: Gypsiferous material

Description of Gypsum Land

Setting

Landform: Hills, plains, ridges

Landform position (two-dimensional): Footslope, shoulder, toeslope, backslope

Landform position (three-dimensional): Crest, nose slope, side slope, head slope

Down-slope shape: Convex

Across-slope shape: Linear

Parent material: Residuum weathered from gypsum

Interpretive groups

Land capability (nonirrigated): 8s

Soil Information for All Uses

Soil Reports

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

AOI Inventory

This folder contains a collection of tabular reports that present a variety of soil information. Included are various map unit description reports, special soil interpretation reports, and data summary reports.

Component Legend

This report presents general information about the map units and map unit components in the selected area. It shows map unit symbols and names and the components in each map unit. It also shows the percent of the components in the map units, the kind of component, and the slope range of each component.

Report—Component Legend

Component Legend— Eddy Area, New Mexico						
Map unit symbol and name	Pct. of map unit	Component name	Component kind	Pct. slope		
				Low	RV	High
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes						
	60	Gypsum land	Miscellaneous area		38	
	30	Cottonwood	Series	0	2	3

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Component Legend— Eddy Area, New Mexico						
Map unit symbol and name	Pct. of map unit	Component name	Component kind	Pct. slope		
				Low	RV	High
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes						
	55	Reeves	Series	0	1	1
	30	Gypsum land	Miscellaneous area	0	2	3

Soil Chemical Properties

This folder contains a collection of tabular reports that present soil chemical properties. The reports (tables) include all selected map units and components for each map unit. Soil chemical properties are measured or inferred from direct observations in the field or laboratory. Examples of soil chemical properties include pH, cation exchange capacity, calcium carbonate, gypsum, and electrical conductivity.

Chemical Soil Properties

This table shows estimates of some chemical characteristics and features that affect soil behavior. These estimates are given for the layers of each soil in the survey area. The estimates are based on field observations and on test data for these and similar soils.

Depth to the upper and lower boundaries of each layer is indicated.

Cation-exchange capacity is the total amount of extractable cations that can be held by the soil, expressed in terms of milliequivalents per 100 grams of soil at neutrality (pH 7.0) or at some other stated pH value. Soils having a low cation-exchange capacity hold fewer cations and may require more frequent applications of fertilizer than soils having a high cation-exchange capacity. The ability to retain cations reduces the hazard of ground-water pollution.

Effective cation-exchange capacity refers to the sum of extractable cations plus aluminum expressed in terms of milliequivalents per 100 grams of soil. It is determined for soils that have pH of less than 5.5.

Soil reaction is a measure of acidity or alkalinity. It is important in selecting crops and other plants, in evaluating soil amendments for fertility and stabilization, and in determining the risk of corrosion.

Calcium carbonate equivalent is the percent of carbonates, by weight, in the fraction of the soil less than 2 millimeters in size. The availability of plant nutrients is influenced by the amount of carbonates in the soil.

Gypsum is expressed as a percent, by weight, of hydrated calcium sulfates in the fraction of the soil less than 20 millimeters in size. Gypsum is partially soluble in water. Soils that have a high content of gypsum may collapse if the gypsum is removed by percolating water.

Salinity is a measure of soluble salts in the soil at saturation. It is expressed as the electrical conductivity of the saturation extract, in millimhos per centimeter at 25

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degrees C. Estimates are based on field and laboratory measurements at representative sites of nonirrigated soils. The salinity of irrigated soils is affected by the quality of the irrigation water and by the frequency of water application. Hence, the salinity of soils in individual fields can differ greatly from the value given in the table. Salinity affects the suitability of a soil for crop production, the stability of soil if used as construction material, and the potential of the soil to corrode metal and concrete.

Sodium adsorption ratio (SAR) is a measure of the amount of sodium (Na) relative to calcium (Ca) and magnesium (Mg) in the water extract from saturated soil paste. It is the ratio of the Na concentration divided by the square root of one-half of the Ca + Mg concentration. Soils that have SAR values of 13 or more may be characterized by an increased dispersion of organic matter and clay particles, reduced saturated hydraulic conductivity and aeration, and a general degradation of soil structure.

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Chemical Soil Properties— Eddy Area, New Mexico									
Map symbol and soil name	Depth	Cation-exchange capacity	Effective cation-exchange capacity	Soil reaction	Calcium carbonate	Gypsum	Salinity	Sodium adsorption ratio	
	<i>In</i>	<i>meq/100g</i>	<i>meq/100g</i>	<i>pH</i>	<i>Pct</i>	<i>Pct</i>	<i>mmhos/cm</i>		
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes									
Gypsum land	—	—	—	—	—	—	—	—	—
Cottonwood	0-8	8.0-20	—	7.9-8.4	5-15	0-5	0.0-2.0	0-1	—
	8-60	—	—	—	—	—	—	—	—
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes									
Reeves	0-8	10-20	—	7.9-9.0	10-15	0-1	2.0-8.0	0-4	—
	8-32	10-20	—	7.9-9.0	15-25	0-3	2.0-8.0	0-4	—
	32-60	—	—	—	—	20-80	—	—	—
Gypsum land	—	—	—	—	—	—	—	—	—

Soil Qualities and Features

This folder contains tabular reports that present various soil qualities and features. The reports (tables) include all selected map units and components for each map unit. Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Soil Features

This table gives estimates of various soil features. The estimates are used in land use planning that involves engineering considerations.

A *restrictive layer* is a nearly continuous layer that has one or more physical, chemical, or thermal properties that significantly impede the movement of water and air through the soil or that restrict roots or otherwise provide an unfavorable root environment. Examples are bedrock, cemented layers, dense layers, and frozen layers. The table indicates the hardness and thickness of the restrictive layer, both of which significantly affect the ease of excavation. *Depth to top* is the vertical distance from the soil surface to the upper boundary of the restrictive layer.

Subsidence is the settlement of organic soils or of saturated mineral soils of very low density. Subsidence generally results from either desiccation and shrinkage, or oxidation of organic material, or both, following drainage. Subsidence takes place gradually, usually over a period of several years. The table shows the expected initial subsidence, which usually is a result of drainage, and total subsidence, which results from a combination of factors.

Potential for frost action is the likelihood of upward or lateral expansion of the soil caused by the formation of segregated ice lenses (frost heave) and the subsequent collapse of the soil and loss of strength on thawing. Frost action occurs when moisture moves into the freezing zone of the soil. Temperature, texture, density, saturated hydraulic conductivity (Ksat), content of organic matter, and depth to the water table are the most important factors considered in evaluating the potential for frost action. It is assumed that the soil is not insulated by vegetation or snow and is not artificially drained. Silty and highly structured, clayey soils that have a high water table in winter are the most susceptible to frost action. Well drained, very gravelly, or very sandy soils are the least susceptible. Frost heave and low soil strength during thawing cause damage to pavements and other rigid structures.

Risk of corrosion pertains to potential soil-induced electrochemical or chemical action that corrodes or weakens uncoated steel or concrete. The rate of corrosion of uncoated steel is related to such factors as soil moisture, particle-size distribution, acidity, and electrical conductivity of the soil. The rate of corrosion of concrete is based mainly on the sulfate and sodium content, texture, moisture content, and acidity of the soil. Special site examination and design may be needed if the combination of factors results in a severe hazard of corrosion. The steel or concrete in installations that intersect soil boundaries or soil layers is more susceptible to corrosion than the steel

Custom Soil Resource Report

or concrete in installations that are entirely within one kind of soil or within one soil layer.

For uncoated steel, the risk of corrosion, expressed as *low*, *moderate*, or *high*, is based on soil drainage class, total acidity, electrical resistivity near field capacity, and electrical conductivity of the saturation extract.

For concrete, the risk of corrosion also is expressed as *low*, *moderate*, or *high*. It is based on soil texture, acidity, and amount of sulfates in the saturation extract.

Custom Soil Resource Report

Soil Features— Eddy Area, New Mexico									
Map symbol and soil name	Restrictive Layer			Subsidence		Potential for frost action	Risk of corrosion		
	Kind	Depth to top	Thickness	Hardness	Initial	Total	Uncoated steel	Concrete	
		In	In		In	In			
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes									
Gypsum land		—	—		—	—	High	High	
Cottonwood	Paralithic bedrock	3-12	—	Moderately cemented	—	—	High	Moderate	
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes									
Reeves		—	—		—	—	High	High	
Gypsum land		—	—		—	—	High	High	

Soil Features

This table gives estimates of various soil features. The estimates are used in land use planning that involves engineering considerations.

A *restrictive layer* is a nearly continuous layer that has one or more physical, chemical, or thermal properties that significantly impede the movement of water and air through the soil or that restrict roots or otherwise provide an unfavorable root environment. Examples are bedrock, cemented layers, dense layers, and frozen layers. The table indicates the hardness and thickness of the restrictive layer, both of which significantly affect the ease of excavation. *Depth to top* is the vertical distance from the soil surface to the upper boundary of the restrictive layer.

Subsidence is the settlement of organic soils or of saturated mineral soils of very low density. Subsidence generally results from either desiccation and shrinkage, or oxidation of organic material, or both, following drainage. Subsidence takes place gradually, usually over a period of several years. The table shows the expected initial subsidence, which usually is a result of drainage, and total subsidence, which results from a combination of factors.

Potential for frost action is the likelihood of upward or lateral expansion of the soil caused by the formation of segregated ice lenses (frost heave) and the subsequent collapse of the soil and loss of strength on thawing. Frost action occurs when moisture moves into the freezing zone of the soil. Temperature, texture, density, saturated hydraulic conductivity (Ksat), content of organic matter, and depth to the water table are the most important factors considered in evaluating the potential for frost action. It is assumed that the soil is not insulated by vegetation or snow and is not artificially drained. Silty and highly structured, clayey soils that have a high water table in winter are the most susceptible to frost action. Well drained, very gravelly, or very sandy soils are the least susceptible. Frost heave and low soil strength during thawing cause damage to pavements and other rigid structures.

Risk of corrosion pertains to potential soil-induced electrochemical or chemical action that corrodes or weakens uncoated steel or concrete. The rate of corrosion of uncoated steel is related to such factors as soil moisture, particle-size distribution, acidity, and electrical conductivity of the soil. The rate of corrosion of concrete is based mainly on the sulfate and sodium content, texture, moisture content, and acidity of the soil. Special site examination and design may be needed if the combination of factors results in a severe hazard of corrosion. The steel or concrete in installations that intersect soil boundaries or soil layers is more susceptible to corrosion than the steel or concrete in installations that are entirely within one kind of soil or within one soil layer.

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Custom Soil Resource Report

Soil Features— Eddy Area, New Mexico									
Map symbol and soil name	Restrictive Layer			Hardness	Subsidence		Potential for frost action	Risk of corrosion	
	Kind	Depth to top	Thickness		Initial	Total		Uncoated steel	Concrete
		<i>In</i>	<i>In</i>		<i>In</i>	<i>In</i>			
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes									
Gypsum land		—	—		—	—	Low	High	High
Cottonwood	Paralithic bedrock	3-12	—	Moderately cemented	—	—	Low	High	Moderate
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes									
Reeves		—	—		—	—	Low	High	High
Gypsum land		—	—		—	—	Low	High	High

Soil Features

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Custom Soil Resource Report

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	Kind	Depth to top	Thickness	Hardness	Initial	Total		Uncoated steel	Concrete
		<i>In</i>	<i>In</i>		<i>In</i>	<i>In</i>			
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes									
Gypsum land		—	—		—	—	Low	High	High
Cottonwood	Paralithic bedrock	3-12	—	Moderately cemented	—	—	Low	High	Moderate
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes									
Reeves		—	—		—	—	Low	High	High
Gypsum land		—	—		—	—	Low	High	High

Soil Features

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Custom Soil Resource Report

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	Kind	Depth to top	Thickness	Hardness	Initial	Total		Uncoated steel	Concrete
GC—Gypsum land-Cottonwood complex, 0 to 3 percent slopes		In	In		In	In			
Gypsum land		—	—		—	—	Low	High	High
Cottonwood	Paralithic bedrock	3-12	—	Moderately cemented	—	—	Low	High	Moderate
RG—Reeves-Gypsum land complex, 0 to 3 percent slopes									
Reeves		—	—		—	—	Low	High	High
Gypsum land		—	—		—	—	Low	High	High

References

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- United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. <http://www.glti.nrcs.usda.gov/>
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Custom Soil Resource Report

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210.

Latitude N 32° 46' 33.71"
 Longitude W 104° 15' 34.85"
 Elevation : 3548.8'

PID Response Log Plot
 (parts per million)

Lithologic Well Log

Drilling started 7/23/2008, completed 7/24/2008.

Drilled with Air Rotary by Scarborough

SM - Very Pale Brown (10YR 7/3) very fine to medium grained quartz sand, poorly sorted, angular to subangular, compacted, dry, Pink (5YR 7/3) below 0.7'

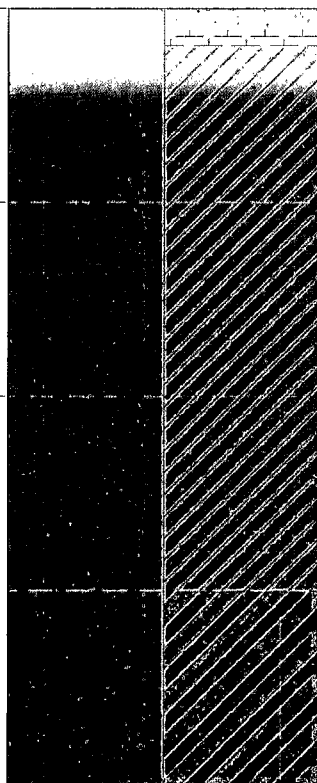
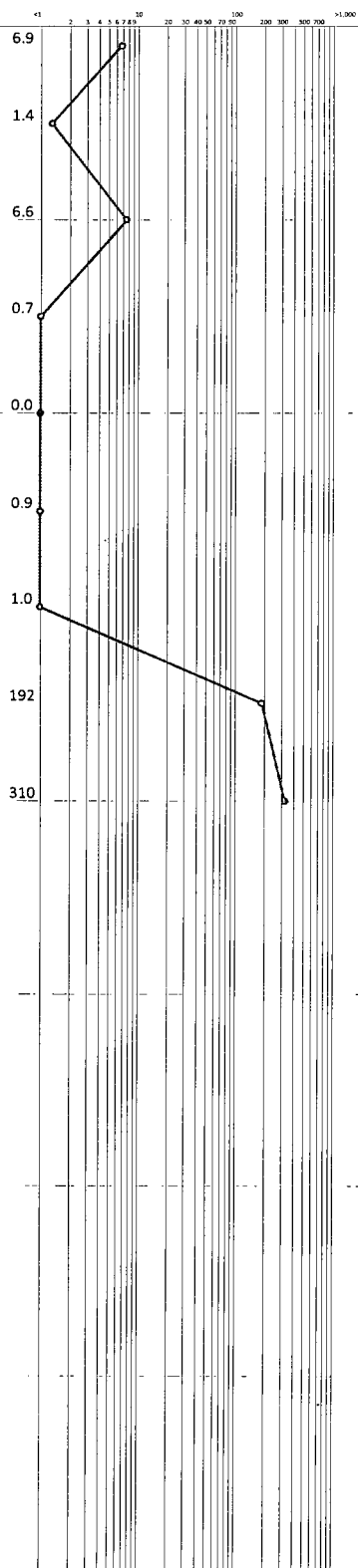
Gypsum - Pink (5YR 7/3) indurated

CL - Red (2.5YR 4/6) very fine grained quartz sand, moist, with Gypsum stringers, low plasticity

Abundant Gypsum in thin below 25'

CL - Dark Reddish Brown (2.5YR 3/4) with Reddish Brown to Reddish Gray matter, firm to stiff, low plasticity, blocky, hydrocarbon odor below 35'

Total Depth 40'



Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Laarson &
 Associates, Inc.
 Environmental Consultants

PID Response Log Plot
(parts per million)

Lithologic Well Log

Drilling started 6/16/2009, completed 6/16/2009.

Drilled with Air Rotary by Scarborough

GW- Gravel

CL - Yellowish Red (5YR 4/6) very fine grained quartz sand, weak, slight moisture

Gypsum - Gray to Pale Brown (10YR 6/1- 10YR 6/2) thin to thick bedded, friable to hard

CL - Olive Gray (5YR 4/2) very fine grained quartz sand, blocky, moist, medium plasticity

Gypsum - Gray to Pale Brown (10YR 6/1- 10YR 6/2) thin to massive, moderately hard

CL - Dark Reddish Brown (5YR 3/3) very fine grained quartz sand, soft, blocky, moist, low plasticity, interbedded with gypsum beds approximately 1-2 feet thick

Gypsum - Gray to Pale Brown (10YR 6/1- 10YR 6/2) thin to massive

Shale - Gray (10YR 6/1) thin bedded silty

Gypsum - Gray to Pale Brown (10YR 6/1- 10YR 6/2) thin to massive, friable to hard

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

Frontier Field Services, LLC.

Empire ABO Gas Plant

Sec. 3, T-18-S, R-27-E

Eddy County, New Mexico

Larson &
Associates, Inc.
Environmental Consultants

Latitude N 32° 46' 33.28"
 Longitude W 104° 15' 39.45"
 Elevation : 3544.3'

PID Response Log Plot (parts per million)

Lithologic Well Log

Drilling started 6/16/2009, completed 6/16/2009.

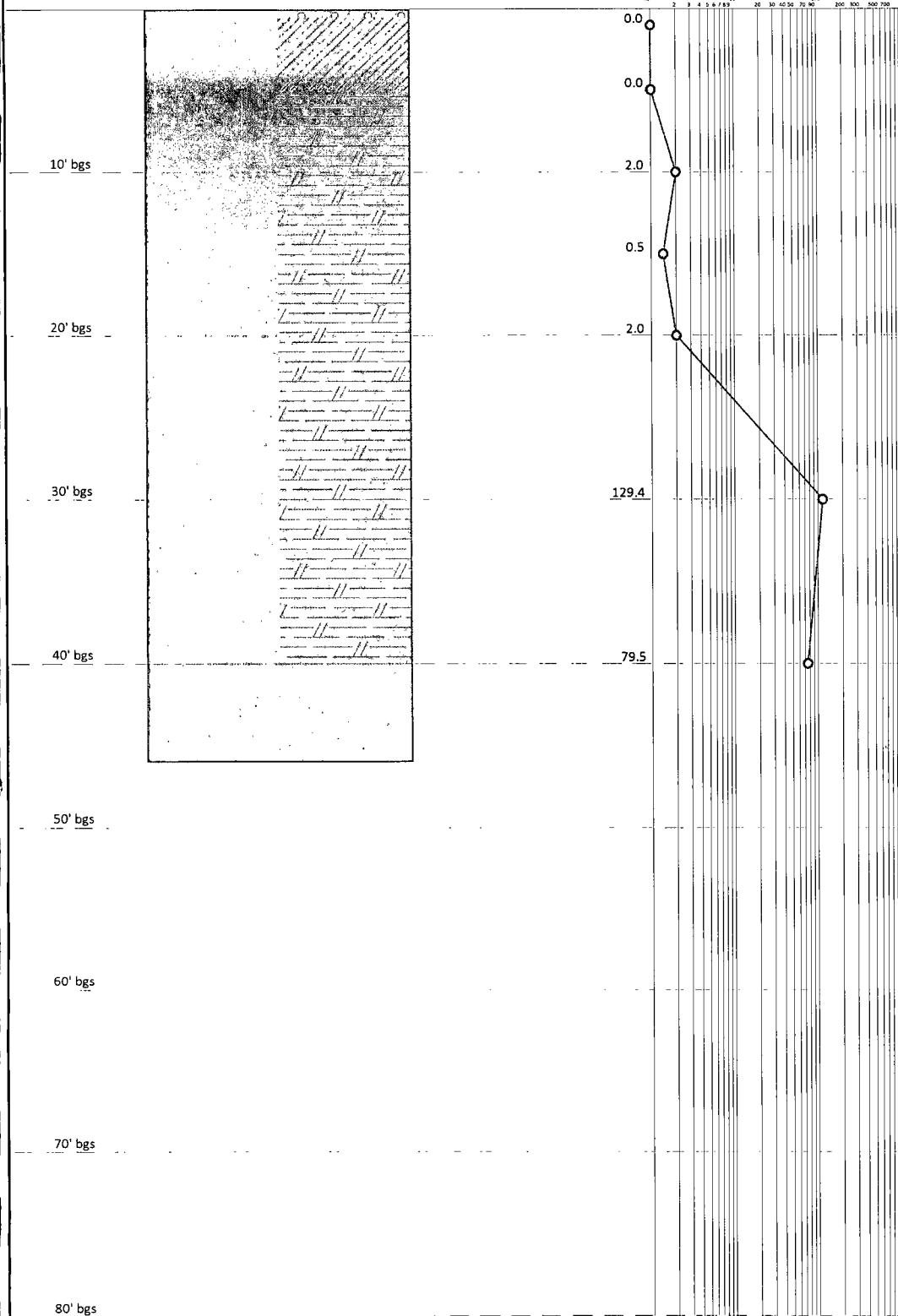
Drilled with Air Rotary by Scarborough

GW- Gravel

CL - Pink (7.5YR 7/3) very fine grained quartz sand,
 dry, weak. Grayish Brown to Light Olive Brown
 (2.5YR 5/2 to 2.5YR 5/3)

Gypsum - Gray to Pale Brown (10YR 6/1 to 6/2) thin
 to massive, hard to friable, interbedded with
 grayish brown (2.5YR 5/2) silty clay

Bluish Gray (GLE2 5/1) below 25', hydrocarbon
 odor, moist at 40'



Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

LAarson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 34.25"
 Longitude W 104° 15' 36.29"
 Elevation : 3549.9'

PID Response Log Plot
 (parts per million)

Lithologic Well Log

Drilling started 6/16/2009, completed 6/16/2009.

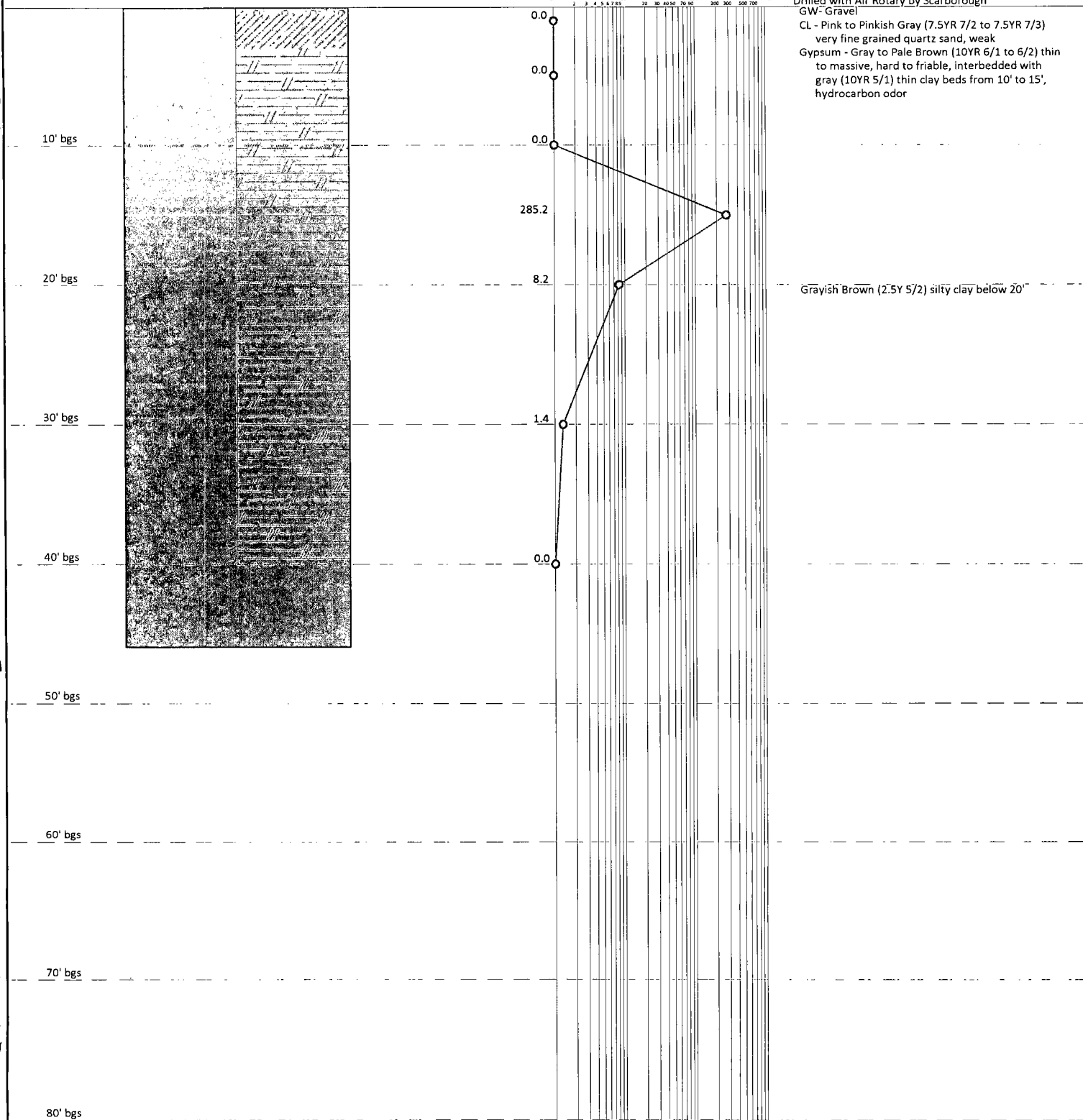
Drilled with Air Rotary by Scarborough

GW - Gravel

CL - Pink to Pinkish Gray (7.5YR 7/2 to 7.5YR 7/3)

very fine grained quartz sand, weak

Gypsum - Gray to Pale Brown (10YR 6/1 to 6/2) thin
 to massive, hard to friable, interbedded with
 gray (10YR 5/1) thin clay beds from 10' to 15',
 hydrocarbon odor



Grayish Brown (2.5Y 5/2) silty clay below 20'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 33.07"
 Longitude W 104° 15' 39.18"
 Elevation : 3546.0'

PID Response Log Plot
 (parts per million)

Lithologic Well Log

Drilling started 6/17/2009, completed 6/17/2009.

Drilled with Air Rotary by Scarborough

GW- Gravel

CL - Pink to Light Brown (7.5YR 7/3 to 7.5YR 6/3)
 very fine grained quartz sand, dry

Gypsum - Gray to Pale Brown (10YR 5/1 to 6/1) thin
 to massive, hard to friable, wet at 7',
 interbedded with yellowish brown (10YR 5/4)
 sandy clay at 9', dry below 10' with thin pinkish
 gray to reddish brown (5YR 7/2 to 4/4) beds of
 silty and sandy clay, wet below 30'

10' bgs

20' bgs

30' bgs

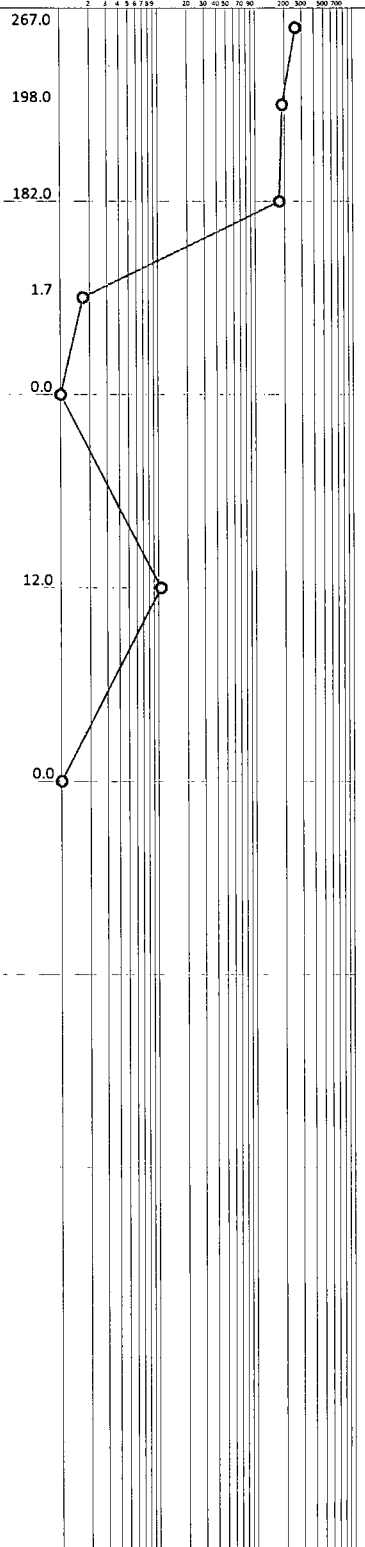
40' bgs

50' bgs

60' bgs

70' bgs

80' bgs



Grayish Brown (2.5Y 5/2) silty clay below 20'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

JWW

N 32° 46' 30.86"
W 104° 15' 39.78"
TOC 3544.44'
Ground 3541.80'

Locking Steel
Cover

Well Completion Log

2.64" Stickup
5" Borehole
4" Sch 40 PVC
Casing

2' - 12.5' Bentonite

12.5' Top of Sand
15.35' Top of Screen

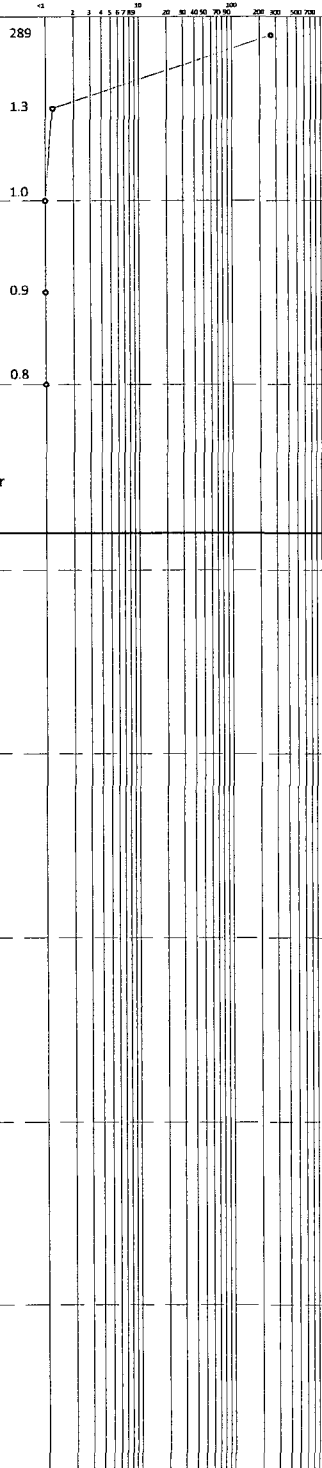
4" - 0.010 Slotted PVC Screen

Groundwater
28.80' bgs
7/24/08

10/20 Oglebay
Norton Silica Sand
Filter Pack

49.5' Bottom of Screen
Cap

PID Response Log Plot (parts per million)



Lithologic Well Log

Drilling started 7/24/2008, completed 7/28/2008.
Drilled with Air Rotary by Scarborough Drilling.
ML - Pale brown (10YR 8/3 to 8/4) soft, dry, silt
SC - Pinkish gray (7.5 YR 7/2) to Pale brown (10YR
6/3) very fine grained quartz sand with
abundant gypsum in thin stringers
Gypsum - Gray to Pale brown (10YR 6/1 to 6/2)
massive to thin bedded; units of thin bedded clay
below 25' (7.5 YR 4/2)

NOTE: Natural gas condensate (about 2-3 feet) in
boring at 30', air drilling suspended

Inter-bedded with thin units of sand and sandy
clay below 30'

Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson &
Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

www.ose.state.nm.us

1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER) MW10				OSE FILE NUMBER(S)									
	WELL OWNER NAME(S) Frontier Field Services, LLC.				PHONE (OPTIONAL)									
	WELL OWNER MAILING ADDRESS PO Box 7				CITY Loco Hills		STATE N.M.		ZIP 88255					
	WELL LOCATION (FROM GPS)		DEGREES LATITUDE 32		MINUTES 46		SECONDS 30.86 N		* ACCURACY REQUIRED: ONE TENTH OF A SECOND					
2. OPTIONAL	WELL LOCATION (FROM GPS)		DEGREES LONGITUDE 104		MINUTES 15		SECONDS 39.78 W		* DATUM REQUIRED: WGS 84					
	DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS Empire ABO Gas Plant Artesia, New Mexico													
	(2.5 ACRE) 1/4		(10 ACRE) 1/4		(40 ACRE) 1/4		(160 ACRE) 1/4		SECTION 3					
	SUBDIVISION NAME Empire ABO Gas Plant				LOT NUMBER		BLOCK NUMBER		UNIT/TRACT					
3. DRILLING INFORMATION	LICENSE NUMBER WD1188		NAME OF LICENSED DRILLER Lane Scarborough				NAME OF WELL DRILLING COMPANY John Scarborough Drilling, Inc.							
	DRILLING STARTED 07/24/2008		DRILLING ENDED 07/28/2008		DEPTH OF COMPLETED WELL (FT) 50		BORE HOLE DEPTH (FT)		DEPTH WATER FIRST ENCOUNTERED (FT) 28.80					
	COMPLETED WELL IS: <input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)						STATIC WATER LEVEL IN COMPLETED WELL (FT)							
	DRILLING FLUID: <input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:													
4. WATER BEARING STRATA	DRILLING METHOD: <input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:													
	DEPTH (FT)		BORE HOLE DIA. (IN)		CASING MATERIAL		CONNECTION TYPE (CASING)		INSIDE DIA. CASING (IN)		CASING WALL THICKNESS (IN)		SLOT SIZE (IN)	
	FROM +2		TO 15		5		sch 40 pvc		casing		4			
	15		50		5				screen		4		0.010	
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)		FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)						YIELD (GPM)			
	FROM 		TO 											
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA										TOTAL ESTIMATED WELL YIELD (GPM)				

FOR OSE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

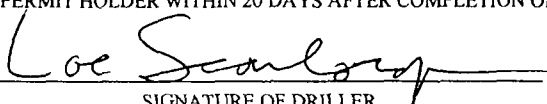
FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 1 OF 2	

MWD

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
		2-11.5	50				
		5		cement		poured	
		5		bentonite		poured	
		5		10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?	
	FROM	TO				
	0	25	25	ML- Pale brown, soft, dry	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO	
				SC- Pinkish gray to pale brown, vfg quartz sand with abundant	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO	
				gypsum in thin stringers	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Gypsum- Gray to pale brown, massive to thin bedded. Clay	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO	
				units of thin bedded clay below 25'	<input type="checkbox"/> YES <input type="checkbox"/> NO	
	25	50	25	Clay - Units of thin bedded clay below 25'	<input type="checkbox"/> YES <input checked="" type="checkbox"/> NO	
				Note: Natural gas condensate (about 2'-3') in boring at	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				30', air drilling suspended, water drilled to total depth	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Water about 28.8"	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Inter-bedded with thin units of sand and sandy clay below 30'	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL					

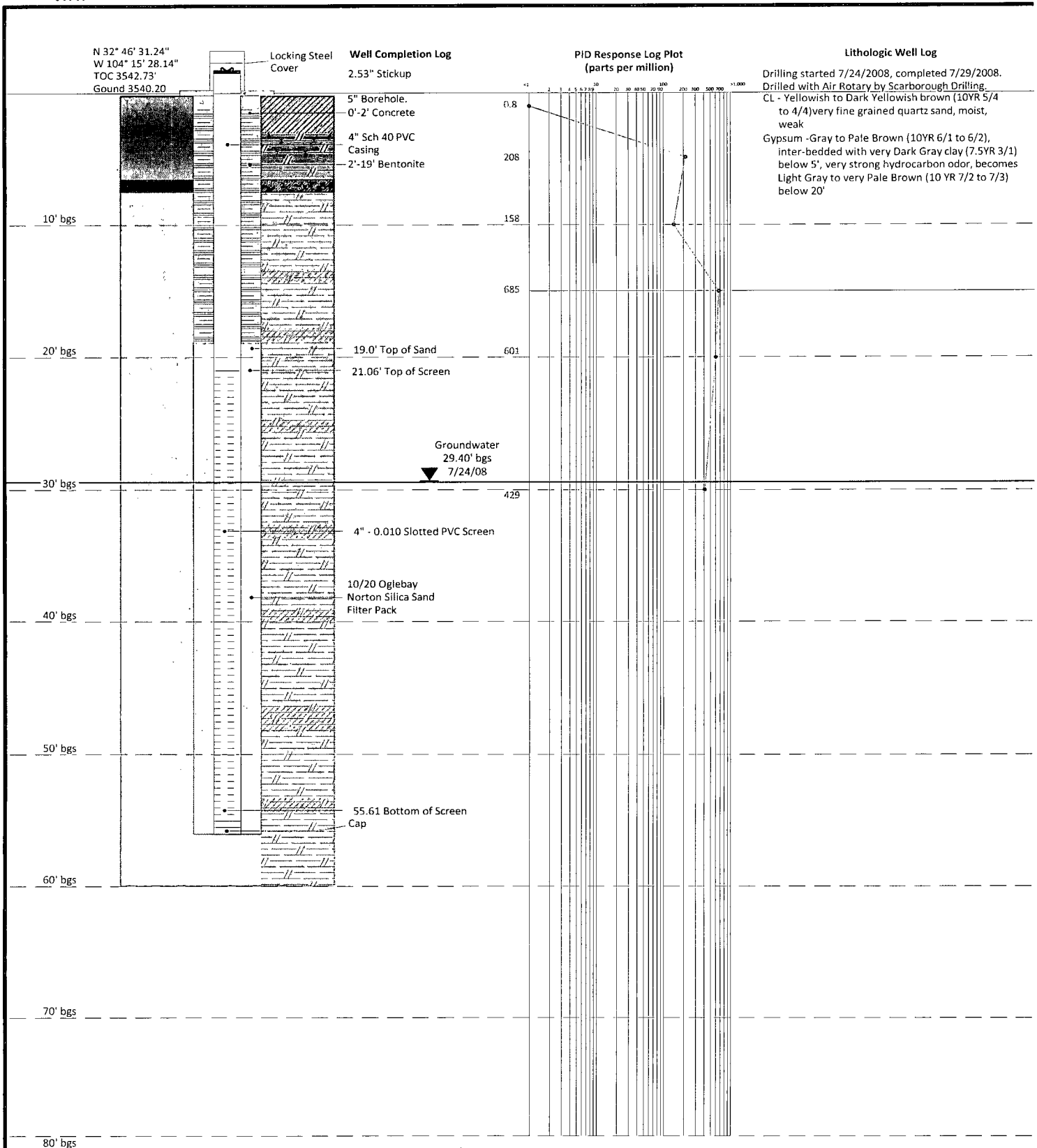
7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.
	ADDITIONAL STATEMENTS OR EXPLANATIONS:	

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
	 SIGNATURE OF DRILLER	1-20-09 DATE

FOR USE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION		PAGE 2 OF 2



MW-11 Boring & Completion Log

Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson & Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

www.ose.state.nm.us

1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER)				OSE FILE NUMBER(S)			
	MW11							
	WELL OWNER NAME(S)				PHONE (OPTIONAL)			
	Frontier Field Services, LLC.							
	WELL OWNER MAILING ADDRESS				CITY STATE ZIP			
PO Box 7				Loco Hills N.M. 88255				
WELL LOCATION (FROM GPS)	DEGREES		MINUTES		SECONDS		* ACCURACY REQUIRED: ONE TENTH OF A SECOND * DATUM REQUIRED: WGS 84	
	LATITUDE		32 46 31.24 N					
	LONGITUDE		104 15 28.14 W					
DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS								
Empire ABO Gas Plant Artesia, New Mexico								
2. OPTIONAL	(2.5 ACRE)	(10 ACRE)	(40 ACRE)	(160 ACRE)	SECTION	TOWNSHIP	RANGE	
	1/4	1/4	1/4	1/4	3	18	27	
	SUBDIVISION NAME				LOT NUMBER	BLOCK NUMBER	UNIT/TRACT	
	Empire ABO Gas Plant							
HYDROGRAPHIC SURVEY					MAP NUMBER	TRACT NUMBER		
3. DRILLING INFORMATION	LICENSE NUMBER		NAME OF LICENSED DRILLER			NAME OF WELL DRILLING COMPANY		
	WD1188		Lane Scarborough			John Scarborough Drilling, Inc.		
	DRILLING STARTED		DRILLING ENDED		DEPTH OF COMPLETED WELL (FT)	BORE HOLE DEPTH (FT)	DEPTH WATER FIRST ENCOUNTERED (FT)	
	07/24/2008		07/29/2008		55		29.40	
	COMPLETED WELL IS: <input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)					STATIC WATER LEVEL IN COMPLETED WELL (FT)		
	DRILLING FLUID: <input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:							
	DRILLING METHOD: <input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:							
	DEPTH (FT)		BORE HOLE DIA. (IN)	CASING MATERIAL	CONNECTION TYPE (CASING)	INSIDE DIA. CASING (IN)	CASING WALL THICKNESS (IN)	SLOT SIZE (IN)
	FROM	TO						
	+2	20	5	sch 40 pvc	casing	4		
20	55	5		screen	4		0.010	
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)	FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)			YIELD (GPM)	
	FROM	TO						
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA						TOTAL ESTIMATED WELL YIELD (GPM)		

FOR OSE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

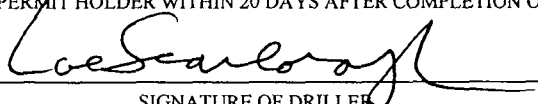
FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 1 OF 2	

mw 11

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
	2	19	5	bentonite		poured	
	19	55	5	10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?		
	FROM	TO			<input type="checkbox"/> YES	<input type="checkbox"/> NO	
		0	55	55	CL - Yellowish to dark yellowish brown, vfg quartz sand, silt	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					clay, moist weak	<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
					Gypsum- Gray to pale brown, interbedded with very dark	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					gray clay below 5', very strong hydrocarbon odor, becomes	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					light gray to very pale brown below 20'	<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
						<input type="checkbox"/> YES	<input type="checkbox"/> NO
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL						

7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:	
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.	
	ADDITIONAL STATEMENTS OR EXPLANATIONS:		

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
	 SIGNATURE OF DRILLER	01/20/2009 DATE

N 32° 46' 24.69"
W 104° 15' 28.14"
TOC 3525.25'
Ground 3522.60'

Locking Steel
Cover

Well Completion Log
2.65" Stickup

PID Response Log Plot
(parts per million)

Lithologic Well Log

Drilling started 7/25/2008, completed 7/29/2008.
Drilled with Air Rotary by Scarborough Drilling.

ML - Very Pale brown (10YR 8/3 to 7/3), very fine
grained quartz, silt, soft, moist

Gypsum - Light Grayish Brown to Dark Gray (10YR
6/2 to 4/1) thin bedded to massive, inter-bedded
with thin beds of gray clay about 6" to 1' thick,
light Yellowish Gray to light Yellowish Brown clay
(2.5Y 6/2 to 6/4) below 25', Red (2.5 YR 4/6) at
30'

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

5" Borehole.
0'-2' Concrete

4" Sch 40 PVC
Casing

2' - 34.00' Bentonite

34.0' Top of Sand

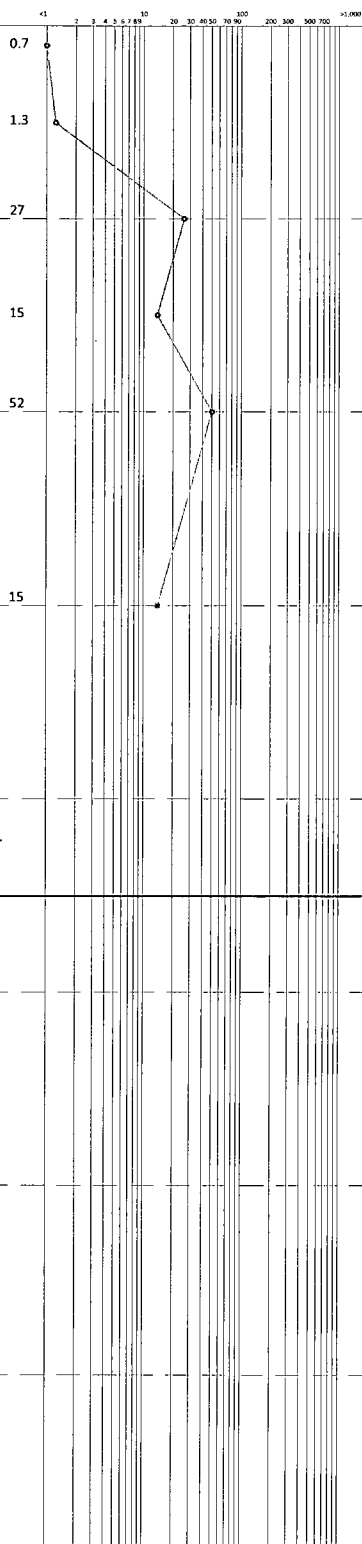
36.17' Top of Screen

Groundwater
44.90' bgs
7/24/08

10/20 Oglebay
Norton Silica Sand
Filter Pack

4" - 0.010 Slotted PVC Screen

70.72 Bottom of Screen
Cap



Clay content increases below 40'

Mudstone, Red (2.5 YR 4/6), very fine grained
quartz sand, inter-bedded with thin gypsum
beds, soft

Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson &
Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

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1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER) MW12				OSE FILE NUMBER(S)						
	WELL OWNER NAME(S) Frontier Field Services, LLC.				PHONE (OPTIONAL)						
	WELL OWNER MAILING ADDRESS PO Box 7				CITY Loco Hills		STATE N.M.		ZIP 88255		
	WELL LOCATION (FROM GPS)	DEGREES LATITUDE 32		MINUTES 46		SECONDS 24.69 N		* ACCURACY REQUIRED: ONE TENTH OF A SECOND * DATUM REQUIRED: WGS 84			
		LONGITUDE 104		15		28.14 W					
DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS Empire ABO Gas Plant Artesia, New Mexico											
2. OPTIONAL	(2.5 ACRE) 1/4	(10 ACRE) 1/4	(40 ACRE) 1/4	(160 ACRE) 1/4	SECTION 3	TOWNSHIP 18 <input type="checkbox"/> NORTH <input checked="" type="checkbox"/> SOUTH	RANGE 27 <input checked="" type="checkbox"/> EAST <input type="checkbox"/> WEST				
	SUBDIVISION NAME Empire ABO Gas Plant				LOT NUMBER	BLOCK NUMBER	UNIT/TRACT				
	HYDROGRAPHIC SURVEY					MAP NUMBER	TRACT NUMBER				
3. DRILLING INFORMATION	LICENSE NUMBER WD1188		NAME OF LICENSED DRILLER Lane Scarborough				NAME OF WELL DRILLING COMPANY John Scarborough Drilling, Inc.				
	DRILLING STARTED 07/24/2008		DRILLING ENDED 07/29/2008		DEPTH OF COMPLETED WELL (FT) 85		BORE HOLE DEPTH (FT)		DEPTH WATER FIRST ENCOUNTERED (FT) 44.90		
	COMPLETED WELL IS: <input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)						STATIC WATER LEVEL IN COMPLETED WELL (FT)				
	DRILLING FLUID: <input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:										
	DRILLING METHOD: <input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:										
	DEPTH (FT)		BORE HOLE DIA. (IN)	CASING MATERIAL	CONNECTION TYPE (CASING)	INSIDE DIA. CASING (IN)	CASING WALL THICKNESS (IN)	SLOT SIZE (IN)			
	FROM	TO									
	+2		36	5	sch 40 pvc	casing	4				
	36		85	5		screen	4			0.010	
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)	FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)					YIELD (GPM)		
	FROM	TO									
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA							TOTAL ESTIMATED WELL YIELD (GPM)				

FOR OSE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

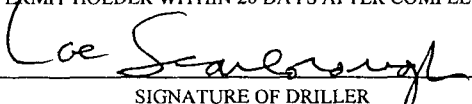
FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 1 OF 2	

mw 18

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
	2	19	5	bentonite		poured	
	19	85	5	10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?	
	FROM	TO				
	0	85	85	ML - Pale brown, very pale brown, vfg quartz, soft, moist	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
				Gypsum- Light grayish brown, to dark gray thin	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				bedded to massive, interbedded with thin beds of gray	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				clay about 6" to 1' thick, light yellowish gray to light yellowish	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				gray to light yellowish brown clay at 30'	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL					

7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:	
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.	
	ADDITIONAL STATEMENTS OR EXPLANATIONS:		

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
	 SIGNATURE OF DRILLER	01/20/2009 DATE

FOR USE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION		PAGE 2 OF 2

JWW

N 32° 46' 36.94"
W 104° 15' 31.00"
TOC 3561.40'
Ground 3558.50'

Locking Steel
Cover

Well Completion Log
2.90" Stickup

PID Response Log Plot
(parts per million)

Lithologic Well Log

Drilling started 7/25/2008, completed 7/29/2008.
Drilled with Air Rotary by Scarborough Drilling,
asphalt

ML - Yellowish Red (5YR 5/6), silt, very fine grained
quartz sand, silt, soft, moist

SC - Brownish yellow to dark yellowish brown
(10YR 6/6 to 4/6), very fine grained quartz sand,
abundant gypsum, moist

Gypsum - Light Gray to Light Brownish Gray (10YR
7/2 to 6/2) thin bedded to massive, inter-bedded
with units of silty clay, Yellowish Red (5YR 5/6)
very fine grained quartz sand, approximately
1.0' to 2.0' thick

Less clay below 20'

Gypsum - Interbedded with thin Sandstone units,
approximately 1.0' thick below 30.0', Pinkish White
(5YR 8/2) very fine grained quartz sand, poorly
sorted, weakly cemented

Groundwater
59.65' bgs
7/24/08

5" Borehole.
0'-2' Concrete4" Sch 40 PVC
Casing

2' - 48.06' Bentonite

48.06' Top of Sand

50.61' Top of Screen

4" - 0.010 Slotted PVC Screen

10/20 Oglebay
Norton Silica Sand
Filter Pack

85.16' Bottom of Screen
Cap

Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson &
Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

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1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER) MW13				OSE FILE NUMBER(S)				
	WELL OWNER NAME(S) Frontier Field Services, LLC.				PHONE (OPTIONAL)				
	WELL OWNER MAILING ADDRESS PO Box 7				CITY Loco Hills		STATE N.M.	ZIP 88255	
	WELL LOCATION (FROM GPS)		DEGREES LATITUDE 32	MINUTES 46	SECONDS 36.94 N	* ACCURACY REQUIRED: ONE TENTH OF A SECOND * DATUM REQUIRED: WGS 84			
		LONGITUDE 104		15		31.00 W			
DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS Empire ABO Gas Plant Artesia, New Mexico									
2. OPTIONAL	(2.5 ACRE) 1/4	(10 ACRE) 1/4	(40 ACRE) 1/4	(160 ACRE) 1/4	SECTION 3	TOWNSHIP 18 <input type="checkbox"/> NORTH <input checked="" type="checkbox"/> SOUTH	RANGE 27 <input checked="" type="checkbox"/> EAST <input type="checkbox"/> WEST		
	SUBDIVISION NAME Empire ABO Gas Plant				LOT NUMBER	BLOCK NUMBER	UNIT/TRACT		
	HYDROGRAPHIC SURVEY				MAP NUMBER		TRACT NUMBER		
3. DRILLING INFORMATION	LICENSE NUMBER WD1188		NAME OF LICENSED DRILLER Lane Scarborough			NAME OF WELL DRILLING COMPANY John Scarborough Drilling, Inc.			
	DRILLING STARTED 07/24/2008		DRILLING ENDED 07/29/2008		DEPTH OF COMPLETED WELL (FT) 85	BORE HOLE DEPTH (FT)	DEPTH WATER FIRST ENCOUNTERED (FT) 59.65		
	COMPLETED WELL IS: <input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)						STATIC WATER LEVEL IN COMPLETED WELL (FT)		
	DRILLING FLUID: <input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:								
	DRILLING METHOD: <input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:								
	DEPTH (FT)		BORE HOLE DIA. (IN)	CASING MATERIAL	CONNECTION TYPE (CASING)	INSIDE DIA. CASING (IN)	CASING WALL THICKNESS (IN)	SLOT SIZE (IN)	
	FROM	TO							
	+2		50	5	sch 40 pvc	casing	4		
	50		85	5		screen	4		0.010
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)	FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	YIELD (GPM)				
	FROM	TO							
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA						TOTAL ESTIMATED WELL YIELD (GPM)			

FOR OSE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

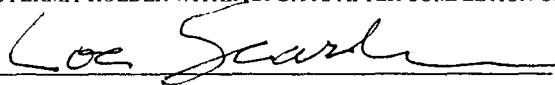
FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION		PAGE 1 OF 2

mw13

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
		2	10				
	10	85	5	10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?	
	FROM	TO				
	0	85	85	ML -Yellowish red silt, vfg quartz sand, soft, moist	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				SC - Brownish yellow to dark yellowish brown, vfg quartz sand,	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				abundant gypsum, moist	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Gypsum- Light brownish gray thin	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				bedded to massive, interbedded with units of silty clay.	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Yellowish red, vfg quartz sand	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Less clay below 20'	<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Gypsum - interbedded with thin sandstone. Pinkish white	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				vfg quartz sand poorly sorted	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL					

7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.
	ADDITIONAL STATEMENTS OR EXPLANATIONS:	

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
	 SIGNATURE OF DRILLER	01/20/2009 DATE

FOR USE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 2 OF 2	

JWW

N 32° 46' 23.48"
W 104° 15' 26.42"
TOC 3520.32'
Ground 3517.70'

Locking Steel
Cover

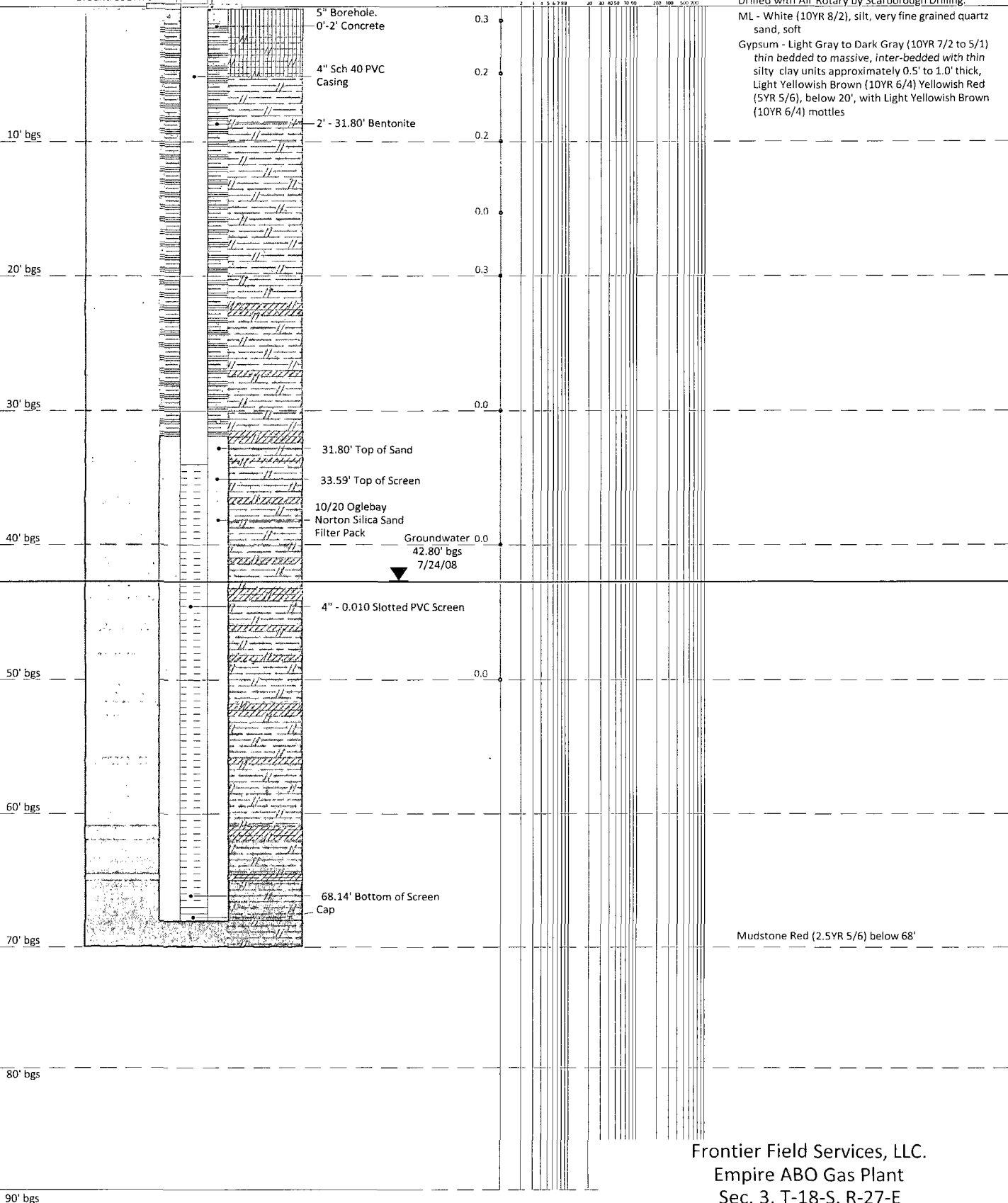
Well Completion Log
2.62" Stickup

PID Response Log Plot
(parts per million)

Lithologic Well Log

Drilling started 7/25/2008, completed 7/30/2008.
Drilled with Air Rotary by Scarborough Drilling.

ML - White (10YR 8/2), silt, very fine grained quartz sand, soft
Gypsum - Light Gray to Dark Gray (10YR 7/2 to 5/1) thin bedded to massive, inter-bedded with thin silty clay units approximately 0.5' to 1.0' thick, Light Yellowish Brown (10YR 6/4) Yellowish Red (5YR 5/6), below 20', with Light Yellowish Brown (10YR 6/4) mottles



Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson & Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

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1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER) MW14				OSE FILE NUMBER(S)			
	WELL OWNER NAME(S) Frontier Field Services, LLC.				PHONE (OPTIONAL)			
	WELL OWNER MAILING ADDRESS PO Box 7				CITY Loco Hills		STATE N.M.	ZIP 88255
	WELL LOCATION (FROM GPS)	DEGREES LATITUDE 32	MINUTES 46	SECONDS 23.48 N	* ACCURACY REQUIRED: ONE TENTH OF A SECOND * DATUM REQUIRED: WGS 84			
DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS Empire ABO Gas Plant Artesia, New Mexico								
2. OPTIONAL	(2.5 ACRE) 1/4	(10 ACRE) 1/4	(40 ACRE) 1/4	(160 ACRE) 1/4	SECTION 3	TOWNSHIP 18 <input type="checkbox"/> NORTH <input checked="" type="checkbox"/> SOUTH	RANGE 27 <input checked="" type="checkbox"/> EAST <input type="checkbox"/> WEST	
	SUBDIVISION NAME Empire ABO Gas Plant				LOT NUMBER	BLOCK NUMBER	UNIT/TRACT	
	HYDROGRAPHIC SURVEY				MAP NUMBER		TRACT NUMBER	
3. DRILLING INFORMATION	LICENSE NUMBER WD1188		NAME OF LICENSED DRILLER Lane Scarborough			NAME OF WELL DRILLING COMPANY John Scarborough Drilling, Inc.		
	DRILLING STARTED 07/25/2008		DRILLING ENDED 07/30/2008		DEPTH OF COMPLETED WELL (FT) 69.5	BORE HOLE DEPTH (FT)	DEPTH WATER FIRST ENCOUNTERED (FT) 59.65	
	COMPLETED WELL IS: <input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)					STATIC WATER LEVEL IN COMPLETED WELL (FT)		
	DRILLING FLUID: <input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:							
	DRILLING METHOD: <input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:							
	DEPTH (FT)		BORE HOLE DIA. (IN)	CASING MATERIAL	CONNECTION TYPE (CASING)	INSIDE DIA. CASING (IN)	CASING WALL THICKNESS (IN)	SLOT SIZE (IN)
	FROM	TO						
	+2		5	sch 40 pvc	casing	4		
	33.5		5		screen	4		0.010
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)	FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	YIELD (GPM)			
	FROM	TO						
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA					TOTAL ESTIMATED WELL YIELD (GPM)			

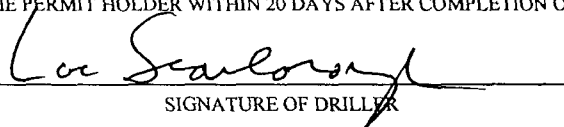
FOR OSE INTERNAL USE		WELL RECORD & LOG (Version 6/9/08)	
FILE NUMBER	POD NUMBER	TRN NUMBER	
LOCATION			PAGE 1 OF 2

mw14

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
	2	30	5	bentonite		poured	
	30	69.5	5	10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?	
	FROM	TO			<input type="checkbox"/> YES	<input type="checkbox"/> NO
	0	69.5	69.5	ML -White silt, vfg quartz sand, soft	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				Gypsum - Lt. gray to dark gray, thin bedded to massive, inter-	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				bedded with thin silty clay units. yellowish brown, yellowish	<input type="checkbox"/> YES	<input type="checkbox"/> NO
				red below 20' with light yellowish brown mottles	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
				Clay becomes red below 68'	<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
					<input type="checkbox"/> YES	<input type="checkbox"/> NO
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL					

7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.
	ADDITIONAL STATEMENTS OR EXPLANATIONS:	

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
	 SIGNATURE OF DRILLER	01/20/2009 DATE

FOR USE INTERNAL USE		WELL RECORD & LOG (Version 6/9/08)	
FILE NUMBER	POD NUMBER	TRN NUMBER	
LOCATION			PAGE 2 OF 2

JWW

N 32° 46' 41.84"
W 104° 15' 37.43"
TOC 3562.45'
Ground 3559.70'

Locking Steel
Cover

Well Completion Log
2.75" Stickup

PID Response Log Plot
(parts per million)

Lithologic Well Log

Drilling started 7/30/2008, completed 7/30/2008.
Drilled with Air Rotary by Scarborough Drilling.

ML - Yellowish Red (5YR 5/6 to 4/6), silty clay, very fine grained quartz sand, abundant gypsum stringers, dry, stiff, Grayish Brown to Dark Grayish Brown (2.5YR 5/2 to 4/6) below 15', inter-bedded with gypsum beds

Gypsum - White to Light Gray (10YR 8/1 to 7/1) inter-bedded with thin clay units of Reddish Yellow to Gray (5YR 6/4 to 5/1), inter-bedded with light Gray to Light Brownish Gray (2.5YR 7/2 to 6/2), silt and clay below 35'

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

90' bgs

5" Borehole.
0'-2' Concrete
4" Sch 40 PVC
Casing
2' - 39.5' Bentonite

39.5' Top of Sand
41.98' Top of Screen

10/20 Oglebay
Norton Silica Sand
Filter Pack

4" - 0.010 Slotted PVC Screen

Groundwater
62.5' bgs
7/30/08

76.53' Bottom of Screen
Cap

Inter-bedded with gray clay (10YR 5/1 to 6/1)
below 75', wet at 75'

Frontier Field Services, LLC.
Empire ABO Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

Larson & Associates, Inc.
Environmental Consultants



WELL RECORD & LOG

OFFICE OF THE STATE ENGINEER

www.ose.state.nm.us

1. GENERAL AND WELL LOCATION	POD NUMBER (WELL NUMBER)				OSE FILE NUMBER(S)				
	MW15								
	WELL OWNER NAME(S)				PHONE (OPTIONAL)				
	Frontier Field Services, LLC.								
	WELL OWNER MAILING ADDRESS				CITY STATE ZIP				
PO Box 7				Loco Hills N.M. 88255					
WELL LOCATION (FROM GPS)	DEGREES		MINUTES		SECONDS		* ACCURACY REQUIRED: ONE TENTH OF A SECOND * DATUM REQUIRED: WGS 84		
	LATITUDE		46		41.84 N				
LONGITUDE		104		15		37.43 W			
DESCRIPTION RELATING WELL LOCATION TO STREET ADDRESS AND COMMON LANDMARKS									
Empire ABO Gas Plant Artesia, New Mexico									
2. OPTIONAL	(2.5 ACRE)	(10 ACRE)	(40 ACRE)	(160 ACRE)	SECTION	TOWNSHIP	RANGE		
	1/4	1/4	1/4	1/4	3	18	27		
	SUBDIVISION NAME				LOT NUMBER	BLOCK NUMBER	UNIT/TRACT		
Empire ABO Gas Plant									
HYDROGRAPHIC SURVEY					MAP NUMBER	TRACT NUMBER			
3. DRILLING INFORMATION	LICENSE NUMBER		NAME OF LICENSED DRILLER			NAME OF WELL DRILLING COMPANY			
	WD1188		Lane Scarborough			John Scarborough Drilling, Inc.			
	DRILLING STARTED		DRILLING ENDED		DEPTH OF COMPLETED WELL (FT)		BORE HOLE DEPTH (FT)		
	07/30/2008		07/30/2008		80		35.00		
	COMPLETED WELL IS:					STATIC WATER LEVEL IN COMPLETED WELL (FT)			
	<input type="checkbox"/> ARTESIAN <input type="checkbox"/> DRY HOLE <input checked="" type="checkbox"/> SHALLOW (UNCONFINED)								
	DRILLING FLUID:								
	<input checked="" type="checkbox"/> AIR <input type="checkbox"/> MUD <input type="checkbox"/> ADDITIVES - SPECIFY:								
	DRILLING METHOD:								
	<input checked="" type="checkbox"/> ROTARY <input type="checkbox"/> HAMMER <input type="checkbox"/> CABLE TOOL <input type="checkbox"/> OTHER - SPECIFY:								
4. WATER BEARING STRATA	DEPTH (FT)		THICKNESS (FT)	FORMATION DESCRIPTION OF PRINCIPAL WATER-BEARING STRATA (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)				YIELD (GPM)	
	FROM	TO							
	+2	42	5	sch 40 pvc					
	42	80	5	screen				0.010	
METHOD USED TO ESTIMATE YIELD OF WATER-BEARING STRATA				TOTAL ESTIMATED WELL YIELD (GPM)					

FOR OSE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 1 OF 2	

MWIS

5. SEAL AND PUMP	TYPE OF PUMP: <input type="checkbox"/> SUBMERSIBLE <input type="checkbox"/> JET <input checked="" type="checkbox"/> NO PUMP - WELL NOT EQUIPPED <input type="checkbox"/> TURBINE <input type="checkbox"/> CYLINDER <input type="checkbox"/> OTHER - SPECIFY:						
	ANNULAR SEAL AND GRAVEL PACK	DEPTH (FT)		BORE HOLE DIA. (IN)	MATERIAL TYPE AND SIZE	AMOUNT (CUBIC FT)	METHOD OF PLACEMENT
		FROM	TO				
		0	2				
		2	42				
	42	80	5	10/20 silica sand		poured	

6. GEOLOGIC LOG OF WELL	DEPTH (FT)		THICKNESS (FT)	COLOR AND TYPE OF MATERIAL ENCOUNTERED (INCLUDE WATER-BEARING CAVITIES OR FRACTURE ZONES)	WATER BEARING?	
	FROM	TO				
	0	69.5	69.5	ML -Yellowish red, silty clay, vfg quartz sand, abundant	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Gypsum strings, dry, stiff, grayish brown to dark	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				grayish brown inter-bedded with gypsum beds	<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Gypsum - White to Light gray inter-bedded with thin clay	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				units of reddish yellow to gray, inter-bedded with light gray	<input type="checkbox"/> YES <input type="checkbox"/> NO	
				to light brownish gray silt, and clay below 35'	<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
				Inter-bedded with gray clay below 75'	<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
					<input type="checkbox"/> YES <input type="checkbox"/> NO	
	ATTACH ADDITIONAL PAGES AS NEEDED TO FULLY DESCRIBE THE GEOLOGIC LOG OF THE WELL.					

7. TEST & ADDITIONAL INFO	WELL TEST	METHOD: <input type="checkbox"/> BAILER <input type="checkbox"/> PUMP <input type="checkbox"/> AIR LIFT <input type="checkbox"/> OTHER - SPECIFY:
		TEST RESULTS - ATTACH A COPY OF DATA COLLECTED DURING WELL TESTING, INCLUDING START TIME, END TIME, AND A TABLE SHOWING DISCHARGE AND DRAWDOWN OVER THE TESTING PERIOD.
	ADDITIONAL STATEMENTS OR EXPLANATIONS:	

8. SIGNATURE	THE UNDERSIGNED HEREBY CERTIFIES THAT, TO THE BEST OF HIS OR HER KNOWLEDGE AND BELIEF, THE FOREGOING IS A TRUE AND CORRECT RECORD OF THE ABOVE DESCRIBED HOLE AND THAT HE OR SHE WILL FILE THIS WELL RECORD WITH THE STATE ENGINEER AND THE PERMIT HOLDER WITHIN 20 DAYS AFTER COMPLETION OF WELL DRILLING:	
		01/20/2009
	SIGNATURE OF DRILLER	DATE

FOR USE INTERNAL USE

WELL RECORD & LOG (Version 6/9/08)

FILE NUMBER	POD NUMBER	TRN NUMBER
LOCATION	PAGE 2 OF 2	

Latitude N 32° 46' 50.74"
 Longitude W 104° 15' 36.00"
 Elevation : 3582.60'
 TOC Elevation : 3585.46'

Well Completion Log

2.86' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/23/2009, completed 6/24/2009.

Drilled with Air Rotary by Scarborough.

ML - Light Yellowish Brown (10YR 6/4) silt, very fine grained quartz sand

CL - Very Pale Brown to Reddish Brown (10YR 7/3 to 2.5YR 5/4) silty sandy clay, very fine grained quartz sand, moderately firm, dry

Gypsum - Gray to White (10YR 6/1 to 8/1) thin to massive interbedded with units of fine grained quartz sand, and Reddish Brown (5YR 5/4) silty clay; massive to thin bedded gypsum below 30' Gray to White (10YR 6/1 to 8/1)

Interbedded with units of silt and silty clay below 45', very Pale Brown (10YR 8/3) to Gray (10YR 5/1 to 6/1) below 60'

Thin to massive gypsum below 70'

Gypsum Gray to White (10YR 6/1 to 8/1)

Interbedded with thin sand units below 95' Pale to Light Yellowish Brown (10YR 6/3 to 6/4) very fine grained quartz sand, wet, clayey from 105' to 110'

Mudstone- Red (2.5YR 4/6) silty very fine grained quartz sand at 112'
 Total depth at 115'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 41.70"
 Longitude W 104° 15' 29.16"
 Elevation : 3568.00'
 TOC Elevation : 3570.84'

Well Completion Log

2.84' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/23/2009, completed 6/23/2009.
 Drilled with Air Rotary by Scarborough

SP - Brown (10YR 4/4 to 5/4) silty clayey sand very fine grained quartz sand, slightly moist
 CL - Reddish Brown (5YR 5/4) silty clay, very fine grained quartz sand, interbedded with gypsum

Gypsum - Gray to White (10YR 6/1 to 8/1) thin to massive interbedded with thin units of Olive Yellow to Light Olive Brown (2.5YR 5/6 to 6/6) silty clay, massive to thin bedded gypsum from 20' to 40', interbedded with fine grained quartz sand and silty clay from 40' to 60' Pale Yellow to Reddish Brown (2.5YR 7/4 to 5YR 5/4)

Massive to thin bedded gypsum from 60'-80'

Interbedded with silty sand and silty clay below 85'
 Pale Brown (10YR 6/3) very fine grained quartz sand

Total depth at 98.02'

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

90' bgs

100' bgs

110' bgs

7.25" Borehole.
 0' - 2' Concrete
 4" Sch 40 PVC
 Casing

~ 2' - 62'
 Bentonite

61.70' Top of Sand
 63.54' Top of Screen

Groundwater
 ~75.77' bgs
 7/13/09

8/16 Oglebay Norton
 Silica Sand Filter Pack

4" - 0.020 Slotted PVC Screen

98.02 Bottom of Screen
 Cap

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson &
 Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 31.17"
 Longitude W 104° 15' 47.46"
 Elevation : 3529.70'
 TOC Elevation : 3532.63'

Well Completion Log

2.93' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/24/2009, completed 6/24/2009.
 Drilled with Air Rotary by Scarborough

ML - Pale Brown (10YR 8/3 to 8/4) silty soft. Light Brown (10YR 8/3) below 5', Reddish Yellow (10YR 8/3) minor clay below 10'

SP - Reddish Yellow (7.5YR 6/6) silty sand, very fine grained quartz sand, loose. Light Brownish Gray (10YR 6/2) medium grained quartz sand from 28' to 31' damp at 31'

Gypsum - Gray to White (10YR 6/1 to 8/1) thin to massive, interbedded with thin sandstone units very fine grained quartz sand, discolored sandstone units at 40', hydrocarbon odor, Gray to Very Dark Gray (10YR 5/1 to 3/1) moist below 40'

Shale - Red (2.5YR 4/6) silty very fine grained quartz sand

Total depth at 54'

7.25" Borehole. 124.00
 0' - 2' Concrete
 4" Sch 40 PVC Casing
 ~ 2' - 32' Bentonite 202.00
 10' bgs
 20' bgs 136.00
 30' bgs 112.00
 Groundwater ~34.40' bgs 7/13/09
 32' Top of Sand
 33.47' Top of Screen
 40' bgs 130.00
 8/16 Oglebay Norton Silica Sand Filter Pack
 50' bgs
 52.92' Bottom of Screen
 CAP
 60' bgs
 70' bgs
 80' bgs

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 28.40"
 Longitude W 104° 15' 40.98"
 Elevation : 3540.60'
 TOC Elevation : 3543.34'

Well Completion Log

2.74' Stickup

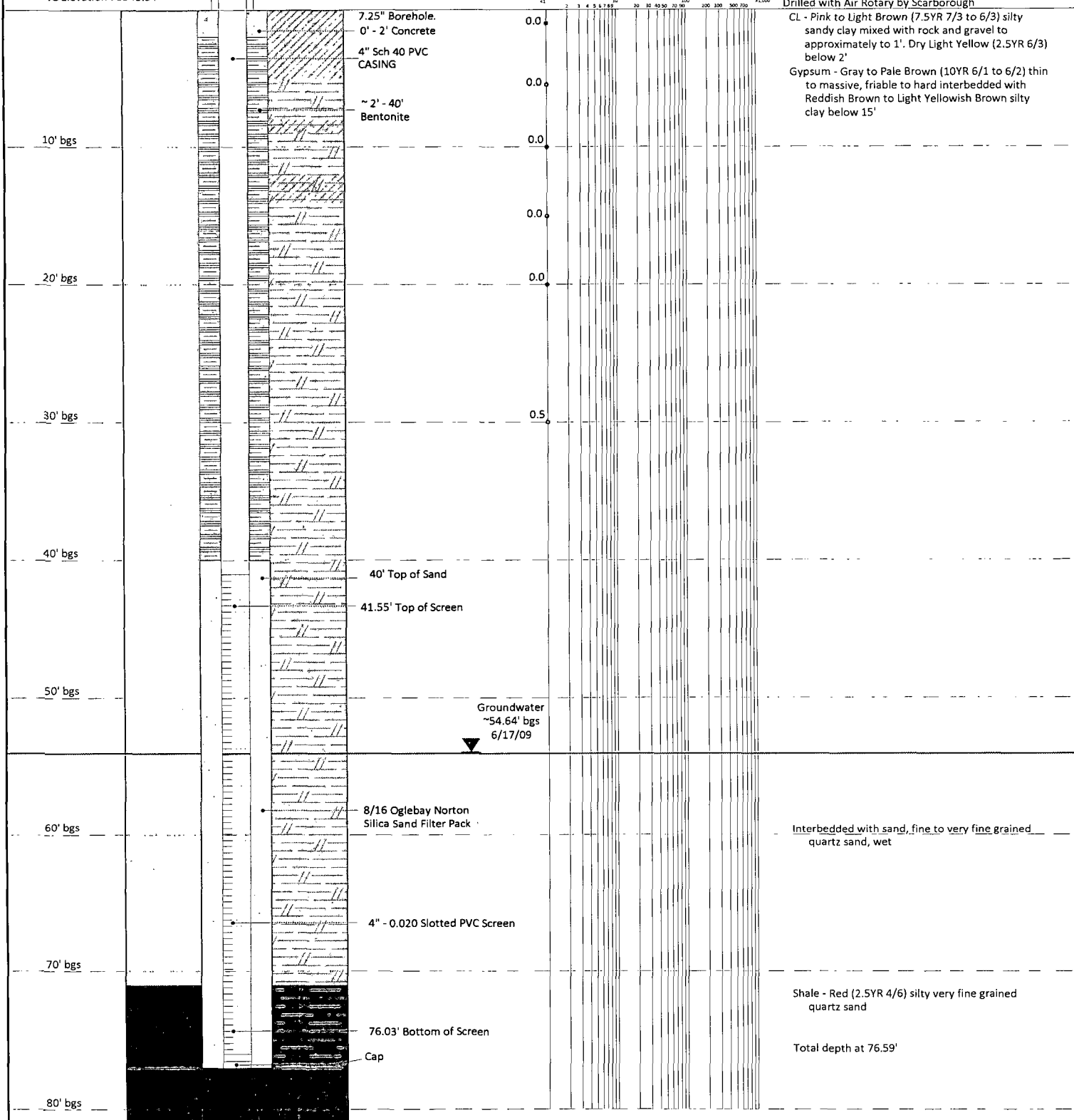
PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/16/2009, completed 6/17/2009.
 Drilled with Air Rotary by Scarborough

CL - Pink to Light Brown (7.5YR 7/3 to 6/3) silty sandy clay mixed with rock and gravel to approximately to 1'. Dry Light Yellow (2.5YR 6/3) below 2'
 Gypsum - Gray to Pale Brown (10YR 6/1 to 6/2) thin to massive, friable to hard interbedded with Reddish Brown to Light Yellowish Brown silty clay below 15'



Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson &
 Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 28.85"
 Longitude W 104° 15' 34.77"
 Elevation : 3538.70'
 TOC Elevation : 3541.47'

Well Completion Log

2.71' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/17/2009, completed 6/18/2009.
 Drilled with Air Rotary by Scarborough

CL - Light Brown (7.5YR 6/4) very fine grained
 quartz sand, dry, mixed with caliche and gravel
 from 0' to 2'

Gypsum - Gray to Very Pale Brown (10YR 7/2 to
 7/3) thin to massive beds friable to hard,
 interbedded with Reddish Brown (5YR 4/3 to
 4/4) clay and silty clay, very firm clay diminishes
 below 15'

Damp at 30'

Groundwater
 ~52.94' bgs
 7/14/09 4.0

7.25" Borehole.
 0' - 2' Concrete
 4" Sch 40 PVC
 Casing

~ 2' - 40'
 Bentonite

40' Top of Sand
 41.44' Top of Screen

8/16 Oglebay Norton
 Silica Sand Filter Pack

4" - 0.020 Slotted PVC Screen

75.97' Bottom of Screen
 Cap

Shale - Red (2.5YR 4/6) silty very fine grained
 quartz sand

Total depth at 77'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson &
 Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 30.46"
 Longitude W 104° 15' 34.03"
 Elevation : 3540.20'
 TOC Elevation : 3543.15'

Well Completion Log

2.95' Stickup

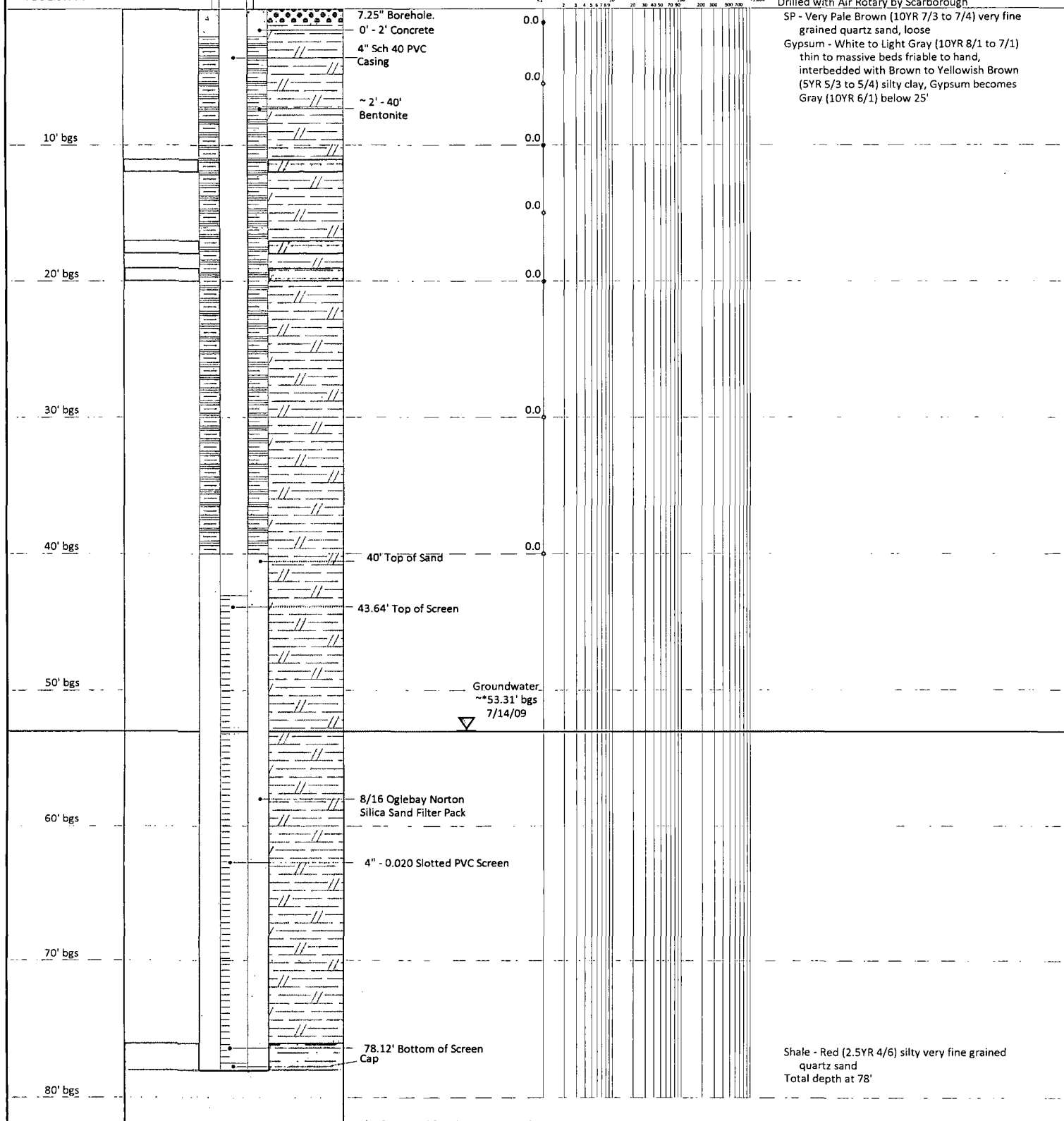
PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/18/2009, completed 6/18/2009.
 Drilled with Air Rotary by Scarborough

SP - Very Pale Brown (10YR 7/3 to 7/4) very fine grained quartz sand, loose
 Gypsum - White to Light Gray (10YR 8/1 to 7/1) thin to massive beds friable to hand, interbedded with Brown to Yellowish Brown (5YR 5/3 to 5/4) silty clay, Gypsum becomes Gray (10YR 6/1) below 25'



* - Corrected for Phase-Separated Hydrocarbons in Groundwater

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 32.04"
 Longitude W 104° 15' 32.29"
 Elevation : 3542.9'
 TOC Elevation : 3545.87'

Well Completion Log

2.97' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/18/2009, completed 6/19/2009.
 Drilled with Air Rotary by Scarborough

CL - Brown (7.5YR 4/4) silty sandy clay, very fine grained quartz sand, stiff at 11'

Gypsum - White to Gray (10YR 8/1 to 6/1) thin to massive, friable to hard interbedded with very dark gray (10YR 3/1) silty clay below 5' and reddish brown (2.5YR 4/4) below 10', wet at 22'

10' bgs

7.25" Borehole.
 0' - 2' Concrete
 4" Sch 40 PVC Casing

~ 2' - 11'
 Bentonite

11' Top of Sand

13.07' Top of Screen

Groundwater
 ~19.34' bgs
 7/13/09

20' bgs

8/16 Oglebay Norton
 Silica Sand Filter Pack

30' bgs

4" - 0.020 Slotted PVC Screen

37.52' Bottom of Screen
 Cap

40' bgs

Gypsum - White to Gray (10YR 8/1 to 6/1) thin to massive, friable to hard interbedded with very dark gray (10YR 3/1) silty clay below 5' and reddish brown (2.5YR 4/4) below 10', wet at 22'
 Total depth at 38'

50' bgs

60' bgs

70' bgs

80' bgs

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 31.27"
 Longitude W 104° 15' 28.78"
 Elevation : 3539.20'
 TOC Elevation : 3542.21'

Well Completion Log

3.01' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/19/2009, completed 6/19/2009.
 Drilled with Air Rotary by Scarborough

SM - Pink (7.5YR 7/3) very fine grained quartz sand, abundant rock shards from 0' to 2'

Gypsum - White to Gray (10YR 8/1 to 6/1) thin to massive friable, interbedded with Reddish Brown (2.5YR 4/4) silty clay, becomes Light Brown (7.5YR 6/4) below 20', lessens below 25'

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

90' bgs

7.25" Borehole.
 0' - 2' Concrete
 4" Sch 40 PVC Casing
 ~ 2' - 47' Bentonite

0.0

0.0

0.0

0.0

0.0

0.0

26.5

47' Top of Sand
 48.87' Top of Screen
 8/16 Oglebay Norton Silica Sand Filter Pack

Groundwater
 ~59.41' bgs
 7/13/09

4" - 0.020 Slotted PVC Screen

83.35' Bottom Of Screen
 CAP

Very hard between 42' and 44', interbedded with thin units of Brown (10YR 5/3) silty clay and sandstone below 45'

Total depth at 84'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson & Associates, Inc.
 Environmental Consultants

Latitude N 32° 46' 31.27"
 Longitude W 104° 15' 28.78"
 Elevation : 3539.20'
 TOC Elevation : 3542.21'

Well Completion Log

3.01' Stickup

PID Response Log Plot

(parts per million)

Lithologic Well Log

Drilling started 6/19/2009, completed 6/19/2009.
 Drilled with Air Rotary by Scarborough

SM - Pink (7.5YR 7/3) very fine grained quartz sand, abundant rock shards from 0' to 2'

Gypsum - White to Gray (10YR 8/1 to 6/1) thin to massive friable, interbedded with Reddish Brown (2.5YR 4/4) silty clay, becomes Light Brown (7.5YR 6/4) below 20', lessens below 25'

10' bgs

20' bgs

30' bgs

40' bgs

50' bgs

60' bgs

70' bgs

80' bgs

90' bgs

7.25" Borehole.
 0' - 2' Concrete
 4" Sch 40 PVC
 Casing

~ 2' - 47'
 Bentonite

0.0

0.0

0.0

0.0

0.0

0.0

26.5

Groundwater
 ~59.41' bgs
 7/13/09

47' Top of Sand
 48.87' Top of Screen

8/16 Oglebay Norton
 Silica Sand Filter Pack

4" - 0.020 Slotted PVC Screen

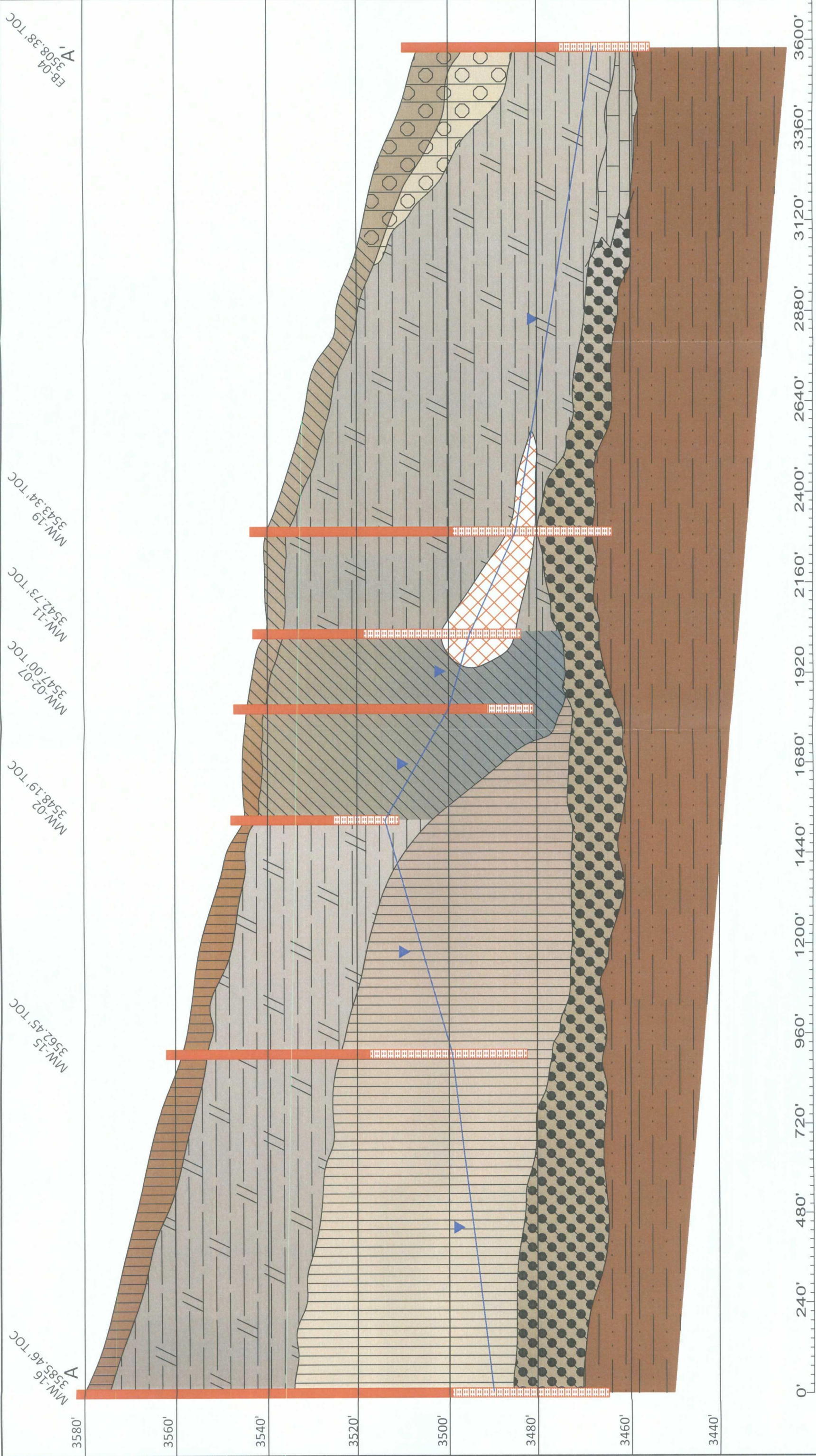
83.35' Bottom Of Screen
 CAP

Very hard between 42' and 44', interbedded with thin units of Brown (10YR 5/3) silty clay and sandstone below 45'

Total depth at 84'

Frontier Field Services, LLC.
 Empire ABO Gas Plant
 Sec. 3, T-18-S, R-27-E
 Eddy County, New Mexico

Larson &
 Associates, Inc.
 Environmental Consultants



Legend

- Silty Fine Sand
- Silty Sand
- Gypsum
- Shale
- Inorganic Silts and Fine Sand
- Clay
- PSH Emulsion
- Screened Interval
- Potentiometric Surface
- 1" = 150' Horizontal
- 1" = 20' Vertical
- 7.5 : 1 Vertical To Horizontal Exaggeration

Frontier Field Services
Empire - Abo Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

N 32° 46' 33.7"
W 104° 15' 37.2"

Larson & Associates, Inc.
Environmental Consultants

Figure - Northwest to Southeast Cross Section A to A'

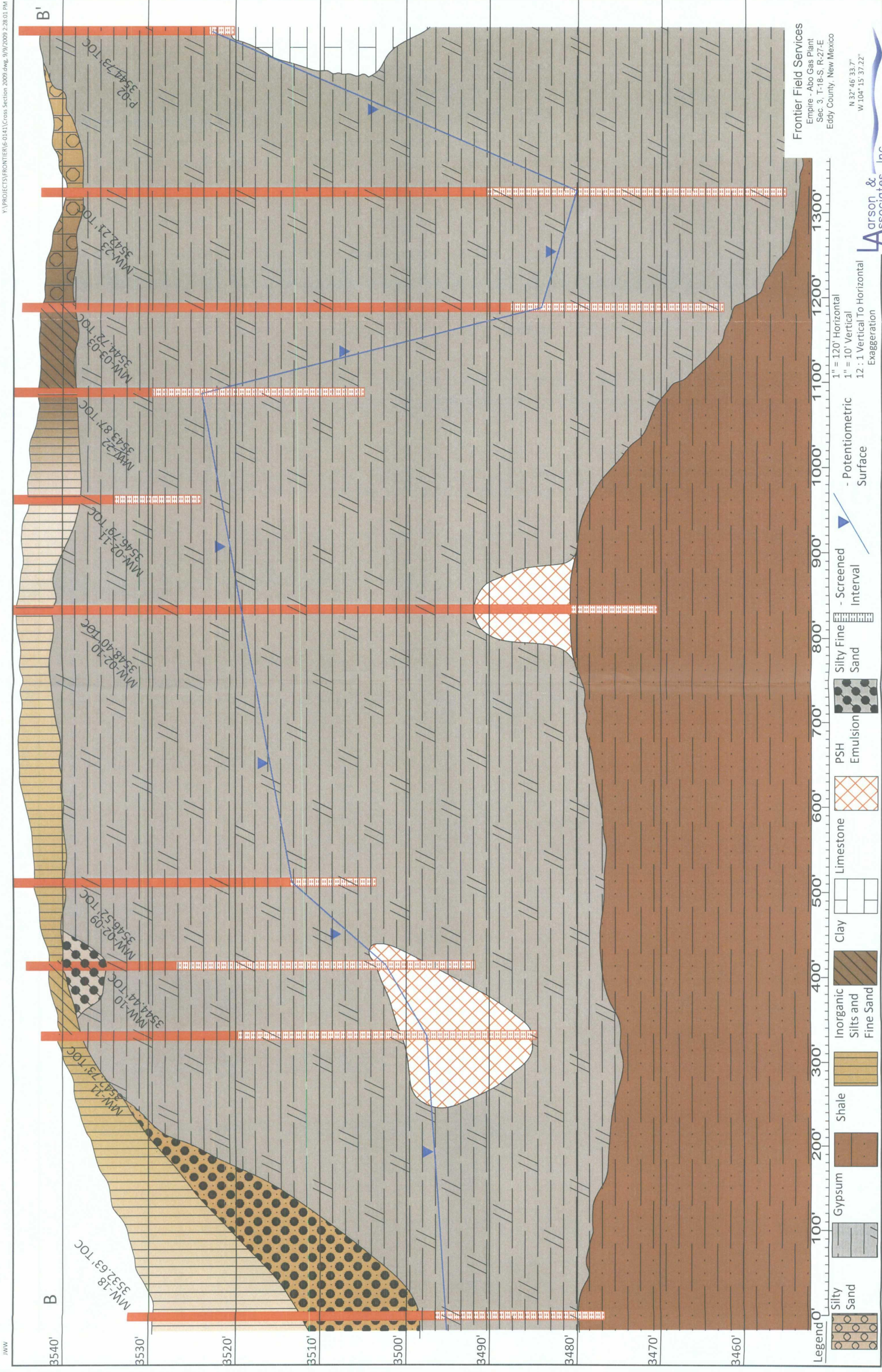
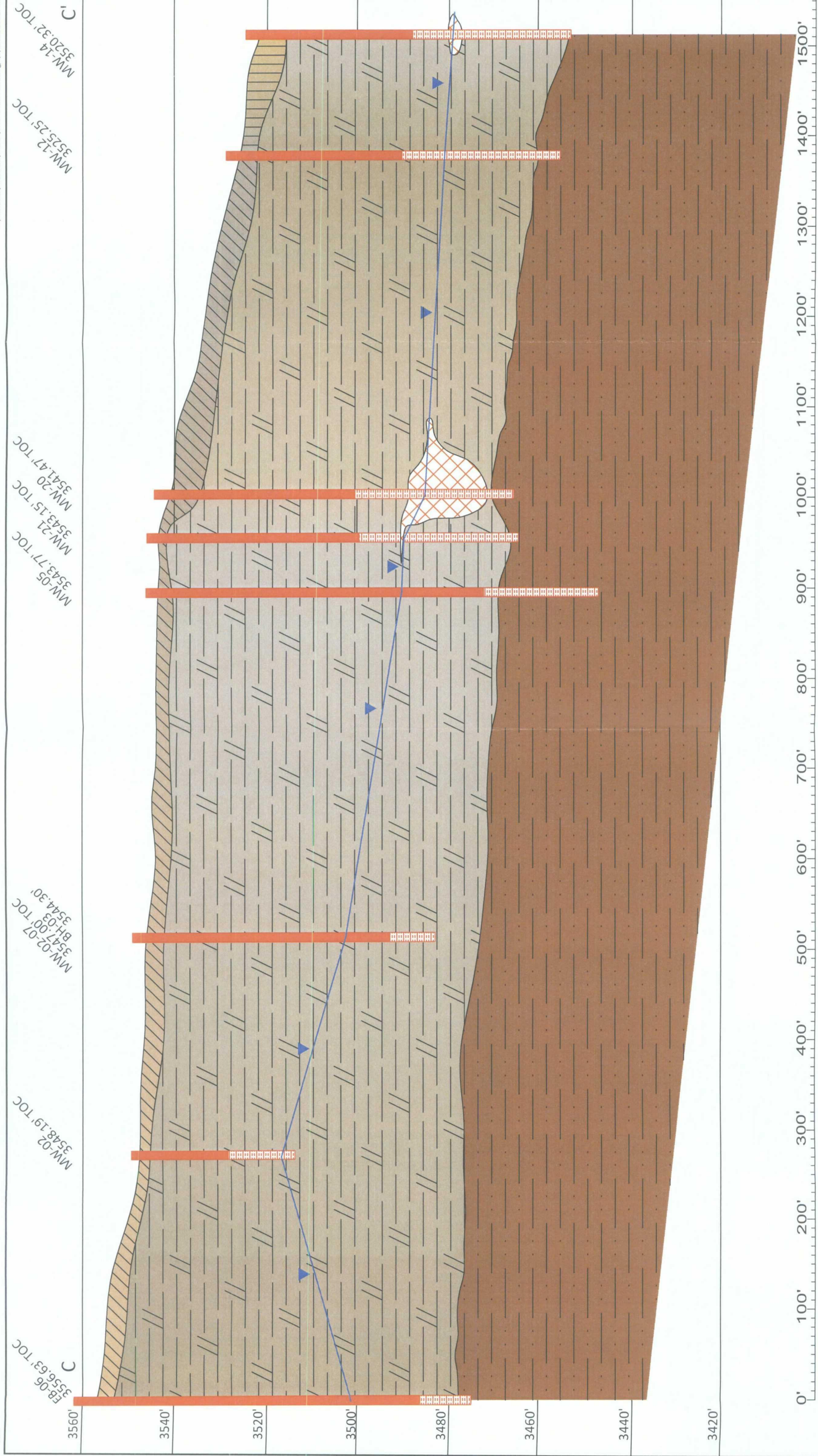
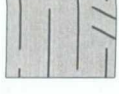


Figure - Northwest to Southeast Cross Section B to B'



Legend



Gypsum
Shale
Inorganic Silts and Fine Sand
Clay
PSH Emulsion

- Screened Interval
- Potentiometric Surface

1" = 150' Horizontal
1" = 20' Vertical
7.5 : 1 Vertical To Horizontal Exaggeration

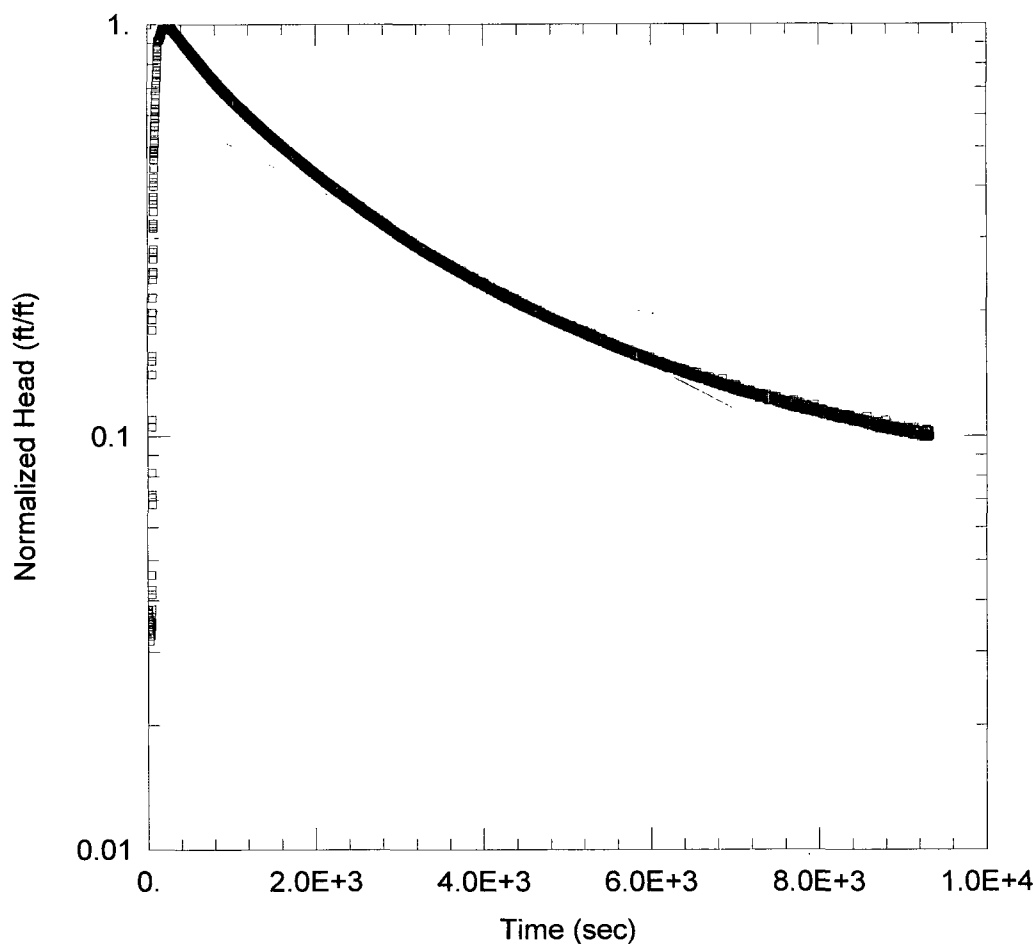
Frontier Field Services
Empire - Abo Gas Plant
Sec. 3, T-18-S, R-27-E
Eddy County, New Mexico

N 32° 46' 33.7"
W 104° 15' 37.2"

Larson & Associates, Inc.
Environmental Consultants

Figure - Northwest to Southeast Cross Section C to C'

Well ID	Falling Head Hydraulic Conductivity (ft/day)				Rising Head Hydraulic Conductivity (ft/day)			
	Test 1	Test 2	Test 3	Average	Test 1	Test 2	Test 3	Average
MW-15	0.06085	0.0593		0.0601				
MW-17	0.1593	0.155		0.1572				
EB-08	0.3992	0.3686	0.06535	0.2777	0.5876	0.2016	0.07751	0.2889
P-01	14.92	0.78	1.71	5.8033	19.24	0.575	0.2358	6.6836
P-05	0.3106	0.4365	0.4051	0.3841	0.3482	0.1414	0.1135	0.2010
Notes		Falling Head Average		1.3365	Rising Head Average			2.3912
Yellow Indicates Outlier		Cumulative Average						1.8796
Data		Biased Data Average (No P-01 Test 1 Data Used)						0.3574



MW-15 TEST 1 FALLING HEAD

Data Set: Z:\...MW-15 Test 1 Falling Head.aqt

Date: 08/11/09

Time: 16:50:04

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: MW-15 Test 1 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 18.8 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (MW-15 Test 1 Falling Head)

Initial Displacement: 6.15 ft

Static Water Column Height: 15.22 ft

Total Well Penetration Depth: 77. ft

Screen Length: 35. ft

Casing Radius: 0.166 ft

Well Radius: 0.35 ft

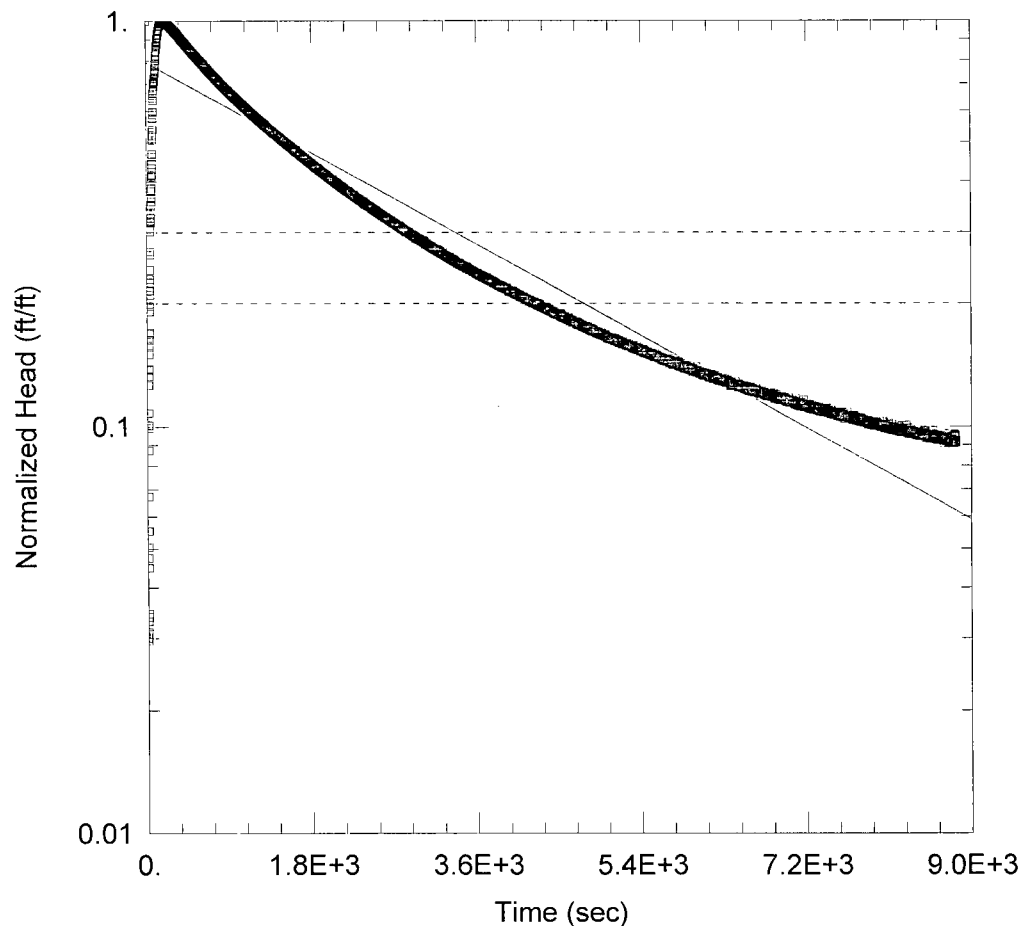
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.06085$ ft/day

$y_0 = 3.984$ ft



MW-15 TEST 2 FALLING HEAD

Data Set:

Date: 08/17/09

Time: 13:58:52

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: MW-15 Test 2 Falling Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 20. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (MW-15 Test 2 Falling Head)

Initial Displacement: 6.17 ft

Static Water Column Height: 15.31 ft

Total Well Penetration Depth: 35. ft

Screen Length: 35. ft

Casing Radius: 0.166 ft

Well Radius: 0.35 ft

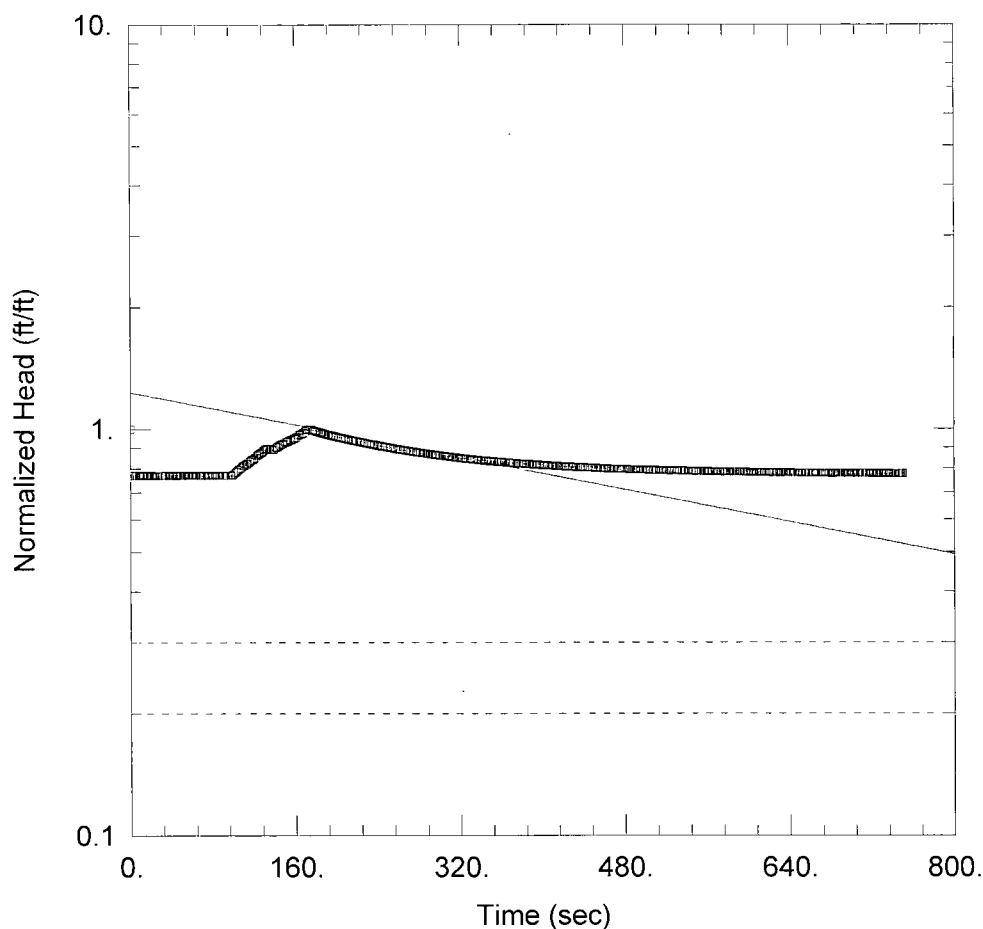
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0593$ ft/day

$y_0 = 4.887$ ft



MW-17 TEST 1 FALLING HEAD

Data Set: Z:\...MW-17 Test 1 Falling Head.aqt

Date: 08/18/09

Time: 09:24:48

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: MW-17 Test 1 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 30. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (MW-17 Test 1 Falling Head)

Initial Displacement: 24.75 ft

Static Water Column Height: 19.26 ft

Total Well Penetration Depth: 35. ft

Screen Length: 35. ft

Casing Radius: 0.166 ft

Well Radius: 0.35 ft

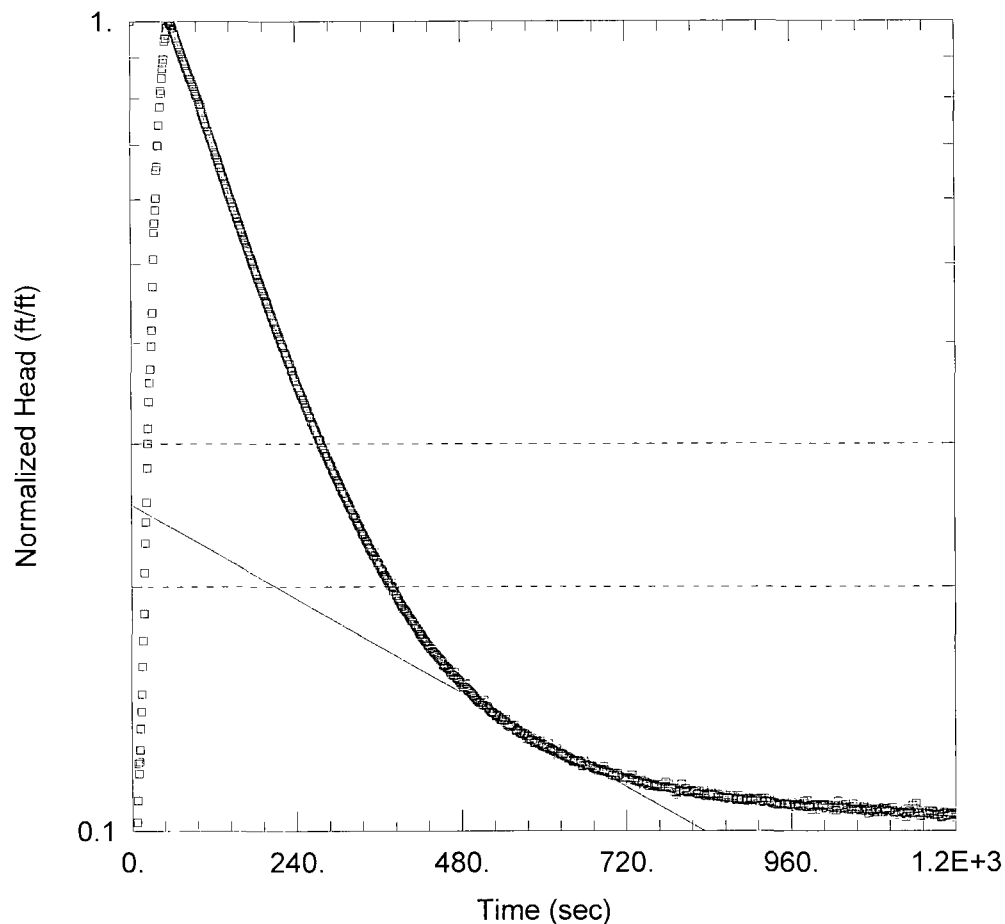
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.1593$ ft/day

$y_0 = 30.43$ ft



MW-17 TEST 2 FALLING HEAD

Data Set: Z:\...MW-17 Test 2 Falling Head.aqt

Date: 08/18/09

Time: 10:01:43

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: MW-17 Test 2 Falling Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 30. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (MW-17 Test 2 Falling Head)

Initial Displacement: 7.4 ft

Static Water Column Height: 19.35 ft

Total Well Penetration Depth: 35. ft

Screen Length: 35. ft

Casing Radius: 0.166 ft

Well Radius: 0.35 ft

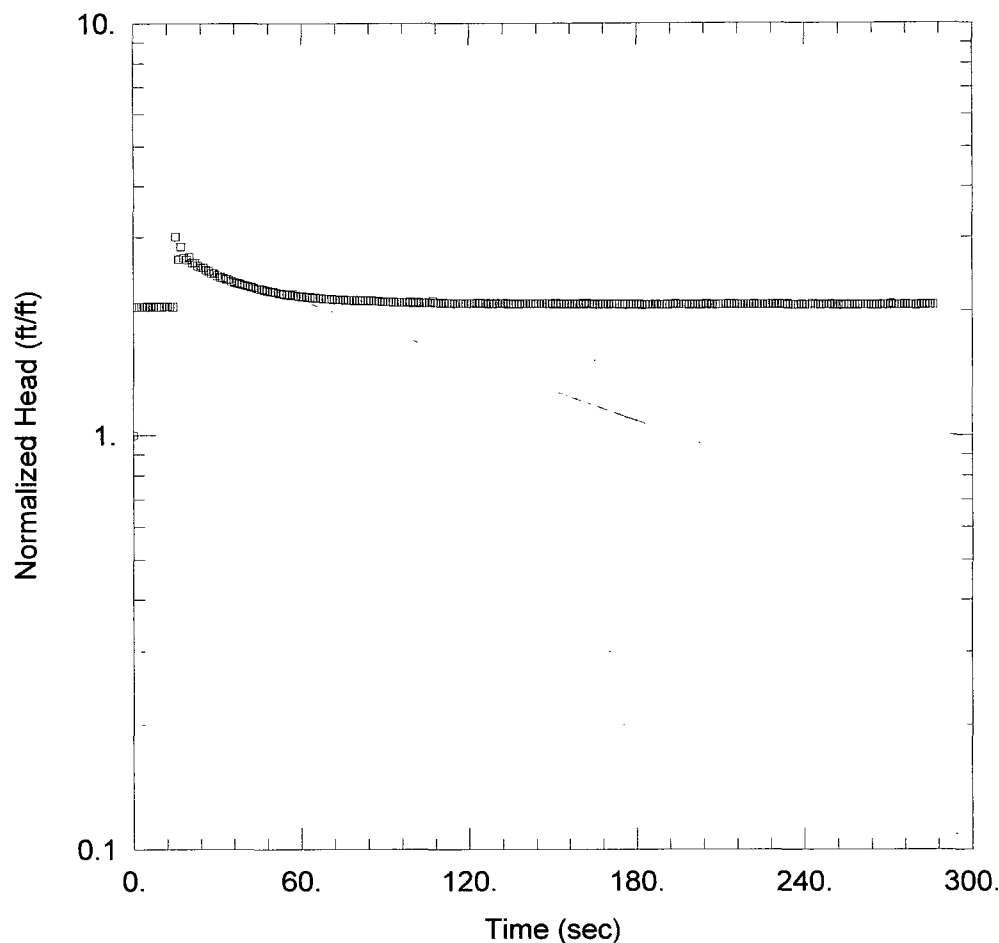
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.155$ ft/day

$y_0 = 1.866$ ft



EB-08 TEST 1 FALLING HEAD

Data Set: Z:\...\EB-08 Test 1 Falling Head.aqt

Date: 08/11/09

Time: 11:43:12

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.61 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 1 Falling Head)

Initial Displacement: 1.3 ft

Static Water Column Height: 22.65 ft

Total Well Penetration Depth: 23. ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.21 ft

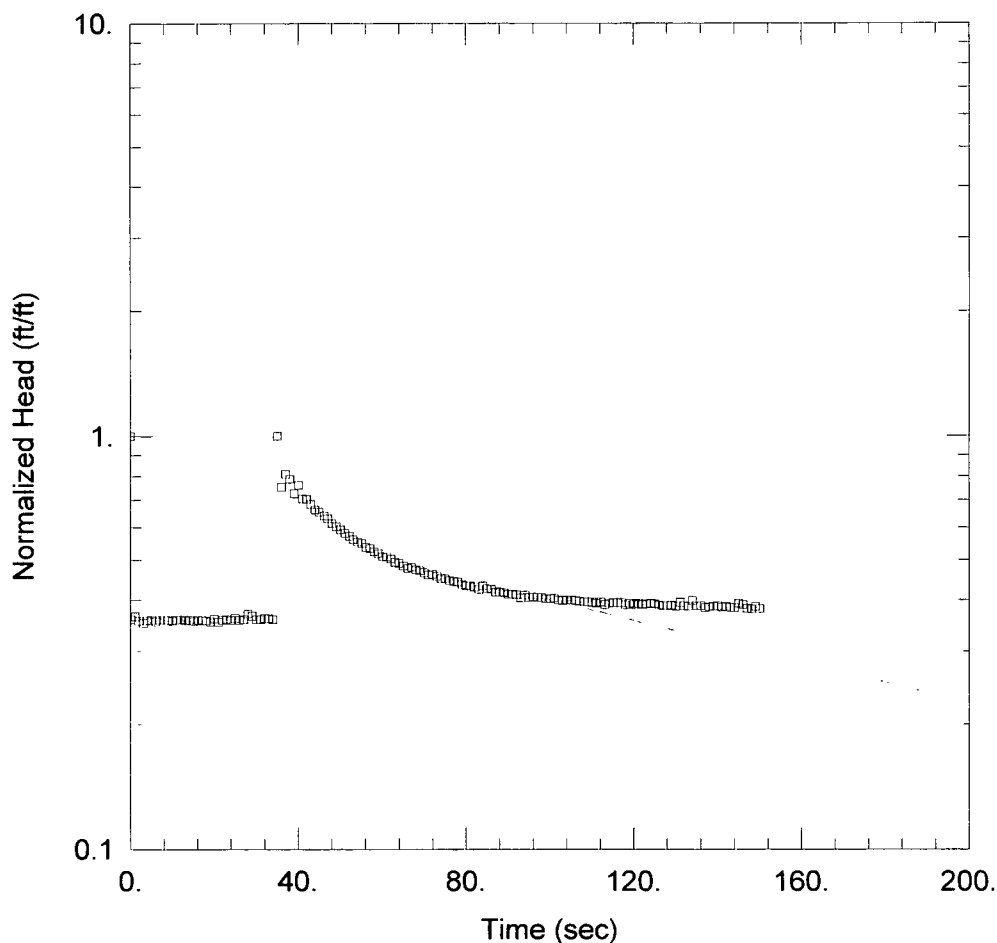
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.3992$ ft/day

$y_0 = 3.847$ ft



EB-08 TEST 2 FALLING HEAD

Data Set: Z:\...\EB-08 Test 2 Falling Head.aqt

Date: 08/11/09

Time: 14:43:41

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08 Test 2 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.84 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 2 Falling Head)

Initial Displacement: 1.835 ft

Static Water Column Height: 22.66 ft

Total Well Penetration Depth: 23. ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

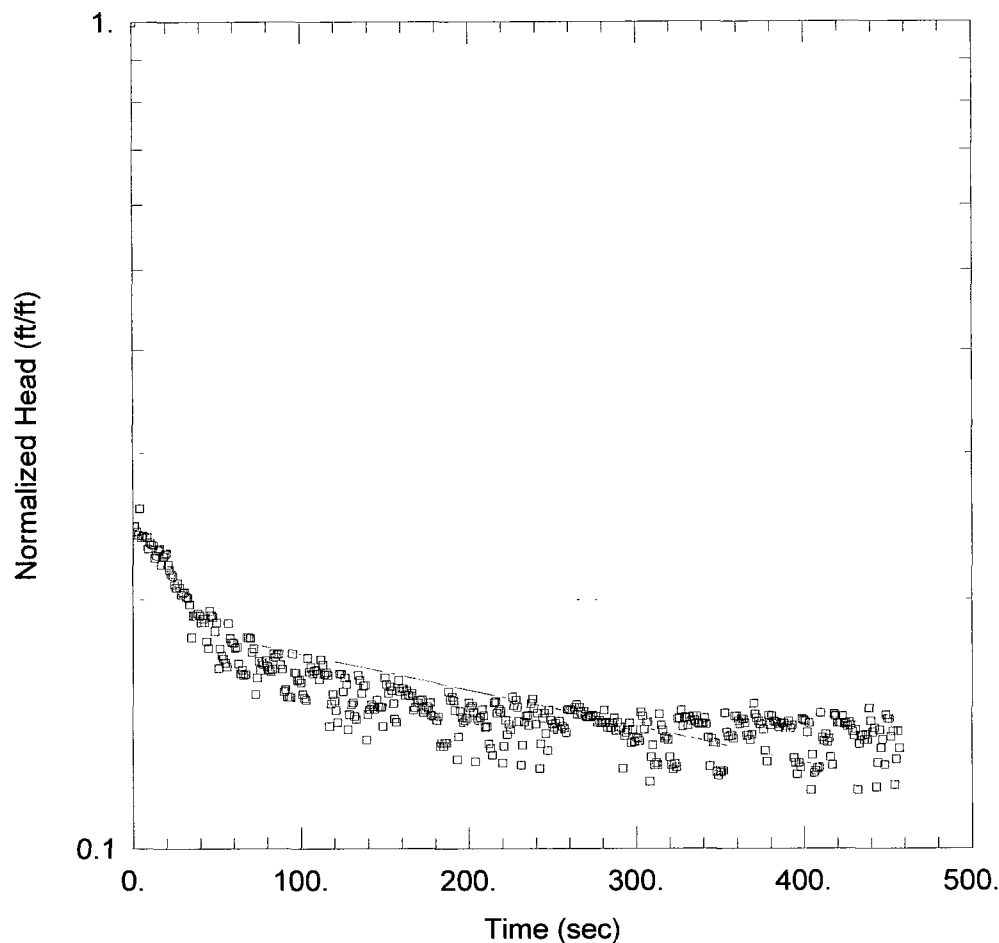
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.3686$ ft/day

$y_0 = 1.302$ ft



EB-08 TEST 3 FALLING HEAD

Data Set: Z:\...\EB-08 Test 3 Falling Head.aqt

Date: 08/11/09

Time: 15:50:52

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08 Test 3 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.61 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 3 Falling Head)

Initial Displacement: 2.5 ft

Static Water Column Height: 22.65 ft

Total Well Penetration Depth: 23. ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

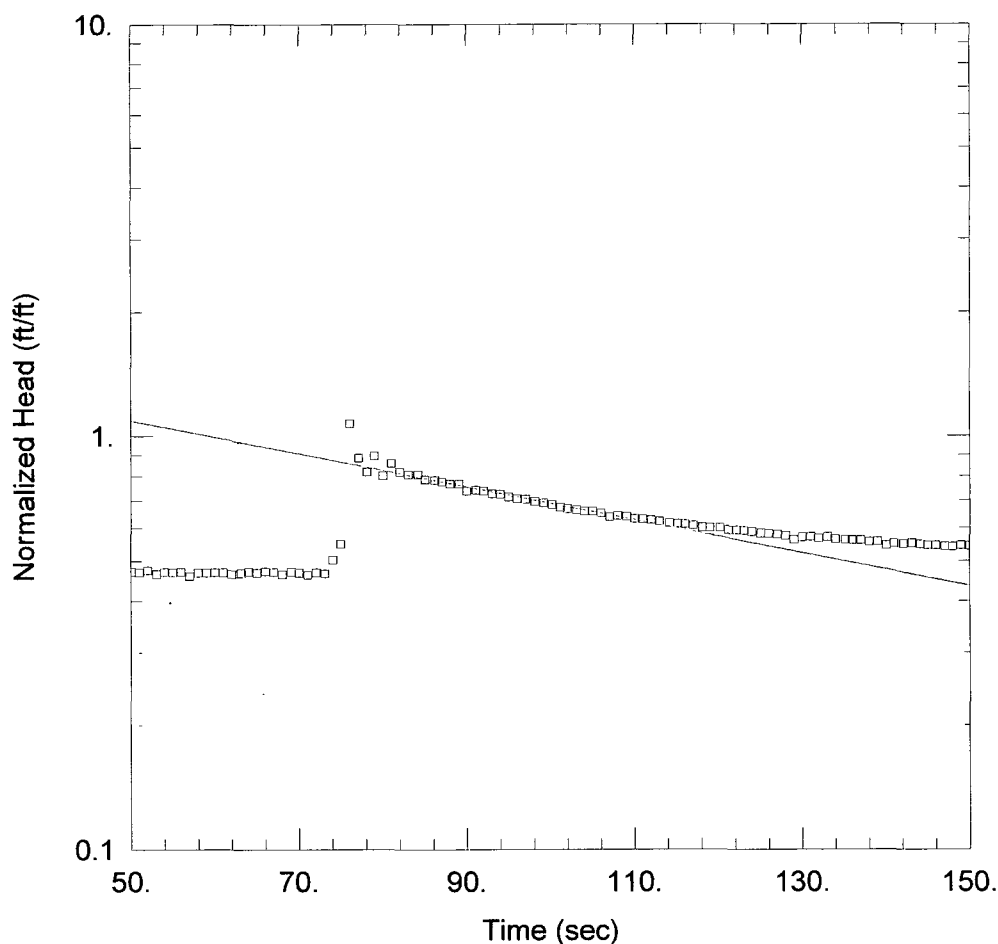
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.06535$ ft/day

$y_0 = 0.4753$ ft



RISING HEAD, SLUG OUT (TRANSLATED)

Data Set: Z:\...\EB-08 test 1 Rising head, translated.aqt

Date: 08/11/09

Time: 15:15:12

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.61 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 1 Rising Head)

Initial Displacement: 1.5 ft

Static Water Column Height: 22.69 ft

Total Well Penetration Depth: 22.69 ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

Gravel Pack Porosity: 0.

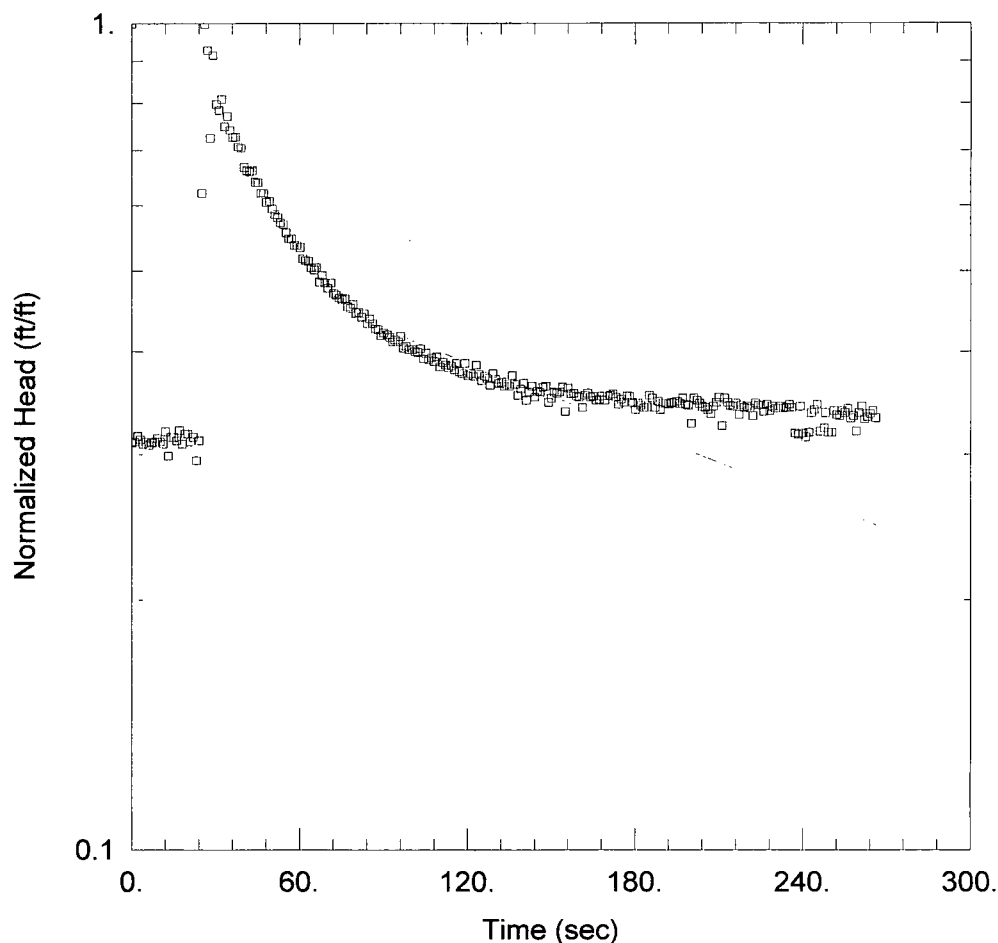
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.5876$ ft/day

$y_0 = 2.589$ ft



EB-08 TEST 2 RISING HEAD

Data Set: Z:\...\EB-08 Test 2 Rising head, translated.aqt

Date: 08/11/09

Time: 15:13:15

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08 Test 2 Rising Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.61 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 2 Rising Head)

Initial Displacement: 1. ft

Static Water Column Height: 22.66 ft

Total Well Penetration Depth: 23. ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

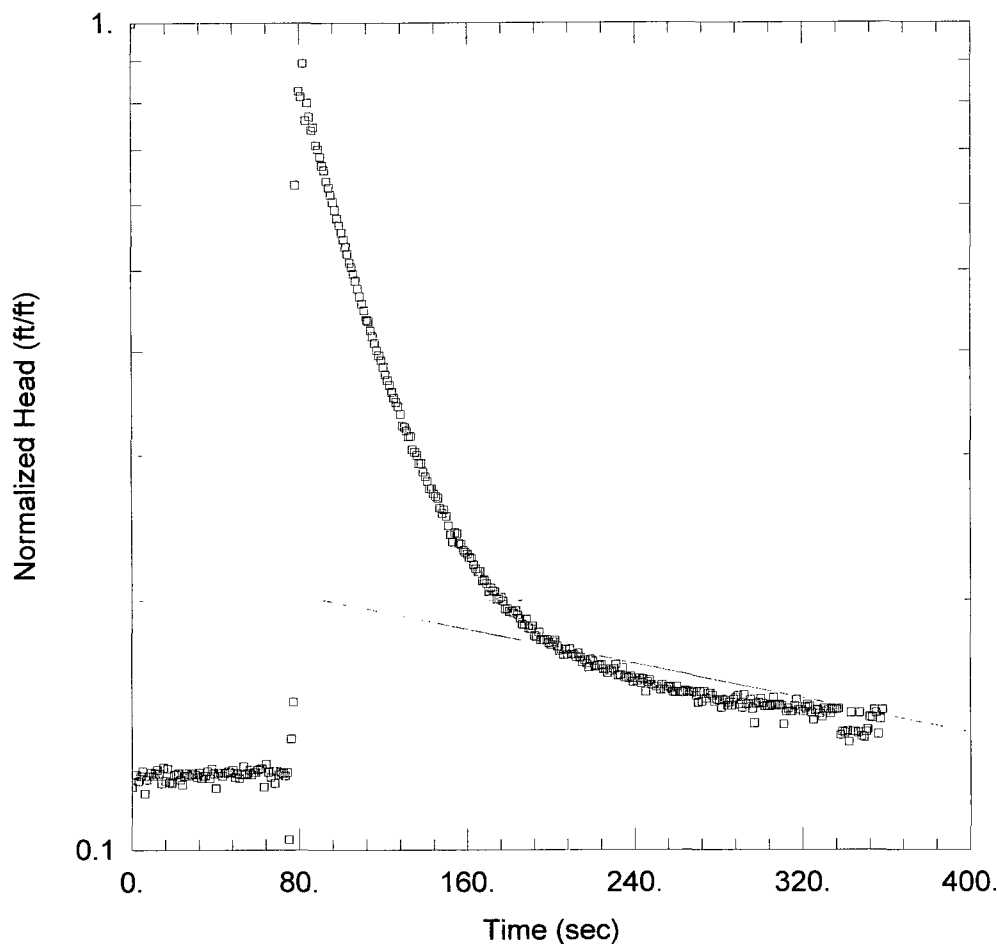
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.2016$ ft/day

$y_0 = 0.5627$ ft



EB-08 TEST 3 RISING HEAD TRANSLATED

Data Set: Z:\...\EB-08 Test 3 Rising head, translated.aqt

Date: 08/11/09

Time: 16:19:51

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: EB-08 Test 3 Rising Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 23.61 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (EB-08 Test 3 Rising Head)

Initial Displacement: 2.4 ft

Static Water Column Height: 22.65 ft

Total Well Penetration Depth: 23. ft

Screen Length: 15. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

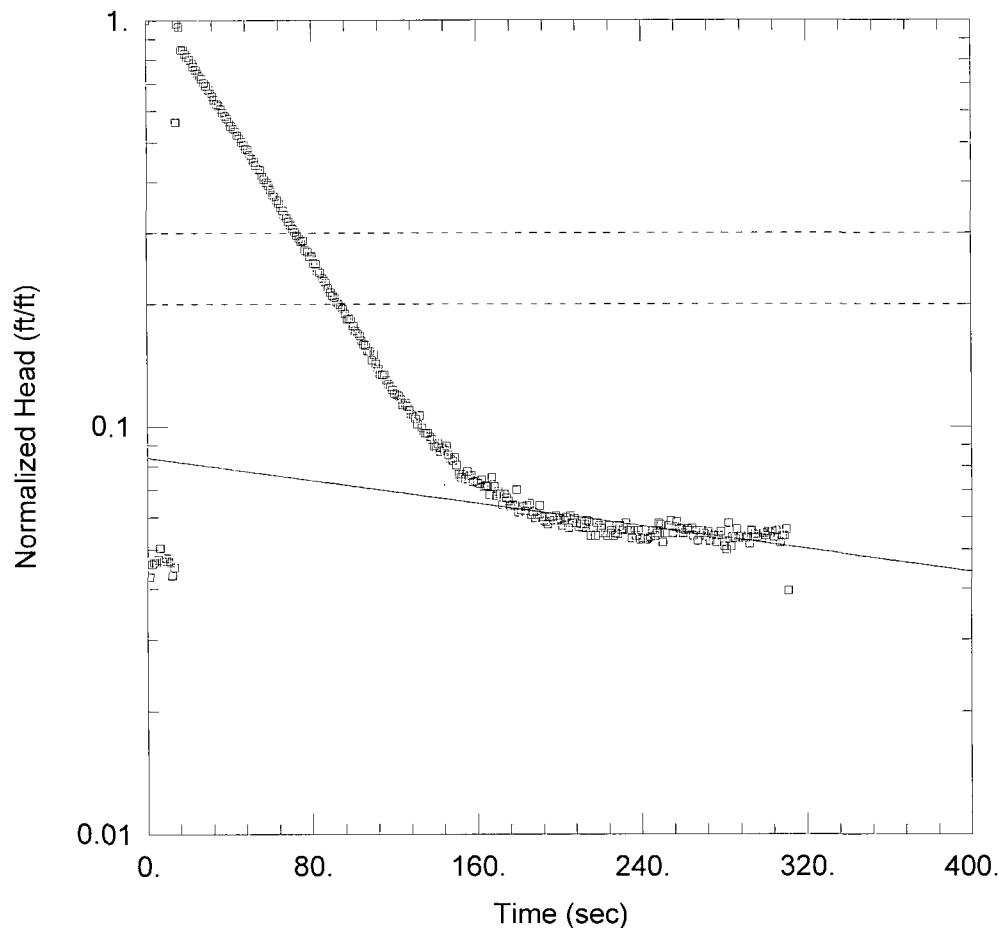
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.07751$ ft/day

$y_0 = 0.5359$ ft



P-01 TEST 1 FALLING HEAD

Data Set: Z:\...\P-01 Test 1 Falling Head.aqt

Date: 08/18/09

Time: 11:41:58

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 1 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-01 Test 1 Falling Head)

Initial Displacement: 2.5 ft

Static Water Column Height: 15.73 ft

Total Well Penetration Depth: 16. ft

Screen Length: 10. ft

Casing Radius: 0.833 ft

Well Radius: 0.25 ft

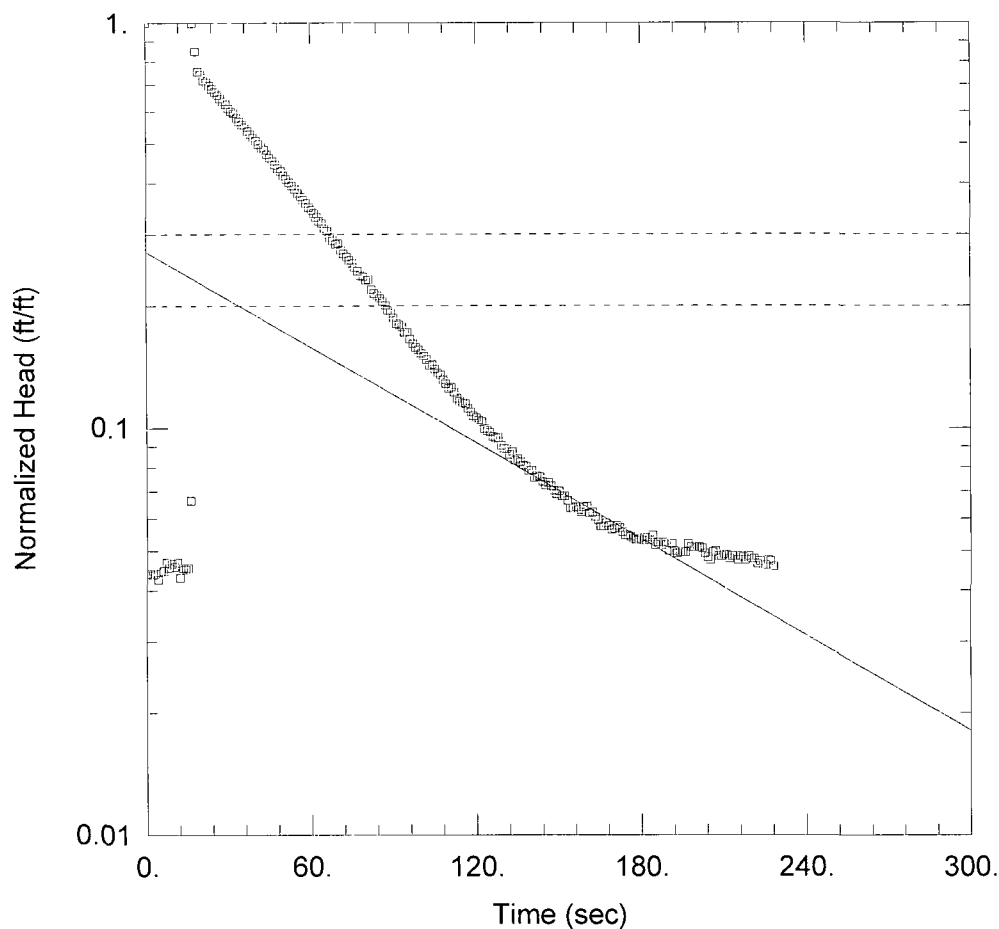
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 14.92$ ft/day

$y_0 = 0.2099$ ft



P-01 TEST 2 FALLING HEAD

Data Set: Z:\...\P-01 Test 2 Falling Head.aqt

Date: 08/18/09

Time: 12:58:41

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 2 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (P-01 Test 2 Falling Head)

Initial Displacement: 2.86 ft

Static Water Column Height: 15.73 ft

Total Well Penetration Depth: 15.12 ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

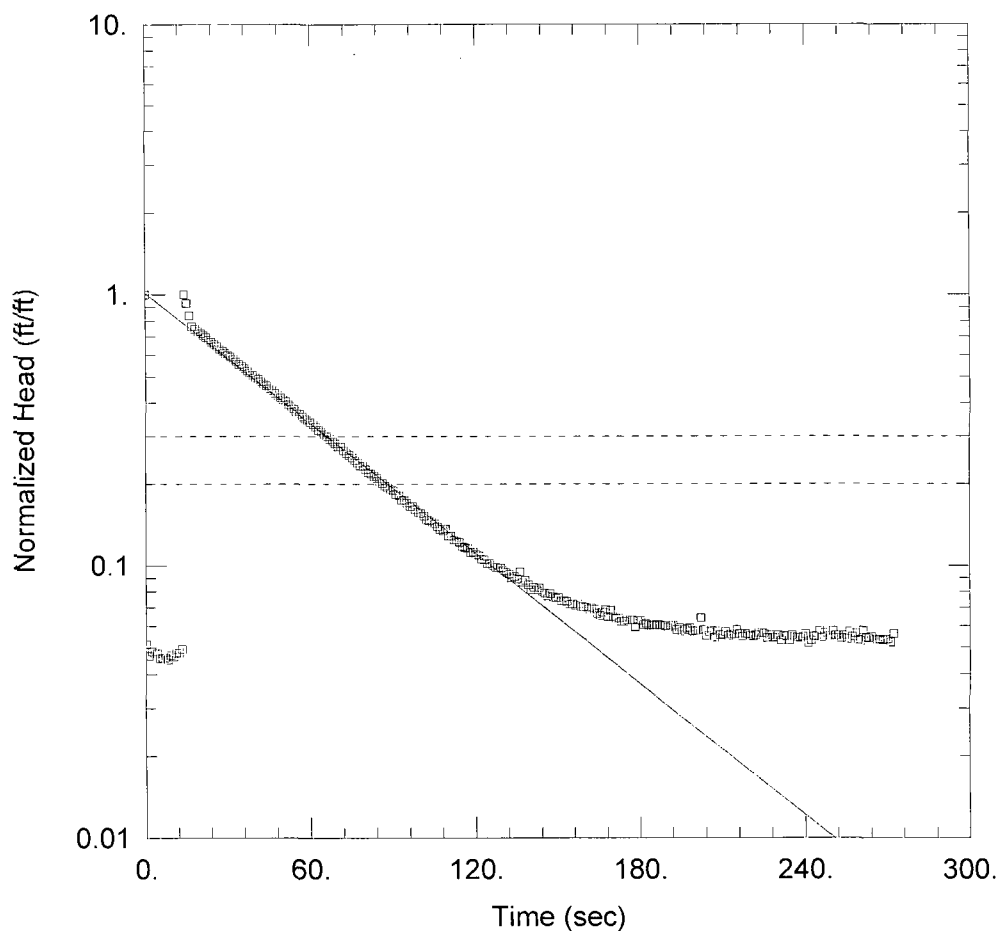
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.78 ft/day

y0 = 0.7776 ft



P-01 TEST 3 FALLING HEAD

Data Set: Z:\...\P-01 Test 3 Falling Head.aqt

Date: 08/18/09

Time: 16:50:34

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 3 Falling Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-01 Test 3 Falling Head)

Initial Displacement: 2.81 ft

Static Water Column Height: 15.73 ft

Total Well Penetration Depth: 15.73 ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

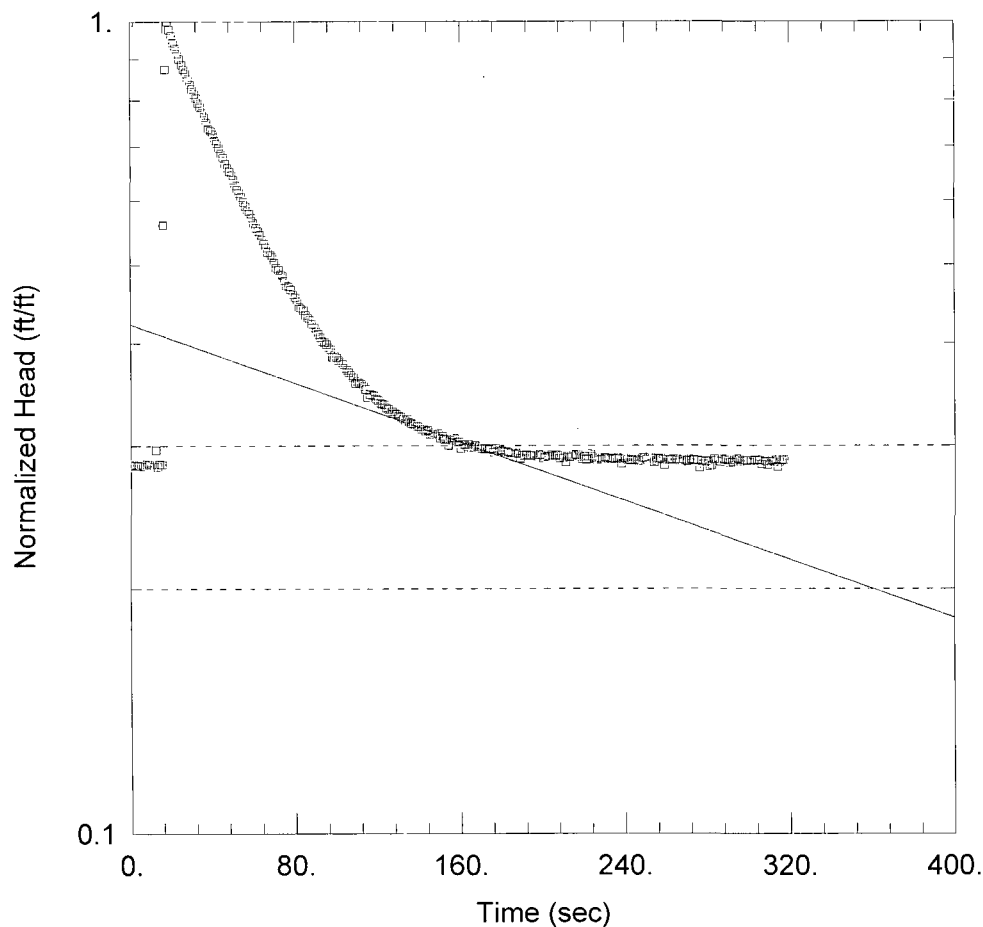
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 1.71$ ft/day

$y_0 = 2.848$ ft



P-01 TEST 1 RISING HEAD

Data Set: Z:\...\P-01 Test 1 Rising Head.aqt

Date: 08/18/09

Time: 12:34:03

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 1 Rising Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-01)

Initial Displacement: 3.04 ft

Static Water Column Height: 15.73 ft

Total Well Penetration Depth: 15.73 ft

Screen Length: 10. ft

Casing Radius: 0.833 ft

Well Radius: 0.25 ft

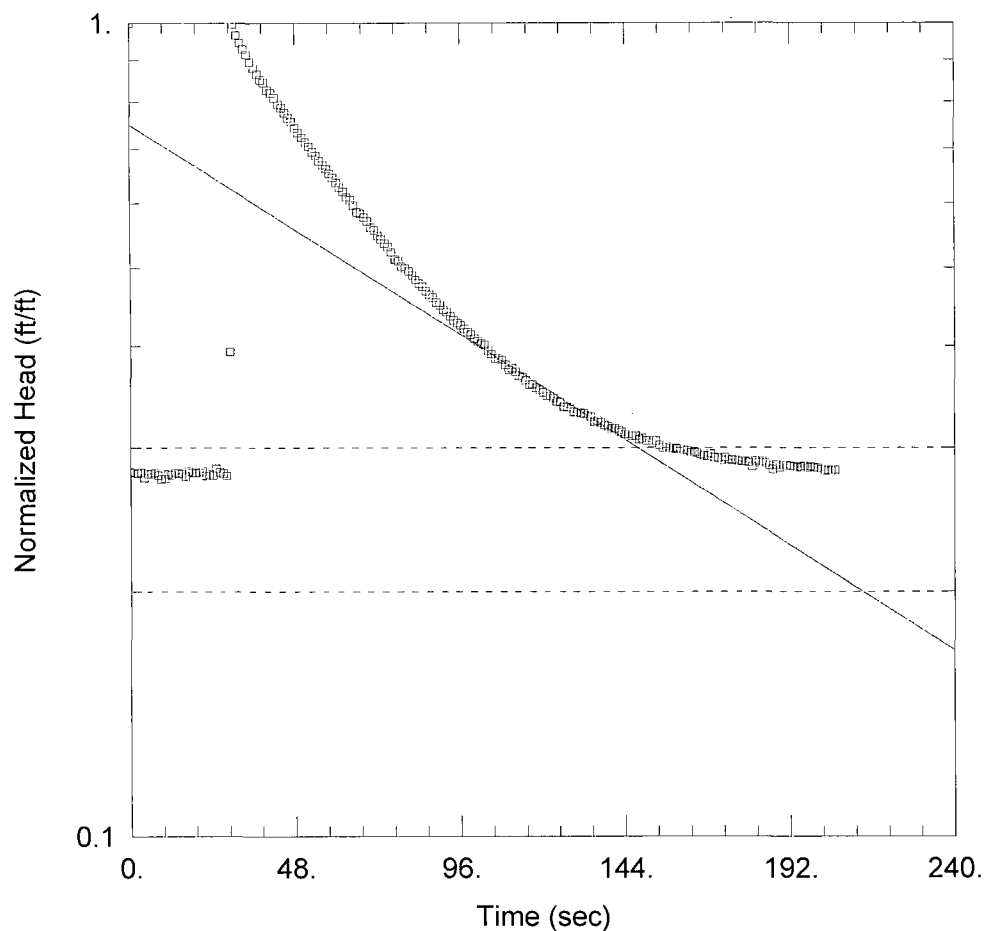
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 19.24$ ft/day

$y_0 = 1.284$ ft



P-01 TEST 2 RISNING HEAD

Data Set: Z:\...\P-01 Test 2 Rising Head.aqt

Date: 08/18/09

Time: 16:07:11

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 2 Rising Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-01 Test 2 Rising Head)

Initial Displacement: 3.12 ft

Static Water Column Height: 15.13 ft

Total Well Penetration Depth: 15.73 ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

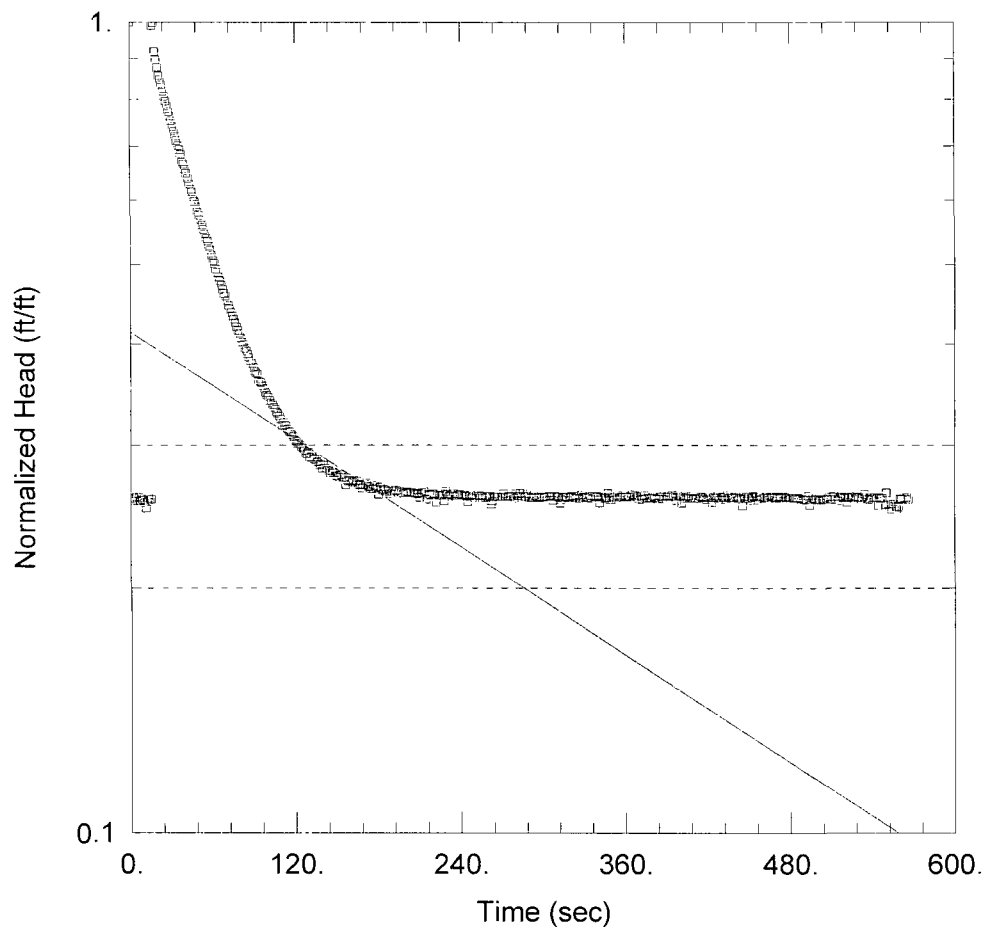
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.575$ ft/day

$y_0 = 2.34$ ft



P-01 TEST 3 RISING HEAD

Data Set: Z:\...\P-01 Test 3 Rising Head.aqt

Date: 08/19/09

Time: 09:45:45

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-01 Test 3 Rising Head

Test Date: 7/31/09

AQUIFER DATA

Saturated Thickness: 15.73 ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-01 Test 3 Rising Head)

Initial Displacement: 3.3 ft

Static Water Column Height: 15.73 ft

Total Well Penetration Depth: 15.73 ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

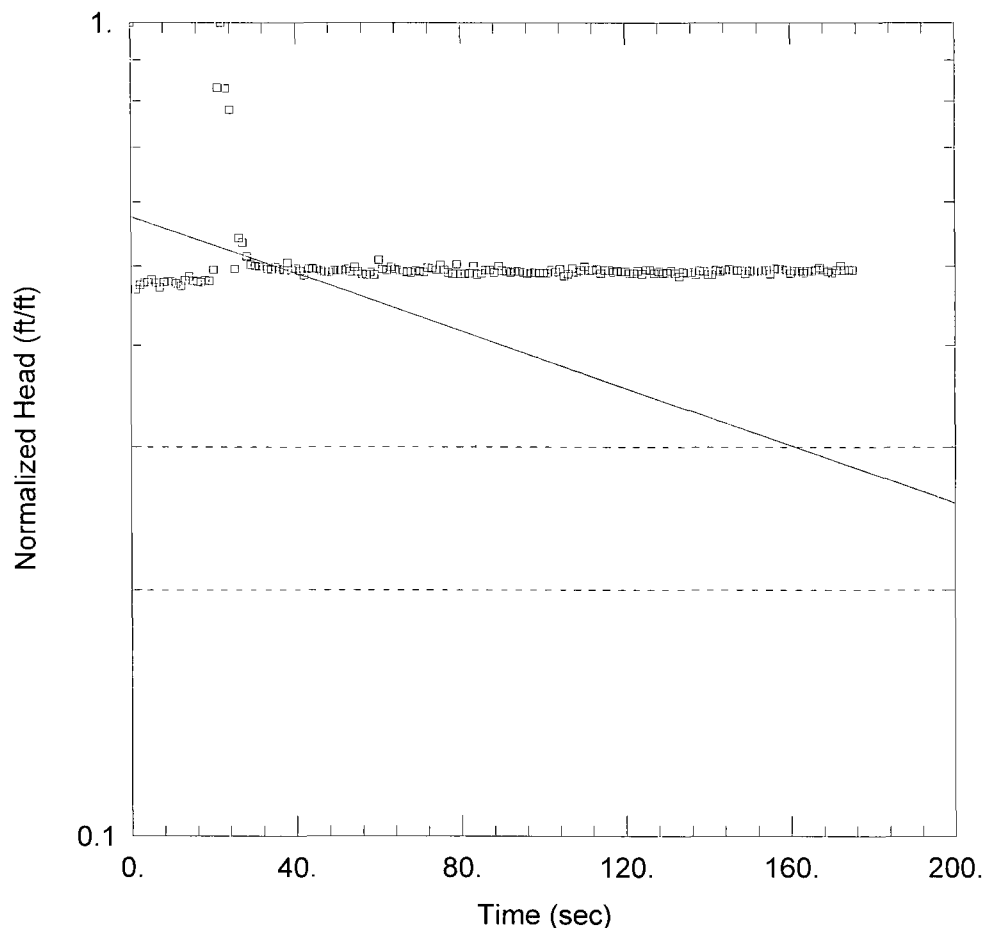
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.2358$ ft/day

$y_0 = 1.364$ ft



P-05 TEST 1 FALLING HEAD

Data Set: Z:\...\P-05 Test 1 Falling Head.aqt

Date: 08/19/09

Time: 10:40:05

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 1 Falling Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (P-05 Test 1 Falling Head)

Initial Displacement: 1.152 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

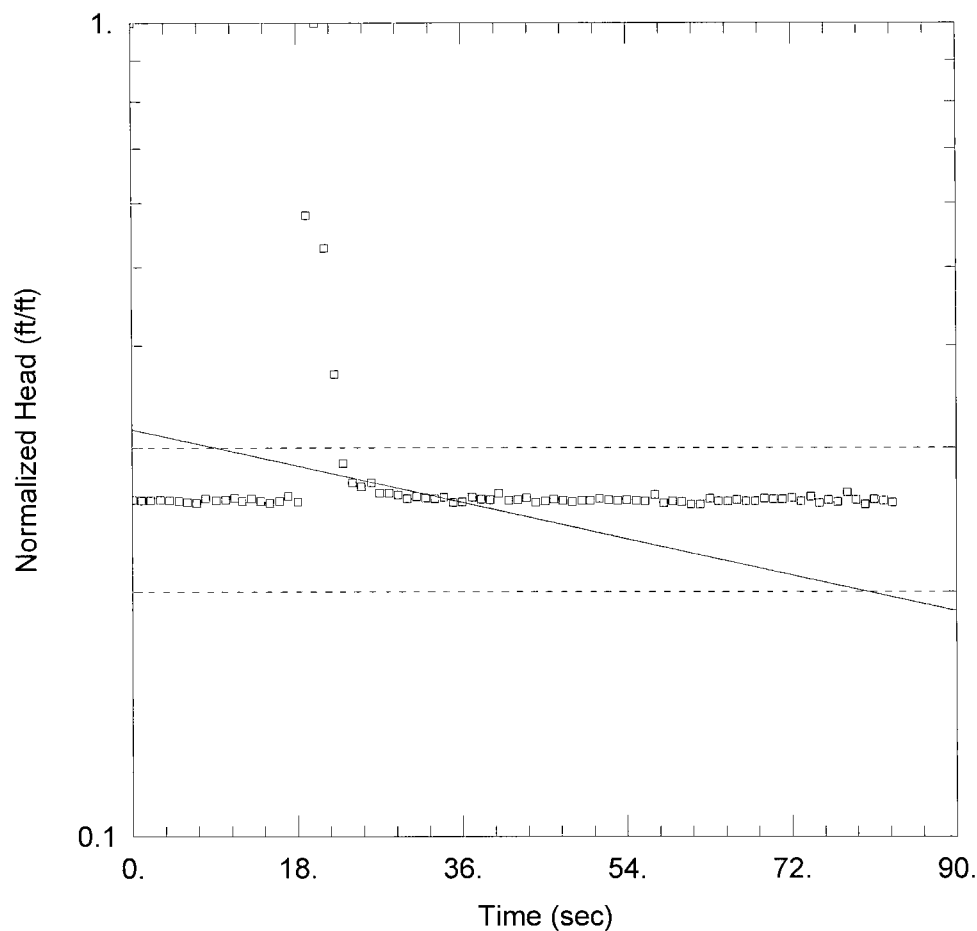
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.3106 ft/day

y0 = 0.6636 ft



P-05 TEST 2 FALLING HEAD

Data Set: Z:\...\P-05 Test 2 Falling Head.aqt

Date: 08/19/09

Time: 13:43:55

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 2 Falling Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (P-05 Test 2 Falling Head)

Initial Displacement: 2.184 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

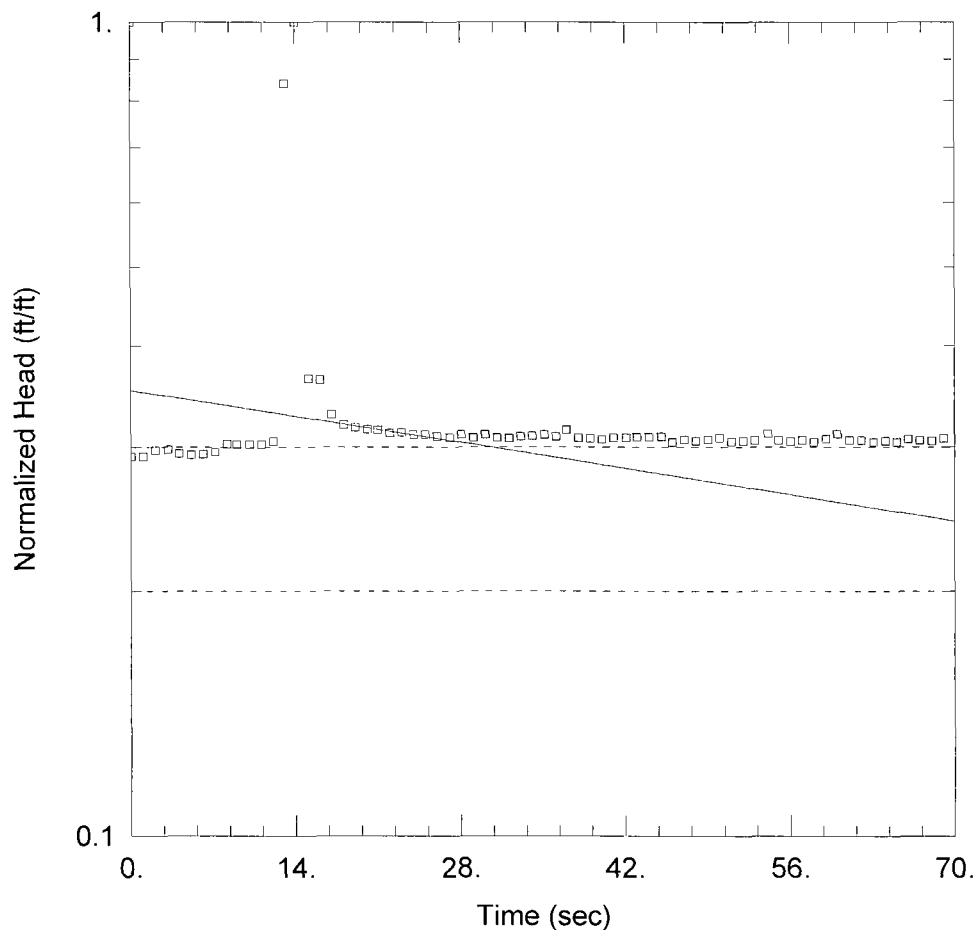
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.4365 ft/day

y0 = 0.6901 ft



P-05 TEST 3 FALLING HEAD

Data Set: Z:\...\P-05 Test 3 Falling Head.aqt

Date: 08/19/09

Time: 15:16:05

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 3 Falling Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-05 Test 3 Falling Head)

Initial Displacement: 1.857 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

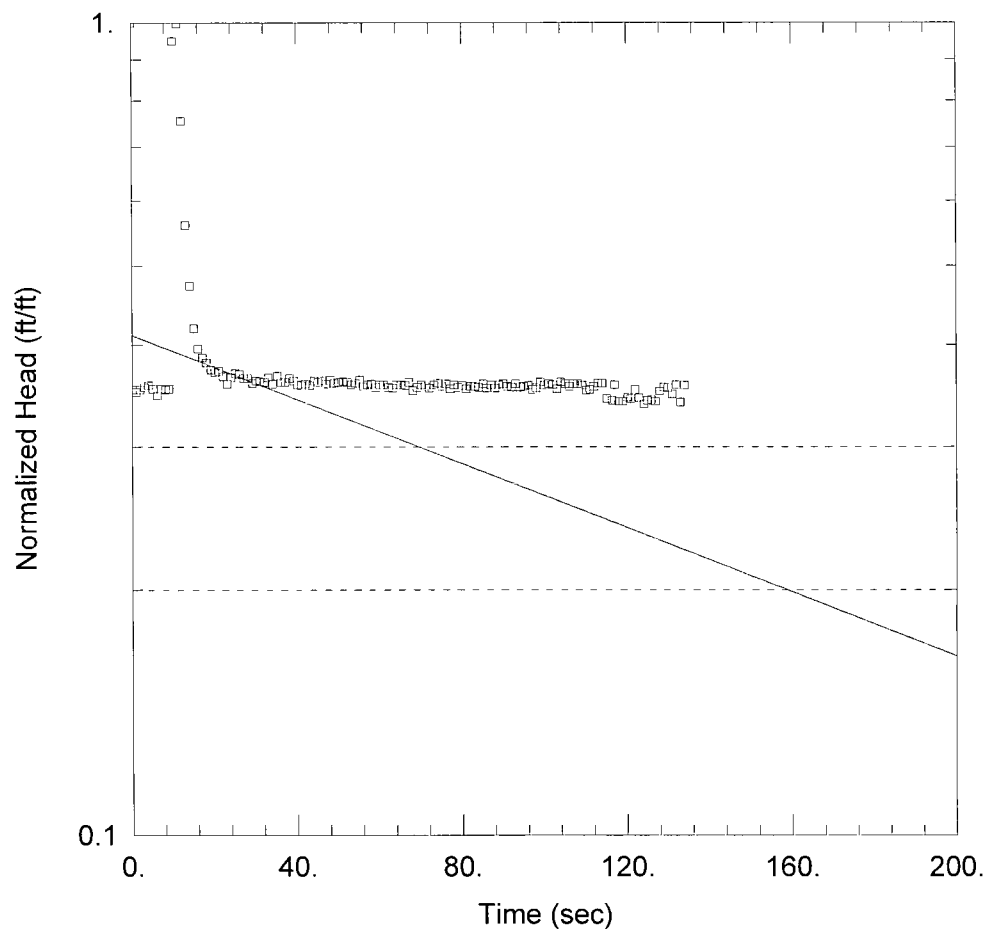
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.4051$ ft/day

$y_0 = 0.6547$ ft



P-05 TEST 1 RISING HEAD

Data Set: Z:\...\P-05 Test 1 Rising Head.aqt

Date: 08/19/09

Time: 12:58:34

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 1 Rising Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-05 Test 1 Rising Head)

Initial Displacement: 1.22 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

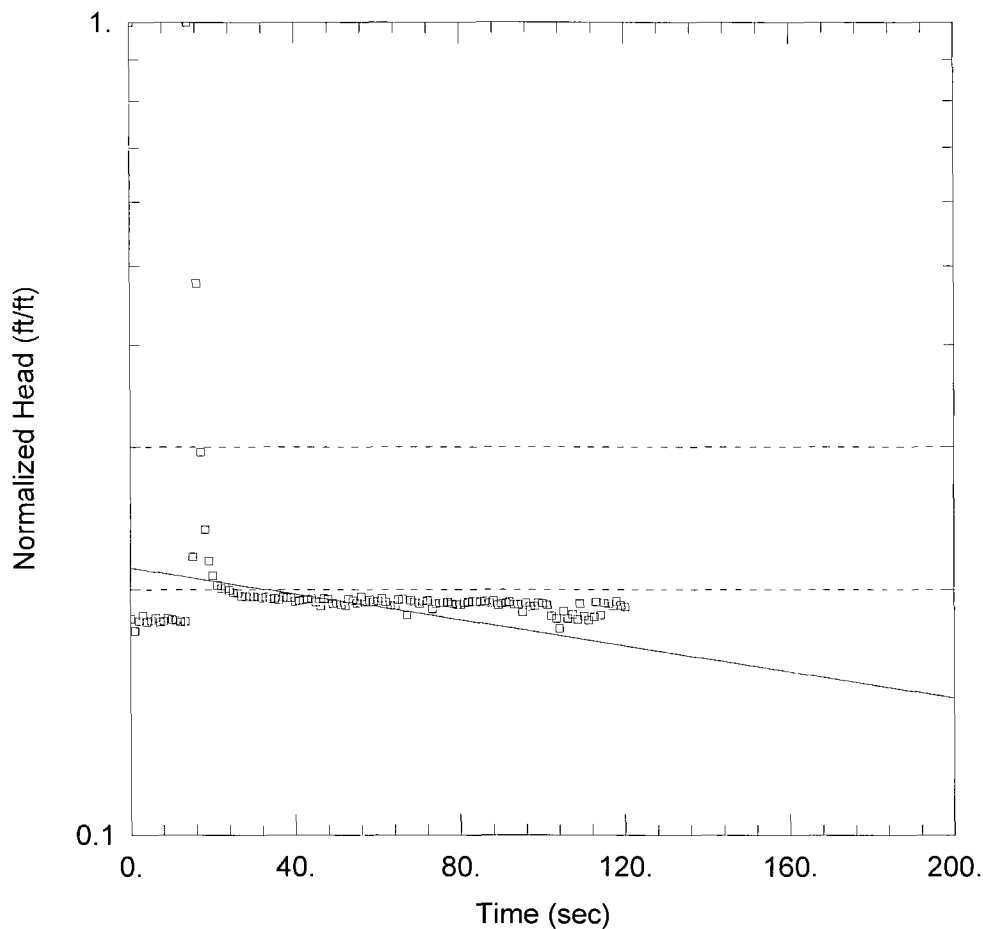
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.3482$ ft/day

$y_0 = 0.5018$ ft



P-05 TEST 2 RISING HEAD

Data Set: Z:\...\P-05 Test 2 Rising Head.aqt

Date: 08/19/09

Time: 14:55:37

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 2 Rising Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-05 Test 2 Rising Head)

Initial Displacement: 2.373 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

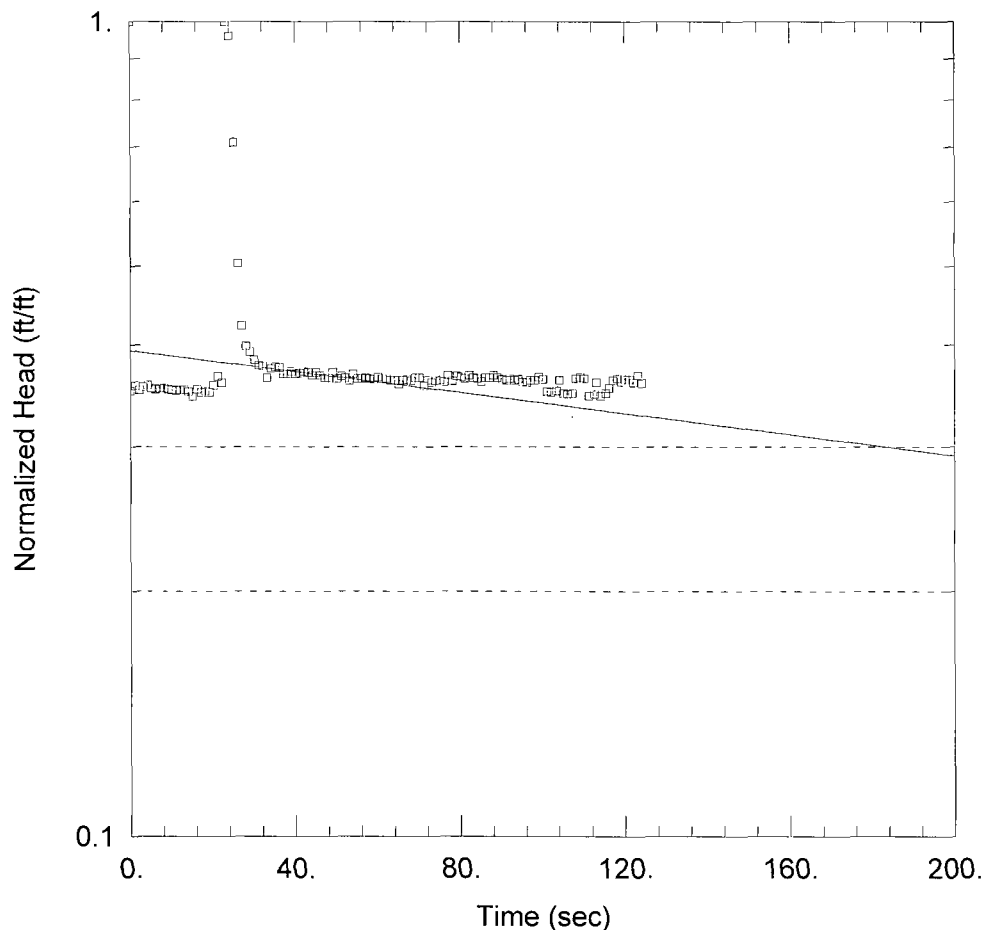
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.1414$ ft/day

$y_0 = 0.5047$ ft



P-05 TEST 3 RISING HEAD

Data Set: Z:\...\P-05 Test 3 Rising Head.aqt

Date: 08/19/09

Time: 15:27:00

PROJECT INFORMATION

Company: Larson & Associates, Inc.

Client: Frontier Field Services

Project: 6-0141

Location: Empire Abo Gas Plant

Test Well: P-05 Test 3 Rising Head

Test Date: 8/03/09

AQUIFER DATA

Saturated Thickness: 12. ft

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (P-05 Test 3 Rising Head)

Initial Displacement: 1.224 ft

Static Water Column Height: 10.57 ft

Total Well Penetration Depth: 10. ft

Screen Length: 10. ft

Casing Radius: 0.0833 ft

Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.1135$ ft/day

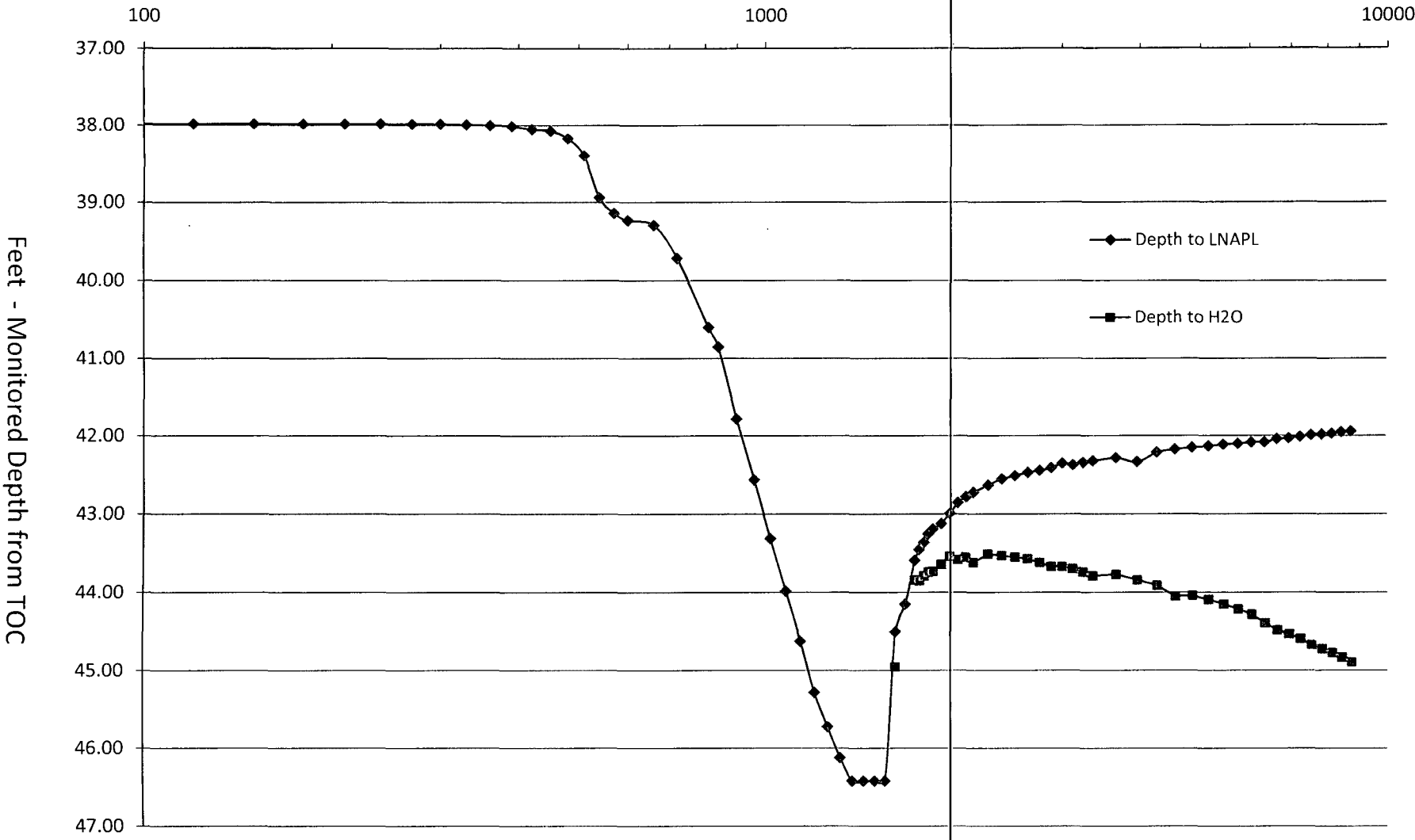
$y_0 = 0.4817$ ft

MW-11 LNAPL Pump-Down and Recovery
Test
September 17, 2008

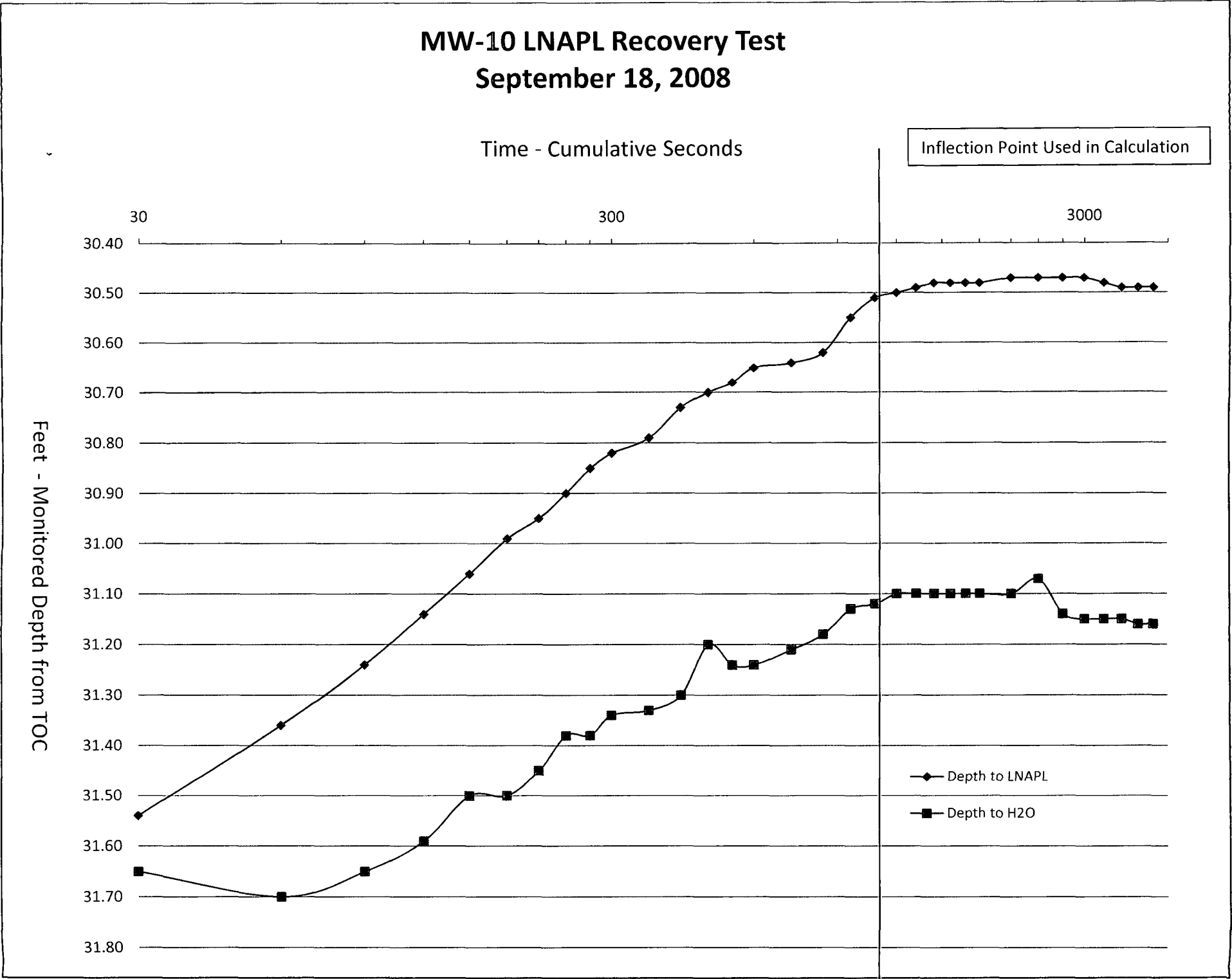
Initial Gauging Data:
LNAPL - 37.95'
H2O - 57.65'

Time - Cumulative Seconds

Inflection Point Used in Calculation



Obs. No.	Time Sec	Depth to LNAPL	Depth to H ₂ O	Obs. No.	Time Sec	Depth to LNAPL	Depth to H ₂ O	Static D-LNAPL	Static D-H ₂ O	Corrected D-GW
1	30	37.97		39	1740	43.59	43.84	37.95	57.65	41.89
2	60	37.98		40	1770	43.45	43.85	Specific Gravity of 0.8 g/cm ³ , based on RT Hicks Consultant 11/18/1996 report.		
3	90	37.98		41	1800	43.36	43.79			
4	120	37.98		42	1830	43.25	43.74			
5	150	37.98		43	1860	43.19	43.73			
6	180	37.98		44	1920	43.12	43.64			
7	210	37.98		45	1980	42.99	43.54	Charting and calculation based upon <i>Determination of a Realistic Estimate of Formation Product Thickness Using Monitor Wells: A Field Bailout Test</i> by Thomas S. Gruszczenski (no date).		
8	240	37.98		46	2040	42.85	43.58			
9	270	37.98		47	2100	42.78	43.55			
10	300	37.98		48	2160	42.72	43.62			
11	330	37.99		49	2280	42.63	43.51			
12	360	38.00		50	2400	42.55	43.53	Step Number 5 – Inflection Point 6 – S.G. corrected 7 – Measured Product Thickness 8 – Inflection Product Thickness 9 – Capillary Fringe Height		
13	390	38.01		51	2520	42.51	43.55			
14	420	38.05		52	2640	42.47	43.57			
15	450	38.07		53	2760	42.44	43.62			
16	480	38.17		54	2880	42.41	43.67			
17	510	38.40		55	3000	42.35	43.67	45/1980 sec 41.89 0.55 5.04 4.49		
18	540	38.94		56	3120	42.37	43.70			
19	570	39.14		57	3240	42.34	43.74			
20	600	39.23		58	3360	42.32	43.79			
21	660	39.29		59	3660	42.28	43.77			
22	720	39.71		60	3960	42.33	43.84			
23	810	40.60		61	4260	42.21	43.91			
24	840	40.85		62	4560	42.17	44.05			
25	900	41.78		63	4860	42.15	44.04			
26	960	42.56		64	5160	42.13	44.09			
27	1020	43.31		65	5460	42.11	44.15			
28	1080	43.98		66	5760	42.10	44.21			
29	1140	44.62		67	6060	42.08	44.28			
30	1200	45.28		68	6360	42.08	44.39			
31	1260	45.72		69	6660	42.04	44.48			
32	1320	46.12		70	6960	42.03	44.53			
33	1380	46.42		71	7260	42.01	44.59			
34	1440	46.42		72	7560	41.99	44.67			
35	1500	46.42		73	7860	41.98	44.72			
36	1560	46.42	Pump Off	74	8160	41.97	44.77			
37	1620	44.50	44.95	75	8460	41.95	44.83			
38	1680	44.15		76	8760	41.94	44.89			



Obs. No.	Time Sec	Depth to LNAPL	Depth to H ₂ O
1	30	31.54	31.65
2	60	31.36	31.7
3	90	31.24	31.65
4	120	31.14	31.59
5	150	31.06	31.5
6	180	30.99	31.5
7	210	30.95	31.45
8	240	30.90	31.38
9	270	30.85	31.38
10	300	30.82	31.34
11	360	30.79	31.33
12	420	30.73	31.3
13	480	30.70	31.2
14	540	30.68	31.24
15	600	30.65	31.24
16	720	30.64	31.21
17	840	30.62	31.18
18	960	30.55	31.13
19	1080	30.51	31.12
20	1200	30.50	31.10
21	1320	30.49	31.10
22	1440	30.48	31.10
23	1560	30.48	31.10
24	1680	30.48	31.10
25	1800	30.48	31.10
26	2100	30.47	31.10
27	2400	30.47	31.07
28	2700	30.47	31.14
29	3000	30.47	31.15
30	3300	30.48	31.15
31	3600	30.49	31.15
32	3900	30.49	31.16
33	4200	30.49	31.16

Static
D-LNAPL
29.76

Static
D-H2O
41.25

Corrected
D-GW
32.058

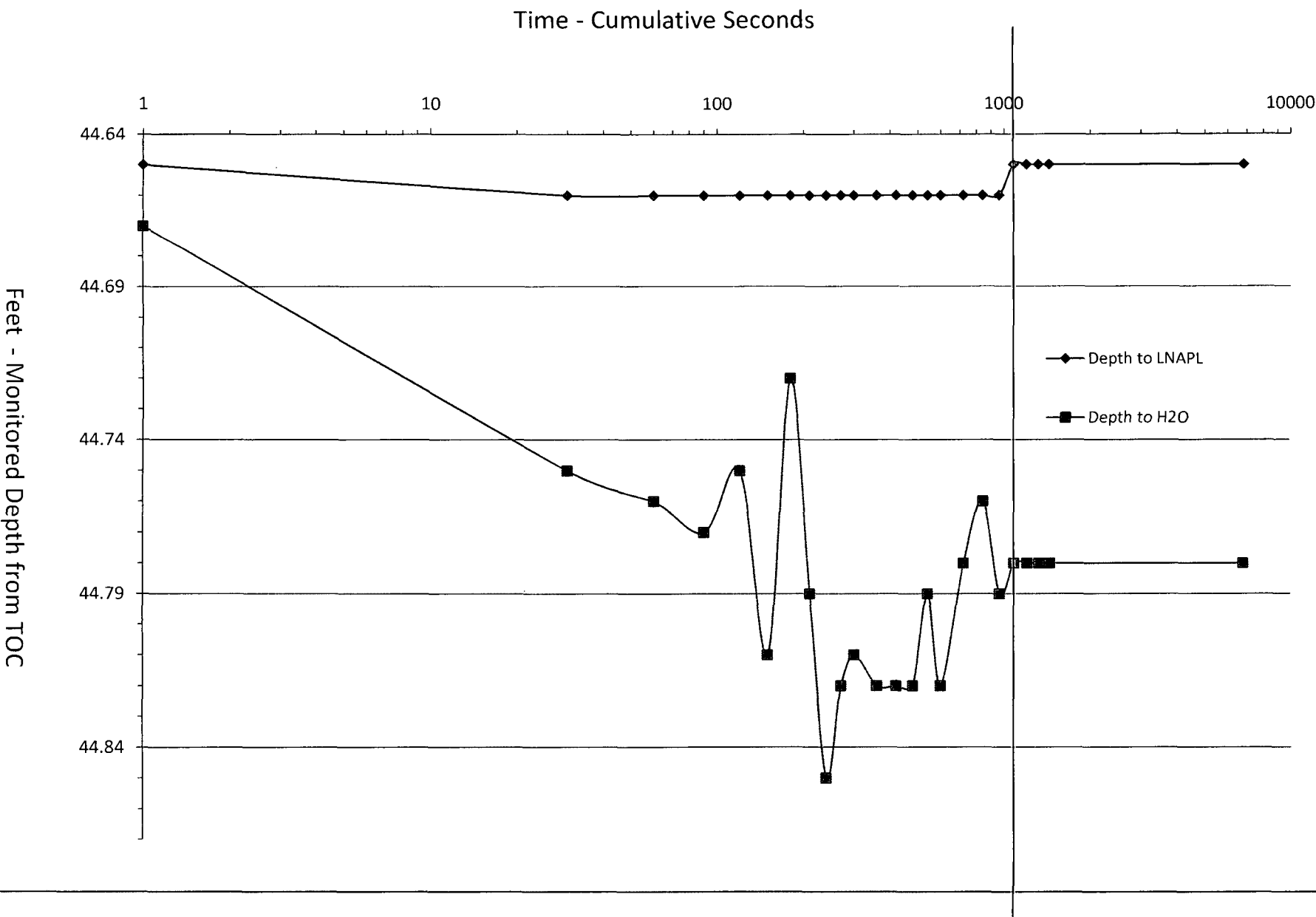
Specific Gravity of 0.8 g/cm³, based on RT Hicks Consultant 11/18/1996 report.

Charting and calculation based upon *Determination of a Realistic Estimate of Formation Product Thickness Using Monitor Wells: A Field Bailout Test* by Thomas S. Gruszczenski (no date).

Step Number	
5 – Inflection Point	19/1080 sec
6 – S.G. corrected	32.058
7 – Measured Product Thickness	0.61
8 – Inflection Product Thickness	0.75
9 – Capillary Fringe Height	0.14

MW-14 LNAPL Recovery Test
September 18, 2008

Inflection Point Used in Calculation



Obs. No.	Time Sec	Depth to LNAPL	Depth to H ₂ O
1	0	44.65	44.67
2	30	44.66	44.75
3	60	44.66	44.76
4	90	44.66	44.77
5	120	44.66	44.75
6	150	44.66	44.81
7	180	44.66	44.72
8	210	44.66	44.79
9	240	44.66	44.85
10	270	44.66	44.82
11	300	44.66	44.81
12	360	44.66	44.82
13	420	44.66	44.82
14	480	44.66	44.82
15	540	44.66	44.79
16	600	44.66	44.82
17	720	44.66	44.78
18	840	44.66	44.76
19	960	44.66	44.79
20	1080	44.65	44.78
21	1200	44.65	44.78
22	1320	44.65	44.78
23	1440	44.65	44.78
24	6840	44.65	44.78

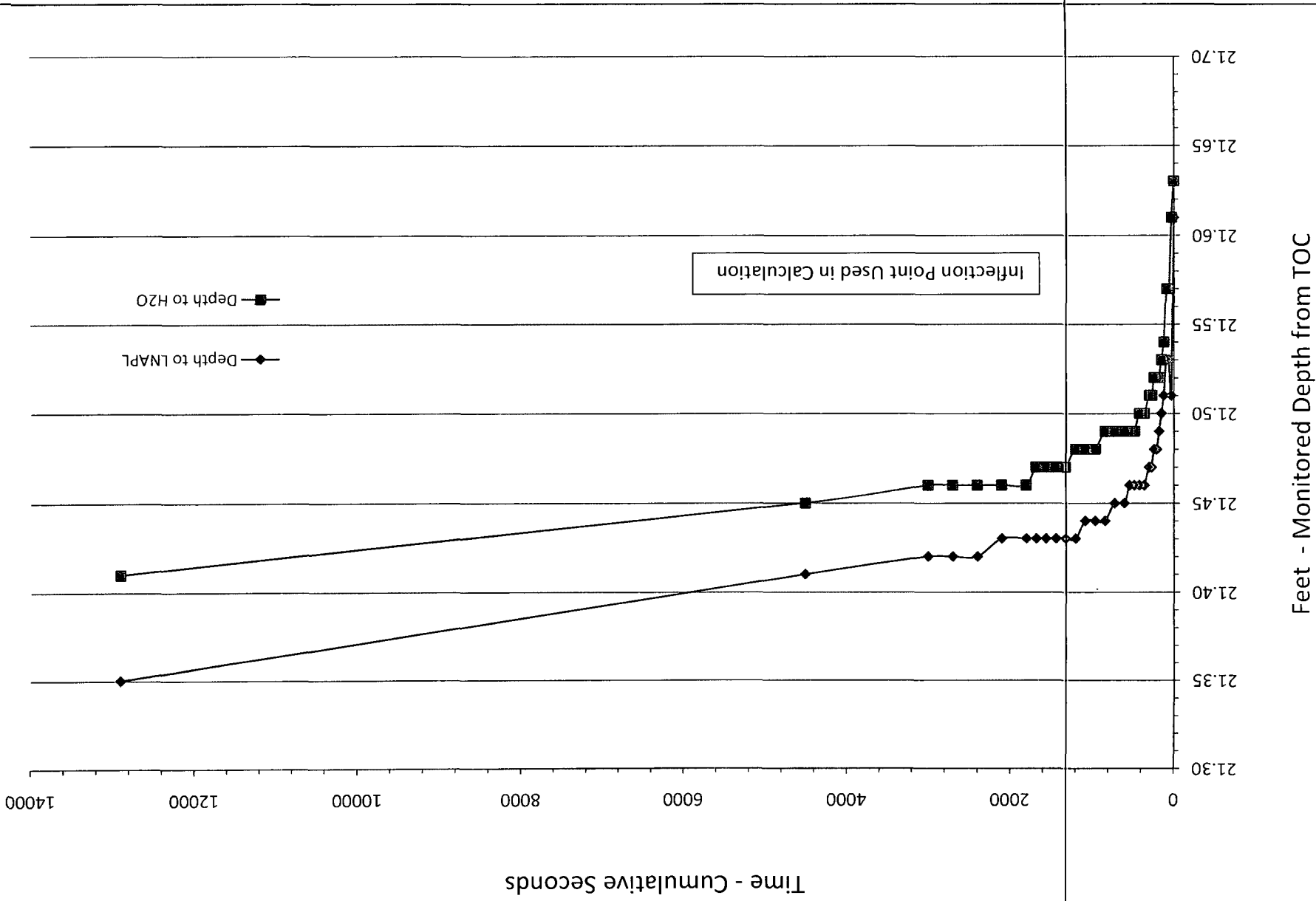
Static D-LNAPL	Static D-H2O	Corrected D-GW
44.63	44.86	44.68

Specific Gravity of 0.8 g/cm³, based on RT Hicks Consultant 11/18/1996 report.

Charting and calculation based upon *Determination of a Realistic Estimate of Formation Product Thickness Using Monitor Wells: A Field Bailout Test* by Thomas S. Gruszczenski (no date).

Step Number	
5 – Inflection Point	20/1080 sec
6 – S.G. corrected	44.68
7 – Measured Product Thickness	0.13
8 – Inflection Product Thickness	0.02
9 – Capillary Fringe Height	0.11

MW-2-11 LNAPL Recovery Test
September 18, 2008



Obs. No.	Time Sec	Depth to LNAPL	Depth to H ₂ O
1	0	21.61	21.63
2	30	21.51	21.61
3	60	21.53	21.57
4	90	21.53	21.57
5	120	21.51	21.54
6	150	21.50	21.53
7	180	21.49	21.52
8	210	21.48	21.52
9	240	21.48	21.52
10	270	21.47	21.51
11	300	21.47	21.51
12	360	21.46	21.5
13	420	21.46	21.5
14	480	21.46	21.49
15	540	21.46	21.49
16	600	21.45	21.49
17	720	21.45	21.49
18	840	21.44	21.49
19	960	21.44	21.48
20	1080	21.44	21.48
21	1200	21.43	21.48
22	1320	21.43	21.47
23	1440	21.43	21.47
24	1560	21.43	21.47
25	1680	21.43	21.47
26	1800	21.43	21.46
27	2100	21.43	21.46
28	2400	21.42	21.46
29	2700	21.42	21.46
30	3000	21.42	21.46
31	4500	21.41	21.45
32	12900	21.35	21.41

Step Number

22/1320

sec

21.34

0.04

0.20

0.16

5 – Inflection Point

6 – S.G. corrected

7 – Measured Product Thickness

8 – Inflection Product Thickness

9 – Capillary Fringe Height

Charting and calculation based upon Determination of a Realistic Estimate of Formation Product Thickness Using Monitor Wells: A Field Bailout Test by Thomas S. Gruszczenksi (no date).

Specific Gravity of 0.8 g/cm³, based on RT Hicks Consultant 11/18/1996 report.

Static

D-LNAPL

21.23

Static

D-H₂O

21.79

Corrected

D-GW

21.34

DETERMINATION OF A REALISTIC ESTIMATE
OF THE ACTUAL
FORMATION PRODUCT THICKNESS
USING MONITOR WELLS:
A FIELD BAILOUT TEST

Thomas S. Gruszczenski

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Suite 250
Atlanta, Georgia 30340

ABSTRACT

Various papers have presented factors affecting the accumulation of product in monitor wells. These factors have correlated the apparent product thickness, as measured in monitor wells, with the actual formation product thickness. This paper outlines a field test to determine a realistic estimate of the actual formation product thickness.

This empirical test is similar to a rising head slug test. Product that has accumulated in a monitor well is bailed out and the rising water/product levels are recorded with time using an oil/water interface probe. This test has been performed on various sites underlain by residual Piedmont soils of the southeastern United States.

The results of this test yield two basic curve types. Type one curves were observed in monitor wells with product accumulation less than several inches. This curve type indicates a one to one correspondence between the measured and actual formation product thickness. Type two curves were observed in monitor wells with product accumulation greater than 12 inches. This curve type indicates an inflection point prior to stabilization of water product levels. This inflection point is the actual equilibrium point during the accumulation of water and product. The stabilized water and product levels recorded represents a psuedoequilibrium caused by the difference in specific gravity and height of capillary fringe. This inflection point indicates a 70% to 95% reduction between the measured and actual formation product thickness.

INTRODUCTION

The use of underground storage tanks to store petroleum products has lead to accidental releases of these products to the subsurface. This leaked product will follow the path of least resistance. If the subsurface is isotropic then this flow path will be downward with increasing horizontal migration with depth. The downward movement of product through the subsurface will first be in the vadose zone. The rate of movement through this zone will be controlled by the product characteristics and the soil characteristics. These characteristics would be a function of the lost product volume, flow rate, viscosity, and specific gravity and also the soil porosity, permeability and water saturation.

If the volume of the leaked product is greater than the absorptive capacity of the soil, provided no impermeable horizons were encountered, the product will accumulate on the capillary fringe, above the water table. This rising of fluid in the formation voids above the phreatic water table is a result of the adhesive tension between the soil grains and the ground water. This adhesive tension, which is a positive force, will draw the ground-water upward until it is balanced by the weight, which is a negative force, of the ground-water being drawn upward, above the phreatic water table. The height of the capillary fringe is primarily a function of the soil grain size. Table 1, lists suggested capillary rises based on soil type (Bear, 1979).

Table 1

<u>Soil Type</u>	<u>Capillary Rise (Inches)</u>
Coarse Sand	3/4 - 2
Sand	4 - 14
Fine Sand	14 - 27
Silt	27 - 59
Clay	78 - 160+

The product does not displace this water due to the immiscibility, difference in surface energy and specific gravity of the two fluids. The capillary pressure will be greatest at the top of the capillary fringe due to the decrease in water saturation. Since water has a greater surface tension than gasoline products, this further increases the pressure difference across the interface, hence giving rise to interfacial tension. Thus, gasoline product will accumulate on top of the capillary fringe, which is 100% saturated with water, and above the phreatic water table.

A monitor well installed in the Piedmont soil of the U.S. and screened across the phreatic water table has a much greater diameter than the average grain size of the aquifer. As such, there is no capillary rise in the well bore of any significance.

The use of monitor wells is the most common method of defining product plumes. It has been recognized by those involved with investigating these plumes that the product thickness measured in a monitor well is an apparent product thickness. This apparent product thickness measured has been commonly accepted to be greater than the actual formation thickness.

Various papers have presented evidence to illustrate the apparent product thickness phenomenon. These papers have presented factors effecting the accumulation of product in monitor wells. The two primary factors are the specific gravity of the product and the height of the capillary fringe. Current literature correlates the apparent product thickness with the actual formation thickness using column tests, formation factors and ratios.

If the measured apparent product thickness is greater than the actual formation product thickness, then at some point during the accumulation of product in the well bore, the apparent product thickness equals the actual product thickness. The following test procedure outlines the methodology for determining a realistic estimate of the actual thickness.

TEST PROCEDURE

The test procedure is similar in performance to a rising head slug test. The equipment necessary to perform the test is listed in Table 2.

Table 2
Testing Equipment

- oil/water interface probe
- bailer
- bucket(s)
- clock
- log book
- pencil

The following steps outline the test procedure:

1. Measure and record the stabilized water/product levels.
2. Bail product/water from well. Bailing should continue until all the product is removed from well bore or until it reaches a constant thickness in bailer after numerous bailer volumes are removed.
3. Record the rising water/product interface levels with time while retrieving the probe. Then record the top of product level. Be consistent with recording the levels, that is, always take top of product reading first then take water/product interface. Timing begins upon taking the first reading. Table 3 lists suggested measuring chronology:

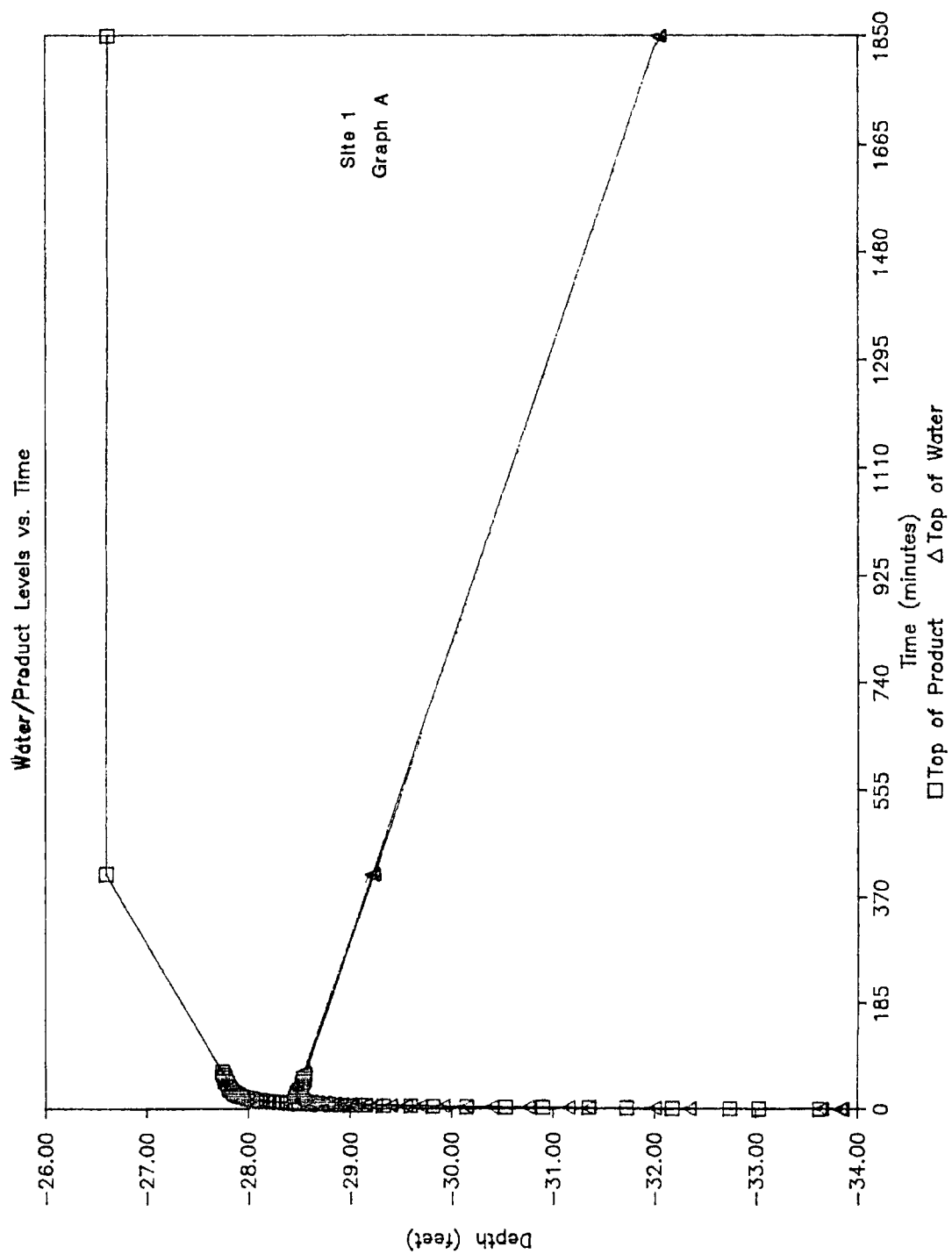
Table 3
Suggesting Reading Frequency

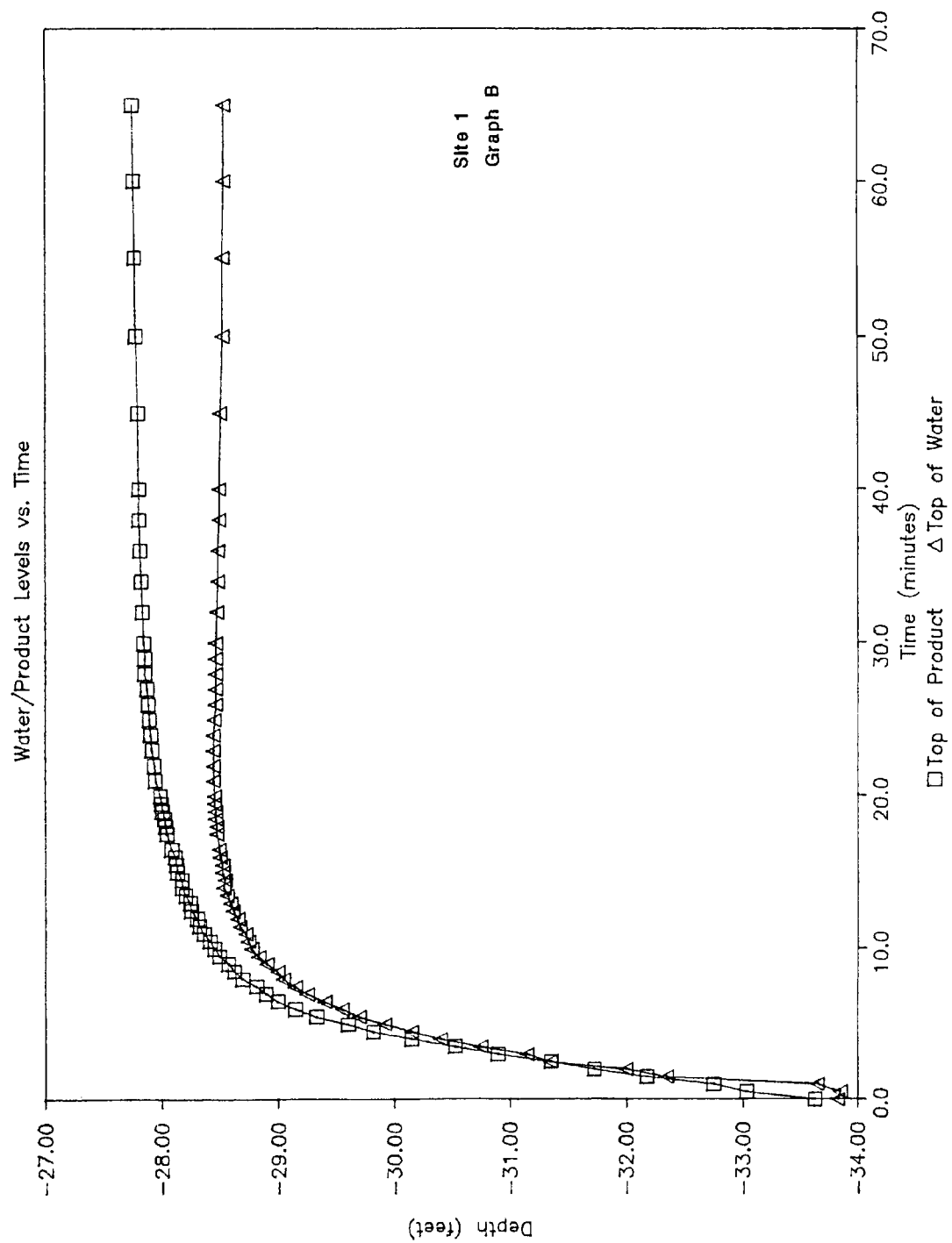
<u>Test Interval</u> (minutes)	<u>Reading Frequency</u> (minutes)
0 - 5	30 sec.
5 - 10	1
10 - 30	2
30 - 60	5
60 - 180	10
180+	As necessary to define slope

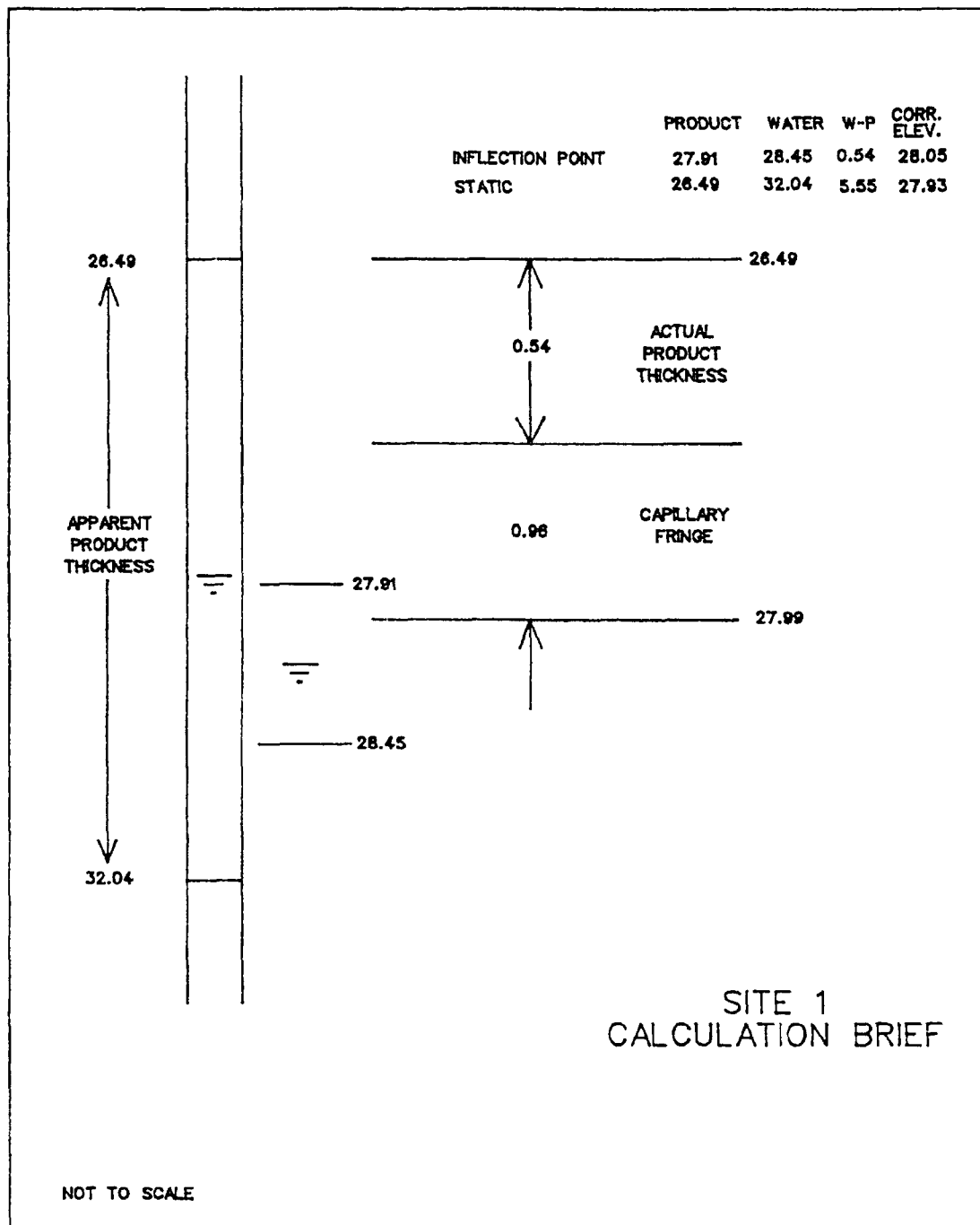
4. Graph water/product levels vs. time.
5. Observe the slope of water/product interface line and determine inflection point.
6. Determine water level in test well using water levels from monitor wells without any product accumulation or correct elevation by accounting for difference in specific gravity.
7. Measure difference between product line and water/product interface line at inflection point. This is the actual product thickness.
8. Determine the difference between water/product interface level at time of inflection and the stabilized top of product level. This is the sum of the actual product thickness and capillary fringe.
9. Subtract the measurement in 8 from measurement in 7 to obtain height of capillary fringe.

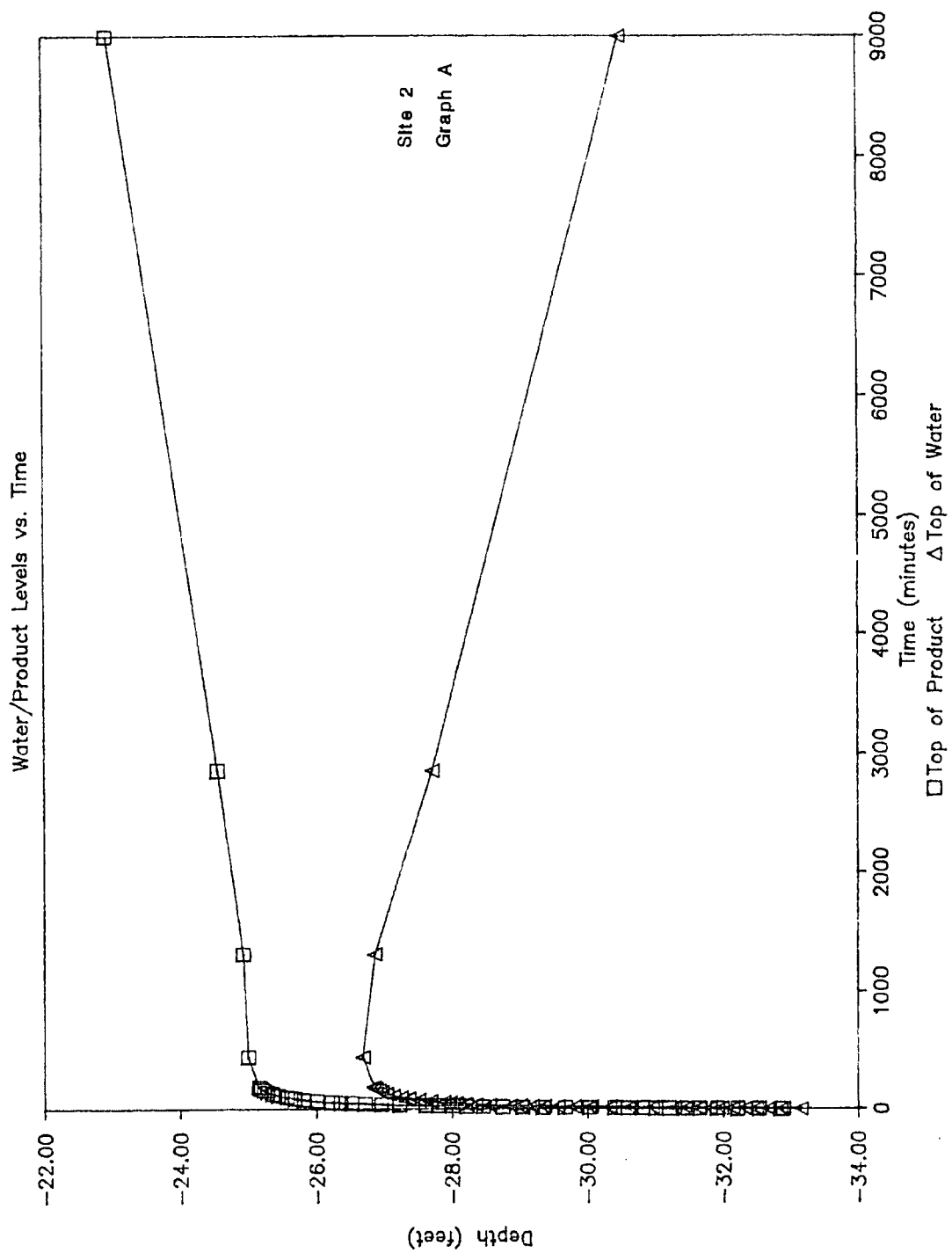
TEST RESULTS

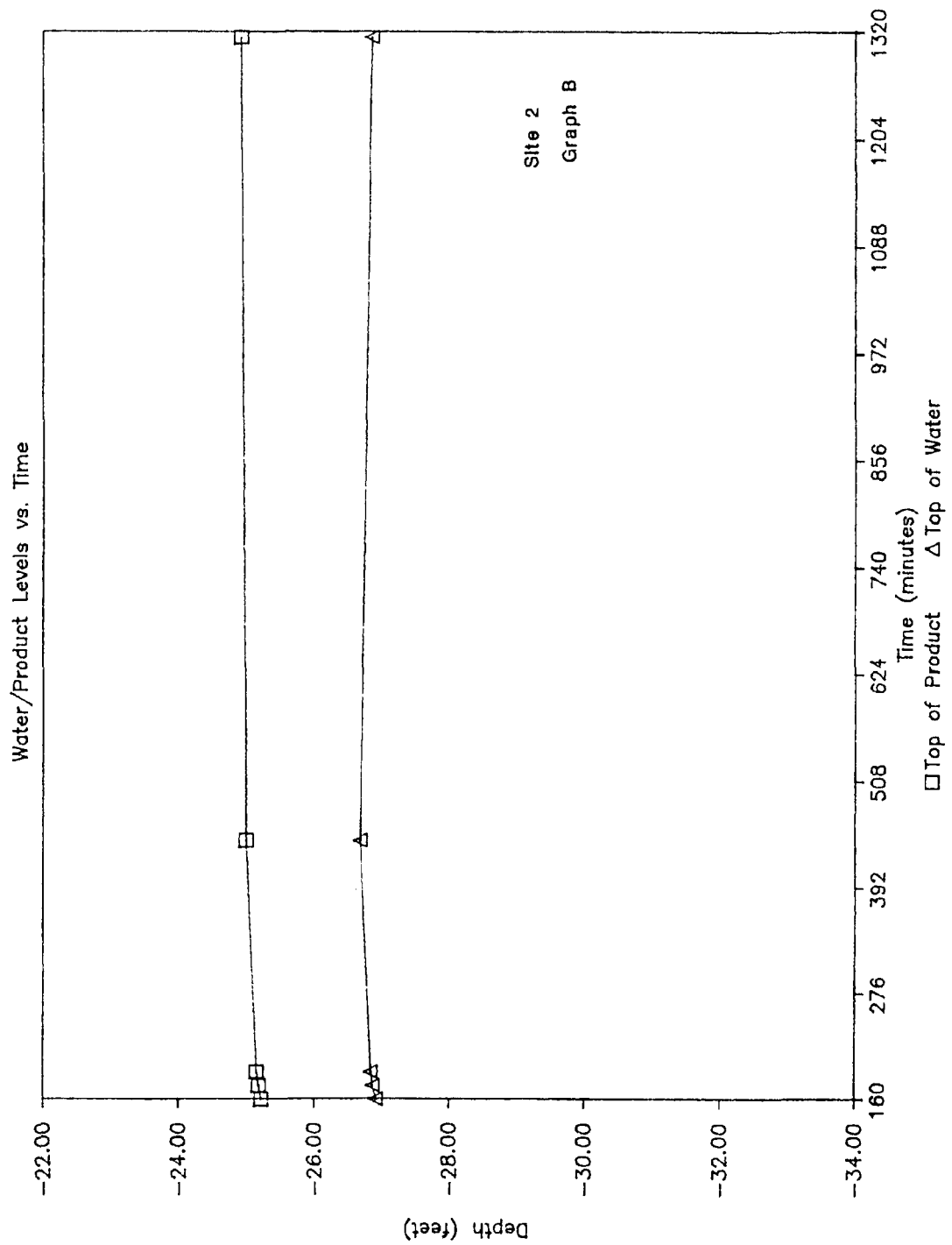
Please refer to the corresponding graphs and calculation brief for each of the four sites. As can be seen from the 'A' graphs, the top of product in the well bore continues to rise with time. However, the water/product interface rises and then starts to fall. The 'B' graphs are an enlarged section of the 'A' graphs illustrates changing from a positive to a negative slope. These site graphs indicate an inflection point prior to the stabilization of the water product levels, and as such they are considered type two curves.

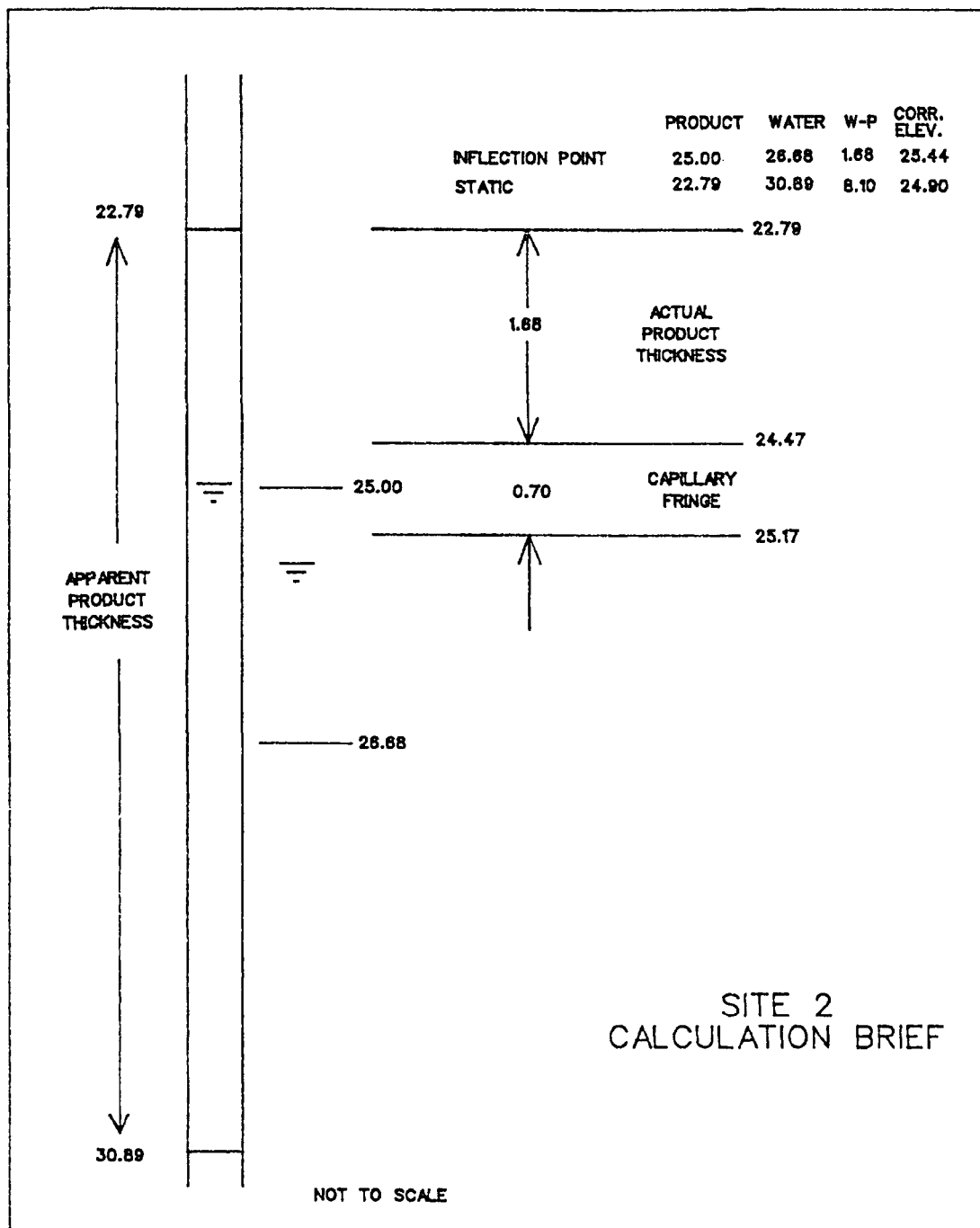


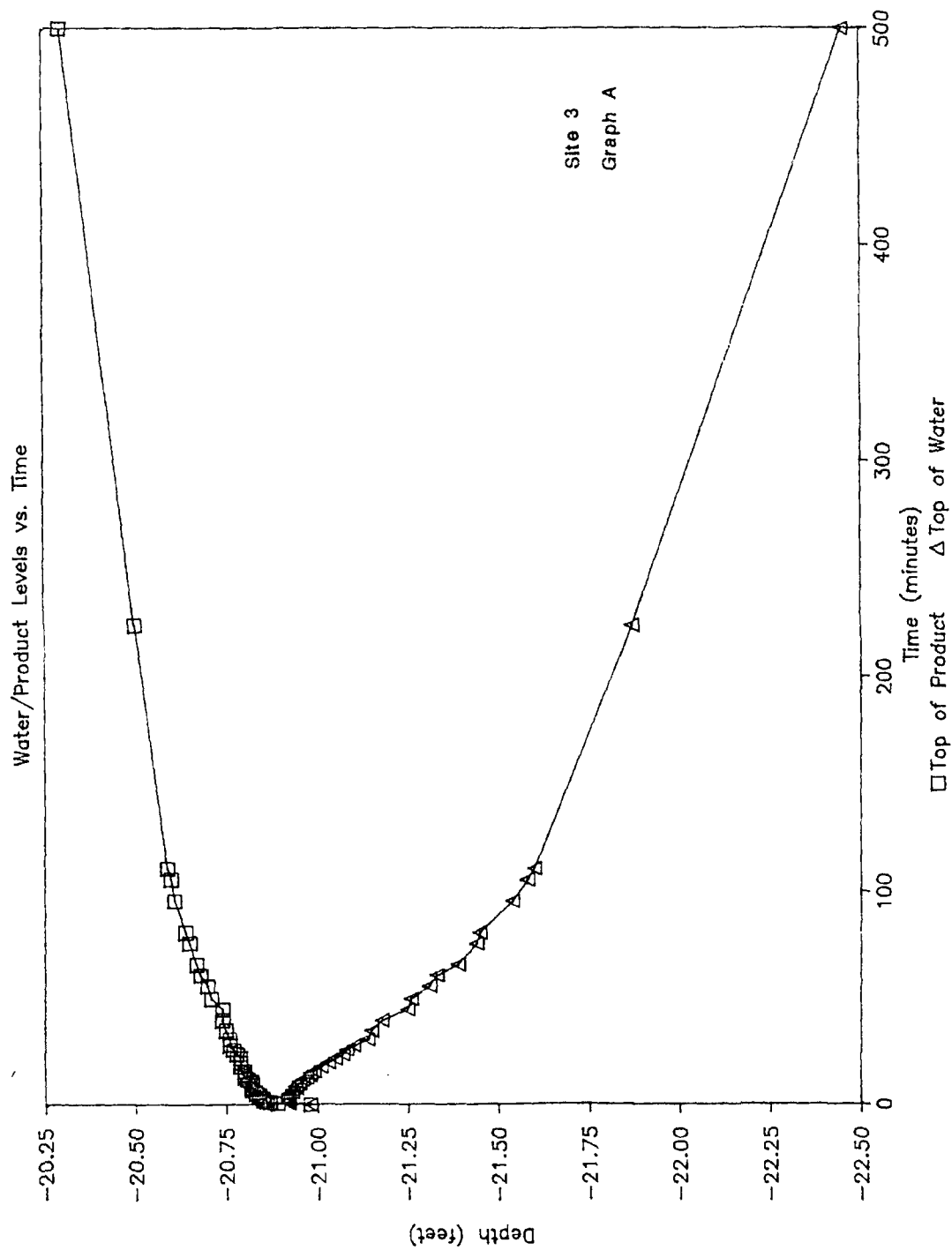


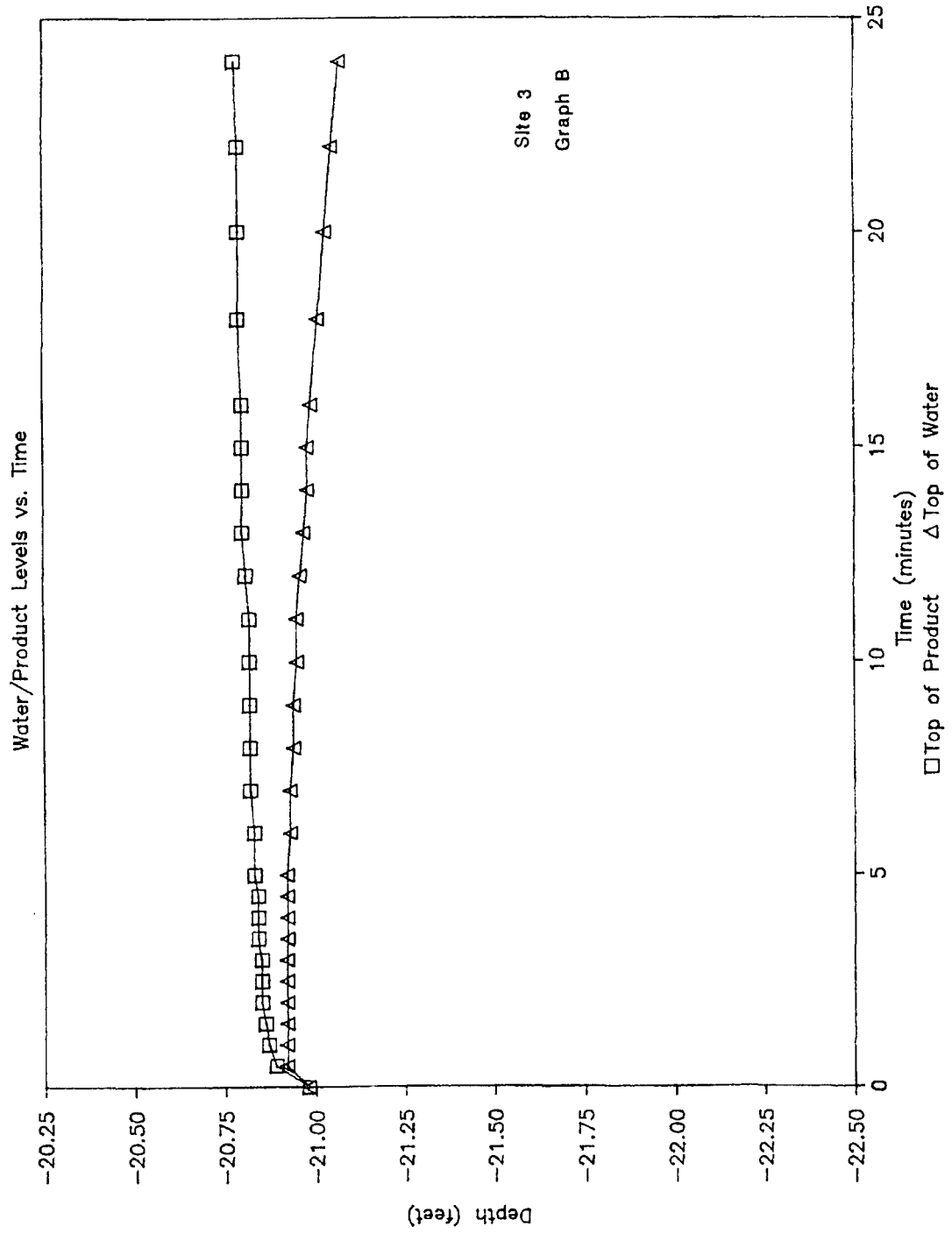


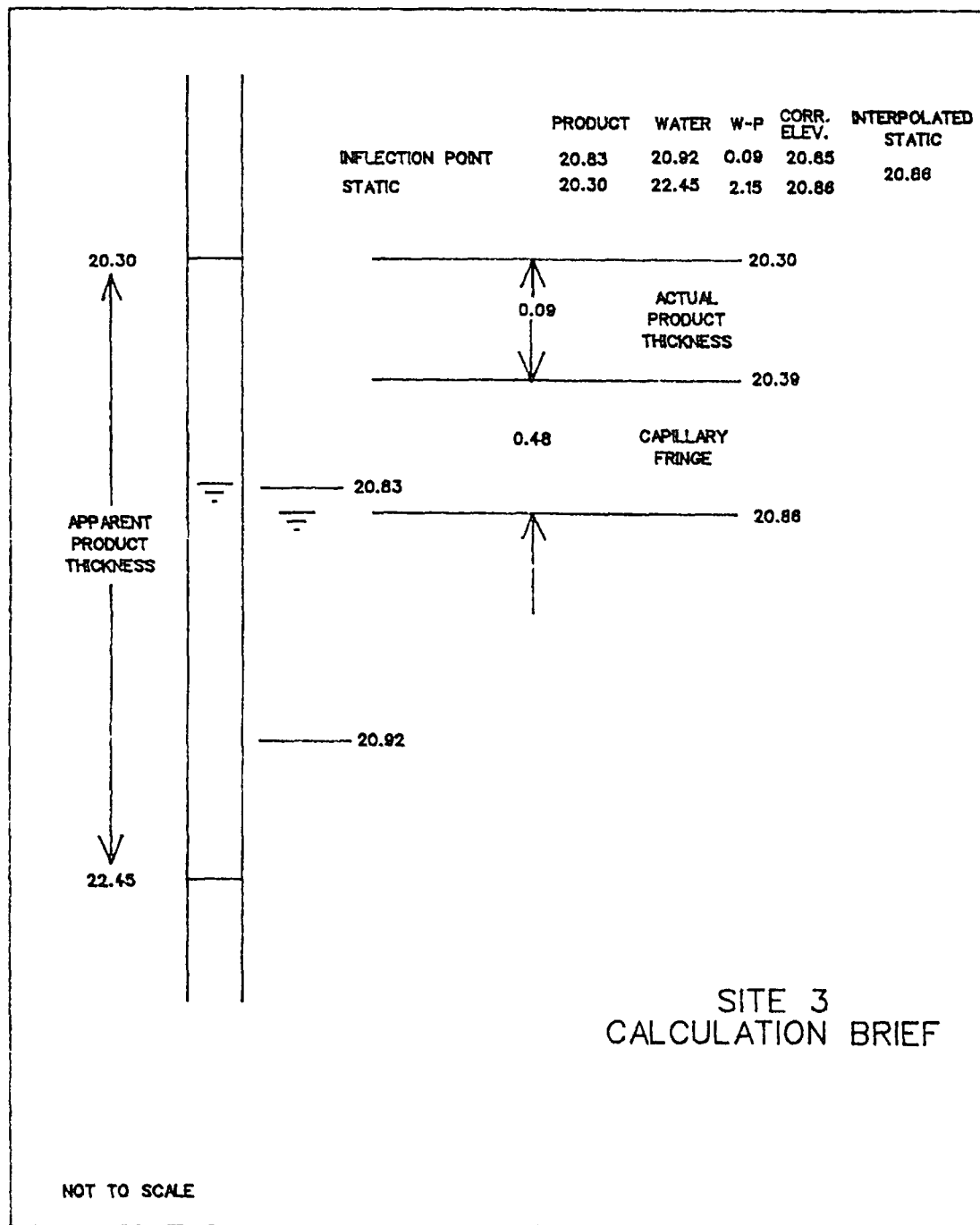


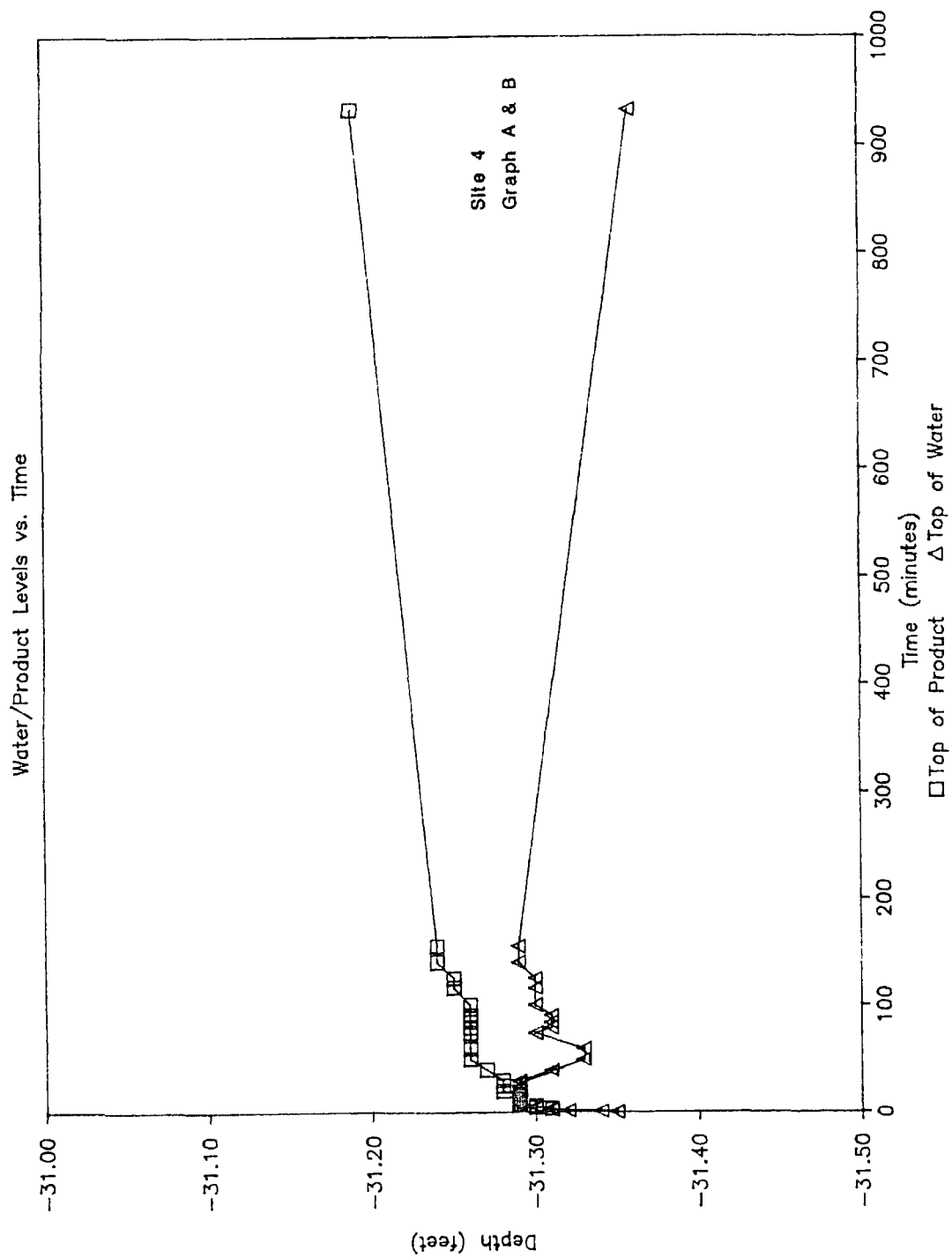


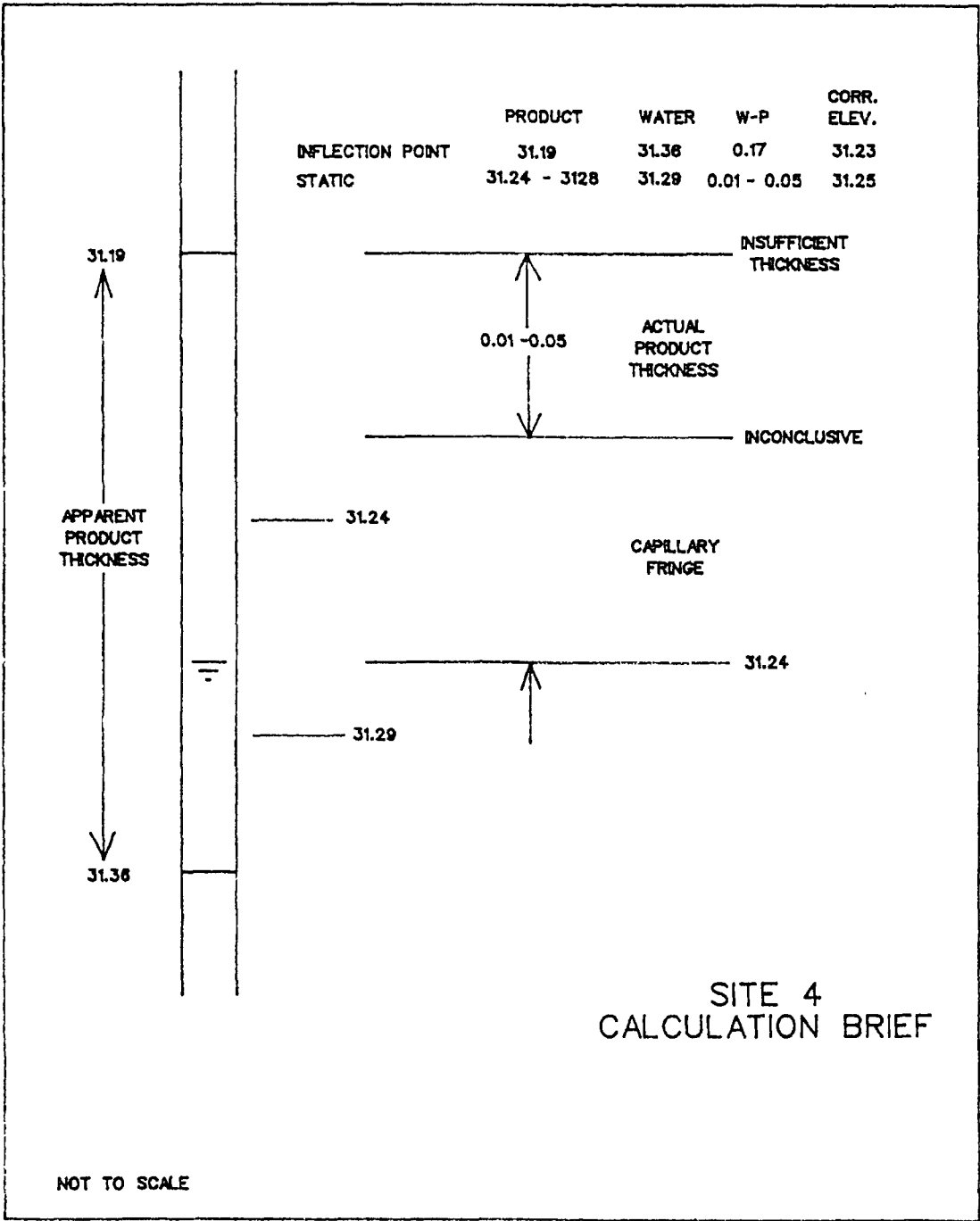












SITE 4
CALCULATION BRIEF

DISCUSSION

Type one curves are characterized by both a rising water/product interface and a rising top of product level. Both a rising water/product interface and a rising top of product level would indicate that the thickness recorded in the monitor well is an actual formation thickness.

Type one curves were observed in original testing. However, subsequent testing performed on the monitor wells with more emphasis on complete bailing of the product from the wells caused a classification change. Since these wells now showed the characteristic rise and fall of water/product elevations observed for the type two curves. Site four is an example of the classification change from type one to type two.

The author maintains that it is possible for this type curve to be observed in sandy aquifers, that is those with a very small capillary fringe. Thus, the concept of a type one curve is still included here.

Type two curves are characterized by a rising product level and a water level that first rises then falls. The point where the water level starts to fall is referred to as the inflection point. The product thickness at this point is the actual product thickness. The stabilized water and product levels that occur after this point is referred to as a psuedoequilibrium.

The four test sites presented here have shown the rise and fall of the water/product interface characterized as Type 2 curve. The inflection point have been shown to correlate with the water table in the vicinity of the well bore from stabilized water/product readings. This water table was interpolated from monitor wells without an accumulation of product on site (Site 3) and interpolated to the test well using the calculated hydraulic gradient. The water table was also calculated by correcting for the difference in specific gravities between the product and water in the well bore. The specific gravity of the product was measured to be 0.74 at Site 1. However, the specific gravity of the product on sites two, three and four was not checked, but was assumed to be 0.74 as the product type was similar. In all sites the water was found to rise to this calculated value, then fall.

The apparent product thickness that is commonly measured during monitoring a site is actually a psuedoequilibrium. This would be the region to the extreme right of the 'A' graphs. This psuedoequilibrium is caused by the drainage of product off of the capillary fringe and the depression of the water in the well bore. The drainage of the product is a result of the head difference between the water table in the well bore and the top of capillary fringe that is supporting the product layer. The depression of the water in the well bore after the inflection point is a result of the difference in specific gravity of two immiscible fluids.

The author maintains that the difference in the actual water table, which has been shown to correlate with the observed inflection point, and the top of the stabilized product level is the sum of the actual formation thickness and the height of the capillary fringe. The soil type across the screened interval at all of the sites presented was generally classified as a fine sand. The values determined for the capillary fringe by this method appear to be reasonable values. An argument could be made that this measurement is the actual product thickness, but this would assume that no capillary fringe exists.

The actual thickness occurring at the inflection point can be explained by comparing the effective permeability values of the two fluids. The effective permeability value is compared rather than the relative permeability value using the assumption that the flow is occurring through separate layers, each of which is assumed to be 100% saturated with the particular fluid phase.

There will be some pendular water remaining in the product layer, which will tend to retard flow. This pendular water will be ignored in order to provide a relative comparison of the effective permeability values.

Given that the fluid phases are considered independent of each other and immiscible, Darcy's Law can be applied to each phase. Thus, Darcy's Law can be rearranged as follows:

$$V = (-k/u) (dP/ds - DG(dz/ds))$$

where: V = Volume flux across unit area in unit time along flow path

K = Intrinsic permeability of medium

U = Viscosity of the fluid

dP/ds = Pressure gradient along flow path

dz/ds = Hydraulic gradient along flow path

D = Density of fluid

G = Acceleration of gravity

The hydraulic gradient and pressure are considered to be small, so that the viscosity of the fluid is the controlling factor in this flow regime. Water has a greater viscosity (kinematic viscosity of 1.217 EE-5 ft 2/sec at STP) than regular gasoline, (kinematic viscosity of 0.73 EE-5 ft 2/sec at STP). Since the viscosity is inversely proportional to the volume flux, the volume flux of the product (gasoline) will be greater than the volume flux of water. In reality, however, the pendular water saturation will tend to reduce the flux of product. As such, the volume flux of product may not be greater than the volume flux of water. Under the assumptions, however, they should be on the same order of magnitude. Since the water has been shown to rise to the actual water table at the inflection point, it follows that sufficient time has passed for this to occur. Given that the water has had

time to reach equilibrium in the well bore, it also follows that the product has had sufficient time to enter the well bore, provided that the volume flux of water is on the same order of magnitude as the product provides. As such, the product accumulation measured at the inflection point is a reasonable estimate of the actual formation thickness.

SUMMARY

Bailing product from a monitor well and recording the recharge of the water and product levels shows that the water will rise then fall. If the product thickness at the point where the water table begins to fall (inflection point) is measured, an actual formation product thickness can be obtained. The increase in product thickness after this point is a result of the product continuing to drain off of the capillary fringe, which is supporting the product. The distance between the inflection point and the measured stabilized top of product readings is the sum of the capillary fringe and the actual formation thickness.

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BIOGRAPHICAL SKETCH

Thomas S. Gruszczenski received his B.S. in Petroleum Engineering from West Virginia University. He is an Engineer in Training and is employed with S&ME, Inc. in Atlanta, Georgia. He is involved with various ground-water contamination investigations with an emphasis on underground storage tank problems.

FRONTIER FIELD SERVICES, LLC
Emmpire Abo Gas Plant
EM-34 Terrain Conductivity Survey

Profile:	100 North				Date:	6/4/2008
Spacing:	200 Feet				Start:	
Direction:	West to East				Stop:	
Scale:	100 mmhos/m				10:52 AM	11:09 AM
		Operator:			ML	RB
STATION	10 HD (mmhos/m)	10 VD (mmhos/m)	20 HD (mmhos/m)	20 VD (mmhos/m)	Comments	
0 East	11.3	I	16.3	I		
200 East	18.6	21.5	15.9	33.5		
400 East	I	50.7	15.3	153.3	Moved location 25 feet north due to fence	
600 East	I	58.6	42.7	I	Electric Substation approximately 25 feet NE	
800 East	9.4	13.9	13.8	21.2		
1000 East	8.1	13.6	12.7	30.1		
1200 East	12.1	14.9	12.3	28.5		

Notes:

FRONTIER FIELD SERVICES, LLC
Emmpire Abo Gas Plant
EM-34 Terrain Conductivity Survey

Profile:	200 North	Date: 6/4/2008			
Spacing:	200 Feet	Start: 08:06 AM			
Direction:	West to East	Stop: 08:28 AM			
Scale:	100 mmhos/m	Operator: ML RB			
STATION	10 HD (mmhos/m)	10 VD (mmhos/m)	20 HD (mmhos/m)	20 VD (mmhos/m)	Comments
0 East	12.0	75.4	10.7	63.6	
200 East	23.8	82.4	43.2	1	
400 East	11.5	46.6	13.4	107.2	
600 East	8.3	27.8	11.2	79.2	
800 East	11.0	40.4	18.0	150.6	Overhead power lines west and south
1000 East	8.8	111.3	34.3	195.4	Overhead power lines south
1200 East	15.4	75.5	31.2	1	Overhead power lines south and west

Notes:

FRONTIER FIELD SERVICES, LLC
Emmpire Abo Gas Plant
EM-34 Terrain Conductivity Survey

Profile: 400 North **Date:** 6/4/2008
Spacing: 200 Feet **Start:** **Stop:**
Direction: East to West 08:33 AM 08:52 AM
Scale: 100 mmhos/m **Operator:** ML RB

STATION	10 HD (mmhos/m)	10 VD (mmhos/m)	20 HD (mmhos/m)	20 VD (mmhos/m)	Comments
0 East	9.2	I	9.1	I	
200 East	16.5	27.4	9.4	11.1	
400 East	4.4	I	13.6	I	Telephone cable (N-S) approx. 2 feet east
600 East	11.4	14.3	11.4	18.2	Gas well 50 feet south and 40 feet east
800 East	6.9	15.4	8.6	40.6	Overhead power line approx. 10 feet west
1000 East	6.1	12.5	8.8	22.6	
1200 East	5.5	10.8	7.3	15.3	

Notes:

FRONTIER FIELD SERVICES, LLC
Empire Abo Gas Plant
EM-34 Terrain Conductivity Survey

Profile:		600 North		Date:		6/4/2008	
Spacing:		200 Feet		Start:		Stop:	
Direction:		West to East		08:55 AM		09:38 AM	
Scale:		100 mmhos/m		Operator:		ML RB	
STATION	10 HD (mmhos/m)	10 VD (mmhos/m)	20 HD (mmhos/m)	20 VD (mmhos/m)	Comments		
0 East	7.2	I	10.0	I			
200 East	11.8	11.4	11.4	12.2			
400 East	19.2	32.5	16.8	29.4			
600 East	12.6	I	11.0	I			
800 East	8.3	I	9.3	I	Overhead power (N-S) approx. 1 foot west		
1000 East	10.0	18.8	10.7	19.3			
1200 East	7.0	32.3	7.0	I	Pipeline (NW-SE) approx. 20 feet east		

Notes:

FRONTIER FIELD SERVICES, LLC
Emmpire Abo Gas Plant
EM-34 Terrain Conductivity Survey

Profile:	800 North	Date:	6/4/2008		
Spacing:	200 Feet	Start:	Stop:		
Direction:	East to West	09:40 AM	10:00 AM		
Scale:	100 mmhos/m	Operator:	ML RB		
STATION	10 HD (mmhos/m)	10 VD (mmhos/m)	20 HD (mmhos/m)	20 VD (mmhos/m)	Comments
0 East	91.1	1	76.9	1	Pipeline (N-S) approx. 10 feet east
200 East	8.4	21.0	10.5	42.1	
400 East	11.1	29.2	10.6	59.3	N-S Reading
600 East	8.6	17.8	9.7	32.5	Pipeline station - moved location 40 feet N
800 East	6.8	10.4	8.8	11.6	Overhead power (N-S) approx. 10 feet west
1000 East	7.1	26.7	4.9	118.4	
1200 East	13.3	10.3	9.4	11.2	

Notes: