East Hobbs San Andres Unit

Water Compatiability Testing

Unit Produced Water is 11850 City Water is 57773

Mixed Water Analysis Report

Mixes at 100°F and 0 psi

| | | P | Predictions of Saturation Index and Amount of Scale in lb/1000bbl | | | | | | | | | |
|------------------------------|-------|------------------------------|---|--|--------|--------------------------------|--------|--------------------------------|--------|-----------------------------|--------|--------------------------|
| Mixes of 11859 and 57773. | | Calcite CaCO ₃ | | Gypsum CaSO ₄ •2H ₂ O | | Anhydrite CaSO ₄ | | Celestite SrSO ₄ | | Barite BaSO ₄ | | CO ₂ Fugacity |
| 11859 | 57773 | Index | Amount | Index | Amount | Index | Amount | Index | Amount | Index | Amount | psi |
| | 100% | 0.09 | 1.8 | -1.56 | | -1.57 | | N/A | | N/A | | 0.2 |
| 1% | 99% | -0.05 | | -1.51 | - 1 | -1.52 | | -2.35 | | -1.27 | | |
| 2% | 98% | -0.13 | - 1 | -1.47 | | -1.47 | | -2.03 | | -0.95 | | 0.4 |
| 3% | 97% | -0 18 | - 1 | -1.43 | | -1.43 | | -1.84 | | -0.77 | | 0.5 |
| 5% | 95% | -0 24 | | -1.35 | | -1.36 | - 1 | -1.60 | | -0.52 | | 0.8 |
| 10% | 90% | -0 28 | | -1.21 | | -1 21 | | -1.27 | | -0.18 | | 1.4 |
| 15% | 85% | -0.26 | | -1.09 | - 1 | -1.10 | | -1.07 | | 0.02 | 0.00 | 2.0 |
| 20% | 80% | -0 23 | | -1.00 | 1 | -1.01 | | 0.92 | | 0.17 | 0.01 | 2.6 |
| 25% | 75% | -0 19 | | -0.93 | | -0.93 | | -0.81 | 1 | 0.28 | 0.02 | 3.2 |
| 30% | 70% | -0 16 | | -0.86 | | -0.86 | - 1 | -0.72 | 1 | 0.38 | 0.03 | 3.9 |
| 40% | 60% | -0 09 | | -0.75 | | -0.75 | | -0.57 | | 0.52 | 0.05 | 5.1 |
| 50% | 50% | -0.02 | | -0.66 | | -0.67 | | -0.46 | | 0.64 | 0.07 | 6.4 |
| 60% | 40% | 0.04 | 7.8 | -0.59 | 1 | -0.59 | | -0.37 | | 0.73 | 0.09 | 7.7 |
| 70% | 30% | 0.09 | 20.8 | -0.53 | - | -0.53 | | -0.30 | | 0.81 | 0.11 | 9.0 |
| 75% | 25% | 0.12 | 27.8 | -0.50 | | -0.50 | | -0.26 | 1 | 0.84 | 0.11 | 9.6 |
| 80% | 20% | 0.14 | 35.2 | -0.47 | | -0.47 | | -0.23 | | 0.88 | 0.12 | 10. |
| 85% | 15% | 0.16 | 42.8 | -0.45 | | -0.44 | | -0.20 | | 0.91 | 0.13 | 111 |
| 90% | 10% | 0.18 | 50.7 | -0.42 | | -0.42 | | -0.17 | | 0.94 | 0.14 | 11 (|
| 95% | 5% | 0.21 | 58.8 | -0.40 | - 1 | -0.40 | 1 | -0.14 | | 0.96 | 0.15 | |
| 97% | 3% | 0.21 | 62.1 | -0 39 | | -0.39 | | -0.13 | - 1 | 0.97 | 0.15 | 12.6 |
| 98% | 2% | 0.22 | 63.8 | -0.39 | | -0.38 | | -0.13 | - 1 | 0.98 | 0.16 | 12 |
| 99% | 1% | 0.22 | 65.5 | -0.38 | | -0 38 | 1 | -0.12 | | 0.98 | 0.16 | 12 8 |
| 100% | | 0.23 | 67.1 | -0.38 | | -0.37 | | -0.12 | | 0.99 | 0.16 | 13 (|

Precipitation of each scale is considered separately; total scale will be less than the sum of the amounts of the five scales,

The amount of scale indicates the severity of the problem; the index (equivalent to Stiff Davis SI) indicates how difficult it is to control the problem.

The CO, fugacity is calculated. Under usual conditions it is essentially the same as the CO partial pressure.

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