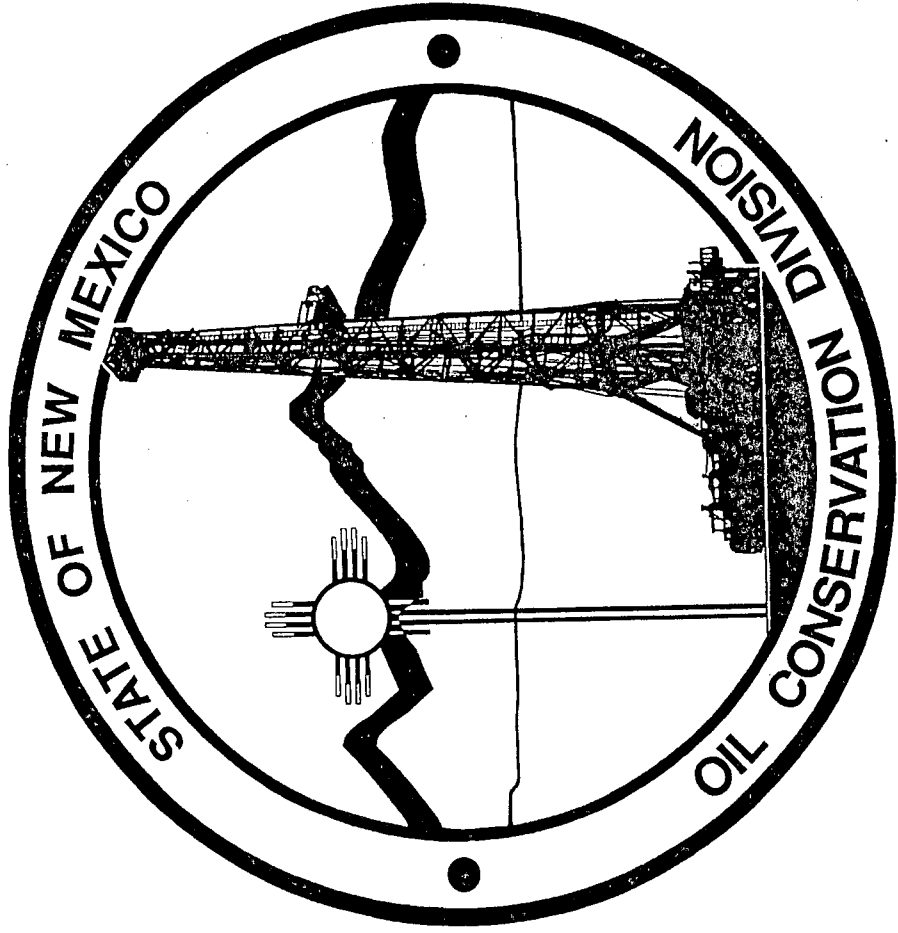
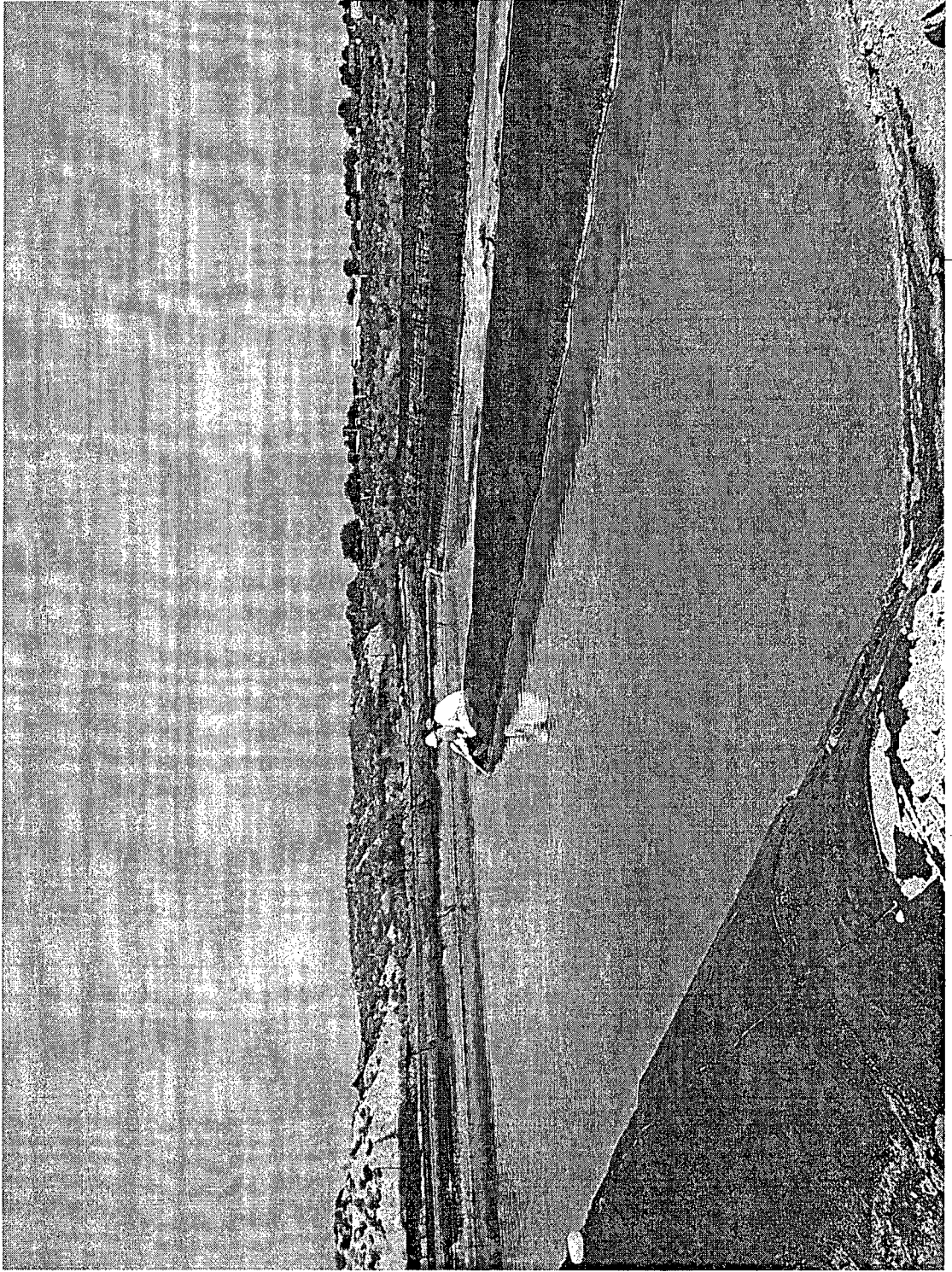


CASE NO. 14015  
OCD EXHIBIT 9



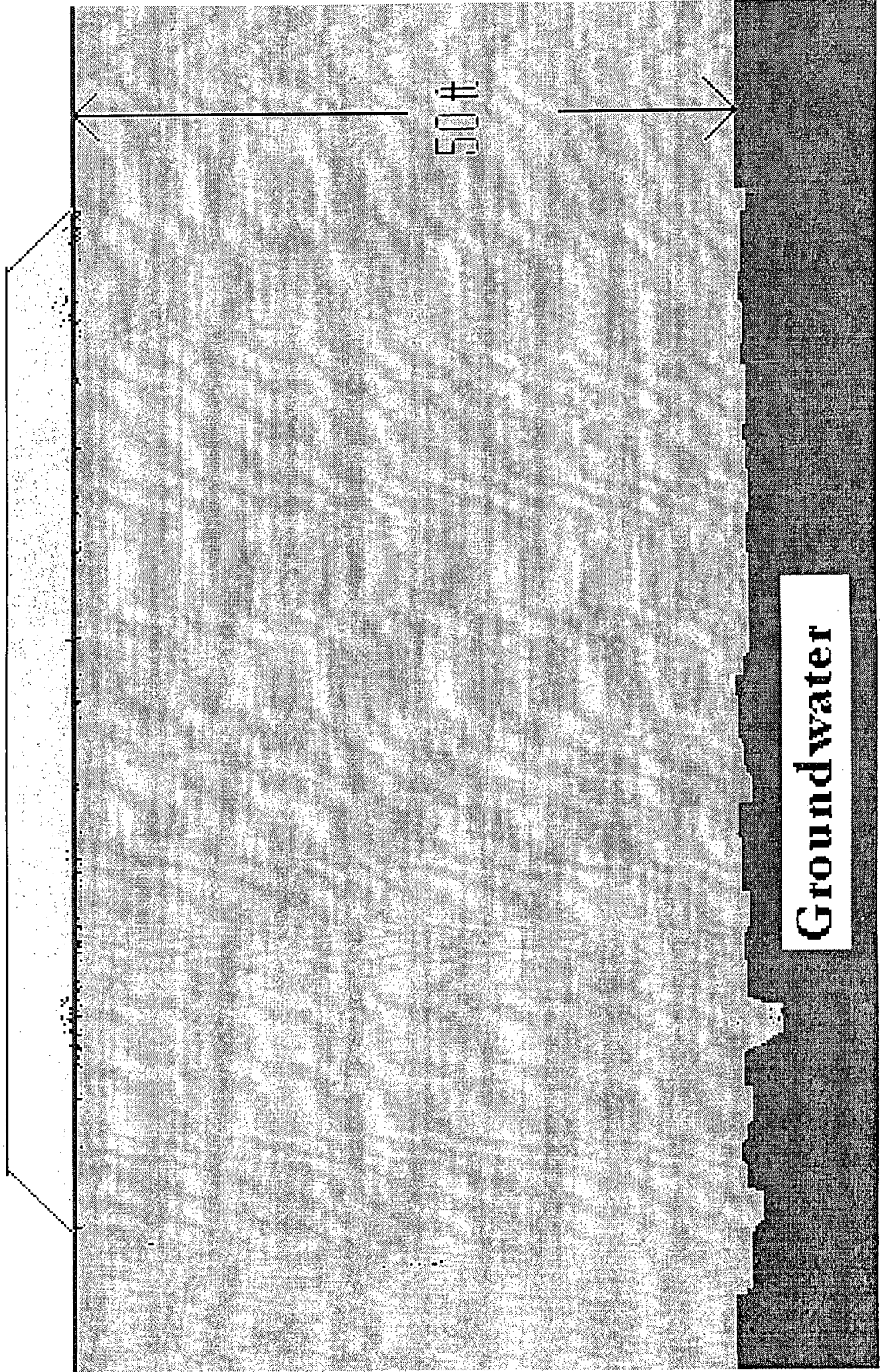
**New Siting Requirement**  
**No Pits within 50 ft of Groundwater**



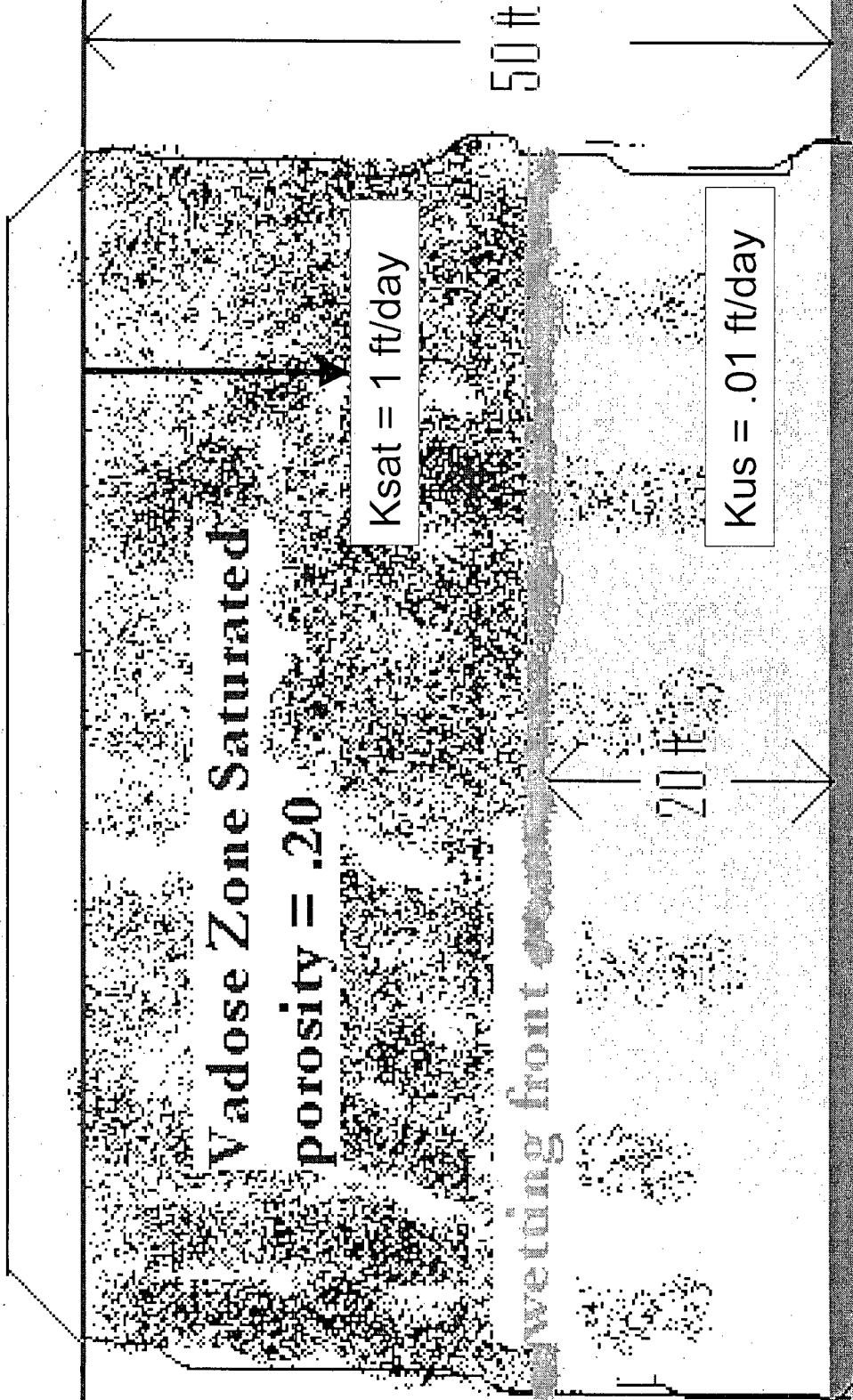
## Pit Failure Scenario

- Drilling pit catastrophic liner failure
- Vadose zone as a *temporary* Safety Net
- Basic hydrology principals and practices

# 150'x150'x6' Drilling Pit



# 150'x150' Drilling Pit



Vadose Zone Saturated  
porosity = .20

$K_{sat} = 1 \text{ ft/day}$

$K_{us} = .01 \text{ ft/day}$

50 ft

20 ft

wetting front

Groundwater

$K$ (cm/s)	$10^2$	$10^1$	$10^0 = 1$	$10^{-1}$	$10^{-2}$	$10^{-3}$	$10^{-4}$	$10^{-5}$	$10^{-6}$	$10^{-7}$	$10^{-8}$	$10^{-9}$	$10^{-10}$
$K$ (ft/day)	$10^5$	10,000	1,000	100	10	1	0.1	0.01	0.001	0.0001	$10^{-5}$	$10^{-6}$	$10^{-7}$
Relative Permeability	Pervious				<u>Semi-Pervious</u>				Impervious				
<u>Aquifer</u>	Good				Poor				None				
Unconsolidated Sand & Gravel	Well Sorted Gravel	Well Sorted Sand or Sand & Gravel		Very Fine Sand, Silt, Loess, Loam									
Unconsolidated Clay & Organic	Peat				Layered Clay				Fat / Unweathered Clay				
Consolidated Rocks	Highly Fractured Rocks	Oil Reservoir Rocks	Fresh Sandstone	Fresh Limestone	Fresh Granite								

## Porosity Ranges for Sediments

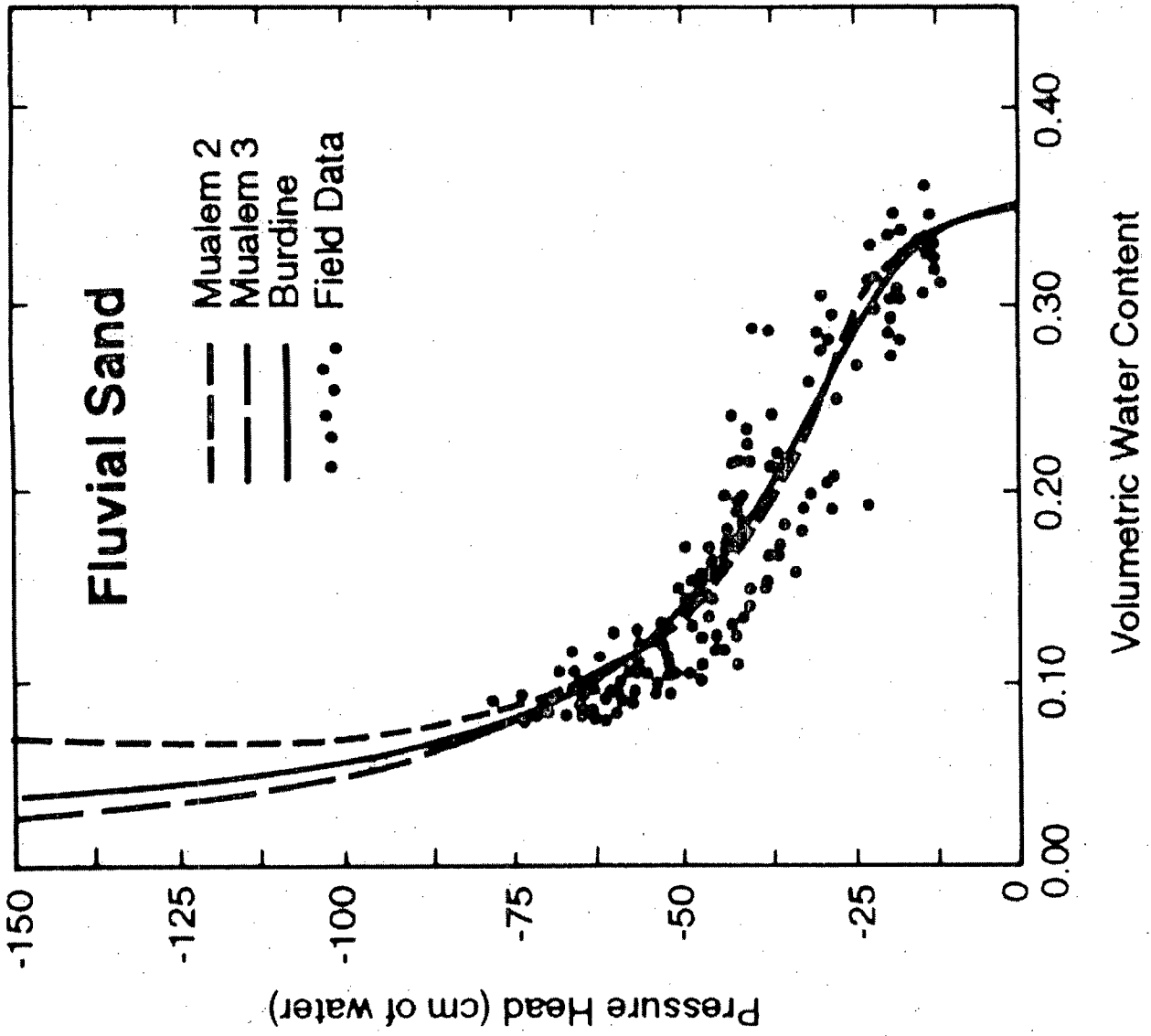
Material	Porosity (%)
well-sorted sand or gravel	25-50
sand and gravel, mixed	20-35
glacial till	10-20
silt	35-50
clay	33-60
(Based on Meinzer (1923a); Davis (1969); Cohen (1965); and MacCary and Lambert (1962) as quoted by C.W. Fetter <sup>2</sup> )	

# Permeability for Sediments

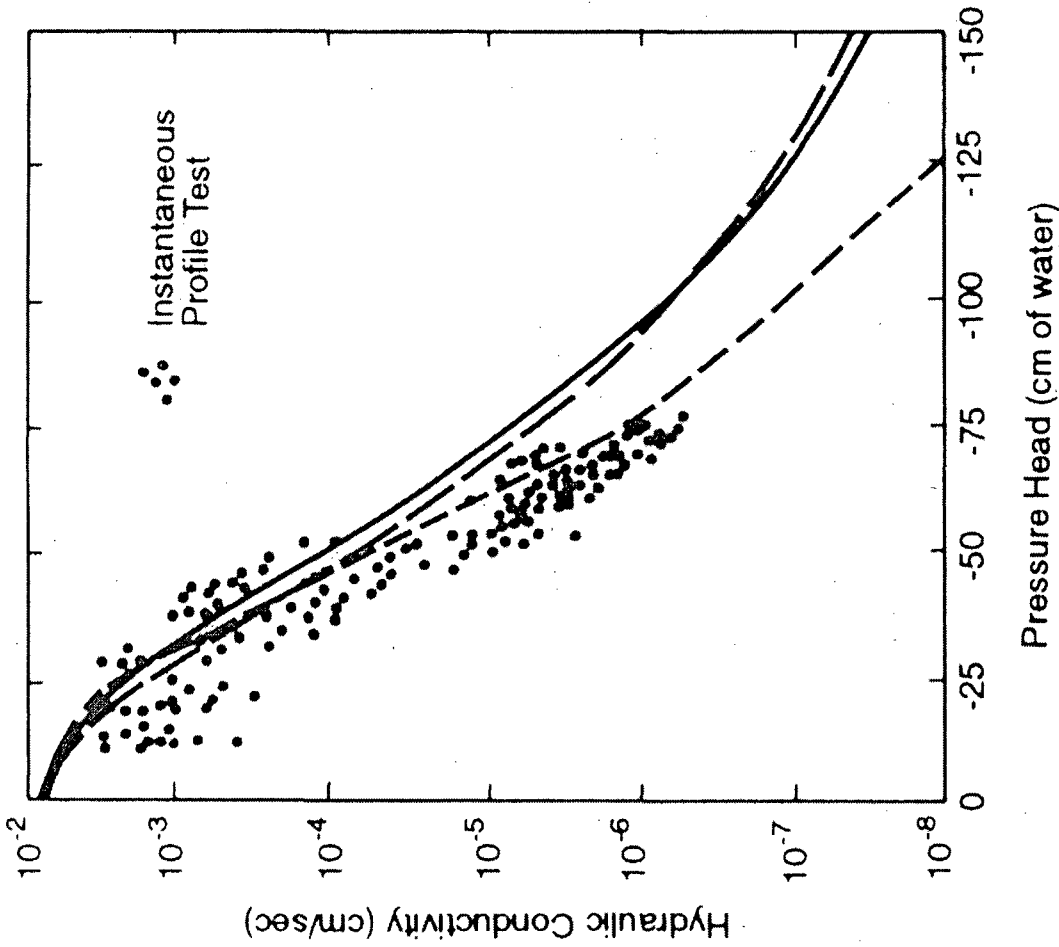
Material	Permeability or Hydraulic Conductivity (cm/s)
well-sorted gravel	$10^{-2}$ to 1
well-sorted sands, glacial outwash	$10^{-3}$ to $10^{-1}$
silty sands, fine sands	$10^{-5}$ to $10^{-3}$
silt, sandy silts, clayey sands, till	$10^{-6}$ to $10^{-4}$
clay	$10^{-9}$ to $10^{-6}$
(C.W. Fetter <sup>2</sup> )	



A

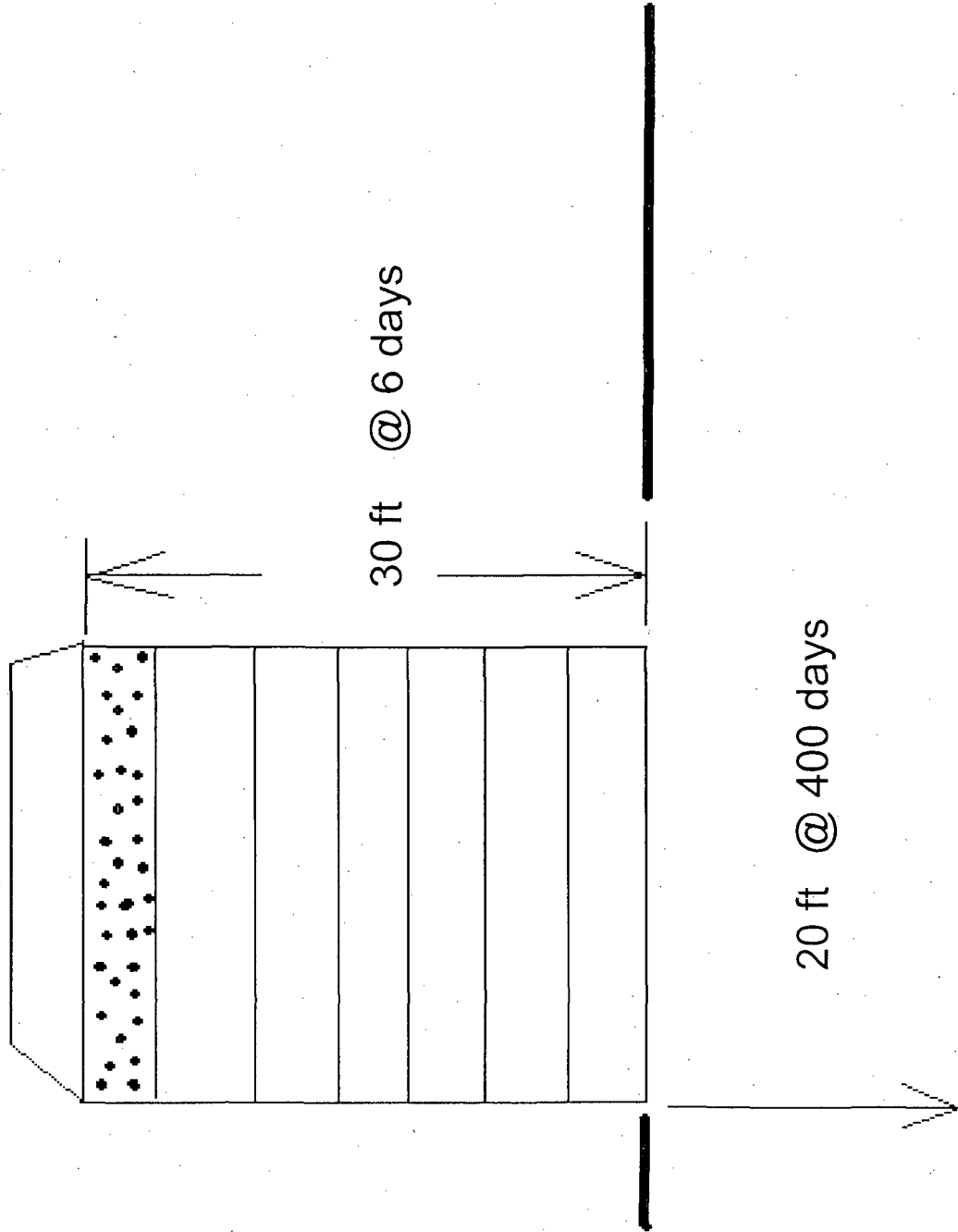


B



(A) Field-measured soil-water retention data (from tensiometers and neutron probes) and nonlinear least-squares fits with SOHYP. (B) Field-measured and calculated hydraulic conductivity. (From Stephens, 1992. With permission.)

# Estimated time of fluid movement



# Time Calculations of Fluid Movement

- $Q = KiA$

$$V = (K^* I)/\eta$$

- How long would it take for fluid to reach 30 feet in saturated zone with  $K_{sat} = 1$  ft/day and  $I = 1$ ?
- $V = \{[1 \text{ ft/day} * 1] / 0.2\} = 5$  ft/day
- $V = 5$  ft/day
- It would take **6 days** at 0.2% porosity with a conductivity of 1 ft/day to reach 30 feet below the bottom of the pit.
- How long would it take the fluid to reach 20 feet below the 30 feet barrier?
- $V = \{[0.01 \text{ ft/day} * 1] / 0.2\} = 0.05$  ft/day
- $V = 0.05$  ft/day = 0.6 inch/day = 20 days/foot
- It would take **400 days (1 year and 35 days)** for the fluid to move 20 feet below the 30 feet barrier in an unsaturated zone with a conductivity of 0.01 ft/day and a porosity of 0.2

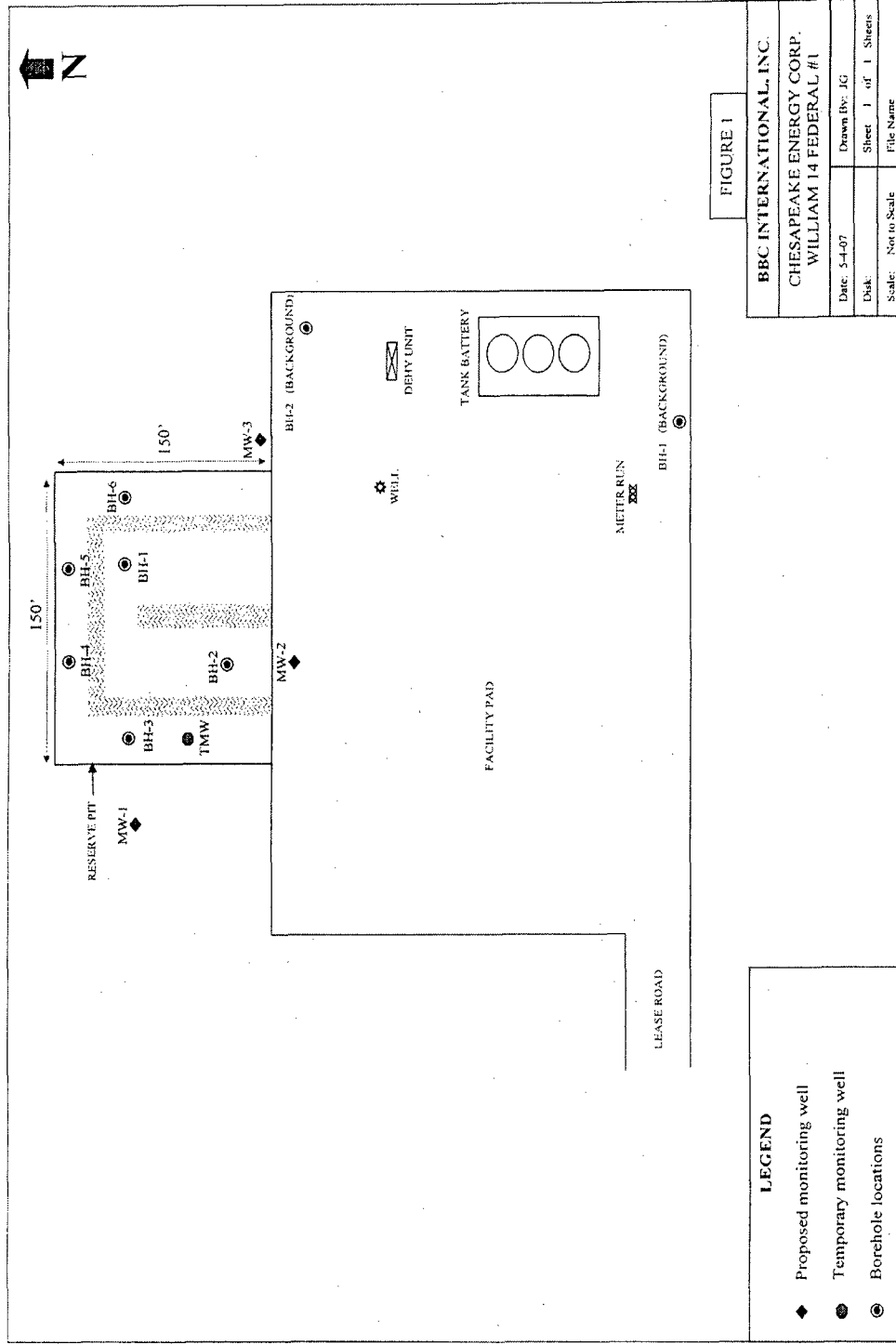
Real time example where the 50 foot safety net provided some protection-

Table 2  
 Chesapeake/Williams 14 Federal #1  
 Lea County, New Mexico  
 Boreholes Soil Samples  
 Sampled on 8/10/05 and 8/11/05

Depth (ft), BPB	Chloride Analysis (mg/kg)					
	BH-1	BH-2	BH-3	BH-4	BH-5	BH-6
0-1	2260	4540	775	3430	4410	832
5-6	3360	794	336	7060	8890	841
10-11	4620	2530	524	1970	6510	429
15-16	3100	1060	451	1620	3550	113
20-21	1110	529	561	44.5	2360	14.3
25-26	1220	795	691	14.8	2090	8.76
30-31	797	603	1010	12.3	901	12.1
35-36	788	1220	2310	12.4	197	57.9
40-41	1790	1770	5010	12.1	60.2	11.1

BPB - Below PII Bottom

# Groundwater depth 50-60 ft- Slight impact



CHLORIDE: 8/17/07 28 ppm

MW #1

(3926.53')

CHLORIDE: 2/6/07	36 ppm
CHLORIDE: 2/14/07	32 ppm
CHLORIDE: 8/21/07	44 ppm

TEMP - MW  
(3926.30')

0.01 F/FT

EXISTING PIT

MW #3

(3925.75')

CHLORIDE: 8/17/07	44 ppm
CHLORIDE: 8/21/07	32 ppm

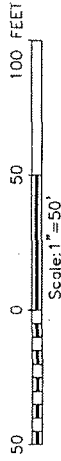
MW #2

(3924.98')

CHLORIDE: 8/17/07	28 ppm
-------------------	--------

WELL

WELL	COORDINATES	ELEVATIONS
MW #1	736151.4 N 790786.1 E	NATURAL GROUND - 3981.05' TOP OF PVC - 3984.13'
MW #2	735948.7 N 790853.7 E	NATURAL GROUND - 3979.23' TOP OF PVC - 3982.60'
MW #3	735979.4 N 791023.5 E	NATURAL GROUND - 3979.60' TOP OF PVC - 3982.60'
TEMP MW	736086.5 N 790858.1 E	NATURAL GROUND - 3971.33' TOP OF PVC - 3972.88'



BBC INTERNATIONAL, INC.

CHESAPEAKE WILLIAMS 14 FEDERAL No. 1  
SECTION 14, TOWNSHIP 15 SOUTH, RANGE 35 EAST,  
N.M.P.M., LEA COUNTY, NEW MEXICO

PROVIDING SURVEYING SERVICES  
SINCE 1948

**JOHN WEST SURVEYING COMPANY**  
412 N. DAL PASO  
HOBBES, N.M. 88240  
(505) 383-3117

Survey Date: 9/5/07	Sheet 1 of 1	Sheets
W.O. Number: 07-11-1235	Drawn By: L.A.	
Date: 9/14/07	DISK: CD#5	07111235

## “50 Foot to Groundwater Justification”

- Task Force non consensus - values ranged from 2 feet to 100 feet
- 50 feet has been an established ranking criteria since 1993
- 50 feet appeared in the non-vulnerable criteria R-7940
- New Part 36 SWMF uses 50 feet as a siting criteria for Ponds
- OCD District policies uses 50 feet as a dig & haul scenario
- 50 feet will provide industry the continued use of pits
- Will not overburden existing closed-loop systems
- New prescriptive pit design and installation requirements
- New Liner requirements minimum of 20 mil
- New Required Monitoring Requirements
- **50 feet provides a safety net in case of pit liner failures**



## *“Conclusions”*

The case for 50 foot separation

- Rule requires stringent prescriptive controls
- 50 foot separation is widely used
- 50 foot requirement would cover most sensitive areas such as river bottoms
- Rule requires de-watering in 30 days and closed in 3<sup>6</sup> months
- All pits will require sampling in vadose zone

50 foot separation?

Does Not

Term

Provide Long Groundwater

Protection of Groundwater  
Protection is available

If a source is available

50 foot separation?

*Should Provide Short Term  
Protection of Groundwater if  
new prescriptive methods are  
employed!*