

BASIN DAKOTA
SECTION 28-T28N-R10W
1st SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365°R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _{ri}	=	2,400 psi	Public Data
P _{ra}	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

RF_t = 0.8524 (fraction)

Rock Properties

Acre - Feet	=	1,615	Planimetered from net sand thickness maps
Average Porosity	=	0.09	(Fraction) \varnothing_{dn} Avg. of offsets
Water Saturation	=	0.44	(Fraction) Avg. of offsets

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1st Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356 A h_\theta (1 - S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(1,615)(0.09)(1 - 0.44)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 580 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(580)$$

$$\text{EUR}_t = 495 \text{ MMCF}$$

CROSS TIMBERS OIL COMPANY
Barry Voigt
11/13/00

BASIN DAKOTA
SECTION 28-T28N-R10W
2nd SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365 °R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _{ri}	=	2,400 psi	Public Data
P _{ra}	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

Rock Properties

Acre - Feet	=	6,102	Planimetered from net sand thickness maps
Average Porosity	=	0.12	(Fraction) \emptyset_{dn} Avg. of offsets
Water Saturation	=	0.46	(Fraction) Avg. of offsets

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2nd Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_o(1-S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(6,102)(0.12)(1-0.46)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 2,819 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(2,819)$$

$$\text{EUR}_t = 2,403 \text{ MMCF}$$

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BASIN DAKOTA
SECTION 28-T28N-R10W
3rd SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365°R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _n	=	2,400 psi	Public Data
P _n	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

Rock Properties

Acre - Feet	=	49,398	Planimetered from net sand thickness maps
Average Porosity	=	0.08	(Fraction) \varnothing_{dn} Avg. of offsets
Water Saturation	=	0.27	(Fraction) Avg. of offsets

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3rd Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_o(1-S_w)}{B_{gi}} MMCF$$

$$GIP = \frac{.04356(49,398)(0.08)(1-0.27)}{0.00611} MMCF$$

$$GIP = 20,567 \text{ MMCF}$$

$$EUR_t = RF_t \times GIP$$

$$EUR_t = (0.8524)(20,567)$$

$$EUR_t = 17,531 \text{ MMCF}$$

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