

BASIN DAKOTA  
SECTION 16-T27N-R10W  
1<sup>ST</sup> SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T <sub>c</sub>	=	365°R	Standing's Correlation
P <sub>c</sub>	=	678 psi	Standing's Correlation
T <sub>r</sub>	=	150 °F	Log Measurement
P <sub>ri</sub>	=	2,400 psi	Public Data
P <sub>ra</sub>	=	400 psi	Estimate
B <sub>gi</sub>	=	0.00611 ft <sup>3</sup> /SCF	Standing & Katz's Correlation
B <sub>ga</sub>	=	0.04139 ft <sup>3</sup> /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RFt = 1 - \frac{B_{gi}}{B_{ga}}$$

*BEFORE DIVISION BY 10*

$$RFt = 1 - \frac{0.00611}{0.04139}$$

*10*

$$RFt = 0.8524 \text{ (fraction)}$$

Rock Properties

Acre - Feet	=	9,934	Planimetered from net sand thickness maps
Average Porosity	=	0.10	(Fraction) $\emptyset_{dn}$ Avg. of offsets
Water Saturation	=	0.40	(Fraction) Avg. of offsets

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1<sup>st</sup> Sand  
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_o(1-S_w)}{B_{gi}} MMCF$$

$$GIP = \frac{.04356(9,934)(0.10)(1-0.40)}{0.00611} MMCF$$

$$GIP = 4,249 \text{ MMCF}$$

$$EUR_t = RF_t \times GIP$$

$$EUR_t = (0.8524)(4,249)$$

$$EUR_t = 3,622 \text{ MMCF}$$

CROSS TIMBERS OIL COMPANY

Barry Voigt  
11/13/00

**BASIN DAKOTA  
SECTION 16-T27N-R10W  
2<sup>nd</sup> SAND**

**Fluid Properties**

Gas Gravity	=	0.646	Gas Analysis
T <sub>c</sub>	=	365°R	Standing's Correlation
P <sub>c</sub>	=	678 psi	Standing's Correlation
T <sub>r</sub>	=	150 °F	Log Measurement
P <sub>ri</sub>	=	2,400 psi	Public Data
P <sub>ra</sub>	=	400 psi	Estimate
B <sub>gi</sub>	=	0.00611 ft <sup>3</sup> /SCF	Standing & Katz's Correlation
B <sub>ga</sub>	=	0.04139 ft <sup>3</sup> /SCF	Standing & Katz's Correlation

**Calculate Theoretical Recovery Factor:**

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

**Rock Properties**

Acre - Feet	=	6,036	Planimetered from net sand thickness maps
Average Porosity	=	0.13	(Fraction) $\emptyset_{dn}$ Avg. of offsets
Water Saturation	=	0.45	(Fraction) Avg. of offsets

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2<sup>nd</sup> Sand  
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_o(1-S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(6,036)(0.13)(1-0.45)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 3,077 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(3,077)$$

$$\text{EUR}_t = 2,623 \text{ MMCF}$$

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**BASIN DAKOTA  
SECTION 16-T27N-R10W  
3<sup>rd</sup> SAND**

**Fluid Properties**

Gas Gravity	=	0.646	Gas Analysis
T <sub>c</sub>	=	365°R	Standing's Correlation
P <sub>c</sub>	=	678 psi	Standing's Correlation
T <sub>r</sub>	=	150 °F	Log Measurement
P <sub>ri</sub>	=	2,400 psi	Public Data
P <sub>ra</sub>	=	400 psi	Estimate
B <sub>gi</sub>	=	0.00611 ft <sup>3</sup> /SCF	Standing & Katz's Correlation
B <sub>ga</sub>	=	0.04139 ft <sup>3</sup> /SCF	Standing & Katz's Correlation

**Calculate Theoretical Recovery Factor:**

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

**Rock Properties**

Acre - Feet	=	25,978	Planimetered from net sand thickness maps
Average Porosity	=	0.09	(Fraction) $\emptyset_{dn}$ Avg. of offsets
Water Saturation	=	0.39	(Fraction) Avg. of offsets

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3<sup>rd</sup> Sand  
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356 A h_\theta (1 - S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(25,978)(0.09)(1 - 0.39)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 10,168 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(10,168)$$

$$\text{EUR}_t = 8,667 \text{ MMCF}$$

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