

BASIN DAKOTA
SECTION 17-T28N-R10W
1st SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365°R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _{ri}	=	2,400 psi	Public Data
P _{ra}	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

(1)

Rock Properties

Acre - Feet	=	2,718	Planimetered from net sand thickness maps
Average Porosity	=	0.11	(Fraction) ϕ_{dn} Avg. of offsets
Water Saturation	=	0.49	(Fraction) Avg. of offsets

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1st Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356 Ah_o (1 - S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(2,718)(0.11)(1-0.49)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 1,087 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(1,087)$$

$$\text{EUR}_t = 927 \text{ MMCF}$$

CROSS TIMBERS OIL COMPANY
Barry Voigt
11/13/00

BASIN DAKOTA
SECTION 17-T28N-R10W
2nd SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365°R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _{ri}	=	2,400 psi	Public Data
P _{ra}	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

Rock Properties

Acre - Feet	=	5,451	Planimetered from net sand thickness maps
Average Porosity	=	0.11	(Fraction) \emptyset_{dn} Avg. of offsets
Water Saturation	=	0.44	(Fraction) Avg. of offsets

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2nd Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356 A h_o (1 - S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(5,451)(0.11)(1-0.44)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 2,394 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(2,394)$$

$$\text{EUR}_t = 2,041 \text{ MMCF}$$

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11/13/00

BASIN DAKOTA
SECTION 17-T28N-R10W
3rd SAND

Fluid Properties

Gas Gravity	=	0.646	Gas Analysis
T _c	=	365°R	Standing's Correlation
P _c	=	678 psi	Standing's Correlation
T _r	=	150 °F	Log Measurement
P _{ri}	=	2,400 psi	Public Data
P _{ra}	=	400 psi	Estimate
B _{gi}	=	0.00611 ft ³ /SCF	Standing & Katz's Correlation
B _{ga}	=	0.04139 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.00611}{0.04139}$$

$$RF_t = 0.8524 \text{ (fraction)}$$

Rock Properties

Acre - Feet	=	30,201	Planimetered from net sand thickness maps
Average Porosity	=	0.08	(Fraction) \emptyset_{dn} Avg. of offsets
Water Saturation	=	0.36	(Fraction) Avg. of offsets

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3rd Sand
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Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_o(1-S_w)}{B_{gi}} \text{ MMCF}$$

$$GIP = \frac{.04356(30,201)(0.08)(1-0.36)}{0.00611} \text{ MMCF}$$

$$\text{GIP} = 11,024 \text{ MMCF}$$

$$\text{EUR}_t = \text{RF}_t \times \text{GIP}$$

$$\text{EUR}_t = (0.8524)(11,024)$$

$$\text{EUR}_t = 9,397 \text{ MMCF}$$

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