

NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Wildcat Formation (Penn) Canyon Dol. County Eddy  
 Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 1/9-10/1963  
 Company Ralph Lowe Lease Indian Basin "A" Well No. 1 (Upper)  
 Unit J Sec. 22 Twp. 21S Rge. 23E Purchaser None  
 Casing 7 Wt. 26.0 I.D. 6.275 Set at 9385 Perf. 7505 To 7572  
 Tubing 2" IORD Wt. 4.70 I.D. 1.995 Set at 7280 Perf. \_\_\_\_\_ To \_\_\_\_\_  
 Gas Pay: From 7505 To 7572 L 7280 xGMix = .667 -GL 4856 Bar.Press. 13.2  
 Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Gas-Gas Dual  
 Date of Completion: 12-24-62 Packer Baker "K" 7280 Reservoir Temp. 146°F

OBSERVED DATA

Tested Through (Prover) (Orifice) (Meter) Type Taps Flange

No.	Flow Data			Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Orifice) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	
SI						2354		Over 72
1.	3.068	1.750	655	14.5	67	2306		6
2.	3.068	1.750	655	30.0	77	2256		6
3.	3.068	1.750	655	60.0	79	2184		6
4.	3.068	1.750	655	90.0	69	2018		6
5.								

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	20.15	98.43		.9933	.9721	1.063	2036
2.	20.15	141.58		.9840	.9721	1.059	2890
3.	20.15	200.23		.9822	.9721	1.059	4079
4.	20.15	245.23		.9915	.9721	1.063	5062
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio 63,331 cf/bbl. Specific Gravity Separator Gas .635  
 Gravity of Liquid Hydrocarbons 58.4 deg. Specific Gravity Flowing Fluid .7451  
 $P_c$  9.936  $(1-e^{-s})$  .284  $P_c$  2367.2  $P_c^2$  5603.5

No.	P <sub>t</sub> (psia)	P <sub>c</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	$\frac{P_w}{P_c}$
1.	2319.2	5378.7	20.23	409.3	116.2	5494.9	108.7	2344.1	.9902
2.	2269.2	5148.3	29.72	884.9	234.2	5383.5	220.1	2320.2	.9901
3.	2167.2	4696.8	40.53	1642.7	466.5	5163.3	440.3	2272.3	.9599
4.	2031.2	4125.8	50.30	2530.1	718.5	4844.3	759.3	2201.0	.9298
5.									

Absolute Potential: 14,250 MCFPD; n .600

COMPANY Ralph Lowe  
 ADDRESS P. O. Box 800, Pecos, Texas  
 AGENT and TITLE Richard P. Jew Mobile P. Service, Petroleum Engineer  
 WITNESSED \_\_\_\_\_  
 COMPANY \_\_\_\_\_

REMARKS Corrections: 7505-7517

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .