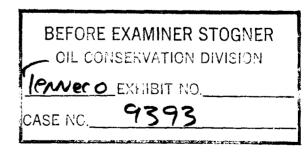
TENNECO OIL COMPANY Exhibits Case 9393 Blanco Mesaverde Gas Pool San Juan County, New Mexico

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Application for Well-head Price Ceiling Category Determination for certain infill wells, for exception to order R-1670-T, and exceptions from well location requirements.



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KELLAHIN, KELLAHIN AND AUBREY

W. Thomas Kellahin Karen Aubrey

Jason Kellahin Of Counsel Attorneys at Law El Patio - 117 North Guadalupe Post Office Box 2265 Santa Fe, New Mexico 87504-2265 May 2, 1988

Telephone 982-4285 Area Code 505

Mr. William J. LeMay Oil Conservation Commission P. O. Box 2088 Santa Fe, New Mexico 87504

"Hand Delivered"

Re: Tenneco Oil Company for Well-Head Price Ceiling Category Determination for certain Infill Wells, for Exception to Order R-1670-T, and for Well Location Requirements, Blanco Mesa-Verde Gas Pool, San Juan County, New Mexico

Dear Mr. LeMay:

On behalf of Tenneco Oil Company, please set the enclosed application for hearing on the next available examiner's docket now set for May 25, 1988.

By copy of this letter and application sent certified mail return-receipt to all offset operators, we are notifying each of them of the right to appear at the hearing either in support or in opposition to this application. Should any such party desire more information about this matter or about the procedures to hearing this application, they may call the Division or the undersigned.

Very try Thomas lahin

WTK:ca Enc.

cc: David Motloch, Esq. (Tenneco)
Mr. Tim Hower (Tenneco)

"Certified-Return Receipt Requested"

All Interested Parties in Application

STATE OF NEW MEXICO DEPARTMENT OF ENERGY AND MINERALS OIL CONSERVATION COMMISSION

IN THE MATTER OF THE APPLICATION OF TENNECO OIL COMPANY FOR WELL-HEAD PRICE CEILING CATEGORY DETERMINATION FOR CERTAIN INFILL WELLS, FOR EXCEPTION TO ORDER R-1670-T, AND EXCEPTIONS FROM WELL LOCATION REQUIREMENTS, BLANCO MESA-VERDE GAS POOL, SAN JUAN COUNTY, NEW MEXICO.

CASE:

APPLICATION

COMES NOW TENNECO OIL COMPANY, by and through its attorneys, Kellahin, Kellahin & Aubrey, and applies to the New Mexico Oil Conservation Division for an order for well-head price ceiling category (Section 103) determination that sixteen infill wells in the Blanco Mesa Verde Gas Pool qualify as New Onshore Production Wells under the exceptions of Section 271.304 and 271.305 of the FERC regulations implementing the Natural Gas Policy Act of 1978, for exception from Order R-1670-T and from well location requirements of the Blanco Mesa Verde Pool Rules, and in support thereof would show the Division:

 Applicant is the operator of sixteen Blanco Mesa
 Verde 320-acre spacing and proration units, each of which currently has an original well and an infill well.

-1-

2. Applicant has determined that in each instance, the original well has reached a stage of depletion whereby a second infill well is now necessary to effectively and efficiently drain a portion of the reservoir covered by the proration and spacing unit which cannot be effectively and efficiently drained by any existing well within the proration unit.

3. Applicant seeks this determination prior to drilling each of the subject wells as exceptions which will qualify under the higher "New Onshore Production Well" category (Section 103) of the FERC regulations.

4. The following are the subject infill wells for which the applicant seeks the necessary jurisdictional agency findings and exceptions from Division Order R-1670-T and Order R-6013 (Administrative procedures for Infill Wells):

EXH. WELL NAME

LOCATION

SPACING UNIT

1 2	Fields LS 7B Neil LS 8B	965' 2055'			2060' 885'	FEL FEL	N/2, E/2,			T32N, T31N,	
3	Gartner LS 1B	1720'	FSL	&	1610'	FWL	W/2,	Sec	28,	T3ØN,	R8W
4	Gartner LS 5B	1620'	FSL	&	1005'	FWL	W/2,		-	T3ØN,	
5	Gartner LS 6B	300'	FNL	&	1230'	\mathbf{FEL}	E/2,			T3ØN,	
6	Mudge LS 9B	2160'	FNL	&	395'	FEL	E/2,		•	T31N,	
7	Mudge LS 8B	845'	FNL	&	174Ø'	FEL	E/2,		•	T31N,	
8	Day A LS 3B	79Ø'	FNL	&	1800'	FEL	E/2,		•	T29N,	
9	Hughes A LS 2B	1125'	FNL	&	1828'	FEL	E/2,			T29N,	
10	Scott LS 3B	79Ø'	FSL	&	185Ø'	FWL	s/2,		•	T32N,	
11	Riddle F LS 1B	1850'	FSL	&	1500'	FWL	W/2,			T28N,	
12	Mudge LS 5B	900'	FSL	&	1190'	FWL	W/2,		•	T31N,	
13	Jacques LS 1B	790'	FNL	&	79Ø'	\mathbf{FEL}	E/2,		•	T31N,	
14	Jones A LS 2B	1650'	FSL	&	99Ø'	FWL	s/2,		-	T28N,	
⁻ ך	Fields LS 4B	185Ø'	FNL	&	145Ø'	FEL	E/2,		•	T32N,	
J	Barrett LS 2B	790'	FNL	&	79Ø'	FEL	E/2,		•	T31N,	

5. In addition, applicant seeks approval of the respective well locations as exceptions to the well location requirements (Rule 2) of the Special Rules and Regulations of the Blanco Mesa Verde Gas Pool.

6. Copies of the plat showing the spacing units, the Blanco Mesa Verde wells and the proposed infill wells are shown on Exhibit 1-16 attached hereto and incorporated by reference.

7. Attached as Exhibit 17 is a list of the offset operators who have been notified of this application pursuant to Division Notice Rules.

Applicant requests that this application be set
 for hearing on the Examiner docket now scheduled for May
 25, 1988.

WHEREFORE, APPLICANT requests that after notice and hearing the application be granted as required.

Respectfully submitted:

W. Thomas Kellahin, Esq.

W. Thomas Kellahih, Esq. P. O. Box 2265 Santa Fe, NM 87501

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DEGOLYER AND MACNAUGHTON ONE ENERGY SQUARE DALLAS, TEXAS 75206

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PREPARED TESTIMONY by A. F. van EVERDINGEN on the NEED of INFILL DEVELOPMENT of the BLANCO-MESA VERDE FORMATIONS in the SAN JUAN BASIN

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Dallas, Texas February 1974

(Revised July 1974)

EXHIBIT 1

DEGOLYER AND MACNAUGHTON ONE ENERGY SQUARE DALLAS, TEXAS 75206

ENCLOSURES to PREPARED TESTIMONY on the BLANCO-MESA VERDE FORMATIONS

- 1. Structure map on "Green Marker Horizon" in the San Juan basin, indicating the synclinal nature of the gas accumulation.
- 2. Distribution of estimated ultimate production per well over the accumulation.
- 3. The Schlumberger logs of two wells 1 mile apart.

4a-4h. Horner-type curves of long-term pressure buildups.

- 5. Table of pressure data.
- 6. Table of production data.
- 7. Detailed data on long-term pressure buildup tests (2 sheets).
- 8. Pressure data in psia.
- 9. P/Z values from 7-day averages versus cumulative production.
- 10. P/Z values from long-term buildup pressures versus cumulative production.
- 11. P/Z values from strat-test pressures versus cumulative production.
- 12. Computed initial gas volume versus yearly average rate per well.
- 13. Computed initial gas volume versus yearly Mesa Verde production.
- 14. Details on computing gas initially in place.
- 15. Graph of strat-test pressure.

DEGOLYER AND MACNAUGHTON ONE ENERGY SQUARE DALLAS, TEXAS 75206

PREPARED TESTIMONY by A. F. van EVERDINGEN on the NEED of INFILL DEVELOPMENT of the BLANCO-MESA VERDE FORMATIONS in the SAN JUAN BASIN

- Q-1 Will you give your name and address, please?
- A. My name is Antonius F. van Everdingen. I reside at 6138 Bandera, Apartment D., Dallas, Texas 75225.
- Q-2 What is your occupation?
- A. I am a senior vice president of DeGolyer and MacNaughton, a firm of petroleum consultants and evaluation engineers in Dallas, Texas. I am employed as a reservoir engineering specialist.
- Q-3 Will you give us a resume of your education, qualifications, and experience?
- A. In 1923, I was graduated from the Technical University in Delft, The Netherlands, as a mining engineer. In 1924, I went to Curacao, Dutch West Indies, to work as a geologist on the fresh-water supply of a subsidiary of the Royal Dutch. I did similar work in Aruba; returned to Holland in 1927; spent some months in Rumania to familiarize myself with rotary drilling; and for the next 4 years worked in Indonesia as an exploitation engineer, returning to The Hague in 1932 to work in the Royal Dutch offices. In 1935, I was lent to the Shell Oil Company. During the succeeding years, while stationed in Houston, I analyzed the production and pressure behavior of reservoirs and prepared estimates of their ultimate production and their value. These reservoirs were located in the United States, Canada, Venezuela, and Colombia. I was head of Shell's Reservoir Engineering Section in Houston until my transfer to New York in 1956. There followed 6 years of work on economic problems in the New York office and in The Hague. I retired at the end of 1962 after 38 years of service. Late in 1963, I joined the firm of DeGolyer and MacNaughton.

- Q-4 What was your primary field of interest during your service with Shell Oil Company and DeGolyer and MacNaughton?
- A. The estimation of ultimate production of gas and oil wells and reservoirs. I always felt the need to understand thoroughly the laws of the flow of fluids through permeable formations. When I was graduated, the flow of fluids was recognized to follow Darcy's law, but fluids were considered incompressible - two-phase flow was still unknown. During the 1930's, fluid compressibility and two-phase flow were recognized as important. Taking fluid compressibility into account, Mr. Hurst and I established procedures to express quantitatively the amounts of water entering into the oil- and gas-bearing portions of reservoirs due to a pressure reduction and to compute quantitatively the pressure drops in reservoirs caused by fluid withdrawals. The results are available in the Transactions of the AIME in "The Applications of LaPlace Transformation to Flow Problems in Reservoirs," Volume 186 (1949), page 305. The methods enable engineers to use the material-balance equation with greater accuracy and more facility than before. In 1953, "The SkirrEffect and Its Influence on the Productive Capacity of a Well" was published in Volume 198, page 171, giving a method of anlayzing well pressures in such a way that the quality of well completions and well treatments could be expressed quantitively. I have lectured on the "Performance Predictions of Several Reservoir Mechanisms" at The University of Texas at Austin, Texas.
- Q-5 Are you a member of any technical societies?
- A. I am a member of the Society of Petroleum Engineers of the AIME. I was a member of the API Committee on Petroleum Reserves from 1955 until my transfer to The Hague in 1960. I am a registered engineer in Texas.
- Q-6 Have you received any professional awards?
- A. Yes sir. The Lester C. Uren award in 1970 for "distinguished achievement in technology of petroleum engineering" and the Anthony F. Lucas Gold Medal in 1968 for "improving the technique of producing petroleum."
- Q-6a What is your experience with the San Juan Basin and the Blanco-Mesa Verde Gas Pool?

- A. The firm of DeGolyer and MacNaughton has worked on various problems in the San Juan practically continuously from 1953 until 1960. I joined the firm in 1963. During the first few years my opinion on some problems in the Blanco-Mesa Verde and Basin Dakota Gas Pools was asked occassionally. My work started in earnest early in 1972. Since then I have spent most of my time analyzing the rates and pressures of the accumulations in the San Juan Basin.
- Q-7 Have you made a reservoir engineering study of the Mesa Verde formation in the Blanco-Mesa Verde Gas Pool in San Juan and Rio Arriba Counties of New Mexico?
- A. Yes, I have, by reviewing and studying the publications and reports on the gas-producing formations in the two counties. In addition, I have reviewed and analyzed core data, logs, and a great number of pressure data on wells in the Mesa Verde. Invariably more than one, sometimes several, productive zones were found present in a well.
- Q-8 What was the purpose of your study?
- A. To determine the effectiveness and the efficiency of the existing wells in draining the resevoir. This requires a determination of the amount of gas initially in place and an estimate of the ultimate production, and in addition, a determination as to whether wells drilled between existing producers would substantially increase the ultimate production of the reservoir.
- Q-9 Please describe the sources of the basic data and other information used in connection with your study.
- A. Good geological descriptions on these formations and reservoirs can be found in the following reports and publications:
 - "A Brief Discussion of the Subsurface Cretaceous Rocks of the San Juan Basin" by Dan Bozanic in the 1955 Four Corners Geological Society Guide Book.
 - 2. "Stratigraphic Gas Development in the Blanco-Mesa Verde Pool of the San Juan Basin" by R. W. Allen in the same publication.

3. "Reservoir Characteristics of Cretaceous Sands of the San Juan Basin" by Wilbur E. Reneau and J. D. Harris, which appears in the 1957 Guide Book.

Furthermore, El Paso made available a mass of pressure data from which buildup curves were prepared. Most of these tests extend over a considerable shut-in period, the maximum being slightly over 3 years. Moreover, 7 days' shut-in pressure data, numerous electric logs, and the results of core analyses, already available in my office were utilized.

- Q-10 Before going into the details of your study, please state generally the conclusions which you have reached concerning the feasibility of infill drilling in the Blanco-Mesa Verde Gas Pool.
 - A. I have made a performance study which entailed consideration of all of the pressure and production data available from all of the wells producing in the Blanco-Mesa Verde Gas Pool. In my opinion, the best information from which to determine the gas in place is contained in the data of the 65 long-term buildup pressure tests. Such data were obtained in the 38 wells distributed throughout the reservoir. By an analysis of this buildup information, together with field production data, I have concluded that 25,000 Bcf of gas and perhaps even more could have been present in the reservoir. Furthermore, the number of wells provided under the current field rules (one well on a 320-acre drill site) are estimated to yield 9,000 Bcf ultimately. It is my opinion that this recovery can be increased to a 15,000 Bcf if the field rules were changed to allow two wells on a 320-acre drilling site as set out in the application.

I have concluded that the producing formations are made up of lenses, some of considerable extent, stacked on top of another. The most permeable lenses occur near the deepest portions of the basin, and their permeability is reduced towards the topographically higher-out boundaries. As a result, the accumulation is saucer-shaped instead of dome-shaped (Exhibit 1). A reduction in permeability and shaling out toward the outside boundaries must occur in all sand bodies, as is plainly evidenced by the presence of gas itself and by the ultimate production per well distributed over the field (Exhibit 2). The form of the reservoir is the inverse of normal accumulations which are emitted by a water-gas contact at their deepest structural position. The sands are so fine grained that small variations in the grain size can reduce the permeability to practically nothing so that sand lenses appearing on one log disappear or have been displaced vertically on the log of the next well. The Schlumberger logs for two wells 1 mile apart, shown in Exhibit 3, clearly demonstrate the variation in position and thickness of such lenses. The occurrence of lenses also introduces uncertainty in the ability of a well to effectively drain the area of the drill site. The combination of these conditions causes me to conclude that infill development of the 320-acre drill site will substantially increase the ultimate gas production from this reservoir.

- Q-11 Does the conclusion you have just expressed concerning infill drilling in the Blanco-Mesa Verde Gas Pool differ from one you previously reached regarding the effect of spacing on recovery efficiency? If I remember, you co-authored the paper "The Relation between Well Spacing and Recovery," published in the API Drilling and Production Practice of 1945, in which any relation between spacing and ultimate production was denied.
 - A. Yes sir, over the years my opinion has changed. I now recognize that conditions do occur which cause such a relationship to exist. Firstly, the Blanco-Mesa Verde Pool of the San Juan Basin is lying in the deepest portion of a large asymmetrical syncline in which the gas accumulation could only be (and has been) kept in place by the lenticular development of the gas-bearing sands.

Secondly, because sands become nonpermeable towards boundaries of the reservoir, the same variations can also be present within the boundaries of the Mesa Verde formations so that gas-bearing sand pockets could exist which have no satisfactory connection to a well.

Thirdly, variations in the size of the small-sized sand grains or in the mixture of these grains not only could cause lenses to exist, but also result in appreciable variations in the productivity of the same lense. Considering the dimensions of the Mesa Verde accumulation, about 50 by 40 miles, and an average net sand thickness of approximately 100 feet in a total gross thickness of 700 feet in the northwest increasing to more than 1,000 feet in the southwest, the existence of such variations appears entirely plausible.

Finally, because the Mesa Verde formation producing in a well often contains several lenses, we can expect a far more complicated pressure behavior than the patterns obtained on wells producing from one, homogeneous horizon. Applying the conclusions of pressure analysis learned from homogeneous sand to the Mesa Verde wells is to say the least unwarranted and probably misleading.

- Q-12 Just how do these comments relate to the feasibility of infill drilling in the Blanco-Mesa Verde Gas Pool?
 - A. From a net sand thickness map, I compute that the Mesa Verde contains 50 million acre-feet of gas-bearing formation. Using the figures published by Reneau and Harris (an average porosity of 9.64 percent and a connate water content of 33.25 percent), and, in addition, a reservoir temperature of 160 degrees F., an initial reservoir pressure of 1.315 psia, a Z-Factor of 0.8631, and 15.025 psia as pressure base, the original gas content is computed to be 11,900 Bcf (5.70 billion for an average well) present in 140 Bcf of net pore space. Accepting an ultimate production of 8,900 Bcf, the figure represents a recovery efficiency of 75 percent.

The volume of gas-bearing sand depends a lot on the quality and availability of the electric logs, the estimator's opinion in interpreting the percentage of connate water present, the assumed lower limit of permeability, etc. As net sand thickness constitutes some 10 percent of the total thickness of the Mesa Verde, the problem is to show that more gas-bearing sand could be present, or better yet, that initially there was more than 12,000 Bcf present in the accumulation.

- Q-13 That, in itself, is not sufficient. You will also have to make it appear highly probable that infill drilling will result in increases in ultimate gas production.
 - A. I agree. Little additional information can be gleaned from further refinement of the old electric logs or reinterpretation of core data. In my opinion, the outcome of such work depends too heavily on the interpreter's opinion on the amount of connate water present and the minimum permeability required in a sand to be productive.

I, therefore, switch to a consideration of the various sets of pressures which can only reflect the effect of gas still present. The pressures to be considered are:

- 1. Those obtained by averaging the casinghead (or tubinghead) pressures of all wells, measured yearly, after 7-day shut in;
- 2. the data of long-term, shut-in pressures available on 38 wells; and,

DEGOLYER AND MACNAUGHTON

- 3. the pressures observed in El Paso's three strat tests.
- O-14 Please discuss all pressures and their determination in some detail.
 - A. We will start with:

(1) The average of the pressures read after 7-day shut in.

The orders as promulgated by the New Mexico Oil Conservation Commission require that annually a 7-day shut-in casinghead and tubinghead pressure be determined and reported in psia. It is customary to use the highest of the two figures. Measurements have been made in the majority of the producers. The yearly field average appears in Column 4 of Enclosure 5.

The pressures, measured at the surface, have been converted to bottom-hole pressures and results are given in Column (5) of the same enclosure.

During the late fifties and early sixties, El Paso Gas conducted 65 long-term pressure buildups in 38 different wells. The data were sufficient to determine average reservoir pressures during the 10-year period 1955-1965. They were 380 psi above the average of all 7-day wellhead pressures, and 267 pounds above the average bottom-hole pressure derived from the 7-day tests. The figures mentioned are all listed on Enclosure 5.

When I mention fully built-up pressures, I have in mind the pressures read on the Horner-type plots above the point where $\Delta t/(t+\Delta t) =$ unity. They are commonly referred to as P* values. The use of these pressures has not found as many advocates as they deserve because, so the argument goes, it takes an infinitely long time to reach the point where $\Delta t/(t + \Delta t) =$ unity, and no infinitely long time is available. Because the P* values cannot be derived from the 7-day pressures measured in gas wells of the Blanco-Mesa Verde reservoir in any way I am familiar with, and because I consider the P* values the best source of pressure

information and will use or refer to such data continuously, I will first clarify their determination, their meaning, and their merits.

(2) Fully built-up reservoir pressures, P* values.

Several times during the productive life of the Blanco-Mesa Verde reservoir, El Paso Natural gas conducted a series of long-term buildup tests. Eight of the curves prepared from their data are shown on Enclosures 4a through 4h. The horizontal scale is always a log scale because the pressure in any well produced at constant rate declines proportional to the log of the time it has been produced so that a straight line is formed by subsequent observations. For wells produced at a constant rate and then shut in, the horizontal scale is used for the log of the shut-in time divided by the time elapsed since completion. The pressure increases (and also the pressures themselves) again form a straight line when plotted on the normal, vertical scale and again can easily be extended and interpreted.

In oil- or water-producing wells (where fluids produced have small and constant compressibility), pressure points start forming a straight line within hours after a well is closed in. Extending this straight line relation to the right and reading the pressure above the point where the ratio of shut-in time divided by the total time is unity gives P^* . This pressure reflects the formation pressure (at the well's location) after correcting for the effect of the withdrawals by the well itself. Stated in a slightly different way, it reflects the pressure at the well's location had no fluid ever been taken out of the well. The difference between P^* and the initial reservoir pressure, therefore, is equal to the effect of all other wells, their total interference. That drop reflects the sum of the interference effects of every well in the reservoir since the moment of their first production.

In gas wells producing from tight formations, more time than 7 days is required before the time-pressure relation straightens out: e.g., the points for the Gartner No. 4 (Enclosures 4e and 4f) do not fall on a straight line until 5 to 6 weeks after the well is shut in, and that period is among the shortest of shut-in times required before straight-line relations are established in the 8 buildup curves composing Enclosure 4. Three months had to elapse before the pressure points in San Juan Unit 28-7 No. 56 did the same (Enclosure 4a), and in the case of Stewart No. 4a, a P* value could not be obtained until the well was shut in more than a year (Endosure 4d). The other five examples required a shut-in period intermediate between these two figures. In my opinion, such a behavior clearly shows that the Blanco-Mesa Verde is a multilayered reservoir. In such reservoirs, the transient pressure stages are an order of magnitude longer than in a single-layered reservoir. (Lefkovits, Hazebroek, Allen and Matthews in "A Study of the Behavior of Bounded Reservoirs Composed of Stratified Layers" in the March 1961 issue of the Society of Petroleum Engineers Journal)

In all cases, straightening out occurs when the pressures are within 10-20 percent of their maximum value; that is, the pressures are in the range in which the compressibility of gas apparently approaches a sufficiently small value so that the flow equation can be used in its simplest form when constant production rates cause pressure drops proportional to the rate times the log of the production time.

The information and values from the P*'s determined in the 38 wells are collected on Enclosure 7 (2 sheets).

The data are available from 1956 through 1962. By assuming that in each of the 38 wells the fully built-up, bottom-hole pressure measured later increased the same percentage above the reported 7-day pressures as measured during the long-term buildup tests, we obtained fully built-up pressures on all 38 wells through 1965. The outcome is given on Enclosure 5 and will be discussed after presenting data from the strat tests.

(3) Strat-test pressures.

In 1957 and the beginning of 1958, El Paso drilled three wells through the Mesa Verde, put in casing, fractured the formations, cleaned out the wells, and then shut them in. They are usually referred to as the three-strat tests; their location is shown on Enclosure 2. The average of the pressures in these three wells appears in column 7 of Enclosure 5. Never produced, they were used solely for the purpose of measuring reservoir pressures and, hence, form the only source of pressure data at points midway between producers. During the years since their completion and up to 1970, the bottom pressures in all three wells roughly parallel each other (Enclosure 15). Since 1971 the pressures are diverging somewhat; those in strat-tests 1 and 3 decline more than the pressures in strat-test 2.

First observe that during the 5 years that pressure data are available on strat tests and on the 38-well group, the average of the strat-tests' pressure is consistently 50 pounds higher (Enclosure 8). To any one doubting whether pressure as high as P^* values can be found, this excess should be convincing. It is presented as proof that the average P^* value of the 38 wells is a valid determination of the pressure existing in the formation drained by the wells. At the same time it shows that still higher pressures are existing in areas not directly drained by a well.

- Q-15 Explain that statement in more detail.
 - A. The pressures in the strat-test wells are higher than those derived from the long-term buildup tests due to the fact that some formations in the strat tests are not present up in the surrounding producers. The surrounding wells will lower the pressures in the most permeable formation easily as far out as the strat tests. These formations are then continuously refilled, that is, repressured by gas from strata in the strat test, not present in the producers, hence the pressures measured are above those in the permeable formations and below the pressures in the least permeable formations. The actual reservoir pressure in the strat test is therefore always higher than measured.

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O-16 Then are you going to use these three pressure series?

A. No, sir. Each series is converted to the P/Z values because these values are proportional to the amount of gas in a unit of pore space. The P/Z data are shown on Enclosure 6. As is customary, we relate all P/Z values to cumulative production; therefore, instead of discussing the pressure series, we will direct our attention to Graphs 9, 10, and 11, where the P/Z values are plotted versus the cumulative production of the Blanco-Mesa Verde.

(The Z factors used reflect conditions in the reservoir and for details of these P/Z calculations, see Enclosure 14)

In normal, single-layered depletion-type reservoirs, these values form a straight line when plotted versus the cumulative withdrawals. Here, several straight lines can be drawn tangential to the points shown.

- Q-17 Just what do those lines mean and how do you use them?
 - A. Each line is drawn through three or more points and is tangential to the P/Z curve. Its slope gives the number of P/Z units lost versus a certain increase in cumulative production.

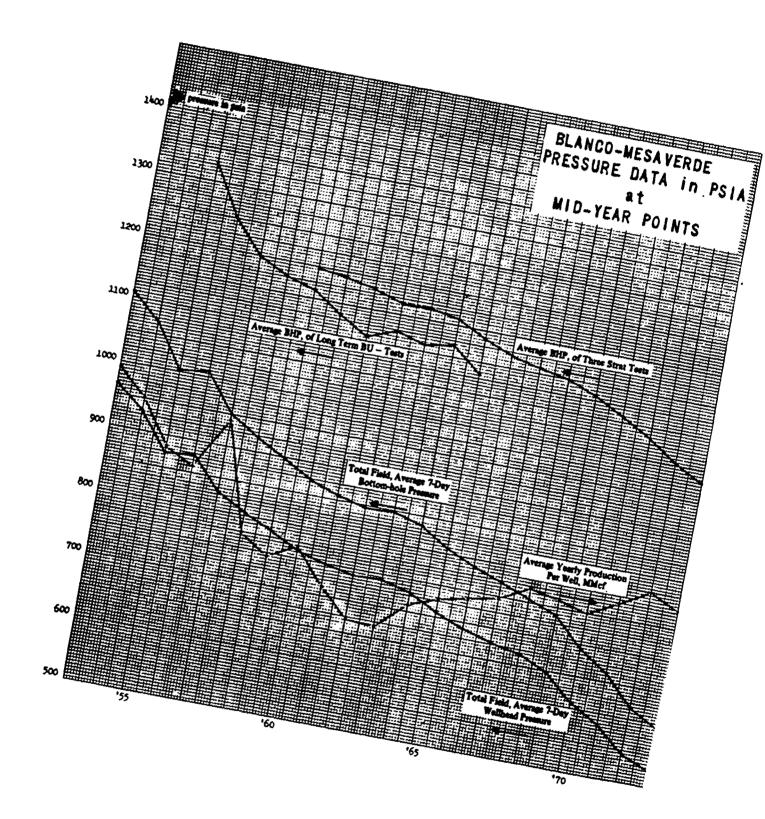
For instance, if we read a P/Z value of 900 when the cumulative gas production is 2,500 Bcf and 800 when the cumulative production is 4,000 Bcf, then such a line indicates a loss of 100 units per 1,500 Bcf of gas produced. At the same time it indicates an amount of gas in place equal to $(800/100) \times 1,500 + 4,000 = 16,000$ Bcf. The slope indicates a decrease of 15 Bcf per unit decrease of P/Z so that the original amount of gas present equals the total number of P/Z values at the time of reading times 15 Bcf, plus the gas already produced.

There is a very clear but not precisely definable connection between the rate of production of an average well and the amount of gas computed as initially present in the Blanco-Mesa Verde formation. The smaller the rate, the larger the volume initially present. For rates, we can also use the yearly production for the entire Mesa Verde so that we have two bases to estimate the gas initially present. Moreover, we can use the average pressure data of the entire field, of the long-term buildup tests, or the strat tests.

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Hence, I computed the average yearly production rate per well during the years the straight lines on Enclosures 9, 10, and 11 are tangential to the pressure curve and plotted the volume of gas indicated by the straight line versus these average rates (Enclosures 12 and 13). Both enclosures show that the smaller the rate the higher the volume of gas present, which is, after all, exactly what we should expect in so heteregeneous a reservoir. The smaller the rate the better the gas can even out pressure differences due to the variations in character of the formations. I think it very safe to conclude that the general trend on both Enclosures 12 and 13 indicates more than 25,000 Bcf of gas as initially present in the Mesa Verde.

- Q-18 Do you have any idea about the magnitude of the additional reserves that could be obtained by a complete infill-drilling program?
 - A. Yes sir, I have some. Current estimates of an ultimate production of 9,000 Bcf are not unreasonable. It represents a 75-percent recovery efficiency. I consider the 75-percent efficiency too liberal. This type of reservoirs, and under the increased density of development, could produce with an efficiency of 60 percent so that the ultimate production is around 15,000 Bcf.
- Q-19 Do you consider that the ultimate production from all areas can be increased by the same percentage?
 - A. No sir, very definitely not. In the center portion of the field the ratio between tight and permeable formations is less than unity so that there infill drilling will produce the least increase in ultimate production, expressed as a percentage. The volume per well may be even smaller than will be obtained from wells in the more outlying areas. In some of these areas, the ultimate of the new wells could well match the ultimate of the existing wells. Locations in areas at present not or barely affected by the withdrawals, are regarded as the major source of gas to bring the ultimate production to the figure quoted.



P-STAR 1 Pour permit

NESAVERDE LONG TERM PRESSURE BUILD-UP DATA FROM VAN EVERDINGEN'S TESTIMONY - 1974

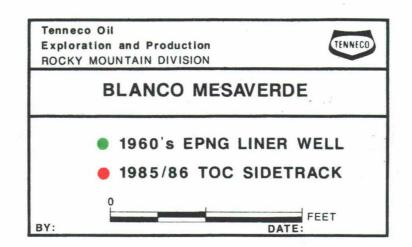
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HOHELL 20	00 000	00 74 A	0	1.) 55						
HOMELL 26	OH, SNG OH, SNG	29 31 8 14 30 8	Aug-51 Oct-51	Ju1-56 Oct-56	1784	1042	1058	16	2645	
PRITCHARD 2	OH , SNG	34 31 9	Jul-52	Jul-58	1823 2197	1050 991	1083 1028	33	2059	
BARNES 7	OH SOF	23 32 11	Oct-54	Jun-59	1698	934	989	37 55	1651 957	
PRITCHARD 2	OH .SNG	34 31 9	Jul-52	Jul-56	1452	980	1040	60	1250	
ATLANTIC 5	DH , SNG	22 31 10	Jun-53	Nay-56	1042	987	1055	68	1177	
SJ 32-9 #29 Barnes 7	OH , SOF	36 32 10	Sep-55	Aug-58	1057	890	960	70	973	
SJ 30-6 #74	OH SOF OH SNG	23 32 11 23 30 7	Oct-54 Apr-53	May-57	923	959	1037	76	624	
SJ 32-9 #29	OH , SOF	36 32 10	Sep-55	Jun-59 Nay-56	2265 232	951 967	1029 1049	78	1360	
HOWELL 20	OH , SNG	29 31 8	Aug-51	Aug-51	8	1067	1150	82 83	157 7	
SJ 32-9 #29	OH,SOF	36 32 10	Sep-55	Feb-61	1982	851	935	84	1441	
SCHMERDFEGER 2	OH , SNG	27 31 9	Jul-52	May-57	1770	921	1006	85	1238	
Jacques 1 Gartner 2	OH SNG	29 31 9	Dec-52	Apr-56	1228	980	1068	88	1087	
ATLANTIC 5	OH , SNG OH , SNG	28 30 8 22 31 10	0ct-51 Jun-53	Jun-59	2805	886	975	89	1402	
ATLANTIC 5	OH , SNG	22 31 10	Jun-53	Ju1-58 Feb-61	1862 2752	893 852	983 942	90 90	1855	
GRAMELING 3	OH , SNG	22 29 9	Aug-51	Aug-56	1843	933	1025	ŝ	2301 483	
HUGHES 1	DH .SNG	19 29 8	Apr-51	Jun-59	2988	858	955	9 7	895	
GRAMBLING 3	OH , SNG	82 29 9	Aug-51	Jul-58	2556	872	972	100	761	
GRAMBLING 3 SJ 30-6 #74	oh , s ng oh , s ng	22 29 9 23 30 7	Aug-51	Nov-62	4139	837	939	102	1083	
LUCERNE 2A	OH, SOF	23 30 7 9 31 10	Apr-53 Sep-54	May-57	1506	950	1056	106	1055	
HOWELL 3A	OH , SNG	4 30 8	Jul-51	Jun-59 Apr-62	1733 3923	866 836	974 951	108	776	
atlantic 5a	OH .SNG	26 31 10	Jan-53	Jun-59	2327	852	981	115 129	1245 725	
RIDDLE 2	OH, SNG	3 30 9	Ju1-53	Jur-59	2160	828	962	134	621	
BARRETT 2	OH ,SOF	19 31 9	Apr-54	Jun-59	1901	859	995	136	1343	
GRAMELING 1A GARTNER 2	DH , SNG DH , SNG	21 28 8 28 30 8	Har-51	May-51	52	9 89	1127	138	15	
MUDGE 5	OH, SNG	3 31 11	Oct-51 Nov-53	May-57 May-56	2046 924	868 931	1007 1072	139	1166	
GARTNER 4	OH , SNG	33 30 8	Dec-52	Feb-56	1180	923	1066	141 143	543 1127	
HUGHES 1	OH , SNG	19 29 8	Apr-51	Oct-57	2368	854	1015	151	734	
ATLANTIC 8A	OH ,SOF	29 31 10	Hay-55	Jur-59	1480	801	953	152	777	
Slinray a2 Gartner 4	OH SOF	10 30 10	Har-55	Jun-56	440	<u>914</u>	1068	154	178	
FIELDS 1	oh , sng oh , sng	33 30 8 25 32 11	Dec-52 Nove-52	Jul-58 Maria 54	2063	877	1034	157	1894	
FIELDS 1	OH , SNG	25 32 11	May-53 Nay-53	May-56 Jul-58	1093 1 8 98	916 892	1076 1057	160 165	312	
LUCERNE 2A	OH, SOF	9 31 10	Sep-54	May-57	974	855	1036	171	485 498	
ATLANTIC SA	OH, SNG	26 31 10	Jan-53	Nay-57	1568	868	1045	178	564	
HUGHES 3A	OH , SNG	27 29 8	Jun-53	May-57	1417	840	1020	160	861	
Barrett 2 Day 4a	OH SOF	19 31 9 8 29 8	Apr-54	May-57	1142	855	1037	182	1028	
SJ 28-6 #37	CSD_FRAG	6 27 6	Jan-56 Oct-55	Ju1-56 Apr-57	193 553	871 817	1060	169	401	
RIDDLE 2	OH , SNG	3 30 9	Jul-53	May-57	1400	797	1013 995	156 198	296 4 38	
ATLANTIC BA	OH .SOF	29 31 10	May-55	May-57	721	803	1007	204	433	
HOWELL 3A	OH,SNG	4 30 8	Jul-51	Aug-58	2562	782	1005	223	1055	
CASE 2 FIELDS 5	CSD, FRAC	8 31 11 28 32 11 28 32 11	Apr-55	May-57	757	821	1073	252	339	
FIELDS 5	CSD, FRAC	28 32 11 28 32 11	Dec-55 Dec-55	May-56 Jul-58	168 967	820	1075	255	67	
SJ 28-6 #30	CSD, FRAC	28 28 6	Nov-55	May-57	543	7 4 5 776	1011 1055	266 279	534 197	
SJ 28-7 #49	CSD, FRAC	21 28 7	Sep-56	Nov-62	2275	715	1008	293	519	
FIELDS 1	CSD, FRAC	25 32 11	Nay-53	Feb-64	3925	626	935	309	685	
SJ 28-7 #43	CSD, FRAC	21 28 7	Sep-56	Jul-58	691	747	1075	328	229	
SJ 28-6 #56 LINDSEY 1A	CSD, FRAC	13 28 7	May-56	Apr-57	329	767	1111	344	159	
ZACHARY 1	CSD, FRAC CSD, FRAC	19 30 8 25 31 11	Nar-56 Dec-55	Jul-56	122	764	1125	361	185	
JONES 4A	CSD, FRAC	13 28 8	Apr-56	Ju1-56 Apr-57	199 363	717 738	1079	362	8 8 207	
SJ 28-6 #56	CSD, FRAC	13 28 7	May-56	Jur-59	1118	695	1102 1094	364 399	203 378	
SJ 30-6 \$100	CSD, FRAC	35 30 7	Dec-55	Jul-58	954	646	1081	435	534	
STEWART 4	CSD, FRAC	28 30 10	Kar-56	Jul-58	862	648	1176	526	112	

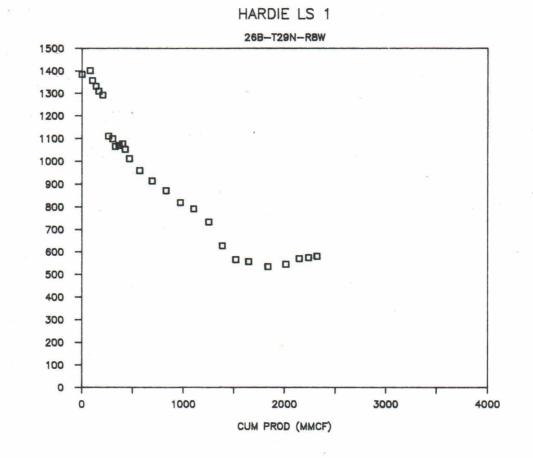
R8 W					
-	4836	· 3003 PO.9.7	160 Thompson	"month	C TANG
Т 30	2790 2010 7094	7390 5704 5544	1022A 1000000 5777 02L 4 5280	** *444 # 59 5476	PNADOR 2136 PNADOR 2136
N	31 32 557 5 3032 109 3145 Broner (adpr 1A 545 54 44A ₂ 4904 144 14 370 544	5500 GARTNER corner 500 510 5200 5200 5500 GARTNER corner 3 5745 5325	A Thompson L-3 5230	7ε 7335 35 1 (aren) Φ 19 5 (με) Φ 19 5 (Livery Q-14 7400 Q05 Q05 S435 S517 R
	1156 Anthony b 22A Anthony For 14-2 53 5288' 2992	2 5425 2 5425 2 5566 2 57 5120	284 5550 0121 7563 3	5483 57	Floridince Howell \$2:30E \$2:1 Floridince 52:35 \$2:30 A \$3565
×	22-4 3270' 42-5 3270' 42-5 3370' 5370' 5600' 3151' 15445		8 5432 7540	21 фию 57 5175 фию 5060	Ф 30 7773 с и 5566
	007 17420 004 17 17420 007 00 174 6 007 00 174 6 000 00 00 00 000 0000000000000000000	Day Ch 3 Day Ch 3 Present Ch 3 5555 Ch 4 Ch 4 5555 S746 S475 54 8 Ch 5 S746 5217 Ch 8-2 Ch 32 7535 Ch 32 Ch 32 7635 Ch 700 Ch 32	3 #4 a 005 5 359 5613 3 5614	A-1 5480' Kondewarr C- C- C- C- C- C- C- C- C- C-	Vondevor 7555 5 0 1 A 5550 5 1 2 Va 556
	20 10 2.4 A 7 3/28 A 6 50 5229 D A 4 5 50 7500 LE 7540 A 13 3/08 7570	E CAL SA 2 5522 7685	A 5405 3 A 5560 47 2 42 7600 A 7 3185'5 7514'	A 570 904 1 11 165 1-E 7640 A 14 570 \$78-3 7550	a 7550 / 1
	22' 5673' 2' CA-12' 340' 51' 55' A'S 5455' 3203' 50' 50' 3132' 10' 1-A 5702' 17'	10 10 10 10 10 10 10 10 10 10 10 10 10 1	7610 15	VAND. 04 A-7 3543' AA 5 7575' 04 -2A 5693' 04 -14 7905 78 6014 14 7905	Иопаличисти флаза 5720 7585 522 7585 13 а 4а 6169 7
Т 29	F 007 0 0 007 0 0 0 0 0 0 0 0 0 0 0 0 0	Cld 10 1720 57 573 10 4 14 15540 5765 3 5	773 20 7920	A 14 6211 D A 19000 A 2 3840	80%0 8129
N	Hughes	20 3144' 5750' 21 52	10 4-4 A 10-7 5904 22 3594	Witch 23 3554	Abrahe Vandesen* ↓ A·2·A ↓ ↓ ↓ A·6 vande 5045 ↓ 4ε 8·2ε 8/28 7640' 24
	5605 0 07 0 7550 7666	5762' HUGHES 1000 021	407 7650 338	ARD120'5 0'14 A 0'44 '544 '544 '544 '544 '569'	Инган Ингания 3 маг 254 2
5	246 021 0274 51 7656 5320 0274 1266 5685 3 302 30765 29	0 02 000 A A 5 420 550 MUGHES A 5 0 A 5 0 A 3 78 490	0 A 3A 00 A 7 0 A 16 3501 7560 57	3335 HARDIE 7550 5 201 1 2019 7584 (5370 5334 6536 (5370 5334 6536 (5757 5034) 664 (6370 5034) 665 (5757 50) 67 (575 50) 67 (5	24 5680 40704 04 00 07 03 1500 13738 1900 5836 2 100 25
	0-4 0-1A 0 7 5235	0 0 8 1346 DA	4 734 UGHE 996 A 3 7867 CA.8 3317 A 3 787 CA.8 3467	04 4 0 0000 5285 04 4 5606 5410 14 5606	Abrohu Abrohu IIII Africa Abrohu IIII Africa Abrohu Abrohu Africa Abrohu Store Abrohu Abrohu Store Abrohu Abrohu Store Abrohu Abrohu Store Abrohu Abrohu Abrohu Abrohu Abrohu Store Abrohu Abrohu Abrohu Abrohu Abrohu Store Abrohu Abrohu Abrohu Abrohu Abrohu<
	08 2675 Princhard C 33 \$73 \$74 \$575 31 \$75 \$75 \$75 \$75 \$75 \$75 \$75 \$75	5/ A 9 2898 - QA - PQ33 - QA - 4865 - A 6 7143 - A 6A 5277'' 33		4 7465 7445 0024 010 578 055 024 3074 3057 2 5132 34	2000 13150 230-13 35 5317'
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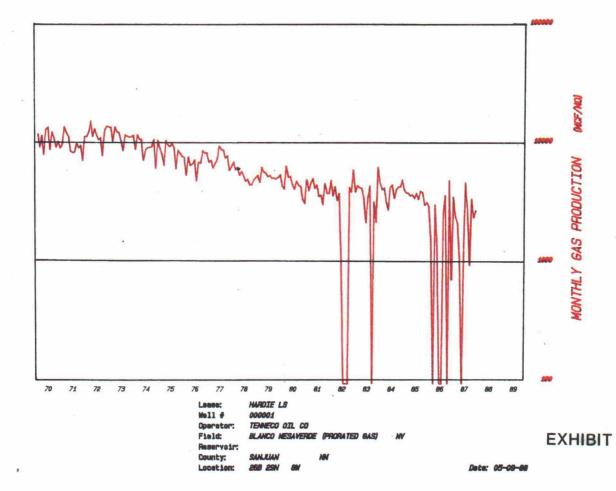
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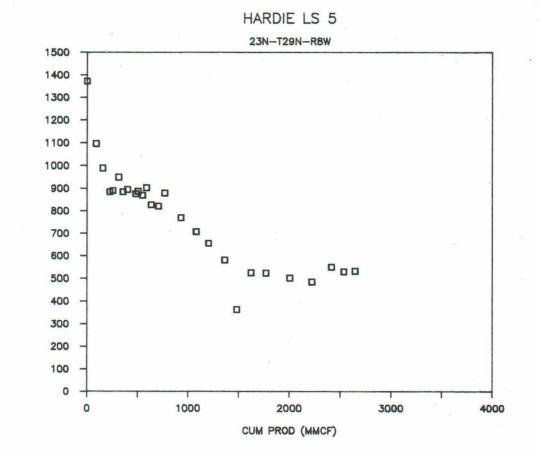
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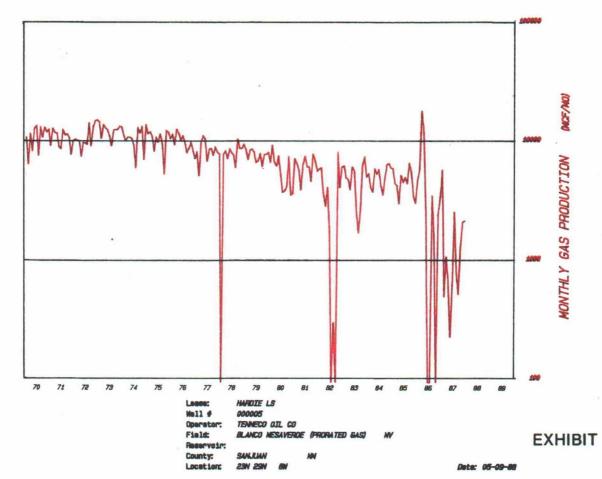




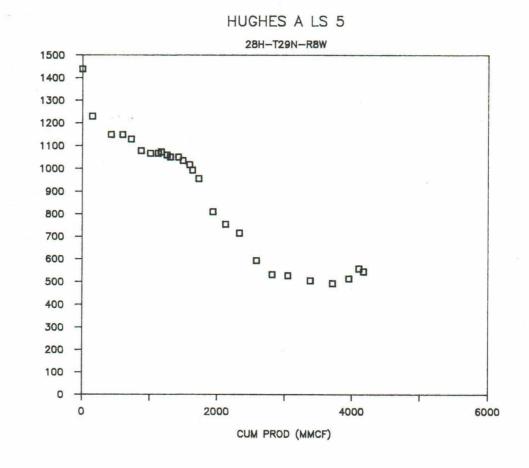




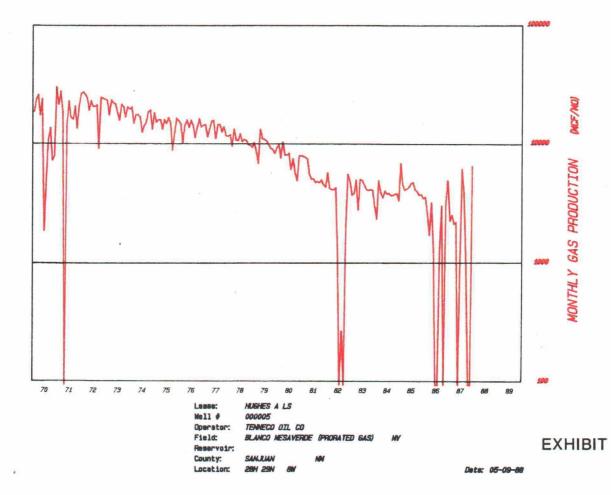


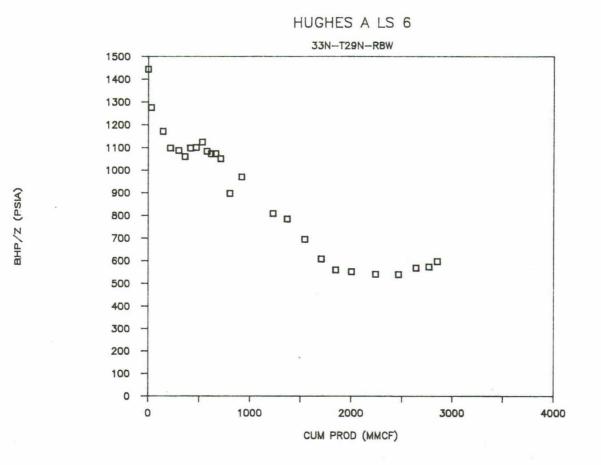


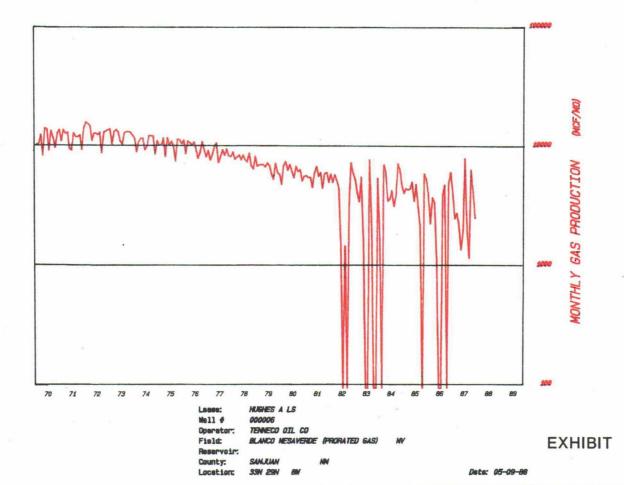
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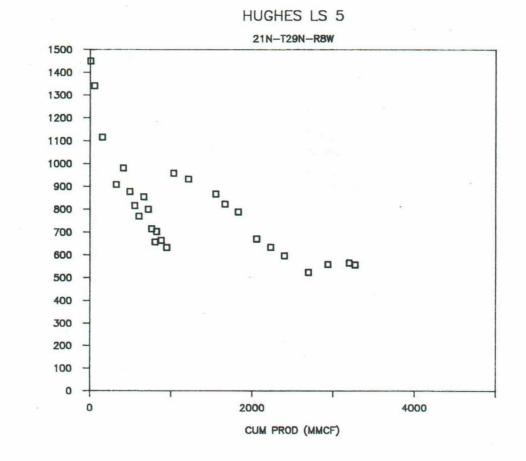


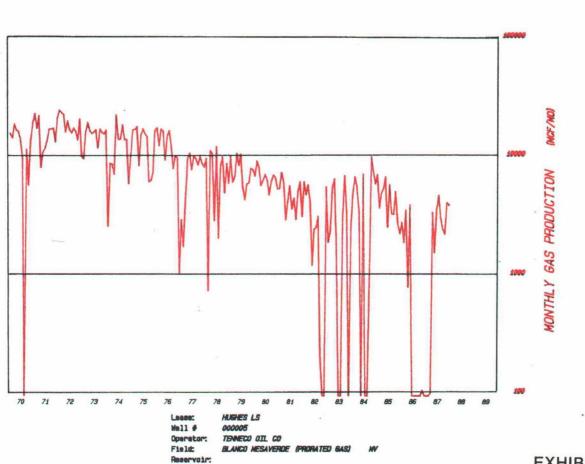












County:

Location

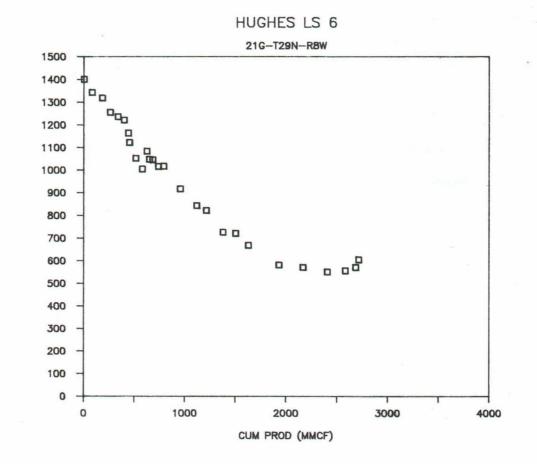
SANLA

21N

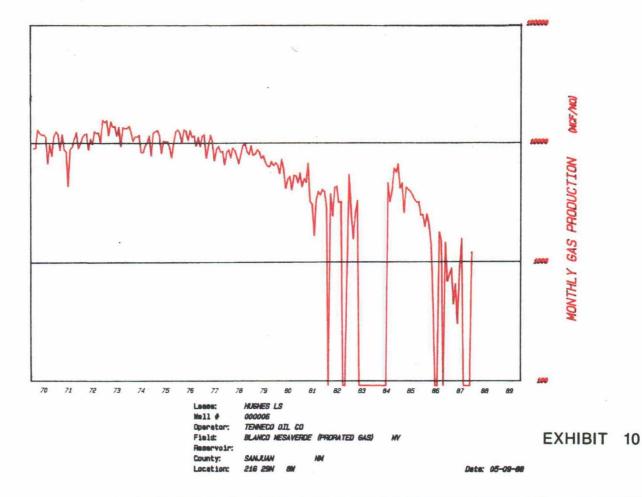
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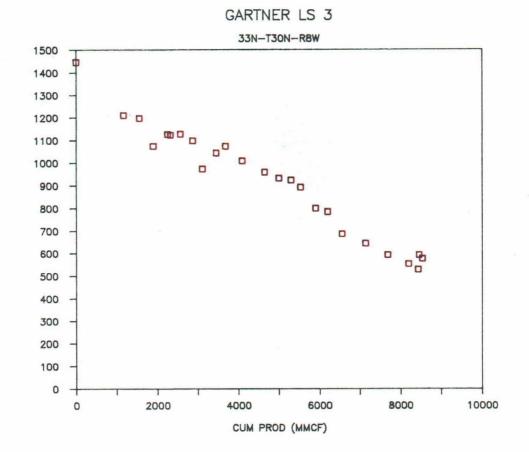
EXHIBIT 9

Dete: 05-09-88

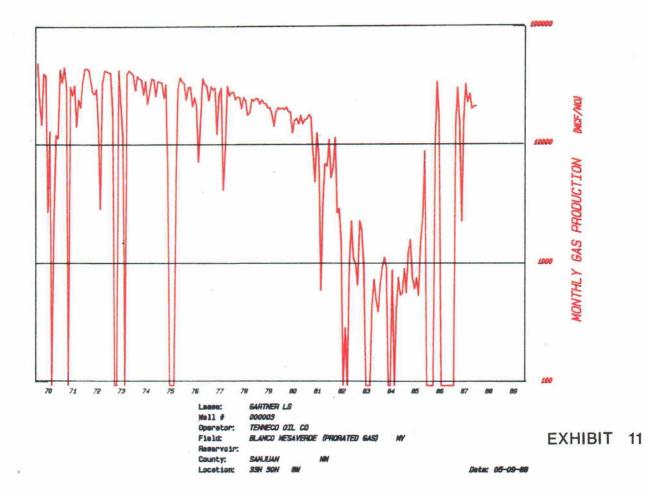


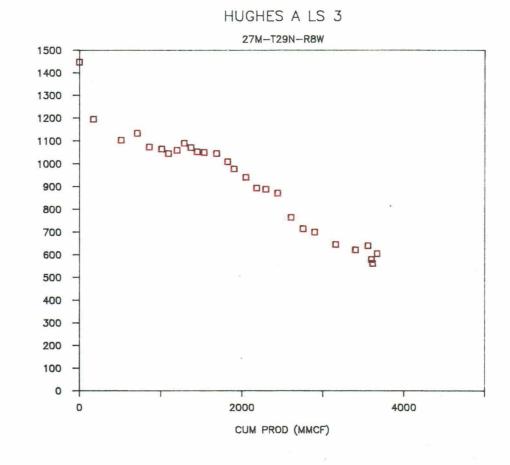
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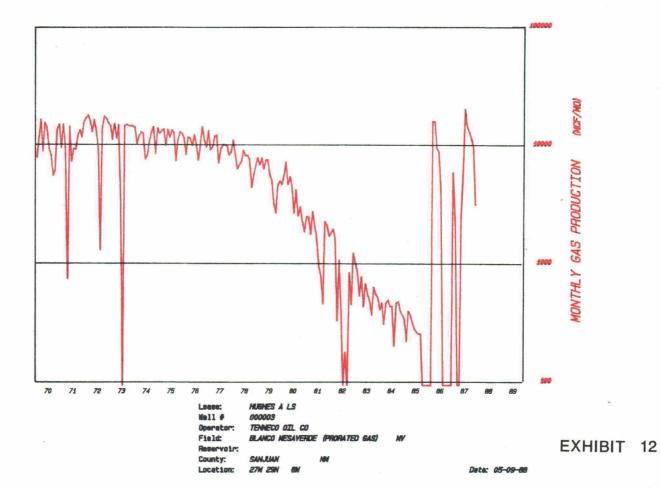


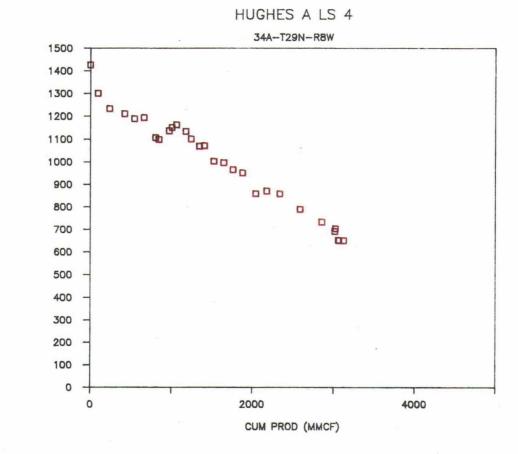


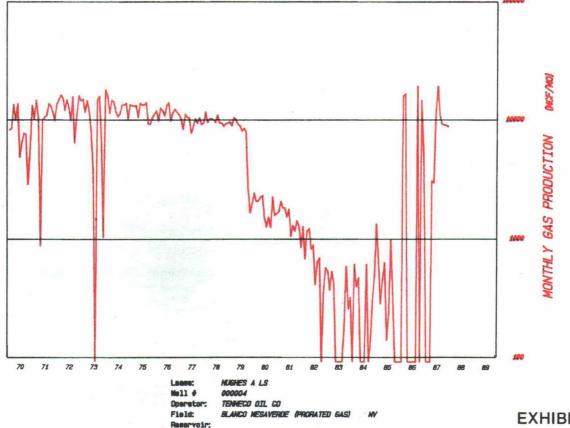










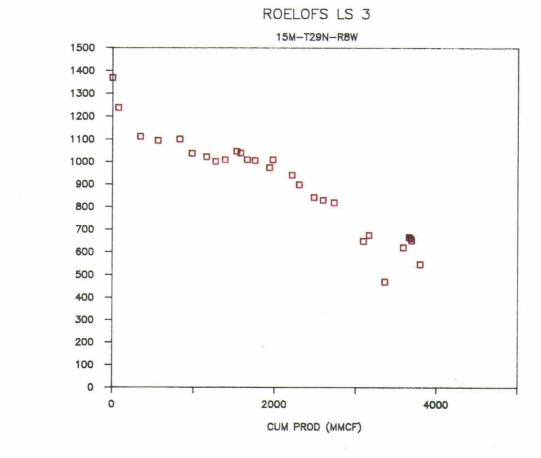


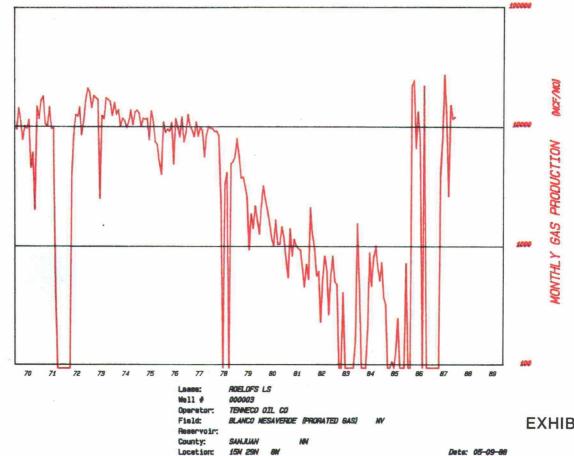
County:

Location

EXHIBIT 13

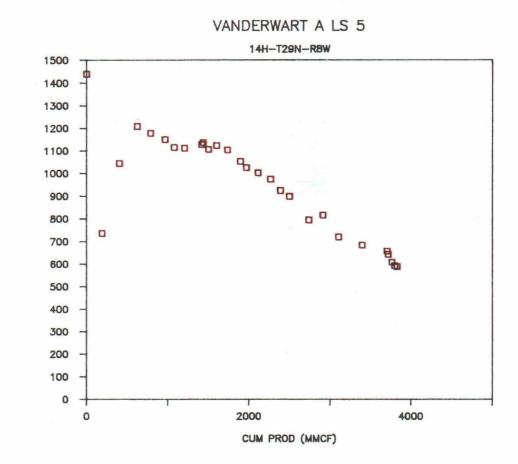
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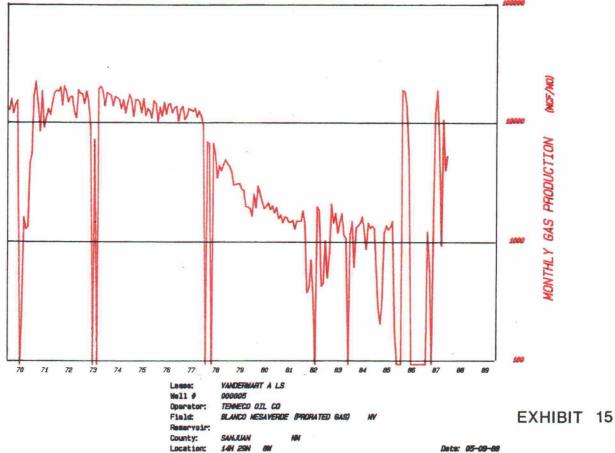




(MSA) Z/AHB

EXHIBIT 14





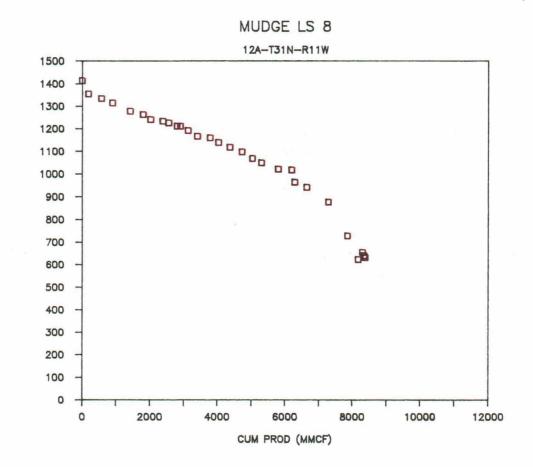
(AISY) Z/AHB

1985/86 MESAVERDE SIDETRACK PROGRAM

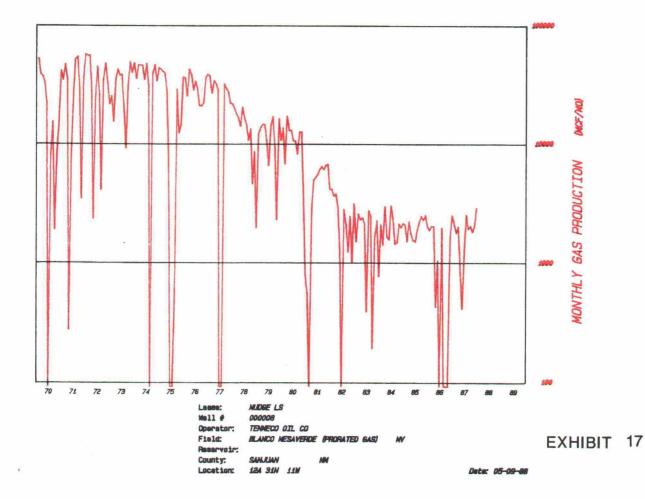
	PRE-ST_RATE (MCFD)	STABILIZED <u>POST-ST_RATE_(MCFD)</u>
HUGHES A LS 3	10	525
HUGHES A LS 4	23	660
VANDEWART A LS 5	40	625
HEATON LS 3	10	850
GARTNER LS 3	25	1100
JONES A LS 1	33	430
BOLACK B LS 1	60	500
ATLANTIC A LS 6	30	650
ROELOFS LS 3	0	800
SJ 28-7 UNIT #6	20	560
SJ 28-7 UNIT #9	15	485
SJ 28-7 UNIT #23	30	440
SJ 28-7 UNIT #26	40	630
SJ 28-7 UNIT #32	_27	640
AVERAGE	26	635

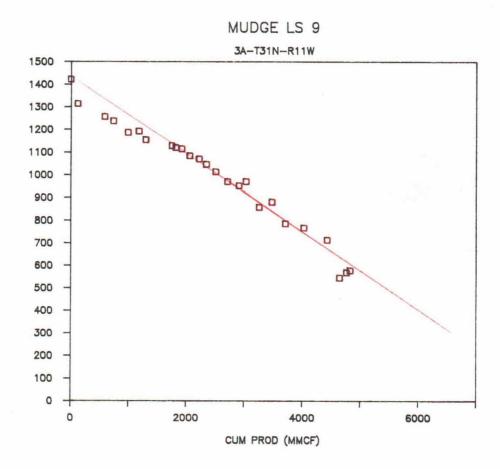
AVERAGE INCREMENTAL INCREASE = 609 MCFD

EXHIBIT 16

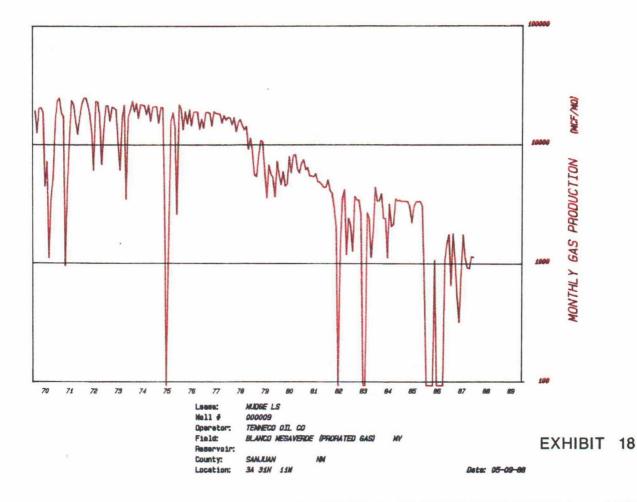




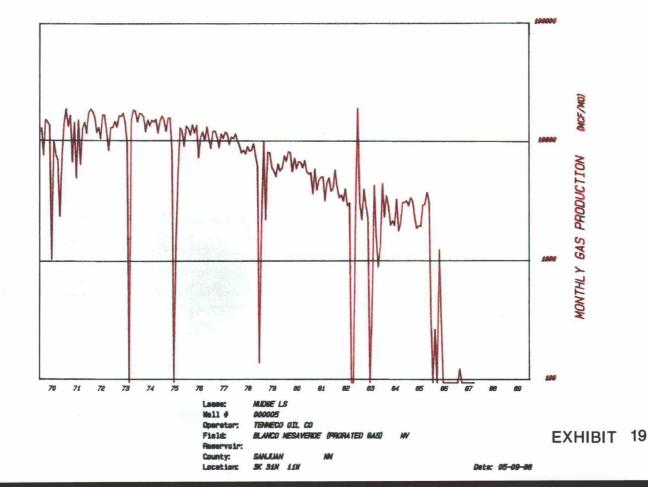






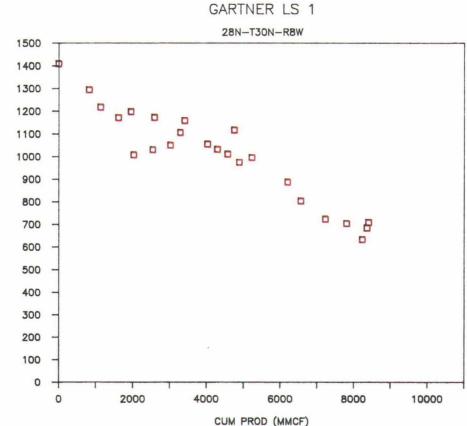


3K-T31N-R11W đ -0 CUM PROD (MMCF)



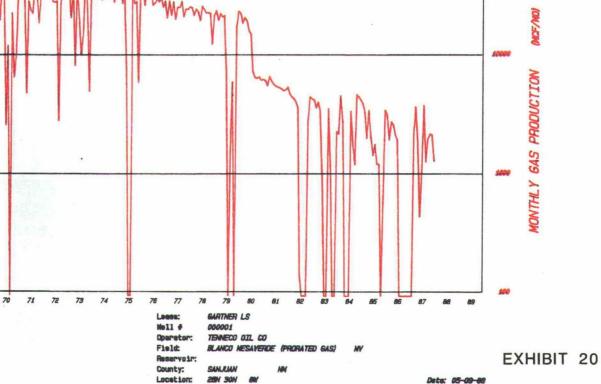
(AIRA) Z/AHB

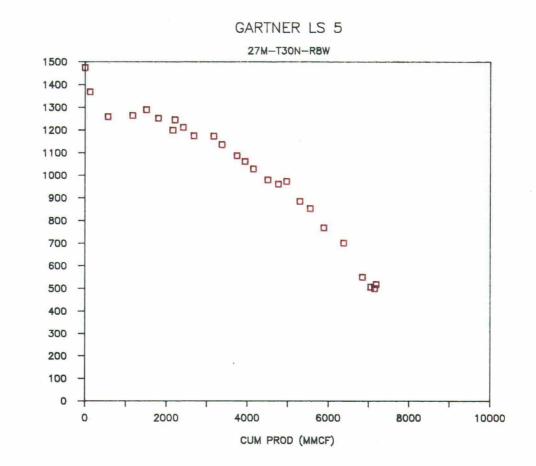
MUDGE LS 5



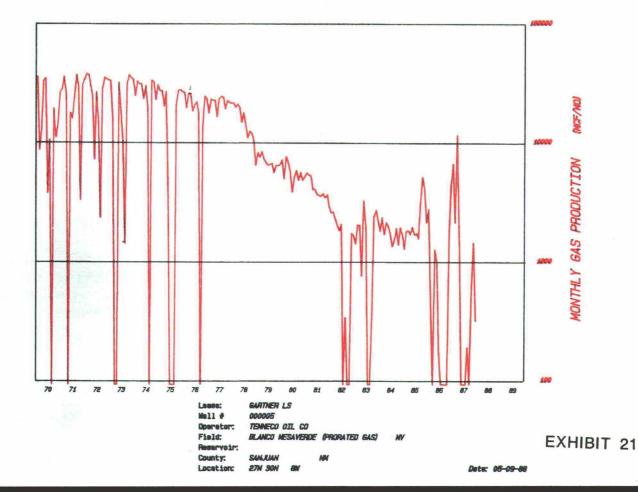


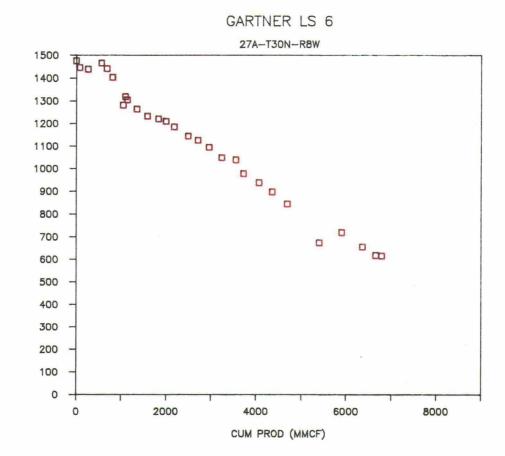
0 2000 4000 6000 8000 10000 CUM PROD (MMCF)













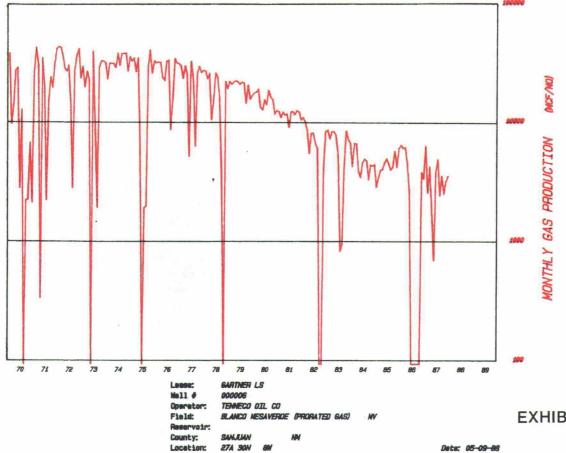
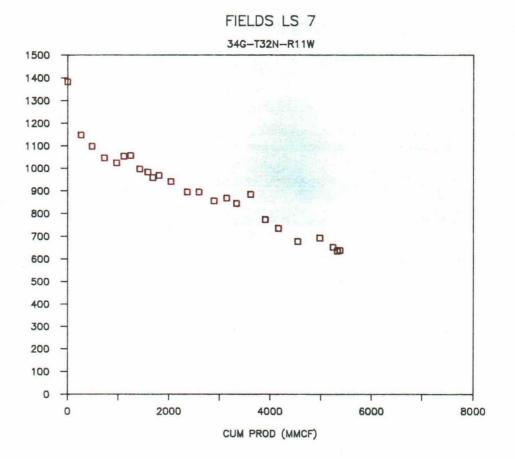
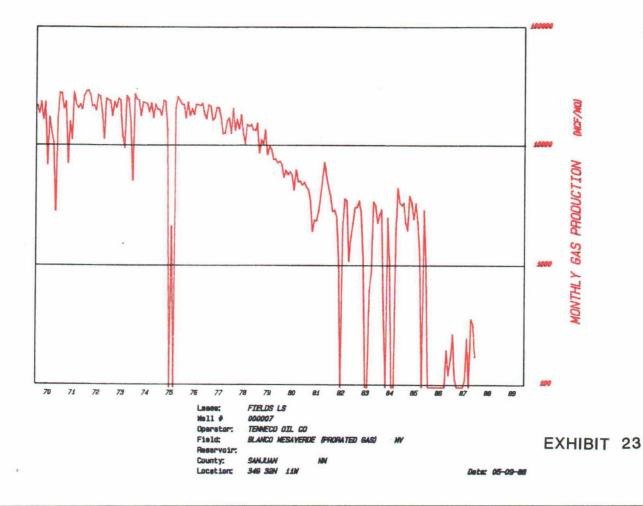
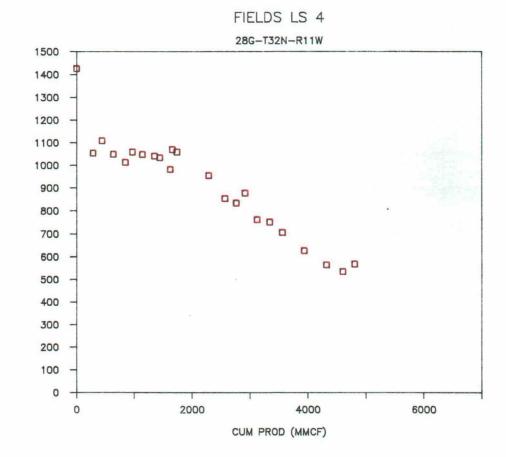


EXHIBIT 22

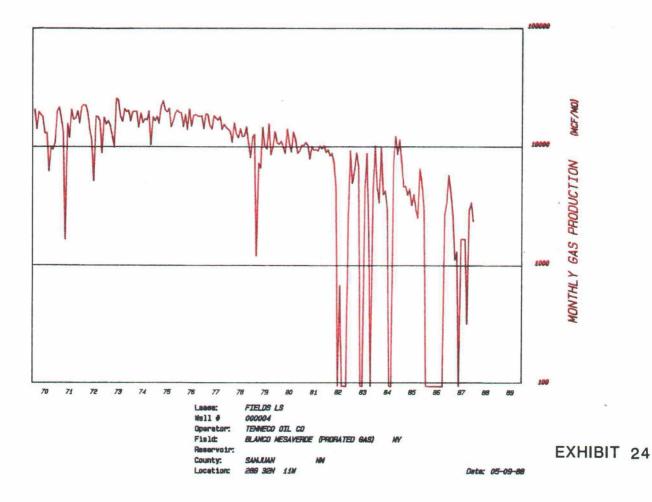


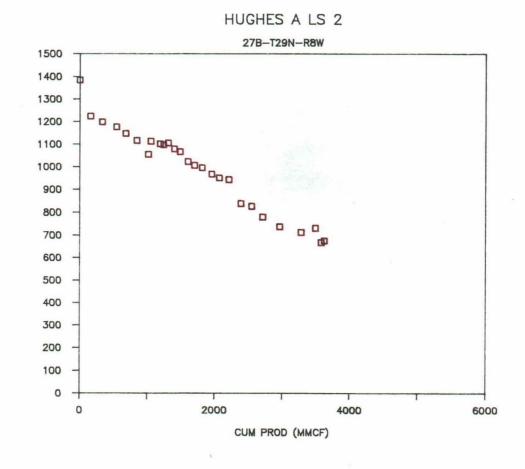




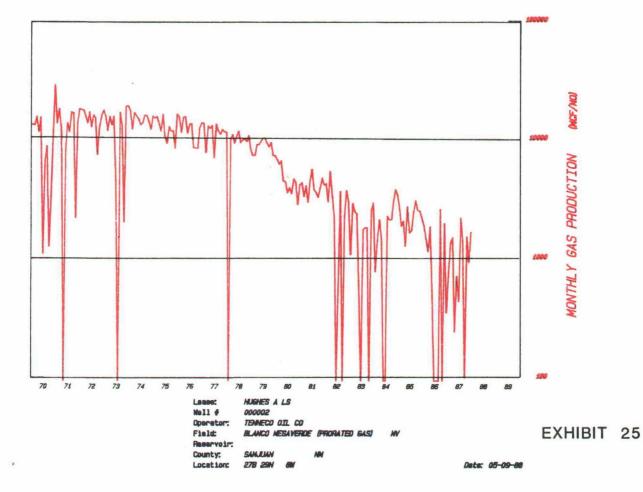




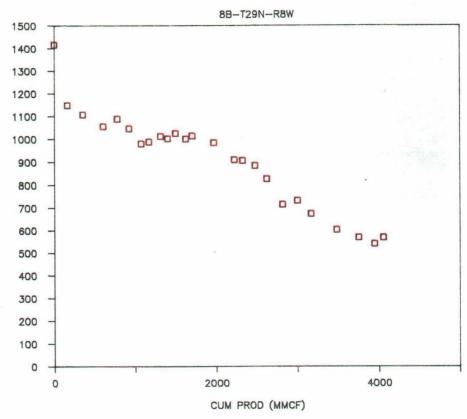




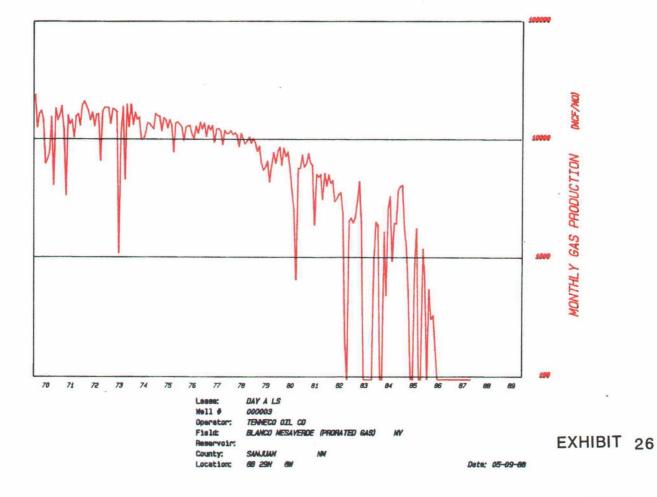


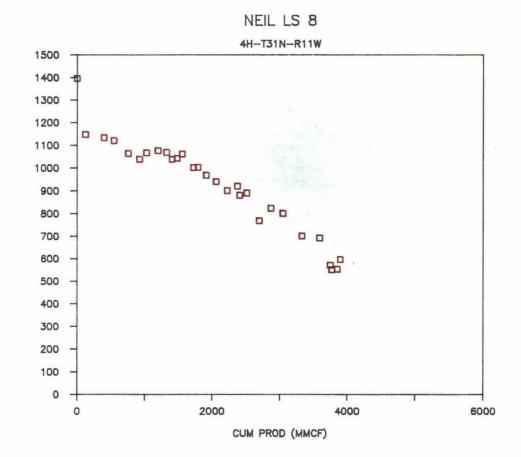




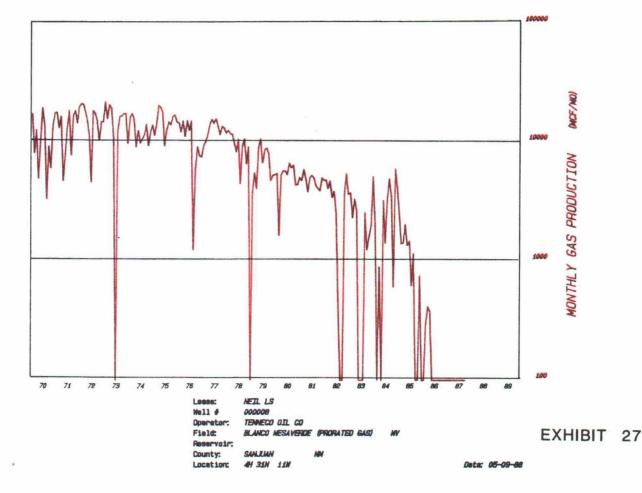


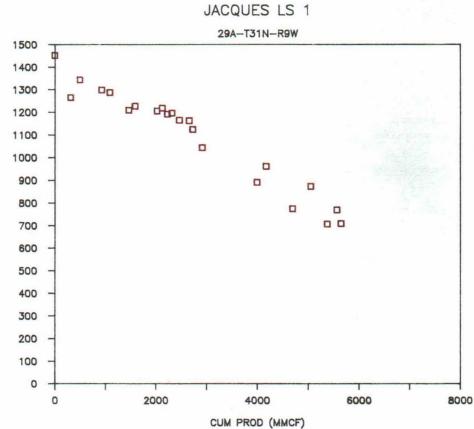




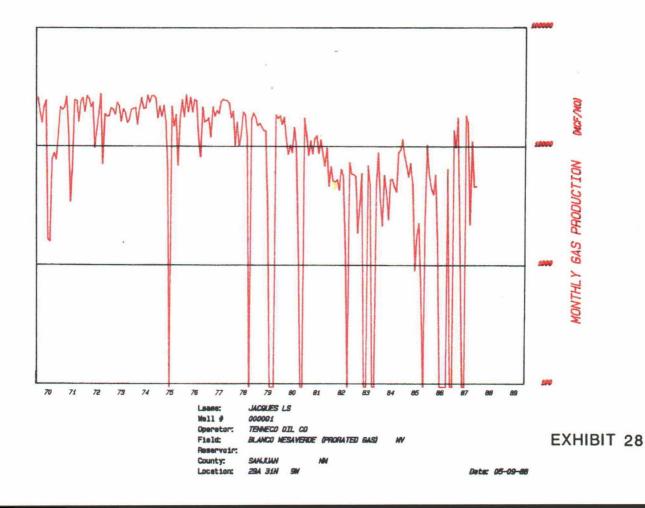


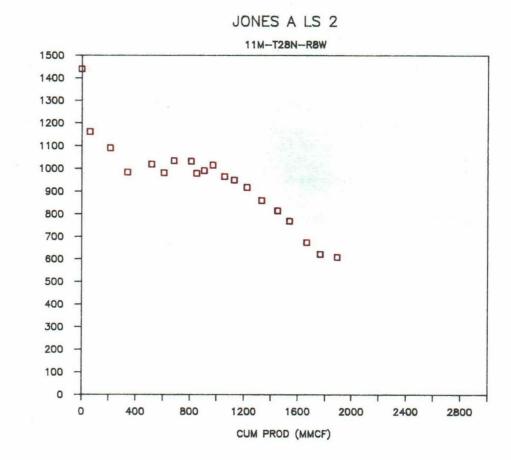




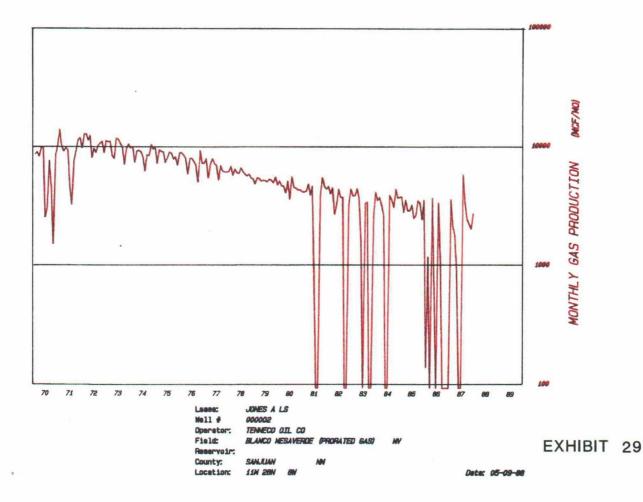


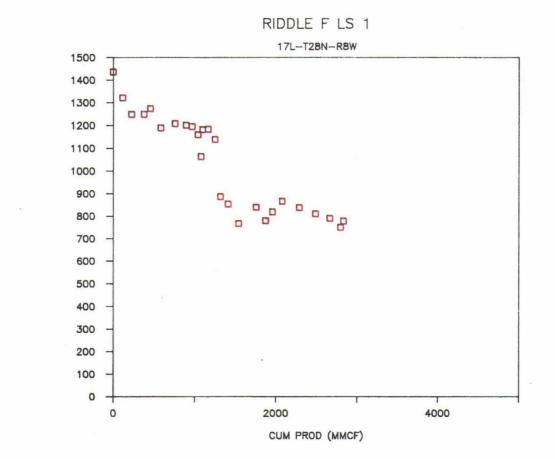


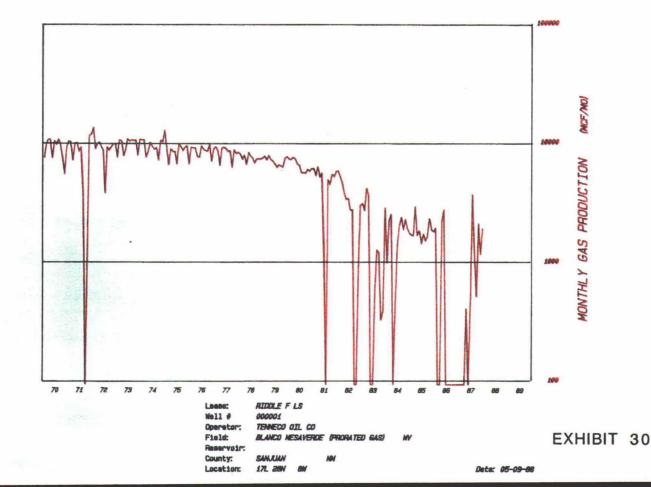






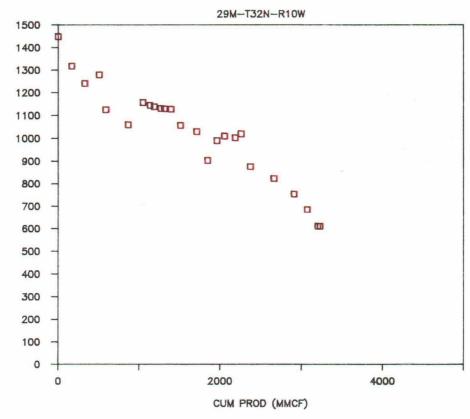




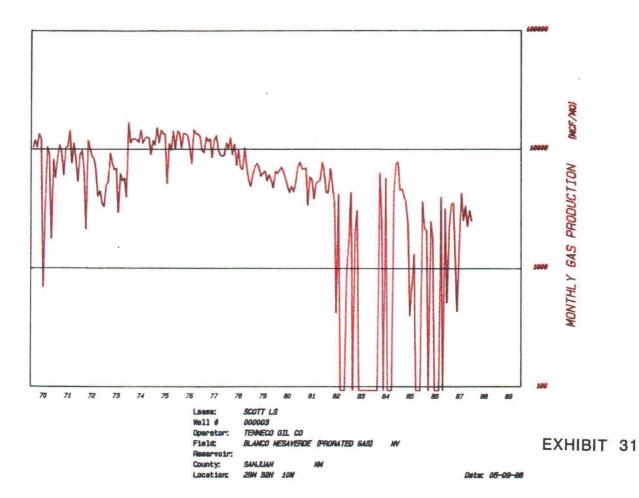


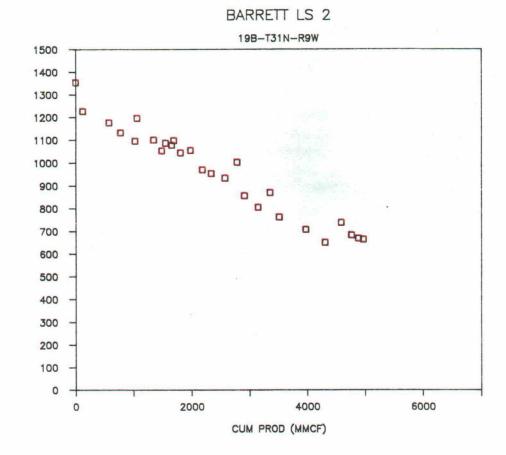
(AISA) Z/AHB











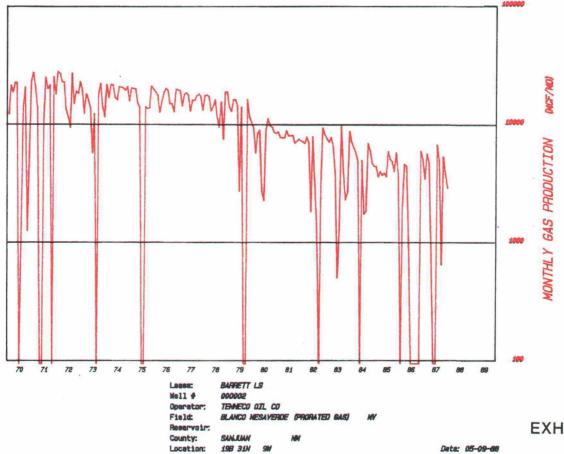
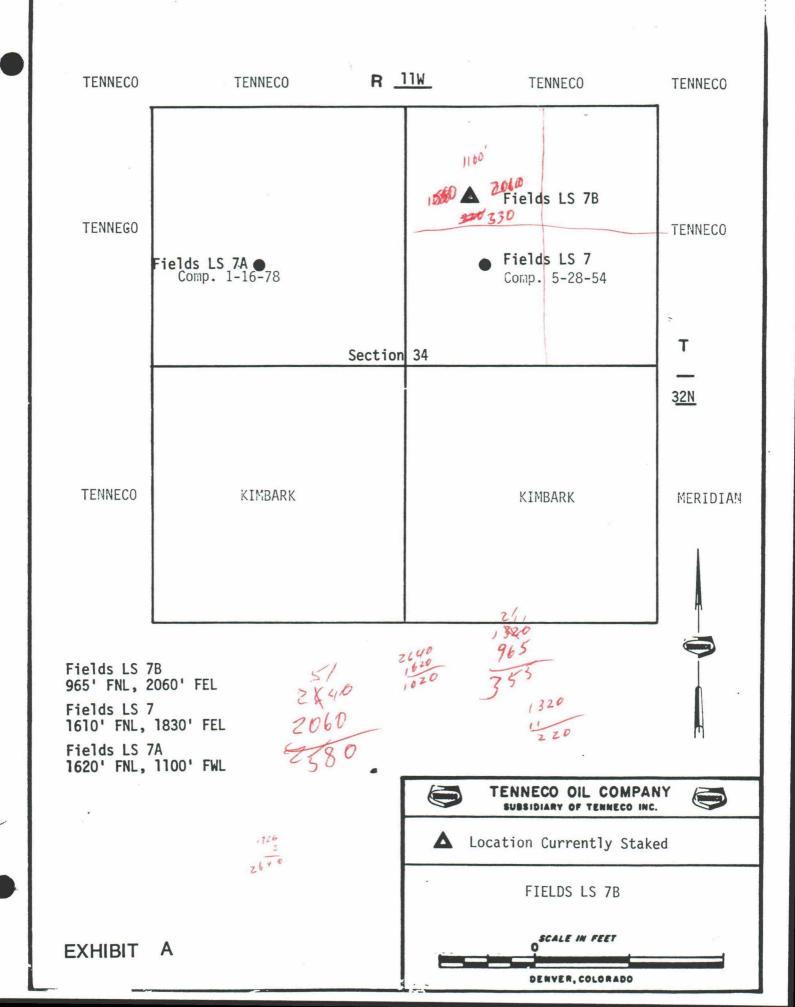
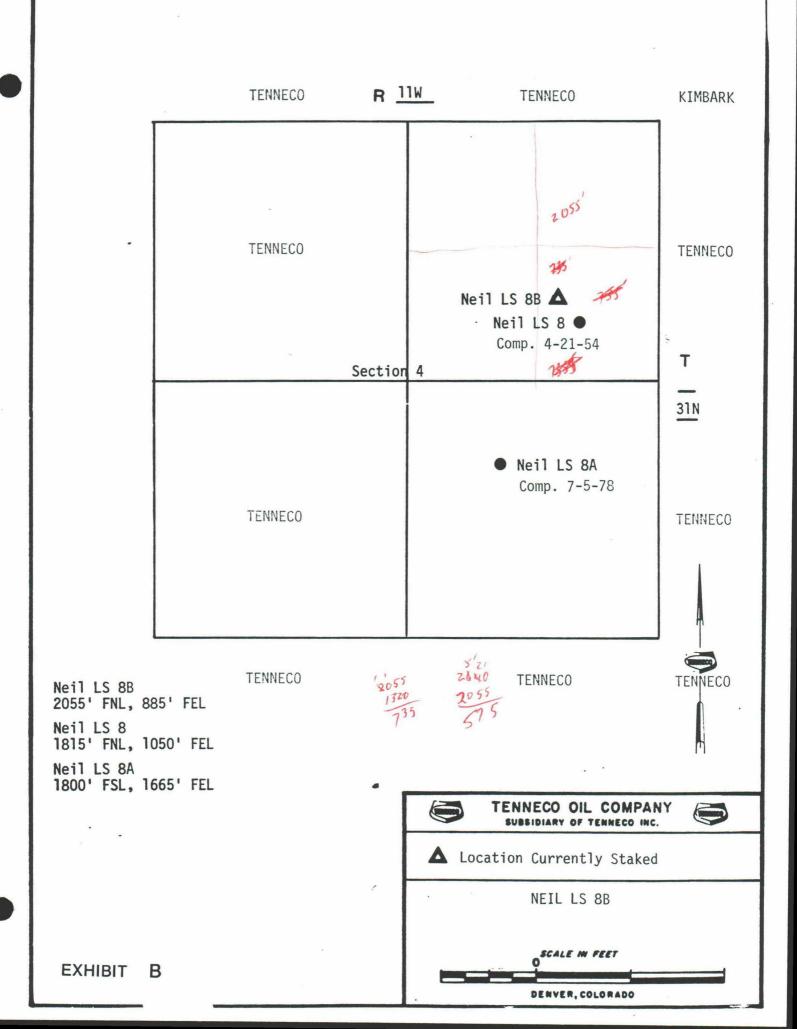
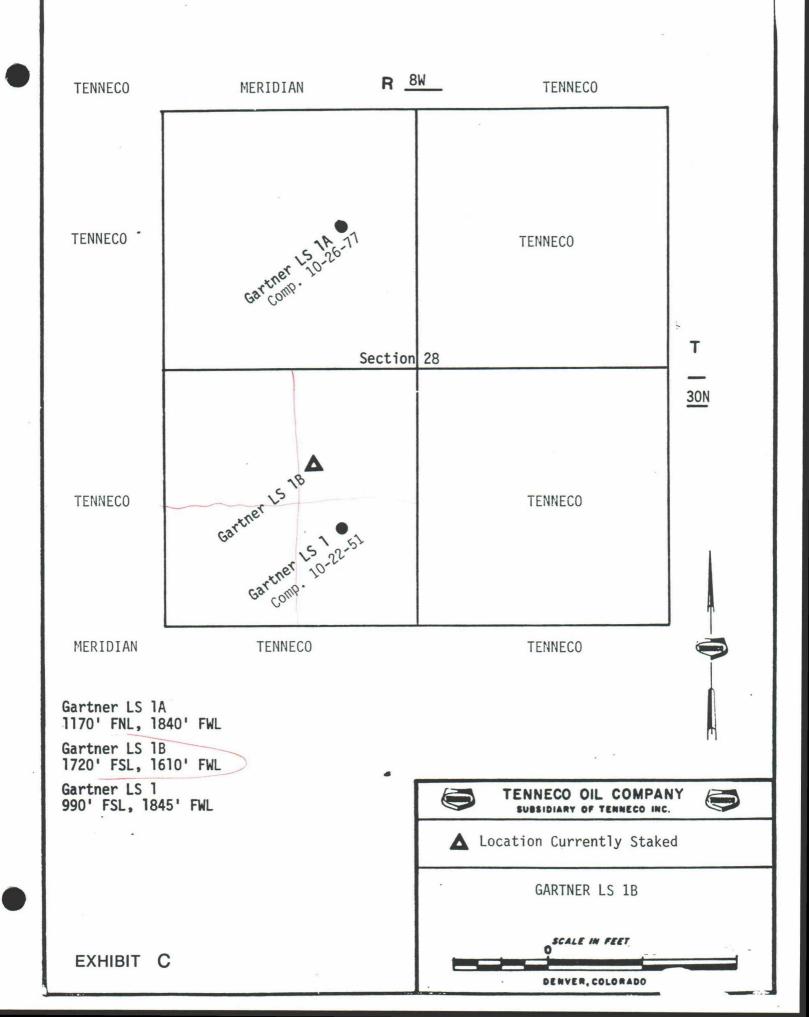
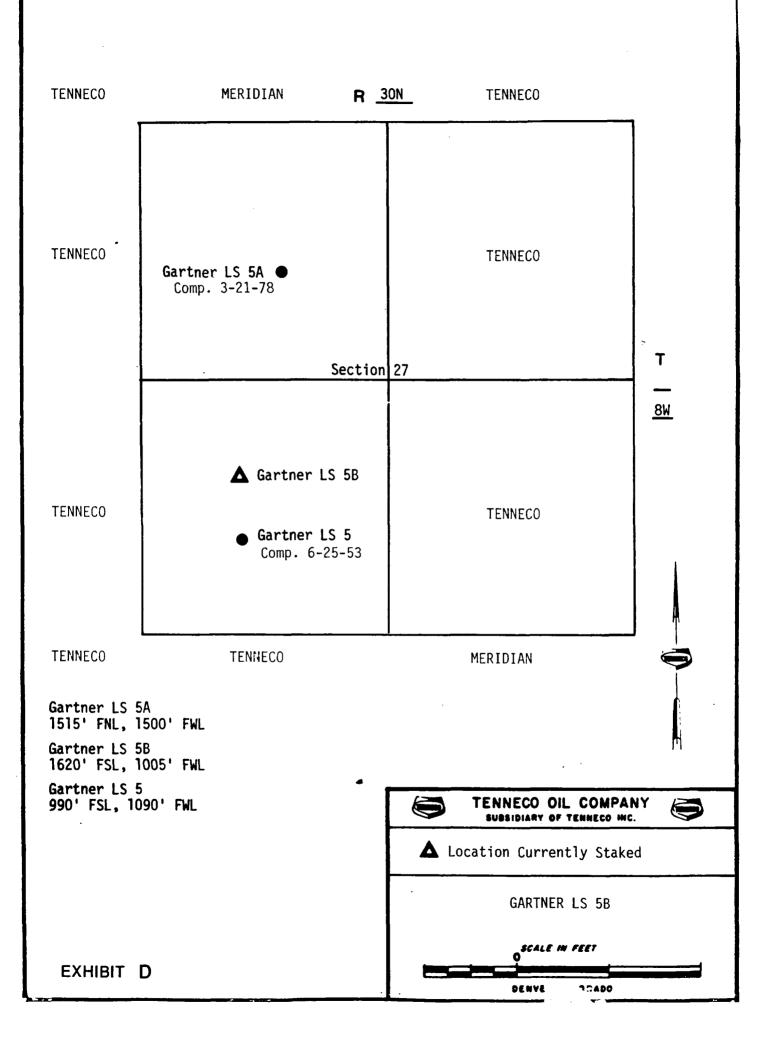


EXHIBIT 32

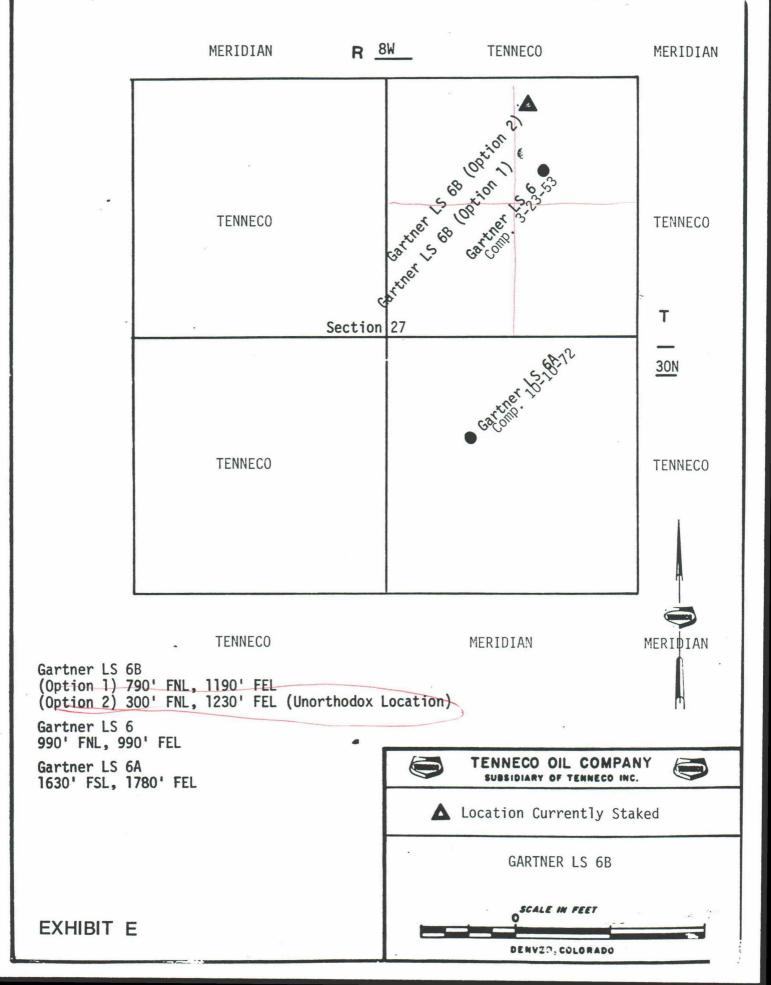


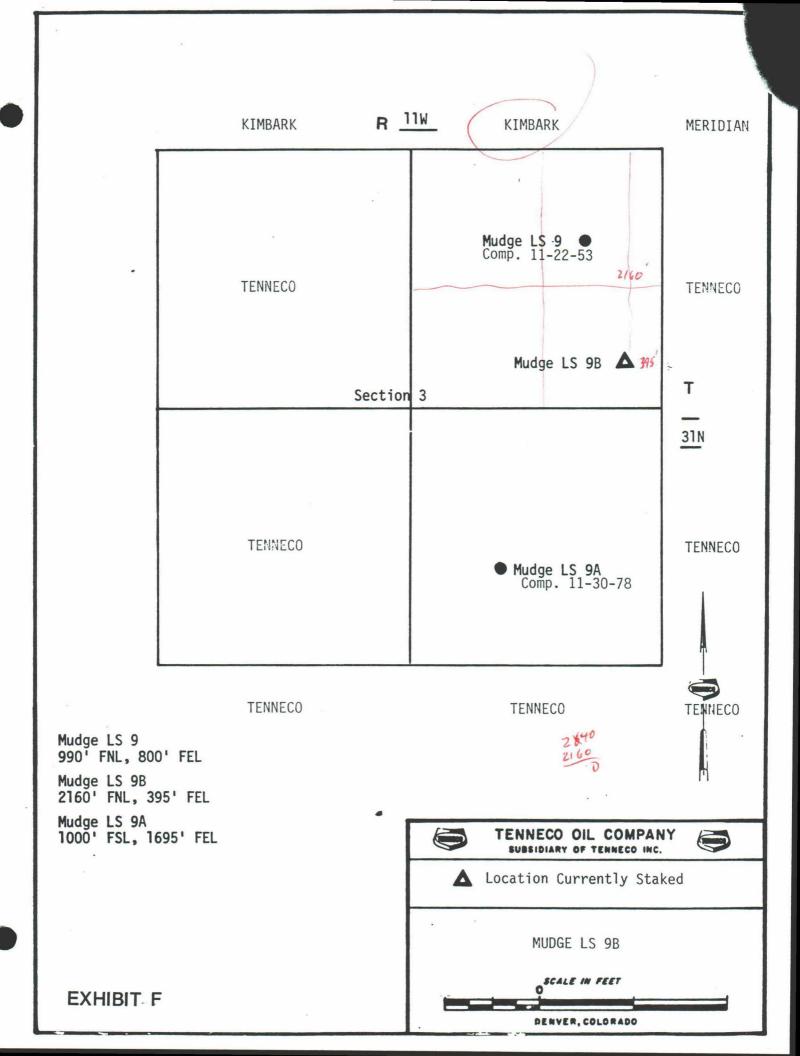


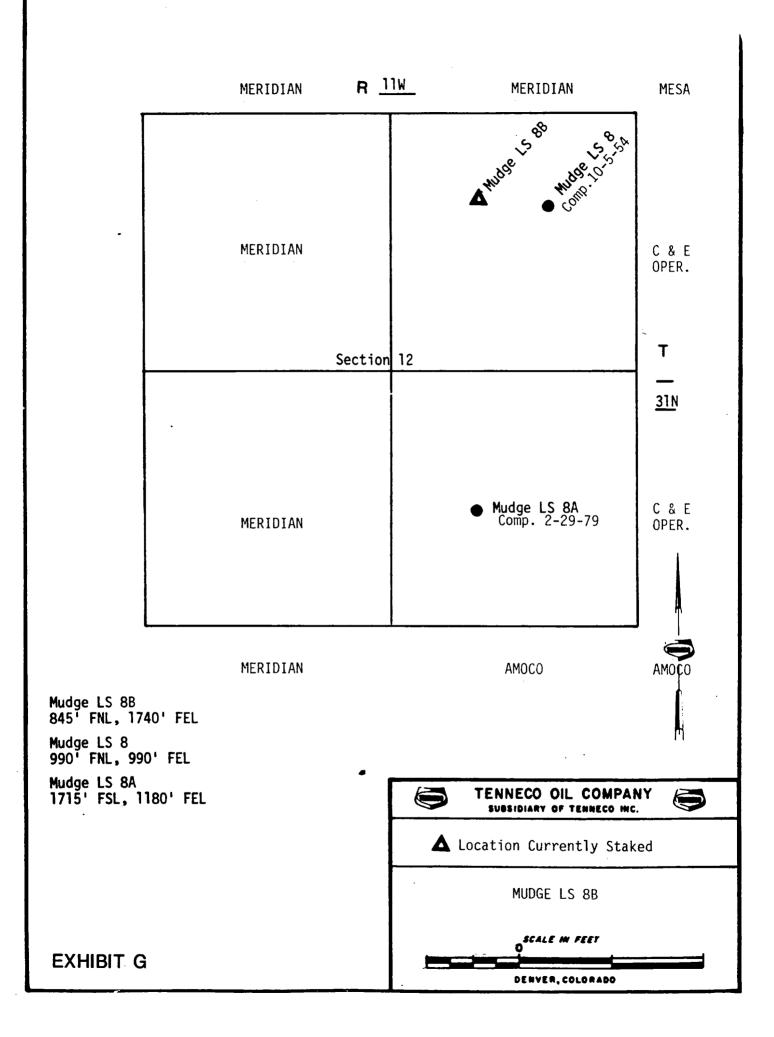


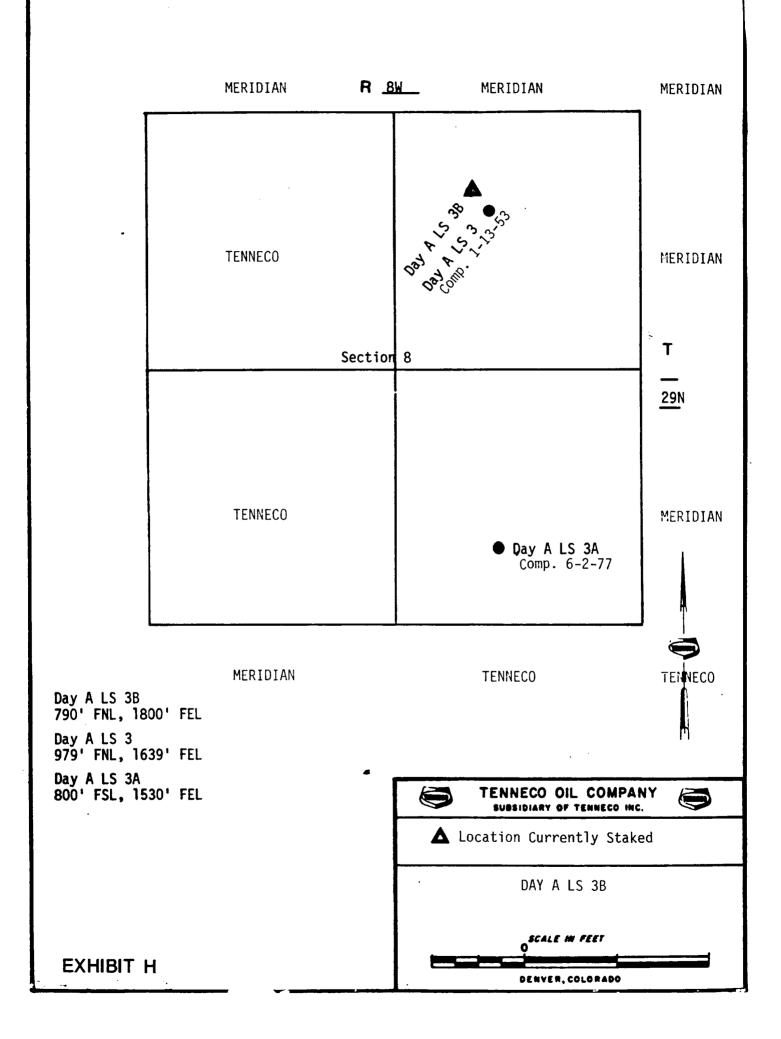


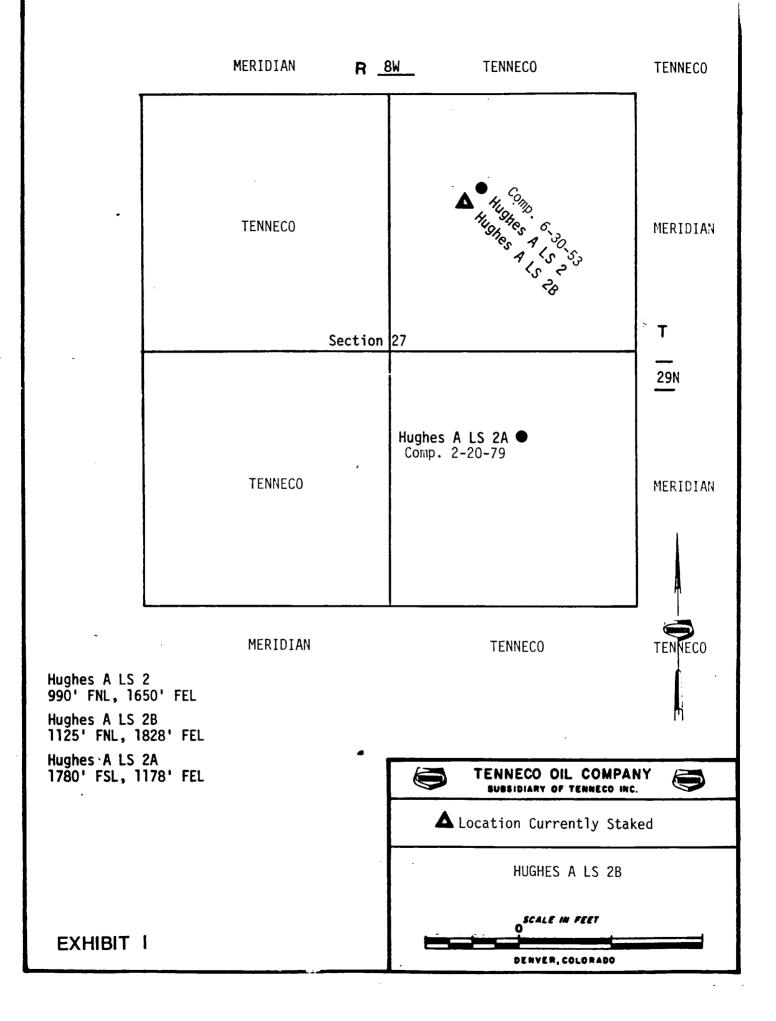
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