

APPLICATION OF ROBERT L. BAYLESS
 Simms Com #1
 Downhole Commingle
 NMOCD Docket #28-93; Case #10831

State of New Mexico
 Energy, Minerals and Natural Resources Department

Form C-122
 Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
 Santa Fe, New Mexico 87504-2088

EXHIBIT NO. 4

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Robert L. Bayless				Lease or Unit Name Simms			
Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 7/20/93		Well No. 1	
Completion Date 10/23/83		Total Depth 8731		Plug Back TD 4150 (B.P.)		Elevation 7023' GL	
Cig. Size 5 1/2"		Wt. d 15.5# 4.950"		Set At 8731		Perforations: From: 3709 To: 3715	
Tbg. Size 2 3/8"		Wt. d 4.7# 1.995"		Set At 3681		Perforations: From: To:	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None		Formation Pictured Cliffs	
Producing Thru Tubing		Reservoir Temp. °F 110		Mean Annual Temp. °F		Baro. Press. P. 12.0 (est.)	
Connection None		L		H		Gg est .65	
% CO ₂		% N ₂		% H ₂ S		Prover	
Meter Run		Taps		Country Rio Arriba		Pool East Blanco P.C.	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F
1.	2" x .750					1060	60	1065	130
2.									
3.									
4.									
5.									

over 9 years!

Calculated BHP = 1176

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$h_w P_m$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor. F _{pv}	Rate of Flow Q, Mcfd
1.	12.365		32	1.0000	1.240	1.020	500
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.05		1.23	0.962	A.P. I Gravity of Liquid Hydrocarbons	De ₁
2.					Specific Gravity Separator Gas	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure	P.S.I.A. P.S.I.
5.					Critical Temperature	R

NO.	P _i ²	P _w	P _w ²	P _c ² · P _w ²
1.	142	20.164	1,139,765	
2.				
3.				
4.				
5.				

P_c 1077 P_c² 1,159,929

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0177$ 2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0150$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 508$

Absolute Open Flow 508 Mcfd @ 15.025 Angle of Slope θ Slope, n .85

Remarks:

Approved By Division Conducted By: Cecil Bell Calculated By: Kevin McCord Checked By: