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State of New Mexico  
 Energy, Minerals and Natural Resources

Form C-103  
 Revised August 1, 2011

OIL CONSERVATION DIVISION  
 1220 South St. Francis Dr.  
 Santa Fe, NM 87505

WELL API NO. 30-025-38576 AND 30-025-42139
5. Indicate Type of Lease STATE <input checked="" type="checkbox"/> FEE <input type="checkbox"/>
6. State Oil & Gas Lease No. V07530-0001
7. Lease Name or Unit Agreement Name Linam AGI
8. Wells Number 1 and 2
9. OGRID Number 36785
10. Pool name or Wildcat Wildcat
4. Well Location Unit Letter K; 1980 feet from the South line and 1980 feet from the West line Section 30 Township 18S Range 37E NMPM County Lea
11. Elevation (Show whether DR, RKB, RT, GR, etc.) 3736 GR

SUNDRY NOTICES AND REPORTS ON WELLS  
 (DO NOT USE THIS FORM FOR PROPOSALS TO DRILL OR TO DEEPEN OR PLUG BACK TO A DIFFERENT RESERVOIR. USE "APPLICATION FOR PERMIT" (FORM C-101) FOR SUCH PROPOSALS.)

1. Type of Well: Oil Well ☐ Gas Well ☒ Other

2. Name of Operator  
DCP Midstream LP

3. Address of Operator  
370 17<sup>th</sup> Street, Suite 2500, Denver CO 80202

4. Well Location  
Unit Letter K; 1980 feet from the South line and 1980 feet from the West line  
Section 30 Township 18S Range 37E NMPM County Lea

11. Elevation (Show whether DR, RKB, RT, GR, etc.)  
3736 GR

12. Check Appropriate Box to Indicate Nature of Notice, Report or Other Data

NOTICE OF INTENTION TO:

PERFORM REMEDIAL WORK ☐ PLUG AND ABANDON ☐  
 TEMPORARILY ABANDON ☐ CHANGE PLANS ☐  
 PULL OR ALTER CASING ☐ MULTIPLE COMPL ☐  
 DOWNHOLE COMMINGLE ☐  
 OTHER: ☐

SUBSEQUENT REPORT OF:

REMEDIAL WORK ☐ ALTERING CASING ☐  
 COMMENCE DRILLING OPNS. ☐ P AND A ☐  
 CASING/CEMENT JOB ☐  
 OTHER: Annual Summary Report and Notification parameter review pursuant to NMOCC R12546-K ☒


13. Describe proposed or completed operations. (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion.

**Annual Summary for 2020 Pursuant to NMOCC R-12546-K and ACO-275 C-103 for Linam AGI#1 and AGI#2 and Request to Continue with Approved Immediate Notification Parameters for Operation of Both Wells**

This is annual summary submittal of data as agreed to between DCP and OCD relative to injection pressure, TAG temperature and casing annulus pressure for Linam AGI#1 until the well is worked over, which occurred in June 2017 and for Linam AGI#2 (API #30-025-42139) which was brought online in October 2015.

The analyses of data from both wells has been submitted monthly as required until the workover of the AGI#1 well and has also been submitted monthly for the AGI#2 well. The AGI#1 well was successfully worked over as planned in June 2017 and has been in use almost exclusively through 2018. In 2020 both wells were used and the effects are noted in the attached annual summary of the data. The purpose of this submittal is to provide OCD with the required summary of data for the 2020 calendar year for the operation of the Linam Ranch AGI Facility and to request to keep the approved immediate notification parameters in place for calendar year 2021.

The summary of the data and supporting tables and figures are attached.

SIGNATURE  TITLE Consultant to DCP Midstream/ Geolex, Inc. DATE 1/21/2021  
 Type or print name Alberto A. Gutierrez, RG E-mail address: aag@geolex.com PHONE: 505-842-8000

**For State Use Only**

APPROVED BY: \_\_\_\_\_ TITLE \_\_\_\_\_ DATE \_\_\_\_\_  
 Conditions of Approval (if any): \_\_\_\_\_

## **ANALYSIS OF 2020 ANNUAL TRENDS AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS FOR OPERATION OF LINAM AGI #1 AND LINAM AGI #2 (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all**

This document presents the results from the analyses of the injection parameter data collected from the Linam AGI #1 and #2 Wells which serve the Linam Ranch Gas Processing Facility near Hobbs, NM. Data from the Linam AGI #1 have been collected continuously since 2012 and have been analyzed on a monthly basis by Geolex and transmitted to DCP for reporting to NMOCD as required by ACO 275 and the approved post-workover C-103. In addition, the Linam AGI #2 well was completed and brought online in October 2015. The AGI #2 well was completed in the same injection zone as the AGI#1 approximately 450 feet to the southwest of AGI #1. From the time that AGI #2 was brought online, injection has been either into both wells simultaneously or solely into one of the two wells. AGI#2 was operated in conjunction with AGI #1 from October 2015 to January 2016 when a switch was made to operate only AGI#1 for the remainder of 2016. In May 2017, DCP switched over to injecting into AGI#2 to allow for the workover of AGI#1. The workover was completed on June 8, 2017 and AGI #1 was brought back online in July 2017 with bottom hole sensors installed. These sensors are now serving to monitor downhole and reservoir conditions since the downhole sensors in AGI #2 failed due to a lightning strike shortly after installation (2015) and will not be able to be repaired until sometime in the future when AGI #2 is worked over. In the meantime, in order to obtain reservoir data which would have been provided by the downhole PT sensors in AGI #2, a slick line with a pressure recorder was placed into AGI #2 and downhole pressure data were collected under both injection and non-injection conditions for the AGI #2 and AGI #1. Since that time the downhole sensors in AGI#1 provide the necessary reservoir data needed to evaluate the performance of the two wells. The system continued operating through 2018 with only AGI #1 active while waiting for independent flow meters to be installed/repared in both wells so that reliable flow information would be available for each well independently. This operational mode (utilizing only AGI #1) continued through April 2019, and to date separate volume meters have not been installed/repared. In May 2019, however, DCP began dividing the flow of acid gas between the two wells by using one or the other well exclusively (see Figure 3). Presently, surface data from both wells is being collected relative to the following parameters:

- Treated Acid Gas (TAG) surface injection pressure (both wells),
- TAG injection temperature (both wells),
- Annular pressure (both wells)
- Bottom Hole pressure and temperature (AGI#1 only beginning 7/2017)
- Overall total TAG flow rate from compressors

The above are the key parameters which are currently being measured in both wells in order to monitor the operations of the wells, prevent hydrate formation and reduce corrosion potential following the workover of AGI#1. While improvements have been implemented in the placement of temperature controls, dehydration of TAG during compression and other systems improvements at the AGI facility, there continue to be variations in the desired and normal operating levels of the above-referenced

parameters. Since these parameters are useful indicators and predictors of potential operational or mechanical problems in the well, various levels of alarms have been established for each of these parameters. These parameters include three which are measured directly (TAG injection pressure, TAG injection temperature and annular pressure) and one (differential pressure) which is a calculated value (the difference between the two measured parameters of injection and annular pressure). The analyses of the long-term trends in these values have been useful in smoothing out shorter-term variations which can be observed from detailed inspection of hourly data and in the development of appropriate alarm bands for each parameter.

The Linam AGI #1 experienced a tubing leak in late 2011 which was partially addressed in a workover conducted in April/May 2012. The leak was detected in the end of 2011, and beginning of 2012 (until the time of the workover) the injection parameters were reviewed, analyzed and reported weekly to the NMOCD. Following the workover in which the tubing leak was repaired, some compromised production casing was detected immediately above the packer depth. At that time, we recommended keeping only approximately 250 psig on the annular space between the tubing and casing in AGI #1 since with annular pressure at this level, under normal operating conditions, this parameter can serve as a useful indicator of when activity should be initiated to prevent damage to the well or trigger a NMOCD shutdown and/or immediate notification requirements. Concern about this compromised casing was eliminated by stacking packers when the well was worked over again in June 2017. All of the data from January 2012 through December 2015 are included in our analysis, but only the post-workover data have been used to develop the recommended alarm and emergency shutdown (ESD) levels in conjunction with the requirements of NMOCD Order 12546-all, ACO-275 and the post-workover C-103.

Furthermore, a similar process has been employed on the Linam AGI#2 since it was brought online in October 2015. As described above, this well is equipped with bottom hole (just at top of packer) P/T measurement capability both inside and outside the tubing. In general, the immediate notification parameters for both wells were developed from this long-term analysis of the injection data. Initial testing of the Linam AGI#2 indicates that the pressure variations induced by flow rate and temperature fluctuations in the Linam AGI#1 are influencing the reservoir as measured in the AGI #2 location. This is to be expected as the new well is completed in the same zone at a distance away from the initial well which we predicted would see the edge of the plume in about 7 years. The Linam AGI #1 has been injecting for approximately 13 years.

Data from AGI #1 were continuously collected and analyzed weekly prior to the original workover in April/May 2012 and then monthly after the workover from June 2012 through December 2017 (see Figure 1). These data collection, analysis and reporting functions continue as required by NMOCD on a monthly basis. Furthermore, since it is necessary to evaluate the data from both wells to know how the system is operating overall, the surface data from AGI #2 are also being collected, analyzed and reported monthly. The reporting requirement for the AGI #2 is only quarterly and now that AGI #1 has been successfully worked over, the reporting for both wells will shift to quarterly as soon as independent reliable volume measurement is available for each well.

The NMOCD also requires that immediate notification parameters and levels be discussed and agreed upon with the agency, and that these be periodically reviewed and updated as needed based on operational or regulatory changes. The immediate notification parameters for both wells have been approved by NMOCD, and DCP requests no changes in these approved values. With this requirement in mind and for the purpose of protecting the mechanical integrity and safety of both wells and the overall AGI facility, Geolex monitors these data under contract to DCP to prevent damage to the wells or violation of regulatory requirements or permit constraints.

After 9.5 years (113 months) of carefully analyzing the performance of AGI #1 on a continuous basis, Geolex has assembled the data and has analyzed observed trends for the post-workover period of June 2012 – December 2020 as can be seen on Figure 2. Several important observations can be made from analyzing these data and taking into consideration important system modifications that have occurred during this time period. These include the following:

1. AGI #1 Post-Workover MIT completed in May 2012
2. AGI #1 MIT test completed November 14, 2012
3. Bleeding of diesel from casing annular space immediately after the November 2012 AGI #1 MIT test.
4. AGI #1 MIT test completed April 30, 2013
5. Addition of diesel in annular space after April 2013 AGI #1 MIT and May 2013 plant shutdown
6. AGI #1 MIT test completed October 30, 2013
7. Failure of the VFD for the cooler on the AGI compressor from February 4 through 9, 2014.
8. AGI #1 MIT test completed April 30, 2014
9. Addition of diesel in annular space after April 2014 AGI #1 MIT
10. AGI #1 MIT test completed September 19, 2014
11. AGI #1 MIT test completed March 19, 2015
12. AGI #1 MIT test completed September 15, 2015
13. AGI #2 brought online with startup in October-November 2015 and operated until January 2016
14. AGI #1 MIT test completed March 22, 2016
15. AGI #2 MIT test completed April 1, 2016
16. AGI #2 TAG lines bled to flare on June 13, 2016 to remove static TAG in line when well is not operating.
17. AGI #1 MIT test completed September 14, 2016
18. AGI #1 Workover completed June 8, 2017 including stacked packer, bottom hole PT gauges
19. AGI #1 MIT test completed June 7, 2017 after workover completion
20. AGI #2 MIT test completed February 16, 2017
21. AGI #2 MIT test completed February 15, 2018
22. AGI #1 MIT test completed June 19, 2018
23. AGI #2 MIT test completed February 15, 2019
24. AGI #1 MIT test completed February 15, 2019
25. AGI #1 MIT test completed February 4, 2020
26. AGI #2 MIT test completed February 4, 2020

The following trends have been observed in the AGI well data and are reflected on Figures 1 & 2:

1. TAG injection pressure which was on a slight increasing trend due to slightly increasing average temperature of injected TAG but began to level off due to temperature decreases in 2017. This trend continued over the last six months of 2018 and all of 2019. The TAG injection pressure and rate has been more variable since 2016 due to inlet flow variations, and AGI#1 was used exclusively from time of the workover in June 2017 through April 2019.
2. Flow of TAG has been split between the two wells since April of 2019 with either one or the other being used exclusively but not simultaneously (see Figure 3).
3. The TAG injection temperature increased slightly with an arithmetic mean of 95°F in 2020 up from 92°F in 2019, 98°F in 2018, 106°F in 2017 and 113°F in 2016.
4. The TAG injection temperature is significantly lower during periods of low flow into either AGI well when the other well one is being used.
5. Pressure in the casing annulus has been consistently tracked; the correlative nature of variable injection temperature, pressure and flowrate, and its arithmetic mean for the period ending 12-31-20 has been approximately 190 psig essentially the same as 191 in 2019. The injection temperature is the largest influencer of this parameter under normal conditions.
6. The pressure differential between the casing annulus and the TAG injection pressure clearly indicates that no communication currently exists between the tubing and casing annulus.
7. The generally low annular pressures observed indicate that the production casing/cement still has good integrity.
8. TAG injection temperatures can now be lower due to the improvement of water reduction in compression which reduces the potential for hydrate formation at lower temperatures. This has allowed for lower injection temperatures throughout the 2018-2020 period.

Given the observations of the trends in the graphs and the competing influence of average injection temperature decrease and that injection volumes have been more variable since 2018, the observed TAG injection pressure changes are predictable and normal. There is no current indication of the reservoir being pressured up to any significant degree by the injection from Linam AGI #1. This was confirmed during the drilling and testing of AGI #2. Upon startup from any shutdown that lasts more than 6-8 hours it is critical to inject methanol along with the TAG for the initial startup period to prevent the formation of hydrates. While this may no longer be necessary due to the changes which were made in the water removal efficiency of the AGI compressor system, it is a good preventative measure. Prior to the increased water removal efficiency, this effect was observed in the period of March 2013 when hydrate formation during one of these events caused a spike in TAG injection pressure of approximately 35% over normal pressures due to partial blockage of the injection line and tubing created by the hydrate formation. This persisted for several hours until the situation was alleviated by the stabilization of the compressor and the simultaneous injection of methanol to cause the hydrates to be reabsorbed into the TAG. Injection pressures and temperatures then returned to normal.

It is also critical to maintain the temperature control on the injected TAG and to avoid rapid temperature or pressure fluctuations during periods when power failures or other mechanical failures may occur. The

extensive and wide variation in TAG injection temperatures observed prior to the failure of the tubing in late 2011, resulted in the formation of free water within the tubing and corrosion resulting in a tubing leak which had to be repaired in April/May 2012. Temperature control changes were implemented and helped to significantly control downward swings in temperature and prevent the formation of hydrates.

However, in February 2014, there was a failure in the VFD for the cooler on the AGI compressor which persisted for five days. During this period of time, the TAG temperature increased to at least 150 °F, and the annular pressure increased dramatically due to the heating of the diesel fluid in the annular space as a result of the elevated TAG injection temperature. TAG temperature as well as annular pressure returned to the normal range once the VFD on the cooler was repaired. The significant spread between TAG injection pressure and the annular pressure maintained even during this heating episode proves the continued integrity of the well, packer, casing and tubing. However, the rise in annular pressure has a potential to damage the integrity of the compromised casing in the well and should be avoided during all subsequent operations. In response to these issues, DCP undertook and successfully completed a project in 2015 to address the temperature fluctuations resulting from compression controls and to increase the efficiency of water removal to the point where all free water is removed from the TAG prior to injection. This significantly reduces hydrate formation potential in the entire system regardless of temperature variations. This has allowed for the lower average injection temperatures observed throughout 2018 and 2019 to not have caused any hydrate formation.

In October 2015, AGI #2 was started up and operated in a startup mode switching back and forth from AGI #1. This effect is reflected in the trend data shown in Figure 2. Due to a volume meter sensor failure and configuration issues which are currently being addressed, only total flow to the AGI system can be reliably measured through 2019. Flow has been split between the two wells since April of 2019, but each well is used exclusively when that is done. For 2020 AGI#2 only operated until July 16, 2020 at 9am when flow was switched to AGI#1 and only AGI#1 was used for the balance of 2020. They are not used simultaneously. See Figure 3 for total flow rate and flow rate to AGI #1 and AGI #1.

## **REVIEW OF STATISTICAL ANALYSIS OF INJECTION PARAMETERS, DEVELOPMENT OF AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all**

The statistical analyses of the injection parameter data were initially conducted for the purpose of establishing normal operating levels for these parameters which are automatically monitored. Several data filtering steps were accomplished to take the hourly data which forms the basis of the analysis in order to smooth out variability and to account for the physical changes in the well and its operation after the repair of the tubing leak in the workover completed in May 2012. Because the configuration of the well changed dramatically after the workover, only data after the well had stabilized post-workover were used in this analysis. Furthermore, the subsequent stacked packer workover of the AGI#1 in June 2017 was completed and essentially only the AGI #1 has been used since then. The bottom hole PT sensors installed during the 2017 workover of AGI #1 have been providing excellent data throughout 2020 and these data are shown on the graph attached here as Figure 4. During 2018 we resolved some communication issues between the Halliburton BHPT panel and the plant DCS system and corrected

some BHPT readings which had been inaccurately reported from 11/2017 to 6/2018 until this issue was detected. In 2018 for the period affected, we downloaded the data directly from the Halliburton panel and corrected the values. A C-103 was submitted with these corrections in July 2018. The corrected values are used in this analysis. No problems with BHPT readings occurred in 2019 or 2020. It is clear from the variation in these parameters when flow is switched between wells that the conditions measured in the BHPT gauge in AGI#1 reflect the values in the reservoir which would be very similar in AGI #2 if the BHPT gauges in the well were operational.

All the data are summarized in Table 1, and the calculated statistical parameters of arithmetic mean and standard deviation were used to establish base levels and variability for each parameter. The results of these analyses resulted in the immediate notification parameters which were approved both for AGI #2 and the parameters required under ACO 275 for AGI#1.

Based on the analysis of observed trends, the immediate notification parameters which were approved for AGI #1 and the parameters previously approved for AGI# 2 and continued through 2020 remain appropriate to continue through 2021. This is DCPs request and the approved immediate notification parameters are detailed below:

The approved immediate notification parameters for Linam AGI #1 are summarized below:

1. Exceedance of the approved MAOP of 2644 psig surface for a period greater than two hours.
2. Failure of a mechanical integrity test (MIT) of the well.
3. Confirmation of any condition that indicates a tubing, packer or casing leak.
4. Any increase of the annular pressure to a value that is greater than 1200 psig
5. Any instance in which differential pressure between the injection tubing and injection tubing annulus is less than 100 psig.
6. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
7. Any workover or maintenance activity that requires intrusive work in the well.

The approved immediate notification parameters for the Linam AGI #2 are summarized below:

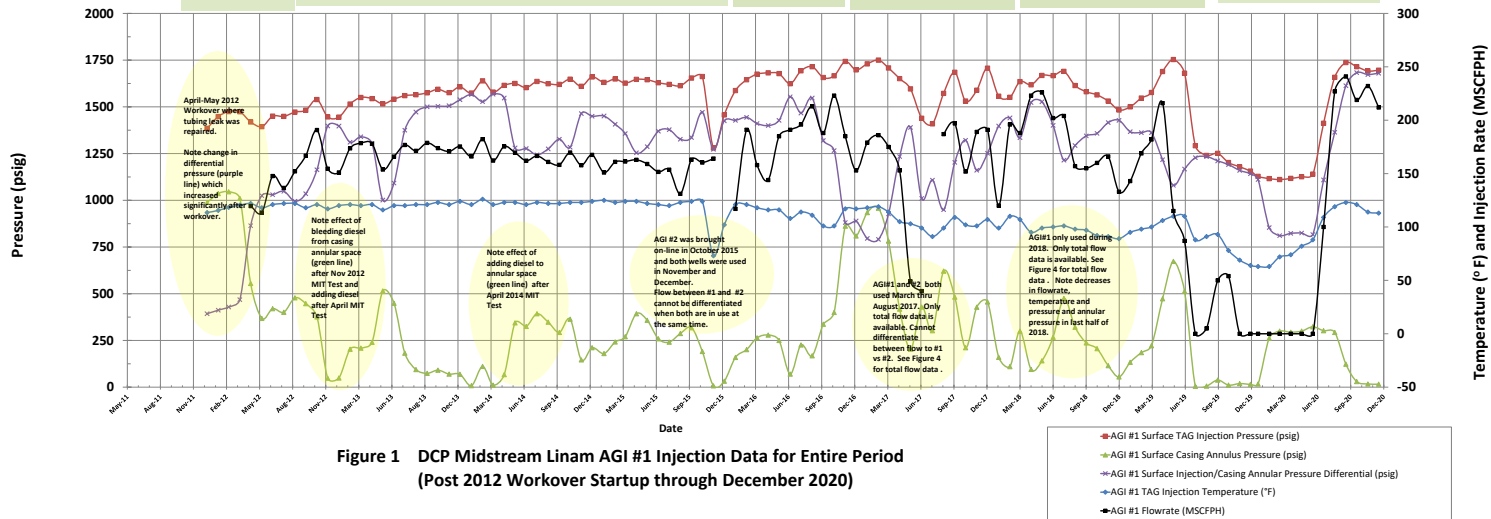
1. Exceedance of the approved MAOP of 2644 psig surface for a period greater than two hours.
2. Failure of a mechanical integrity test (MIT) of the well.
3. Confirmation of any condition that indicates a tubing, packer or casing leak.
4. Any increase of the annular pressure to a value that is more than 80% of the injection pressure.
5. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
6. Any workover or maintenance activity that requires intrusive work in the well.

TABLE 1 SUMMARY DATA ANALYSIS OF LINAM AGI #1 TRENDS FOR JANUARY 2012 THROUGH DECEMBER 2020 (3 PAGES)

DCP MIDSTREAM LINAM RANCH AGI #1 AND #2 CUMULATIVE INJECTION DATA																																
Month Ended				AGI #1 TAG Injection Temperature (°F)		AGI #1 Surface TAG Injection Pressure (psig)		AGI #1 Surface Casing Annulus Pressure (psig)		AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)		AGI #1 Average Bottom Hole Pressure (psig)		AGI #1 Average Bottom Hole Temperature (°F)		Total Flowrate (MSCFPH)		AGI #1 Flowrate (MSCFPH)		AGI #2 Flowrate (MSCFPH)		AGI #2 Surface TAG Injection Temperature (°F)		AGI #2 Surface TAG Injection Pressure (psig)		AGI #2 Surface Casing Annulus Pressure (psig)		AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)				
January	2012	Jan-12	Jan-12	Jan-12	114	1385	989	393									N/A	N/A	0										No Flow Data Available			
February	2012	Feb-12	Feb-12	Feb-12	116	1448		1036	412								N/A	N/A	0											No Flow Data Available		
March	2012	Mar-12	Mar-12	Mar-12	118	1475		1046	429								N/A	N/A	0											No Flow Data Available		
April	2012	Apr-12	Apr-12	Apr-12	121	1474		1010	468								N/A	N/A	0											No Flow Data Available		
May	2012	May-12	May-12	May-12	122	1419		555	864								120	120	0											Plant Workover and Shutdown		
June	2012	Jun-12	Jun-12	Jun-12	118	1394		368	1025								113	113	0											Plant Workover and Shutdown		
July	2012	Jul-12	Jul-12	Jul-12	121	1450		420	1030								148	148	0													
August	2012	Aug-12	Aug-12	Aug-12	122	1449		401	1048								137	137	0													
September	2012	Sep-12	Sep-12	Sep-12	122	1472		478	995								152	152	0													
October	2012	Oct-12	Oct-12	Oct-12	118	1482		447	1035								167	167	0													
November	2012	Nov-12	Nov-12	Nov-12	121	1539		376	1163								191	191	0											November 14, 2012 MIT Test		
December	2012	Dec-12	Dec-12	Dec-12	117	1446		48	1398								155	155	0													
January	2013	Jan-13	Jan-13	Jan-13	120	1445		49	1397								151	151	0													
February	2013	Feb-13	Feb-13	Feb-13	121	1515		203	1311								174	174	0													
March	2013	Mar-13	Mar-13	Mar-13	120	1550		209	1340								179	179	0													
April	2013	Apr-13	Apr-13	Apr-13	121	1544		240	1304								178	178	0											April 30, 2013 MIT Test		
May	2013	May-13	May-13	May-13	116	1516		515	1001								154	154	0													
June	2013	Jun-13	Jun-13	Jun-13	120	1541		449	1092								166	166	0													
July	2013	Jul-13	Jul-13	Jul-13	120	1560		177	1375								177	177	0													
August	2013	Aug-13	Aug-13	Aug-13	121	1565		94	1472								171	171	0													
September	2013	Sep-13	Sep-13	Sep-13	121	1575		74	1500								179	179	0													
October	2013	Oct-13	Oct-13	Oct-13	123	1594		91	1503								174	174	0											October 30, 2013 MIT Test		
November	2013	Nov-13	Nov-13	Nov-13	121	1576		70	1506								171	171	0													
December	2013	Dec-13	Dec-13	Dec-13	124	1607		69	1538								175	175	0													
January	2014	Jan-14	Jan-14	Jan-14	121	1574		8	1566								166	166	0													
February	2014	Feb-14	Feb-14	Feb-14	126	1639		111	1528								182	182	0													
March	2014	Mar-14	Mar-14	Mar-14	121	1579		11	1568								162	162	0													
April	2014	Apr-14	Apr-14	Apr-14	123	1615		123	1547								175	175	0												April 30, 2014 MIT Test	
May	2014	May-14	May-14	May-14	123	1625		344	1280								170	170	0													
June	2014	Jun-14	Jun-14	Jun-14	121	1603		325	1277								162	162	0													
July	2014	Jul-14	Jul-14	Jul-14	123	1636		393	1243								167	167	0													
August	2014	Aug-14	Aug-14	Aug-14	122	1624		348	1275								161	161	0													
September	2014	Sep-14	Sep-14	Sep-14	122	1620		293	1327								158	158	0												September 19, 2014 MIT Test	
October	2014	Oct-14	Oct-14	Oct-14	123	1648		364	1284								170	170	0													
November	2014	Nov-14	Nov-14	Nov-14	123	1610		146	1464								158	158	0													
December	2014	Dec-14	Dec-14	Dec-14	124	1660		211	1450								168	168	0													
January	2015	Jan-15	Jan-15	Jan-15	125	1631		180	1451								151	151	0													
February	2015	Feb-15	Feb-15	Feb-15	123	1649		242	1407								161	161	0													
March	2015	Mar-15	Mar-15	Mar-15	124	1627		270	1357								161	161	0												March 19, 2015 MIT Test	
April	2015	Apr-15	Apr-15	Apr-15	124	1647		393	1254								163	163	0													
May	2015	May-15	May-15	May-15	122	1645		358	1287								159	159	0													
June	2015	Jun-15	Jun-15	Jun-15	121	1629		259	1370								152	152	0													
July	2015	Jul-15	Jul-15	Jul-15	120	1620		241	1378								154	154	0													
August	2015	Aug-15	Aug-15	Aug-15	123	1613		287	1327								131	131	0													
September	2015	Sep-15	Sep-15	Sep-15	124	1654		318	1336								163	163	0												September 15, 2015 MIT Test	
October	2015	Oct-15	Oct-15	Oct-15	124																											



Month Ended					AGI #1 TAG Injection Temperature (° F)	AGI #1 Surface TAG Injection Pressure (psig)	AGI #1 Surface Casing Annulus Pressure (psig)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig)	AGI #1 Average Bottom Hole Temperature (°F)	Total Flowrate (MSCFPH)	AGI #1 Flowrate (MSCFPH)	AGI #2 Flowrate (MSCFPH)	AGI #2 Surface TAG Injection Temperature (° F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)		
October	2017	Oct-17	Oct-17	Oct-17	102	1531	211	1321	4250	136	152	152	0	63	872	97	776	Plant shutdown 9-19 through 10-3 for a turnaround. Only AGI #1 used during remainder of month. Major software upgrade in DCS. BH sensors not yet integrated into DCS.	
November	2017	Nov-17	Nov-17	Nov-17	101	1589	428	1161	4080	136	189	189	0	56	1013	82	931	Only AGI #1 in use in November. BH sensors not reconnected to DCS until 11-29.	
December	2017	Dec-17	Dec-17	Dec-17	107	1707	456	1252	4080	136	191	191	0	44	1102	84	1017	Only AGI #1 in use.	
January	2018	Jan-18	Jan-18	Jan-18	99	1557	160	1397	4416	133	120	120	0	41	704	177	528	Only AGI #1 in use.	
February	2018	Feb-18	Feb-18	Feb-18	110	1551	110	1441	4458	131	196	196	0	48	785	199	527	Only AGI #1 in use.	
March	2018	Mar-18	Mar-18	Mar-18	107	1635	300	1335	4503	133	188	188	0	58	938	264	673	Only AGI #1 in use.	
April	2018	Apr-18	Apr-18	Apr-18	95	1618	95	1523	4576	131	223	223	0	63	1158	224	934	Only AGI #1 in use.	
May	2018	May-18	May-18	May-18	99	1668	141	1527	4646	131	226	226	0	79	1120	198	921	Only AGI #1 in use.	
June	2018	Jun-18	Jun-18	Jun-18	100	1667	267	1401	4615	132	202	202	0	84	1062	189	873	Only AGI #1 in use.	
July	2018	Jul-18	Jul-18	Jul-18	101	1690	475	1215	4627	132	204	204	0	83	1080	179	901	Only AGI #1 in use.	
August	2018	Aug-18	Aug-18	Aug-18	98	1614	321	1293	4565	131	157	157	0	82	1043	169	874	Only AGI #1 in use.	
September	2018	Sep-18	Sep-18	Sep-18	97	1581	237	1345	4534	130	155	155	0	72	898	154	744	Only AGI #1 in use.	
October	2018	Oct-18	Oct-18	Oct-18	92	1564	206	1358	4525	130	160	160	0	61	830	134	696	Only AGI #1 in use.	
November	2018	Nov-18	Nov-18	Nov-18	91	1531	115	1416	4529	129	166	166	0	64	1143	108	1036	Only AGI #1 in use.	
December	2018	Dec-18	Dec-18	Dec-18	89	1483	55	1428	4480	128	133	133	0	69	1152	85	1067	Only AGI #1 in use.	
January	2019	Jan-19	Jan-19	Jan-19	95	1500	133	1367	4457	129	143	143	0	69	925	68	858		
February	2019	Feb-19	Feb-19	Feb-19	98	1547	185	1362	4484	129	169	169	0	73	936	194	724		
March	2019	Mar-19	Mar-19	Mar-19	100	1577	222	1362	4511	131	182	182	0	78	442	238	161		
April	2019	Apr-19	Apr-19	Apr-19	106	1689	473	1217	4577	133	216	216	0	92	14	229	-215		
May	2019	May-19	May-19	May-19	110	1753	673	1080	4516	136	225	115	110	111	1616	166	1450		
June	2019	Jun-19	Jun-19	Jun-19	110	1680	513	1167	4433	136	199	87	112	112	1595	68	1528		
July	2019	Jul-19	Jul-19	Jul-19	88	1292	5	1228	4279	138	207	0	207	113	1600	113	1487		
August	2019	Aug-19	Aug-19	Aug-19	91	1240	6	1234	4224	138	182	5	176	113	1554	136	1419		
September	2019	Sep-19	Sep-19	Sep-19	93	1251	38	1211	4171	137	169	50	118	111	1484	112	1371		
October	2019	Oct-19	Oct-19	Oct-19	78	1202	11	1191	4156	137	231	54	177	106	1486	35	1451		
November	2019	Nov-19	Nov-19	Nov-19	69	1179	19	1160	4143	137	204	0	204	110	1512	116	1396		
December	2019	Dec-19	Dec-19	Dec-19	64	1156	15	1142	4116	138	195	0	195	111	1494	135	1359		
January	2020	Jan-20	Jan-20	Jan-20	63	1128	17	1111	4096	138	188	0	188	110	1481	54	1427		
February	2020	Feb-20	Feb-20	Feb-20	63	1116	262	854	4085	138	191	0	191	107	1462	137	1324	Perfrom MIT on both wells adjust backside pressure	
March	2020	Mar-20	Mar-20	Mar-20	72	1111	300	811	4085	138	217	0	217	109	1509	59	1450		
April	2020	Apr-20	Apr-20	Apr-20	74	1117	294	823	4095	138	228	0	228	109	1519	35	1485		
May	2020	May-20	May-20	May-20	82	1126	300	825	4098	138	212	0	212	108	1501	10	1491		
June	2020	Jun-20	Jun-20	Jun-20	88	1140	323	817	4109	138	226	0	226	117	1500	127	1373		
July	2020	Jul-20	Jul-20	Jul-20	109	1412	302	1109	4212	139	219	100	119	109	1409	103	1307	Switch flow from #2 to #1 16 July 9am	
August	2020	Aug-20	Aug-20	Aug-20	119	1658	293	1364	4332	141	227	227	0	98	1113	181	932		
September	2020	Sep-20	Sep-20	Sep-20	123	1737	123	1613	4389	143	241	241	0	87	1125	217	909		
October	2020	Oct-20	Oct-20	Oct-20	121	1715	30	1683	4403	142	219	219	0	79	1153	181	973		
November	2020	Nov-20	Nov-20	Nov-20	114	1692	17	1673	4447	140	232	232	0	73	1189	157	1032		
December	2020	Dec-20	Dec-20	Dec-20	113	1696	16	1680	4488	138	212	212	0	63	1225	141	1085		
Average for 2020					95	1387	190	1197	4237	139	218	103	115	97	1349	117	1232		
Standard Deviation 2020					23	276	130	365	155	2	15	108	101	17	163	62	219		
Average for Entire Period					109.3	1545.1	297.4	1247.1	4363.7	135.1	177.3	148.7	27.7	82.9	1099.6	124.4	959.2		
Standard Deviation Entire Period					15.7	161.2	246.5	267.2	188.1	3.8	27.8	60.6	65.1	22.6	565.3	107.0	555.6		
OPERATING CONSTRAINTS BASED ON NMOCC ORDER AND ACO 275																			
MAOP in NMOCC Order is 2644 psig																			



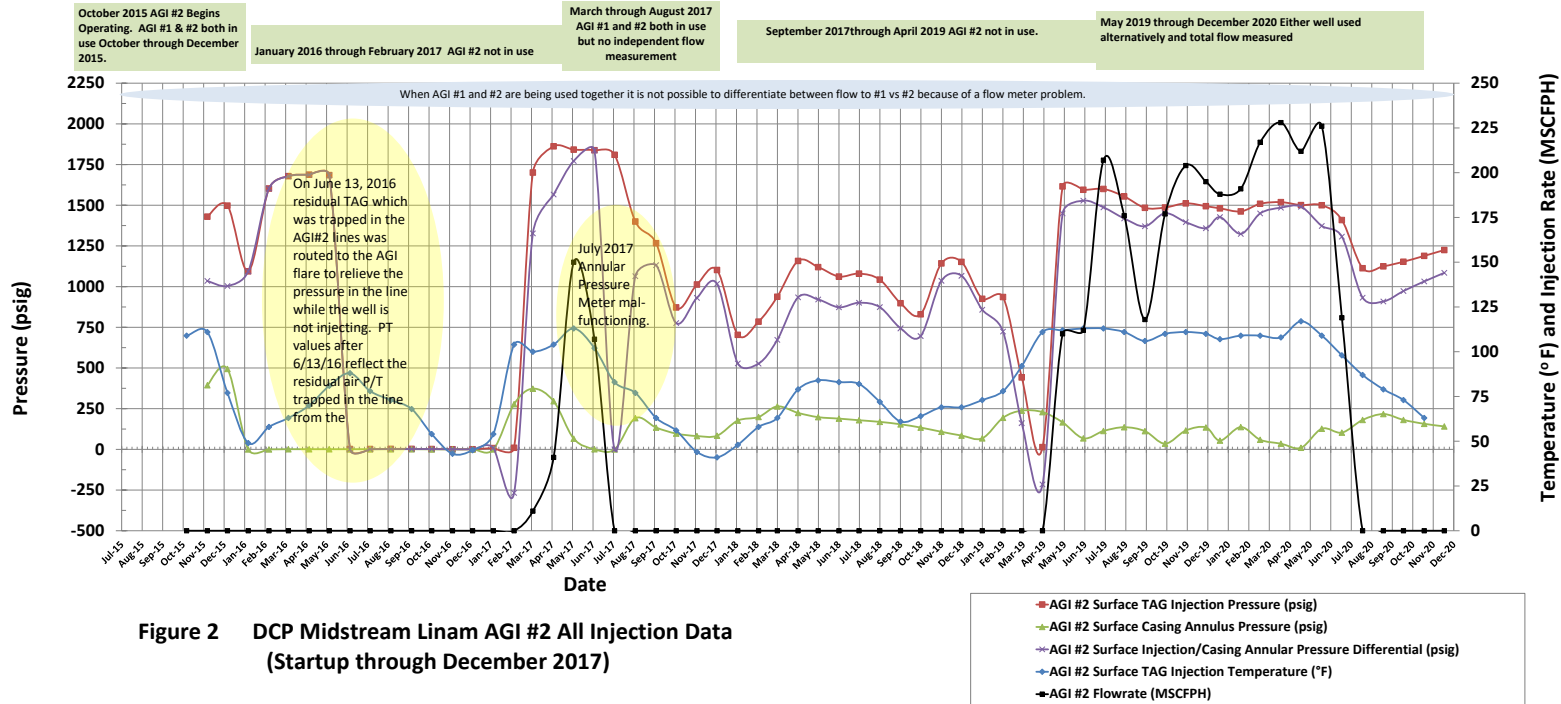
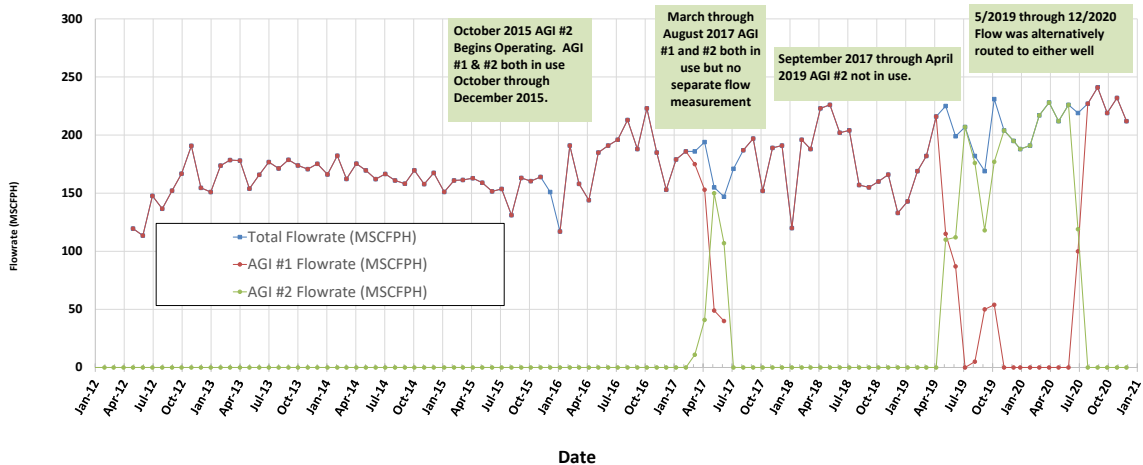
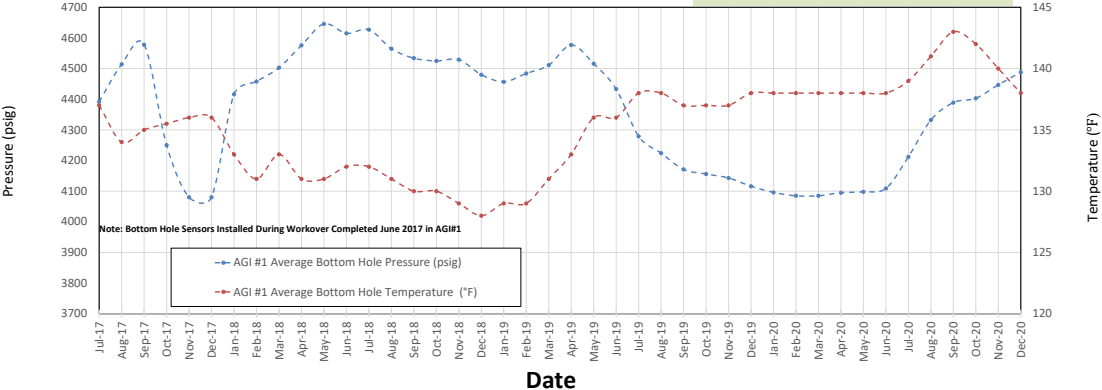


Figure 3 DCP Midstream Linam AGI #1 and #2 Combined Total Flowrate (MSCFPH) (May 2012 through December 2020)



**FIGURE 4    BOTTOM HOLE PRESSURE AND TEMPERATURE - AGI #1**

When AGI #2 is used in conjunction with AGI#1 or alternating between the wells, the effect is noticed on #1 Bottom Hole values for 2019 and 2020



**ANALYSIS OF 2020 ANNUAL TRENDS AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS FOR OPERATION OF LINAM AGI #1 AND LINAM AGI #2 (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all**

This document presents the results from the analyses of the injection parameter data collected from the Linam AGI #1 and #2 Wells which serve the Linam Ranch Gas Processing Facility near Hobbs, NM. Data from the Linam AGI #1 have been collected continuously since 2012 and have been analyzed on a monthly basis by Geolex and transmitted to DCP for reporting to NMOCD as required by ACO 275 and the approved post-workover C-103. In addition, the Linam AGI #2 well was completed and brought online in October 2015. The AGI #2 well was completed in the same injection zone as the AGI#1 approximately 450 feet to the southwest of AGI #1. From the time that AGI #2 was brought online, injection has been either into both wells simultaneously or solely into one of the two wells. AGI#2 was operated in conjunction with AGI #1 from October 2015 to January 2016 when a switch was made to operate only AGI#1 for the remainder of 2016. In May 2017, DCP switched over to injecting into AGI#2 to allow for the workover of AGI#1. The workover was completed on June 8, 2017 and AGI #1 was brought back online in July 2017 with bottom hole sensors installed. These sensors are now serving to monitor downhole and reservoir conditions since the downhole sensors in AGI #2 failed due to a lightning strike shortly after installation (2015) and will not be able to be repaired until sometime in the future when AGI #2 is worked over. In the meantime, in order to obtain reservoir data which would have been provided by the downhole PT sensors in AGI #2, a slick line with a pressure recorder was placed into AGI #2 and downhole pressure data were collected under both injection and non-injection conditions for the AGI #2 and AGI #1. Since that time the downhole sensors in AGI#1 provide the necessary reservoir data needed to evaluate the performance of the two wells. The system continued operating through 2018 with only AGI #1 active while waiting for independent flow meters to be installed/repared in both wells so that reliable flow information would be available for each well independently. This operational mode (utilizing only AGI #1) continued through April 2019, and to date separate volume meters have not been installed/repared. In May 2019, however, DCP began dividing the flow of acid gas between the two wells by using one or the other well exclusively (see Figure 3). Presently, surface data from both wells is being collected relative to the following parameters:

- Treated Acid Gas (TAG) surface injection pressure (both wells),
- TAG injection temperature (both wells),
- Annular pressure (both wells)
- Bottom Hole pressure and temperature (AGI#1 only beginning 7/2017)
- Overall total TAG flow rate from compressors

The above are the key parameters which are currently being measured in both wells in order to monitor the operations of the wells, prevent hydrate formation and reduce corrosion potential following the workover of AGI#1. While improvements have been implemented in the placement of temperature controls, dehydration of TAG during compression and other systems improvements at the AGI facility, there continue to be variations in the desired and normal operating levels of the above-referenced

parameters. Since these parameters are useful indicators and predictors of potential operational or mechanical problems in the well, various levels of alarms have been established for each of these parameters. These parameters include three which are measured directly (TAG injection pressure, TAG injection temperature and annular pressure) and one (differential pressure) which is a calculated value (the difference between the two measured parameters of injection and annular pressure). The analyses of the long-term trends in these values have been useful in smoothing out shorter-term variations which can be observed from detailed inspection of hourly data and in the development of appropriate alarm bands for each parameter.

The Linam AGI #1 experienced a tubing leak in late 2011 which was partially addressed in a workover conducted in April/May 2012. The leak was detected in the end of 2011, and beginning of 2012 (until the time of the workover) the injection parameters were reviewed, analyzed and reported weekly to the NMOCD. Following the workover in which the tubing leak was repaired, some compromised production casing was detected immediately above the packer depth. At that time, we recommended keeping only approximately 250 psig on the annular space between the tubing and casing in AGI #1 since with annular pressure at this level, under normal operating conditions, this parameter can serve as a useful indicator of when activity should be initiated to prevent damage to the well or trigger a NMOCD shutdown and/or immediate notification requirements. Concern about this compromised casing was eliminated by stacking packers when the well was worked over again in June 2017. All of the data from January 2012 through December 2015 are included in our analysis, but only the post-workover data have been used to develop the recommended alarm and emergency shutdown (ESD) levels in conjunction with the requirements of NMOCD Order 12546-all, ACO-275 and the post-workover C-103.

Furthermore, a similar process has been employed on the Linam AGI#2 since it was brought online in October 2015. As described above, this well is equipped with bottom hole (just at top of packer) P/T measurement capability both inside and outside the tubing. In general, the immediate notification parameters for both wells were developed from this long-term analysis of the injection data. Initial testing of the Linam AGI#2 indicates that the pressure variations induced by flow rate and temperature fluctuations in the Linam AGI#1 are influencing the reservoir as measured in the AGI #2 location. This is to be expected as the new well is completed in the same zone at a distance away from the initial well which we predicted would see the edge of the plume in about 7 years. The Linam AGI #1 has been injecting for approximately 13 years.

Data from AGI #1 were continuously collected and analyzed weekly prior to the original workover in April/May 2012 and then monthly after the workover from June 2012 through December 2017 (see Figure 1). These data collection, analysis and reporting functions continue as required by NMOCD on a monthly basis. Furthermore, since it is necessary to evaluate the data from both wells to know how the system is operating overall, the surface data from AGI #2 are also being collected, analyzed and reported monthly. The reporting requirement for the AGI #2 is only quarterly and now that AGI #1 has been successfully worked over, the reporting for both wells will shift to quarterly as soon as independent reliable volume measurement is available for each well.

The NMOCD also requires that immediate notification parameters and levels be discussed and agreed upon with the agency, and that these be periodically reviewed and updated as needed based on operational or regulatory changes. The immediate notification parameters for both wells have been approved by NMOCD, and DCP requests no changes in these approved values. With this requirement in mind and for the purpose of protecting the mechanical integrity and safety of both wells and the overall AGI facility, Geolex monitors these data under contract to DCP to prevent damage to the wells or violation of regulatory requirements or permit constraints.

After 9.5 years (113 months) of carefully analyzing the performance of AGI #1 on a continuous basis, Geolex has assembled the data and has analyzed observed trends for the post-workover period of June 2012 – December 2020 as can be seen on Figure 2. Several important observations can be made from analyzing these data and taking into consideration important system modifications that have occurred during this time period. These include the following:

1. AGI #1 Post-Workover MIT completed in May 2012
2. AGI #1 MIT test completed November 14, 2012
3. Bleeding of diesel from casing annular space immediately after the November 2012 AGI #1 MIT test.
4. AGI #1 MIT test completed April 30, 2013
5. Addition of diesel in annular space after April 2013 AGI #1 MIT and May 2013 plant shutdown
6. AGI #1 MIT test completed October 30, 2013
7. Failure of the VFD for the cooler on the AGI compressor from February 4 through 9, 2014.
8. AGI #1 MIT test completed April 30, 2014
9. Addition of diesel in annular space after April 2014 AGI #1 MIT
10. AGI #1 MIT test completed September 19, 2014
11. AGI #1 MIT test completed March 19, 2015
12. AGI #1 MIT test completed September 15, 2015
13. AGI #2 brought online with startup in October-November 2015 and operated until January 2016
14. AGI #1 MIT test completed March 22, 2016
15. AGI #2 MIT test completed April 1, 2016
16. AGI #2 TAG lines bled to flare on June 13, 2016 to remove static TAG in line when well is not operating.
17. AGI #1 MIT test completed September 14, 2016
18. AGI #1 Workover completed June 8, 2017 including stacked packer, bottom hole PT gauges
19. AGI #1 MIT test completed June 7, 2017 after workover completion
20. AGI #2 MIT test completed February 16, 2017
21. AGI #2 MIT test completed February 15, 2018
22. AGI #1 MIT test completed June 19, 2018
23. AGI #2 MIT test completed February 15, 2019
24. AGI #1 MIT test completed February 15, 2019
25. AGI #1 MIT test completed February 4, 2020
26. AGI #2 MIT test completed February 4, 2020



The following trends have been observed in the AGI well data and are reflected on Figures 1 & 2:

1. TAG injection pressure which was on a slight increasing trend due to slightly increasing average temperature of injected TAG but began to level off due to temperature decreases in 2017. This trend continued over the last six months of 2018 and all of 2019. The TAG injection pressure and rate has been more variable since 2016 due to inlet flow variations, and AGI#1 was used exclusively from time of the workover in June 2017 through April 2019.
2. Flow of TAG has been split between the two wells since April of 2019 with either one or the other being used exclusively but not simultaneously (see Figure 3).
3. The TAG injection temperature increased slightly with an arithmetic mean of 95°F in 2020 up from 92°F in 2019, 98°F in 2018, 106°F in 2017 and 113°F in 2016.
4. The TAG injection temperature is significantly lower during periods of low flow into either AGI well when the other well one is being used.
5. Pressure in the casing annulus has been consistently tracked; the correlative nature of variable injection temperature, pressure and flowrate, and its arithmetic mean for the period ending 12-31-20 has been approximately 190 psig essentially the same as 191 in 2019. The injection temperature is the largest influencer of this parameter under normal conditions.
6. The pressure differential between the casing annulus and the TAG injection pressure clearly indicates that no communication currently exists between the tubing and casing annulus.
7. The generally low annular pressures observed indicate that the production casing/cement still has good integrity.
8. TAG injection temperatures can now be lower due to the improvement of water reduction in compression which reduces the potential for hydrate formation at lower temperatures. This has allowed for lower injection temperatures throughout the 2018-2020 period.

Given the observations of the trends in the graphs and the competing influence of average injection temperature decrease and that injection volumes have been more variable since 2018, the observed TAG injection pressure changes are predictable and normal. There is no current indication of the reservoir being pressured up to any significant degree by the injection from Linam AGI #1. This was confirmed during the drilling and testing of AGI #2. Upon startup from any shutdown that lasts more than 6-8 hours it is critical to inject methanol along with the TAG for the initial startup period to prevent the formation of hydrates. While this may no longer be necessary due to the changes which were made in the water removal efficiency of the AGI compressor system, it is a good preventative measure. Prior to the increased water removal efficiency, this effect was observed in the period of March 2013 when hydrate formation during one of these events caused a spike in TAG injection pressure of approximately 35% over normal pressures due to partial blockage of the injection line and tubing created by the hydrate formation. This persisted for several hours until the situation was alleviated by the stabilization of the compressor and the simultaneous injection of methanol to cause the hydrates to be reabsorbed into the TAG. Injection pressures and temperatures then returned to normal.

It is also critical to maintain the temperature control on the injected TAG and to avoid rapid temperature or pressure fluctuations during periods when power failures or other mechanical failures may occur. The

extensive and wide variation in TAG injection temperatures observed prior to the failure of the tubing in late 2011, resulted in the formation of free water within the tubing and corrosion resulting in a tubing leak which had to be repaired in April/May 2012. Temperature control changes were implemented and helped to significantly control downward swings in temperature and prevent the formation of hydrates.

However, in February 2014, there was a failure in the VFD for the cooler on the AGI compressor which persisted for five days. During this period of time, the TAG temperature increased to at least 150 °F, and the annular pressure increased dramatically due to the heating of the diesel fluid in the annular space as a result of the elevated TAG injection temperature. TAG temperature as well as annular pressure returned to the normal range once the VFD on the cooler was repaired. The significant spread between TAG injection pressure and the annular pressure maintained even during this heating episode proves the continued integrity of the well, packer, casing and tubing. However, the rise in annular pressure has a potential to damage the integrity of the compromised casing in the well and should be avoided during all subsequent operations. In response to these issues, DCP undertook and successfully completed a project in 2015 to address the temperature fluctuations resulting from compression controls and to increase the efficiency of water removal to the point where all free water is removed from the TAG prior to injection. This significantly reduces hydrate formation potential in the entire system regardless of temperature variations. This has allowed for the lower average injection temperatures observed throughout 2018 and 2019 to not have caused any hydrate formation.

In October 2015, AGI #2 was started up and operated in a startup mode switching back and forth from AGI #1. This effect is reflected in the trend data shown in Figure 2. Due to a volume meter sensor failure and configuration issues which are currently being addressed, only total flow to the AGI system can be reliably measured through 2019. Flow has been split between the two wells since April of 2019, but each well is used exclusively when that is done. For 2020 AGI#2 only operated until July 16, 2020 at 9am when flow was switched to AGI#1 and only AGI#1 was used for the balance of 2020. They are not used simultaneously. See Figure 3 for total flow rate and flow rate to AGI #1 and AGI #1.

#### **REVIEW OF STATISTICAL ANALYSIS OF INJECTION PARAMETERS, DEVELOPMENT OF AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all**

The statistical analyses of the injection parameter data were initially conducted for the purpose of establishing normal operating levels for these parameters which are automatically monitored. Several data filtering steps were accomplished to take the hourly data which forms the basis of the analysis in order to smooth out variability and to account for the physical changes in the well and its operation after the repair of the tubing leak in the workover completed in May 2012. Because the configuration of the well changed dramatically after the workover, only data after the well had stabilized post-workover were used in this analysis. Furthermore, the subsequent stacked packer workover of the AGI#1 in June 2017 was completed and essentially only the AGI #1 has been used since then. The bottom hole PT sensors installed during the 2017 workover of AGI #1 have been providing excellent data throughout 2020 and these data are shown on the graph attached here as Figure 4. During 2018 we resolved some communication issues between the Halliburton BHPT panel and the plant DCS system and corrected

some BHPT readings which had been inaccurately reported from 11/2017 to 6/2018 until this issue was detected. In 2018 for the period affected, we downloaded the data directly from the Halliburton panel and corrected the values. A C-103 was submitted with these corrections in July 2018. The corrected values are used in this analysis. No problems with BHPT readings occurred in 2019 or 2020. It is clear from the variation in these parameters when flow is switched between wells that the conditions measured in the BHPT gauge in AGI#1 reflect the values in the reservoir which would be very similar in AGI #2 if the BHPT gauges in the well were operational.

All the data are summarized in Table 1, and the calculated statistical parameters of arithmetic mean and standard deviation were used to establish base levels and variability for each parameter. The results of these analyses resulted in the immediate notification parameters which were approved both for AGI #2 and the parameters required under ACO 275 for AGI#1.

Based on the analysis of observed trends, the immediate notification parameters which were approved for AGI #1 and the parameters previously approved for AGI# 2 and continued through 2020 remain appropriate to continue through 2021. This is DCPs request and the approved immediate notification parameters are detailed below:

The approved immediate notification parameters for Linam AGI #1 are summarized below:

1. Exceedance of the approved MAOP of 2644 psig surface for a period greater than two hours.
2. Failure of a mechanical integrity test (MIT) of the well.
3. Confirmation of any condition that indicates a tubing, packer or casing leak.
4. Any increase of the annular pressure to a value that is greater than 1200 psig
5. Any instance in which differential pressure between the injection tubing and injection tubing annulus is less than 100 psig.
6. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
7. Any workover or maintenance activity that requires intrusive work in the well.

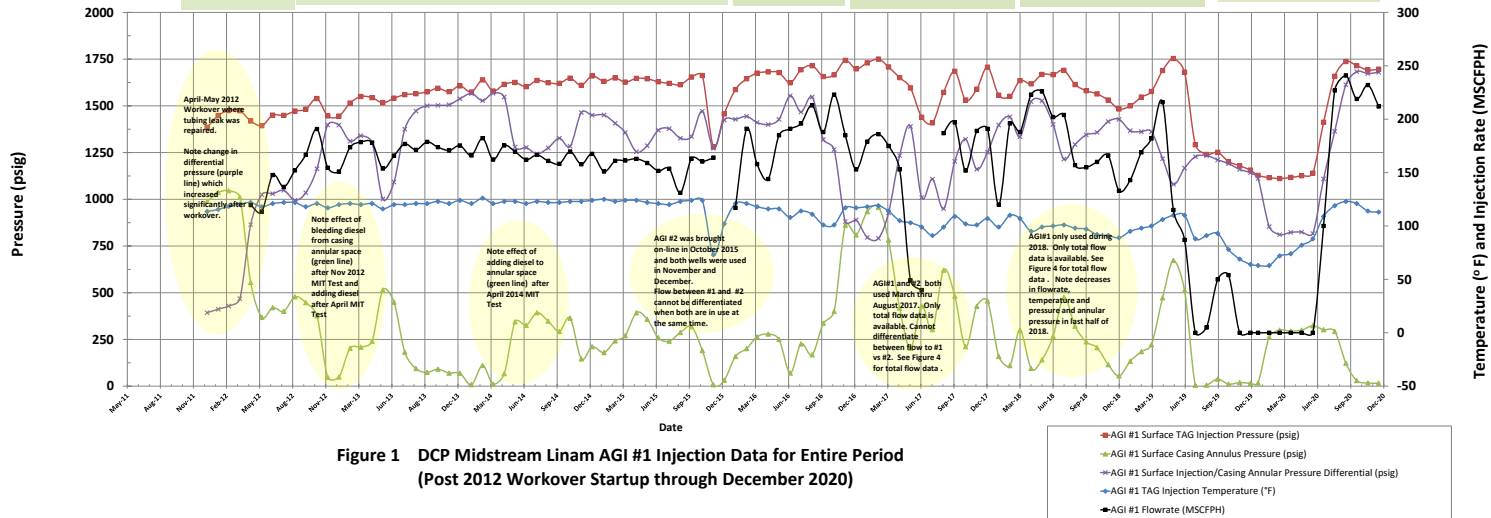
The approved immediate notification parameters for the Linam AGI #2 are summarized below:

1. Exceedance of the approved MAOP of 2644 psig surface for a period greater than two hours.
2. Failure of a mechanical integrity test (MIT) of the well.
3. Confirmation of any condition that indicates a tubing, packer or casing leak.
4. Any increase of the annular pressure to a value that is more than 80% of the injection pressure.
5. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
6. Any workover or maintenance activity that requires intrusive work in the well.

TABLE 1 SUMMARY DATA ANALYSIS OF LINAM AGI #1 TRENDS FOR JANUARY 2012 THROUGH DECEMBER 2020 (3 PAGES)

DCP MIDSTREAM LINAM RANCH AGI #1 AND #2 CUMULATIVE INJECTION DATA																		
Month Ended				AGI #1 TAG Injection Temperature (°F)	AGI #1 Surface TAG Injection Pressure (psig)	AGI #1 Surface Casing Annulus Pressure (psig)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig)	AGI #1 Average Bottom Hole Temperature (°F)	Total Flowrate (MSCFPH)	AGI #1 Flowrate (MSCFPH)	AGI #2 Flowrate (MSCFPH)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)		
January	2012	Jan-12	Jan-12	114	1385	989	393			N/A	N/A	0					No Flow Data Available	
February	2012	Feb-12	Feb-12	116	1448	1036	412					0					No Flow Data Available	
March	2012	Mar-12	Mar-12	118	1475	1046	429					0					No Flow Data Available	
April	2012	Apr-12	Apr-12	121	1474	1010	468					0					No Flow Data Available	
May	2012	May-12	May-12	122	1419	555	864			120	120	0					Plant Workover and Shutdown	
June	2012	Jun-12	Jun-12	118	1394	368	1025			113	113	0					Plant Workover and Shutdown	
July	2012	Jul-12	Jul-12	121	1450	420	1030			148	148	0						
August	2012	Aug-12	Aug-12	122	1449	401	1048			137	137	0						
September	2012	Sep-12	Sep-12	122	1472	478	995			152	152	0						
October	2012	Oct-12	Oct-12	118	1482	447	1035			167	167	0						
November	2012	Nov-12	Nov-12	121	1539	376	1163			191	191	0					November 14, 2012 MIT Test	
December	2012	Dec-12	Dec-12	117	1446	48	1398			155	155	0						
January	2013	Jan-13	Jan-13	120	1445	49	1397			151	151	0						
February	2013	Feb-13	Feb-13	121	1515	203	1311			174	174	0						
March	2013	Mar-13	Mar-13	120	1550	209	1340			179	179	0						
April	2013	Apr-13	Apr-13	121	1544	240	1304			178	178	0					April 30, 2013 MIT Test	
May	2013	May-13	May-13	116	1516	515	1001			154	154	0						
June	2013	Jun-13	Jun-13	120	1541	449	1092			166	166	0						
July	2013	Jul-13	Jul-13	120	1560	182	1375			177	177	0						
August	2013	Aug-13	Aug-13	121	1565	94	1472			171	171	0						
September	2013	Sep-13	Sep-13	121	1575	74	1500			179	179	0						
October	2013	Oct-13	Oct-13	123	1594	91	1503			174	174	0					October 30, 2013 MIT Test	
November	2013	Nov-13	Nov-13	121	1576	70	1506			171	171	0						
December	2013	Dec-13	Dec-13	124	1607	69	1538			175	175	0						
January	2014	Jan-14	Jan-14	121	1574	8	1566			166	166	0						
February	2014	Feb-14	Feb-14	126	1639	111	1528			182	182	0						
March	2014	Mar-14	Mar-14	121	1579	11	1568			162	162	0						
April	2014	Apr-14	Apr-14	123	1615	67	1547			175	175	0					April 30, 2014 MIT Test	
May	2014	May-14	May-14	123	1625	344	1280			170	170	0						
June	2014	Jun-14	Jun-14	121	1603	325	1277			162	162	0						
July	2014	Jul-14	Jul-14	123	1636	393	1243			167	167	0						
August	2014	Aug-14	Aug-14	122	1624	348	1275			161	161	0						
September	2014	Sep-14	Sep-14	122	1620	293	1327			158	158	0					September 19, 2014 MIT Test	
October	2014	Oct-14	Oct-14	123	1648	364	1284			170	170	0						
November	2014	Nov-14	Nov-14	123	1610	146	1464			158	158	0						
December	2014	Dec-14	Dec-14	124	1660	211	1450			168	168	0						
January	2015	Jan-15	Jan-15	125	1631	180	1451			151	151	0						
February	2015	Feb-15	Feb-15	123	1649	242	1407			161	161	0						
March	2015	Mar-15	Mar-15	124	1627	270	1357			161	161	0					March 19, 2015 MIT Test	
April	2015	Apr-15	Apr-15	124	1647	393	1254			163	163	0						
May	2015	May-15	May-15	122	1645	358	1287			159	159	0						
June	2015	Jun-15	Jun-15	121	1629	259	1370			152	152	0						
July	2015	Jul-15	Jul-15	120	1620	241	1378			154	154	0						
August	2015	Aug-15	Aug-15	123	1613	287	1327			133	131	0						
September	2015	Sep-15	Sep-15	124	1654	318	1336			163	163	0					September 15, 2015 MIT Test	
October	2015	Oct-15	Oct-15	124	1662	191	1471			160	160	0					AGI #2 not in use	
November	2015	Nov-15	Nov-15	73	1280	7	1273			164	164	0	109	1430	394	1035	AGI #1 & #2 both in use	
December	2015	Dec-15	Dec-15	102	1457	32	1425			151		0	111	1498	494	1004	AGI #1 & #2 both in use	
January	2016	Jan-16	Jan-16	121	1587	159	1428			117	117	0	77	1094	0	1094	AGI #2 not in use	
February	2016	Feb-16	Feb-16	121	1645	201	1444			191	191	0	49	1603	0	1603	AGI #2 not in use	
March	2016	Mar-16	Mar-16	118	1675	264	1411			158	158	0	58	1679	1	1678	AGI #2 not in use	
April	2016	Apr-16	Apr-16	116	1682	279	1400			144	144	0	63	1688	1	1687	AGI #2 not in use	
May	2016	May-16	May-16	116	1678	250	1428			185	185	0	70	1685	1	1684	AGI #2 not in use	
June	2016	Jun-16	Jun-16	108	1624	70	1554			191	191	0	81	2	1		AGI #2 not in use. TAG trapped in blocked off section of AGI #2 pipe blown down	
July	2016	Jul-16	Jul-16	114	1693	226	1467			196	196	0	88	2	1	1	AGI #2 not in use	
August	2016	Aug-16	Aug-16	111	1715	168	1547			213	213	0	78	3	1	2	AGI #2 not in use	
September	2016	Sep-16	Sep-16	101	1657	337	1320			188	188	0	73	3	1	2	AGI #2 not in use	
October	2016	Oct-16	Oct-16	101	1666	400	1266			223	223	0	68	2	0	2	AGI #2 not in use	
November	2016	Nov-16	Nov-16	117	1743	862	881			185	185	0	54	1	0	1	AGI #2 not in use	
December	2016	Dec-16	Dec-16	117	1698	809	889			153	153	0	43	1	0	1	AGI #2 not in use	
January	2017	Jan-17	Jan-17	118	1730	796	934			179	179	0	45	8	0	8	AGI #2 not in use	
February	2017	Feb-17	Feb-17	119	1750	791				186	186	0	54	10	278	-267	AGI #2 not in use	
March	2017	Mar-17	Mar-17	114	1708	782	927			186	175	11	104	1701	373	1327	Both wells used; #2 flow meter not functioning. AGI #1 for entire month and AGI #2 only from 3-13 to 3-16 and 3-21 to 3-31	
April	2017	Apr-17	Apr-17	105	1651	418	1234			194	153	41	100	1862	296	1566	Both wells used. Flow meter for #2 not working. TAG routed to #1 well exclusively, both wells simultaneously and #2 well exclusively. All TAG routed to #2 from 4-26 onward in anticipation of workover of #1 well.	
May	2017	May-17	May-17	103	1596	203	1390			155	49	150	104	1842	66	1772	Both wells used. #2 Flow Meter not working. TAG Routed to AGI #2 save for 19 hour period from 5-17 to 5-18 when it was routed to AGI #1. AGI #1 workover 5-22 thru 6-8. AGI #2 experienced mechanical blockage resulting in both wells being shut down from 5-25 to 5-31.	
June	2017	Jun-17	Jun-17	99	1439	429	1010			147	40	107	113	1838	1	1837	Both wells used. #2 used from 6-2 through 6-15. Workover of #1 completed 6-8 and successful MIT performed 6-8; #1 back online 6-15. #1 and #2 used simultaneously from 6-15 to 6-30. Mechanical Problem with flow meter for #2 well. Only total flow can be measured; no way to differentiate between #1 and #2 when they are used together.	
July	2017	Jul-17	Jul-17	91	1409	302	1108	4392	137	171	0	102	1810	sensor error	n/a		Both wells used. Annular Pressure Meter for AGI #2 malfunctioning for month of July. Mechanical problem with flow meter for #2 well persists. Bottomhole sensors added to #1 Well as part of workover completed in June and began recording data on 7-20-17	
August	2017	Aug-17	Aug-17	99	1572	621	950	4514	134	187	187	0	83	1400	192	1064	Both wells used. Mechanical problem with flow meter for #2 well persists. Only total flow data available. Annular Pressure meter for AGI #2 back in service 8-11-17. Annular Pressure and differential pressure readings are for period 8-11-17 through 8-31-17.	
September	2017	Sep-17	Sep-17	109	1685	482	1203	4578	135	197	197	0	77	1267	134	1132	Only AGI #1 used. Entire plant shut down from Sept 19 to Sept 30th for a scheduled turnaround. Data available only for first 19 days of September	

Month Ended					AGI #1 TAG Injection Temperature ( F )	AGI #1 Surface TAG Injection Pressure (psig)	AGI #1 Surface Casing Annulus Pressure (psig)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig)	AGI #1 Average Bottom Hole Temperature ( °F)	Total Flowrate (MSCFPH)	AGI #1 Flowrate (MSCFPH)	AGI #2 Flowrate (MSCFPH)	AGI #2 Surface TAG Injection Temperature ( F )	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)	
October	2017	Oct-17	Oct-17	Oct-17	102	1531	211	1321	4250	136	152	152	0	63	872	97	776	Plant shutdown 9-19 through 10-3 for a turnaround. Only AGI #1 used during remainder of month. Major software upgrade in DCS. BH sensors not yet integrated into DCS.
November	2017	Nov-17	Nov-17	Nov-17	101	1589	428	1161	4080	136	189	189	0	56	1013	82	931	Only AGI #1 in use. BH sensors not reconnected to DCS until 11-29.
December	2017	Dec-17	Dec-17	Dec-17	107	1707	456	1252	4080	136	191	191	0	44	1102	84	1017	Only AGI #1 in use.
January	2018	Jan-18	Jan-18	Jan-18	99	1557	160	1397	4416	133	120	120	0	41	704	177	528	Only AGI #1 in use.
February	2018	Feb-18	Feb-18	Feb-18	110	1551	110	1441	4458	131	196	196	0	48	785	199	527	Only AGI #1 in use.
March	2018	Mar-18	Mar-18	Mar-18	107	1635	300	1335	4503	133	188	188	0	58	938	264	673	Only AGI #1 in use.
April	2018	Apr-18	Apr-18	Apr-18	95	1618	95	1523	4576	131	223	223	0	63	1158	224	934	Only AGI #1 in use.
May	2018	May-18	May-18	May-18	99	1668	141	1527	4646	131	226	226	0	79	1120	198	921	Only AGI #1 in use.
June	2018	Jun-18	Jun-18	Jun-18	100	1667	267	1401	4615	132	202	202	0	84	1062	189	873	Only AGI #1 in use.
July	2018	Jul-18	Jul-18	Jul-18	101	1690	475	1215	4627	132	204	204	0	83	1080	179	901	Only AGI #1 in use.
August	2018	Aug-18	Aug-18	Aug-18	98	1614	321	1293	4565	131	157	157	0	82	1043	169	874	Only AGI #1 in use.
September	2018	Sep-18	Sep-18	Sep-18	97	1581	237	1345	4534	130	155	155	0	72	898	154	744	Only AGI #1 in use.
October	2018	Oct-18	Oct-18	Oct-18	92	1564	206	1358	4525	130	160	160	0	61	830	134	696	Only AGI #1 in use.
November	2018	Nov-18	Nov-18	Nov-18	91	1531	115	1416	4529	129	166	166	0	64	1143	108	1036	Only AGI #1 in use.
December	2018	Dec-18	Dec-18	Dec-18	89	1483	55	1428	4480	128	133	133	0	69	1152	85	1067	Only AGI #1 in use.
January	2019	Jan-19	Jan-19	Jan-19	95	1500	133	1367	4457	129	143	143	0	69	925	68	858	
February	2019	Feb-19	Feb-19	Feb-19	98	1547	185	1362	4484	129	169	169	0	73	936	194	724	
March	2019	Mar-19	Mar-19	Mar-19	100	1577	222	1362	4511	131	182	182	0	78	442	238	161	
April	2019	Apr-19	Apr-19	Apr-19	106	1689	473	1217	4577	133	216	216	0	92	14	229	-215	
May	2019	May-19	May-19	May-19	110	1753	673	1080	4516	136	225	115	110	111	1616	166	1450	
June	2019	Jun-19	Jun-19	Jun-19	110	1680	513	1167	4433	136	199	87	112	112	1595	68	1528	
July	2019	Jul-19	Jul-19	Jul-19	88	1292	5	1228	4279	138	207	0	207	113	1600	113	1487	
August	2019	Aug-19	Aug-19	Aug-19	91	1240	6	1234	4224	138	182	5	176	113	1554	136	1419	
September	2019	Sep-19	Sep-19	Sep-19	93	1251	38	1211	4171	137	169	50	118	111	1484	112	1371	
October	2019	Oct-19	Oct-19	Oct-19	78	1202	11	1191	4156	137	231	54	177	106	1486	35	1451	
November	2019	Nov-19	Nov-19	Nov-19	69	1179	19	1160	4143	137	204	0	204	110	1512	116	1396	
December	2019	Dec-19	Dec-19	Dec-19	64	1156	15	1142	4116	138	195	0	195	111	1494	135	1359	
January	2020	Jan-20	Jan-20	Jan-20	63	1128	17	1111	4096	138	188	0	188	110	1481	54	1427	
February	2020	Feb-20	Feb-20	Feb-20	63	1116	262	854	4085	138	191	0	191	107	1462	137	1324	Perfrom MIT on both wells adjust backside pressure
March	2020	Mar-20	Mar-20	Mar-20	72	1111	300	811	4085	138	217	0	217	109	1509	59	1450	
April	2020	Apr-20	Apr-20	Apr-20	74	1117	294	823	4095	138	228	0	228	109	1519	35	1485	
May	2020	May-20	May-20	May-20	82	1126	300	825	4098	138	212	0	212	108	1501	10	1491	
June	2020	Jun-20	Jun-20	Jun-20	88	1140	323	817	4109	138	226	0	226	117	1500	127	1373	
July	2020	Jul-20	Jul-20	Jul-20	109	1412	302	1109	4212	139	219	100	119	109	1409	103	1307	Switch flow from #2 to #1 16 July 9am
August	2020	Aug-20	Aug-20	Aug-20	119	1658	293	1364	4332	141	227	227	0	98	1113	181	932	
September	2020	Sep-20	Sep-20	Sep-20	123	1737	123	1613	4389	143	241	241	0	87	1125	217	909	
October	2020	Oct-20	Oct-20	Oct-20	121	1715	30	1683	4403	142	219	219	0	79	1153	181	973	
November	2020	Nov-20	Nov-20	Nov-20	114	1692	17	1673	4447	140	232	232	0	73	1189	157	1032	
December	2020	Dec-20	Dec-20	Dec-20	113	1696	16	1680	4488	138	212	212	0	63	1225	141	1085	
Average for 2020					95	1387	190	1197	4237	139	218	103	115	97	1349	117	1232	
Standard Deviation 2020					23	276	130	365	155	2	15	108	101	17	163	62	219	
Average for Entire Period					109.3	1545.1	297.4	1247.1	4363.7	135.1	177.3	148.7	27.7	82.9	1099.6	124.4	959.2	
Standard Deviation Entire Period					15.7	161.2	246.5	267.2	188.1	3.8	27.8	60.6	65.1	22.6	565.3	107.0	555.6	
OPERATING CONSTRAINTS BASED ON NMOCC ORDER AND ACO 275																		
MAOP in NMOCC Order is 2644 psig																		



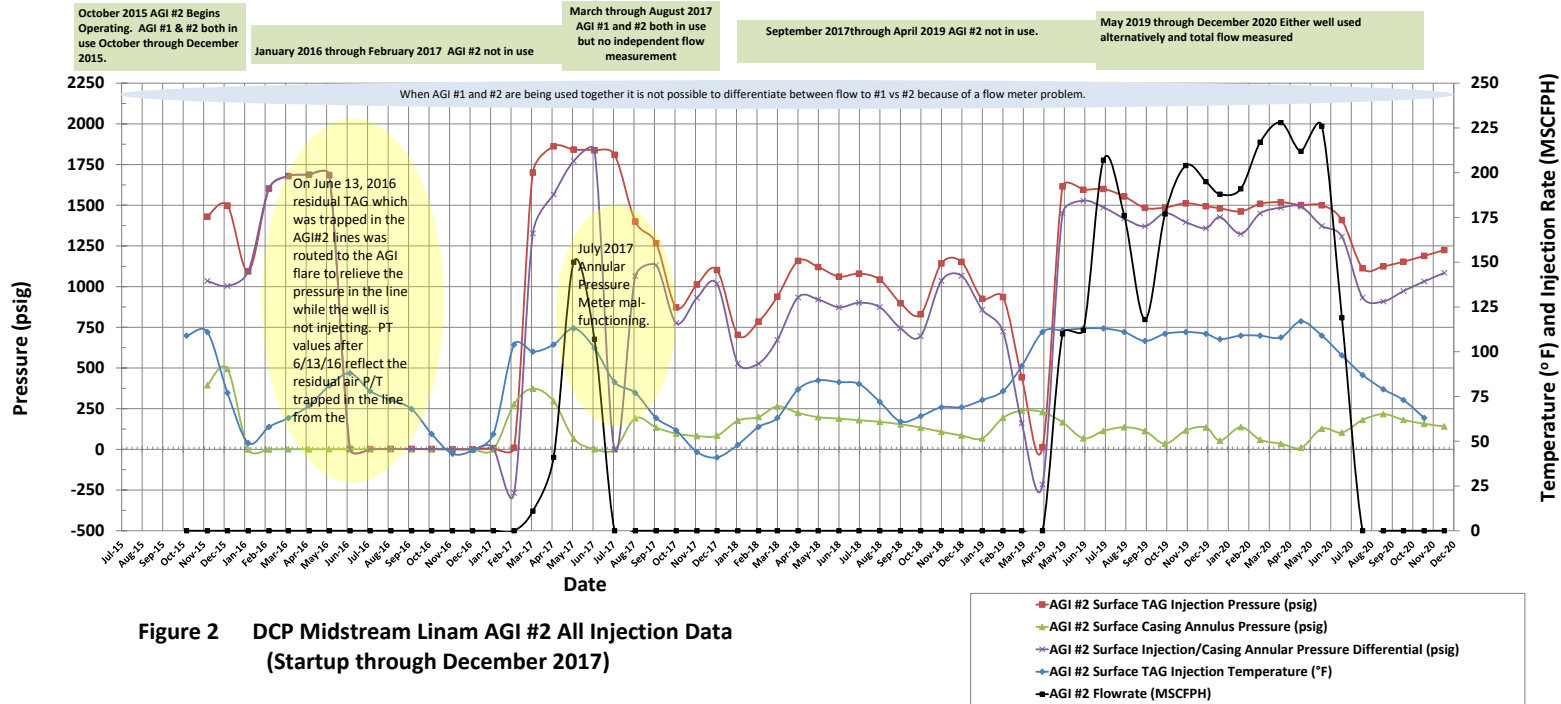
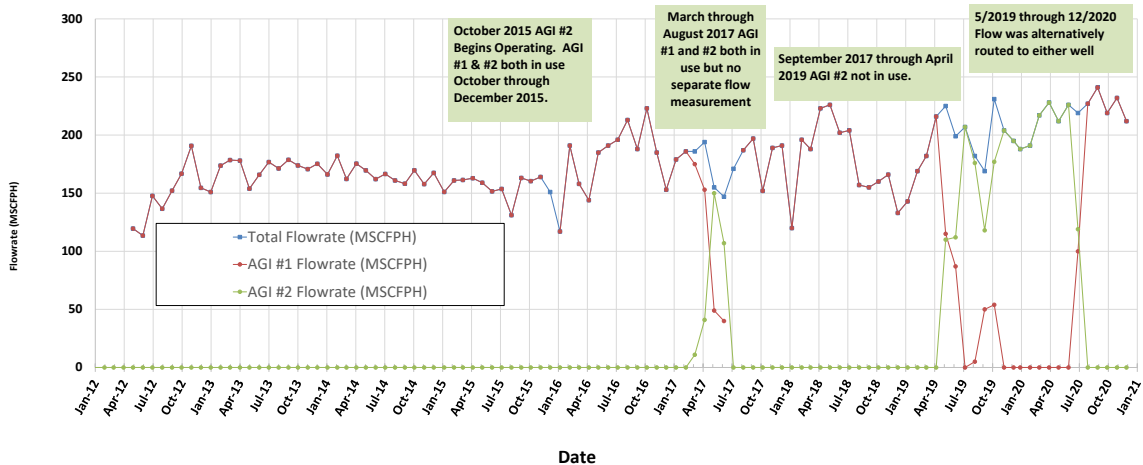


Figure 3 DCP Midstream Linam AGI #1 and #2 Combined Total Flowrate (MSCFPH) (May 2012 through December 2020)





**FIGURE 4 BOTTOM HOLE PRESSURE AND TEMPERATURE - AGI #1**

When AGI #2 is used in conjunction with AGI#1 or alternating between the wells, the effect is noticed on #1 Bottom Hole values for 2019 and 2020

