NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 6-20-87

Company: Amoco Production Company	Connection:		
Pool: Bravo Dome	Formation: Tubb		Unit: BDCDGU
Completion Date: 12-1-80	Total Depth: 2625	Plug Back TD: 2578	Elevation: 4786
Csg. Size: 5.50 / Wt.: 14 / d: 4.9 / Set At: 2625	Perforations: From 2172 To 2372		Farm or Lease Name:
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441 / Set At: 2134	Perforations: From To		Well No.: 1934-011F
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2134		Unit: F / Sec.: 1 / Twp.: 19 / Rge.: 34
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25
County: Union	State: New Mexico		
L:	H:	Gg:	% CO_2: 100 / % N_2: 0 / % H_2S: 0 / Prover: / Meter Run: 4.0 / Taps: Flange

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI											
1.	4.026	x	2.50	199	20	59	295		0		24 hrs
2.	4.026	x	2.50	207	17	59	199	59	0		24 hrs
3.	4.026	x	2.50	221	11	61	207	59	0		24 hrs
4.	4.026	x	2.50	234	8	60	220	61	0		24 hrs
5.							234	60	0		24 hrs

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1838
3.							1697
4.							1459
5.							1250

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

P_c 307.25 P_c^2 94,402

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		211.25	44,626	49,775
2		219.25	48,070	46,332
3		232.25	53,940	40,462
4		246.25	60,639	33,763
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.8966$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.8911$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3475$

Absolute Open Flow 3475 Mcfd @ 15.025 Angle of Slope θ 44.87 Slope, n 0.9955

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	