NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 4-23-85

Company: Amoco Production Company	Connection:		
Pool: Bravo Dome Carbon Dioxide Unit - 640 acre area	Formation: Tubb		Unit: BDCDGU
Completion Date: 12-13-82	Total Depth: 2666	Plug Back TD: 2640	Elevation: 4960
Farm or Lease Name:			
Csg. Size: 5 / Wt.: 13 / d: / Set At: 2666	Perforations: From 2360 To 2580		Well No.: 1934 051J
Tbg. Size: 3.5 / Wt.: 9.3 / d: / Set At: 2307	Perforations: From To		Unit: J / Sec.: 05 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2307		County: UNION
Producing Thru: Tubing	Reservoir Temp. °F: 90° @ 2470	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.2
			State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2470	2470	1.529	100	0	0		4.0	Flange

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					307				
1.	4.026 x 2.00	202	47	56	214.2	50			24 hr.
2.	4.026 x 2.00	231	29	61	243.2	50			24 hr.
3.	4.026 x 2.00	243	24	60	255.2	50			24 hr.
4.	4.026 x 2.00	267	12	62	279.2	50			24 hr.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1665
3.							1393
4.							1299
5.							974

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. P.S.I.A.
Critical Temperature 547 R R

P_c 319.2 P_c^2 101.889

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		214.2		56.007
2		243.2		42.742
3		255.2		36.762
4		279.2		23.936
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.82$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.46$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2427$

Absolute Open Flow 2427 Mcfd @ 15.025 Angle of Slope θ Slope, n .63

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		D. D. Kimble	