

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 6-20-87									
Company Amoco Production Company		Connection									
Pool Bravo Dome		Formation Tubb									
Completion Date 12-30-80		Total Depth 2530'	Plug Back TD 2390'								
Elevation 4720'		Farm or Lease Name									
Csg. Size 5.50	Wt. 14#	d 4.90	Set At 2530'								
Perforations: From 2142'	To 2354'										
Well No. 1934-111G											
Perforations: From	To										
Unit G	Sec. 11	Twp. 19	Rge. 34								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 2096'	County Union								
Producing Thru Tubing	Reservoir Temp. °F 90	Mean Annual Temp. °F 50	Baro. Press. - P _g 12.25								
State New Mexico											
L	H	G _g	% CO ₂ 100								
			% N ₂ 0								
			% H ₂ S. 0								
Prover		Meter Run 4.0	Taps								
FLOW DATA		FLANGE									
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	TUBING DATA Press. p.s.i.g.	Temp. °F	CASING DATA Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	4.026 x 2.50		195	24	59	290	196	59	0		24 hrs
2.	4.026 x 2.50		201	22	59	202	59	0			24 hrs
3.	4.026 x 2.50		212	17	60	212	60	0			24 hrs
4.	4.026 x 2.50		225	12	60	225	60	0			24 hrs
5.											24 hrs
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1.							2050				
2.							1905				
3.							1726				
4.							1542				
5.											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas 1.529						
3.					Specific Gravity Flowing Fluid X X X X X						
4.					Critical Pressure 1072 P.S.I.A.						
5.					Critical Temperature 496 R						
P _c 302.25 P _w 91.355											
NO.	P _t	P _w	P _w ²	P _t ² - P _w ²							
1.		208.25	43,368	47,987	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9037$						
2.		214.25	45,903	45,452	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.9037$						
3.		224.25	50,288	41,067							
4.		237.25	56,287	35,067	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3902$						
5.											
Absolute Open Flow 3902					Mcf/d @ 15.025		Angle of Slope @ 45				
					Slope, n 1.0						
Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.											
Approved by Commission:		Conducted By: RANDY MAHANNAH		Calculated By: RICHARD ROETH		Checked By:					