NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 6-20-87

Company: Amoco Production Company	Connection:			
Pool: Bravo Dome	Formation: Tubb			Unit: BDCDGU
Completion Date: 12-30-80	Total Depth: 2558'	Plug Back TD: 2490'	Elevation: 4780'	Farm or Lease Name:
Csg. Size: 5.50 / Wt.: 14# / d: 4.9 / Set At: 2558	Perforations: From 2173' To 2421'			Well No.: 1934-101J
Tbg. Size: 2.875 / Wt.: 6.5# / d: 2.441 / Set At: 2131'	Perforations: From To			Unit: J / Sec.: 10 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2125'			County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90 #	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
			100	0	0		4.0	Flange

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					306				
1.	4.026 x 2.50	192	26	58	192	58	0		24 hrs
2.	4.026 x 2.50	200	22	59	201	59	0		24 hrs
3.	4.026 x 2.50	211	17	60	211	60	0		24 hrs
4.	4.026 x 2.50	224	14	60	224	60	0		24 hrs
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							2041
3.							1895
4.							1750
5.							1610

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

P_c 318.25 P_c^2 101,283

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		204.25	41,718	59,565
2		213.25	45,475	55,807
3		223.25	49,840	51,442
4		236.25	55,841	45,496
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.7004$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.6997$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3469$

Absolute Open Flow 3469 Mcfd @ 15.025 — Angle of Slope θ 44.9771 — Slope, n 0.9992

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	