

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 7-4-87	
Company Amoco Production Company			Connection		
Pool Bravo Dome			Formation Tubb		Unit BDCDGU
Completion Date 2-25-81		Total Depth 2590	Plug Back TD 2410	Elevation 4717	
Farm or Lease Name		Well No. 2034-231K		Unit Sec. Twp. Rge. K 23 20 34	
Coq. Size 5.5	Wt. 14	d 4.9	Set At 2590	Perforations: From 2151 To 2358	
Top. Size 2.875	Wt. 6.5	d 2.441	Set At 2092	Perforations: From To	
Type Well - Single - Brdenhead - G.C. or G.O. Multiple Single				Packer Set At 2092	County Union
Producing Thru Tubing		Reservoir Temp. °F 90	Mean Annual Temp. °F 50	Baro. Press. - P _a 12.25	State New Mexico
L	H	Cg	% CO ₂ 100	% N ₂ 0	% H ₂ S. 0
				Prover	Meter Run 4.0
				Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							299		0		24 hrs
1.	4.026 x		2.50	196	24	59	198	59	0		24 hrs
2.	4.026 x		2.50	211	18	59	213	59	0		24 hrs
3.	4.026 x		2.50	225	13	61	227	61	0		24 hrs
4.	4.026 x		2.50	239	8	60	242	60	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow O. Mcd
1.							1953
2.							1787
3.							1603
4.							1296
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	0	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons		Deg.
2.					Specific Gravity Separator Gas	1.529	XXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXX	
4.					Critical Pressure	1072	P.S.I.A.
5.					Critical Temperature	496	P.S.I.A.

P _c 311.25		P _c ² 96,876		
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	210.25	44,205	52,671	
2	225.25	50,738	46,139	
3	239.25	57,240	39,636	
4	254.25	64,643	32,234	
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.8393$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5269$

AOF = O $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2982$

Absolute Open Flow	2982	Mcd @ 15.025	Angle of Slope @	34.7833	Slope, n	0.6946
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Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted by: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By:
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