MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 7-4-87	
Company: Amoco Production Company		Connection:		
Pool: Bravo Dome		Formation: Tubb		Unit: BDCDGU
Completion Date: 1-12-81	Total Depth: 2763	Plug Back TD: 2699	Elevation: 4787	Farm or Lease Name:
Csg. Size: 5.50 / Wt.: 14 / d: 4.9 / Set At: 2763		Perforations: From 2263 To 2422		Well No.: 2034-251F
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441 / Set At: 2216		Perforations: From To		Unit: F / Sec.: 25 / Twp.: 20 / Rge.: 34
Type Well – Single – Bradenhead – G.C. or G.O. Multiple: Single		Packer Set At: 2216		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
			100	0	0		4.0	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						290		0		24 hrs
1.	4.026	x 2.125	197	23	60	196	60	0		24 hrs
2.	4.026	x 2.125	212	16	61	211	61	0		24 hrs
3.	4.026	x 2.125	224	11	62	223	62	0		24 hrs
4.	4.026	x 2.125	240	5	61	238	61	0		24 hrs
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1335
2.							1182
3.							1029
4.							757
5.							

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 302.25 P_c^2 91,355

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		208.25	43,368	47,987
2		223.25	49,840	41,514
3		235.25	55,342	36,012
4		250.25	62,625	28,730
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9037$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.7930$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2394$

Absolute Open Flow: 2394 Mcfd @ 15.025 Angle of Slope θ: 42.2049 Slope, n: 0.9069

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	