MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 7-4-87	
Company: Amoco Production Company		Connection		
Pool: Bravo Dome		Formation: Tubb		Unit: BDCDGU
Completion Date: 2-8-81	Total Depth: 2760	Plug Back TD: 2497	Elevation: 4778	Farm or Lease Name
Csg. Size: 5.50 / Wt.: 14 / d: 4.9 / Set At: 2760		Perforations: From 2220 To 2421		Well No.: 2034-261G
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441 / Set At: 2158		Perforations: From To		Unit: G / Sec.: 26 / Twp.: 20 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 2158		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico
L	H	Gg	% CO_2: 100	% N_2: 0
% H_2S: 0	Prover	Meter Run: 4.0	Taps: Flange	

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							286		0		24 hrs
1.	4.026	X	1.50	192	59	60	194	60	0		24 hrs
2.	4.026	X	1.50	206	43	60	208	60	0		24 hrs
3.	4.026	X	1.50	219	29	62	221	62	0		24 hrs
4.	4.026	X	1.50	239	13	61	241	61	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							997
3.							895
4.							789
5.							547

NO.	P_t	Temp. °R	T_f	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 298.25 P_c^2 88,953

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		206.25	42,539	46,414
2		220.25	48,510	40,443
3		233.25	54,405	34,547
4		253.25	64,135	24,817
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9165$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.6744$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1669$

Absolute Open Flow: 1669 Mcfd @ 15.025 | Angle of Slope θ: 38.3938 | Slope, n: 0.7924

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	