NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-21-87	
Company: Amoco Production Company			Connection:		
Pool: Bravo Dome			Formation: Tubb		Unit: BDCDGU
Completion Date: 2-26-81	Total Depth: 2597'		Plug Back TD: 2554'	Elevation: 4696'	Farm or Lease Name:
Csg. Size: 5.50 / Wt.: 14 / d: 4.9 / Set At: 2597			Perforations: From 2150' To 2331'		Well No.: 1934-131B
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441 / Set At: 2087			Perforations: From To		Unit: B / Sec.: 13 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2087'		County: UNION
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico
L:	H:	Gg:	% CO_2: 100	% N_2: 0	% H_2S: 0
Prover:	Meter Run: 4.0	Taps: Flange			

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI											
1.	4.026	x	2.250	193	29	58	294		0		24 hrs
2.	4.026	x	2.250	203	25	58	192	58	0		24 hrs
3.	4.026	x	2.250	212	20	58	202	58	0		24 hrs
4.	4.026	x	2.250	225	14	59	212	58	0		24 hrs
5.							224	59	0		24 hrs

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1725
3.							1590
4.							1491
5.							1349

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. P.S.I.A.
Critical Temperature 496 R R

P_c 306.25 P_c^2 93,789

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		204.25	41,178	52,071
2		214.25	45,903	47,886
3		224.25	50,288	43,501
4		236.25	55,814	37,975
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.8011$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.677$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2910$

Absolute Open Flow 2910 Mcfd @ 15.025 | Angle of Slope θ 41.32 | Slope, n .8793

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	