

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special										Test Date: 6-26-87	
Company: Amoco Production Company					Connection:						
Pool: Bravo Dome					Formation: Tubb					Unit: BDCDGU	
Completion Date: 6-17-81			Total Depth: 2525		Plug Back TD: 2366		Elevation: 4566		Farm or Lease Name:		
Csg. Size: 5.50		Wt.: 14		ID: 4.9		Set At: 2525		Perforations: From 2063 To 2194		Well No.: 1935-151G	
Tbg. Size: 2.875		Wt.: 6.5		ID: 2.441		Set At: 2042		Perforations: From To		Unit Sec. Twp. Rge. G 15 19 35	
Type Well - Single - Broadhead - G.G. or G.O. Multiple										Packer Set At: 2011	
Producing Thru Tubing			Reservoir Temp. °F: 90		Mean Annual Temp. °F: 50		Baro. Press. - P _g : 12.25		State: New Mexico		
L:		H:		Gg:		% CO ₂ : 100		% N ₂ : 0		% H ₂ S: 0	
								Prover:		Meter Run: 4.0	
										Taps: Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							288		0		24 hrs
1.	4.026 x	2.50	208	18	60	206	60	0			24 hrs
2.	4.026 x	2.50	218	14	61	217	61	0			24 hrs
3.	4.026 x	2.50	226	11	61	225	61	0			24 hrs
4.	4.026 x	2.50	289	7	62	238	62	0			24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcd
1.							1804
2.							1613
3.							1450
4.							1253
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas	1.529
3.					Specific Gravity Flowing Fluid	X X X X X
4.					Critical Pressure	1072 P.S.I.A.
5.					Critical Temperature	496 R

P _c 300.25 P _c ² 90.150				
NO.	F _t ²	P _w	P _w ²	P _c ² - P _w ²
1.		218.25	47,633	51,749
2.		230.25	53,015	46,367
3.		238.25	56,763	42,619
4.		251.25	63,126	36,256
5.				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.1434$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.1434$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3457$$

Absolute Open Flow: 3457 Mcfd @ 15.025	Angle of Slope @: 45.0	Slope, n: 1.000
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Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By: RANDY MAHANNAH	Calculated By: RICHARD ROETH	Checked By:
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