NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
AUG 9 1984
OIL CONSERVATION DIVISION
BDCDGU

Type Test: [x] Initial [ ] Annual [ ] Special				Test Date: 5/29/84	
Company: Amoco Production Company		Connection:			
Pool: Bravo Dome		Formation: Tubb			
Completion Date: 7/13/81	Total Depth: 2660'	Plug Back TD: 2596'	Elevation: 4640	Farm or Lease Name:	
Csg. Size: 5-1/2 / Wt.: 14# / d: / Set At: 2652'		Perforations: From 2156 To 2277		Well No.: 2035 281F	
Tbg. Size: 2-7/8 / Wt.: 6.5# / d: 2.438 / Set At: 2148'		Perforations: From To		Unit: F / Sec.: 28 / Twp.: 20N / Rge.: 35E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 2109'		County: Union	
Producing Thru: Tubing	Reservoir Temp. °F: 90 @ 2217'	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico	

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2217	2217	1.529	100	0	0		4.0	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size x Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					333.2	50			1000 HR
1.	4.026 x 2.375	278	9	59	273	50			1.5
2.	4.026 x 2.375	256	18	59	253	50			1.5
3.	4.026 x 2.375	216	36	58	213	50			1.5
4.	4.026 x 2.375	183	52	56	180	50			1.5
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1302
2							1721
3							2240
4							2549
5							

NO.	P_r	Temp. °R	T_r	Z
1				
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX ____
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

P_c 345.5 P_c^2 ____

NO	P_t	P_w	P_w^2	$P_c^2 - P_w^2$
1		285.3		38.0
2		265.3		49.0
3		225.3		68.6
4		192.3		82.4
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.449$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.339$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3412$

Absolute Open Flow 3412 Mcfd @ 15.025 | Angle of Slope θ ____ | Slope, n .787

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		Don White	