

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

RECEIVED

Type Test: ☒ Initial ☐ Annual ☐ Special					Test Date: 5/24/84		AUG 9 1984 OIL CONSERVATION DIVISION BDCDGU	
Company: Amoco Production Company				Connection:				
Pool: Bravo Dome				Formation: Tubb			Unit: BDCDGU	
Completion Date: 7/5/81		Total Depth: 2465		Plug Back TD: 2353		Elevation: 4615		Farm or Lease Name:
Csq. Size: 5-1/2	Wt.: 14#	d:	Set At:	Perforations: From 2060 To 2124			Well No.: 1935 191G	
Tqg. Size: 2-7/8	Wt.: 6.5#	d: 2.438	Set At: 2079	Perforations: From To			Unit: G Soc: 19 Twp: 19N Rge: 35E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single					Packer Set At: 2040		County: Union	
Producing Thru: Tubing		Reservoir Temp. °F: 90 @ 2092		Mean Annual Temp. °F: 50		Baro. Press. - P _a : 12.25		State: New Mexico
L: 2092	H: 2092	G _g : 1.529	% CO ₂ : 100	% N ₂ : 0	% H ₂ S: 0	Prover:	Meter Run: 4.0	Taps: Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							332.5	50			1000 HR
1.	4.026 x 2.375			260	4	58	262	50			1.5
2.	4.026 x 2.375			234	16	57	236	50			1.5
3.	4.026 x 2.375			205	33	60	207	50			1.5
4.	4.026 x 2.375			179	48	60	181	50			1.5
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1							782
2							1576
3							2074
4							2355
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas: 1.529 X X X X X X X X
3.					Specific Gravity Flowing Fluid: X X X X X
4.					Critical Pressure: 1072 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature: 496 R _____ R

P _r : 344.8	P _w : _____	P _w ² : _____	P _c ² - P _w ² : _____	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.252$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.252$
NO.	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3251$	
1	274.3		43.6		
2	248.3		57.2		
3	219.3		70.8		
4	193.3		81.5		
5					

Absolute Open Flow: 3251 Mcfd @ 15.025	Angle of Slope θ: 45	Slope, n: 1.0
Remarks: _____		

Approved By:	Conducted By: _____	Calculated By: Don White	Checked By: _____
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