

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special		Test Date: 4-9-85									
Company: Amoco Production Company		Connection:									
Pool: Bravo Dome Carbon Dioxide		Formation:									
Unit: 640 acre area		Tubb									
Completion Date: 11-17-83	Total Depth: 2672	Plug Back TD: 2520	Elevation: 4822								
Csg. Size: 7	Wt.: 20	Set At: 2672	Perforations: From 2320 To 2450								
Tub. Size: 3.5	Wt.: 9.3	Set At: 2314	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple		Packer Set At: 2283	Well No.: 2034 0316								
Producing Thru: Tubing	Reservoir Temp. °F: 90.0	Mean Annual Temp. °F: 50	Baro. Press. - P _a : 12.2								
L: 2385	H: 2385	G _g : 1.529	% CO ₂ : 100 % N ₂ : 0 % H ₂ S: 0								
Prover: 2385		Meter Run: 4.0	Taps: Flange								
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							307				
1.	4.026 x 1.875			218	50	60	230.2	50			24 hr.
2.	4.026 x 1.875			238	31	61	250.2	50			24 hr.
3.	4.026 x 1.875			263	15	60	265.2	50			24 hr.
4.	4.026 x 1.875			284	7	60	296.2	50			24 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1							1500				
2							1258				
3							1100				
4							626				
5											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.						
1					A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.						
2					Specific Gravity Separator Gas: 1.529 X X X X X X X X						
3					Specific Gravity Flowing Fluid: X X X X X						
4					Critical Pressure: 1072 P.S.I.A. P.S.I.A.						
5					Critical Temperature: 547 R R						
P _c 319.2 P _c ² 101.889											
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$					
1	230.2			48.897	$\frac{P_c^2}{P_c^2 - P_w^2} = 2.08$	$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.67$					
2	250.2			39.289							
3	265.2			31.558							
4	296.2			14.154							
5											
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$					2508						
Absolute Open Flow					2508 Mcfd @ 15.025						
Angle of Slope θ					Slope, n .70						
Remarks:											
Approved By Commission: Conducted By: Calculated By: D. D. Kimble Checked By:											

2034 0316

