OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 6-26-87

Company: Amoco Production Company	Connection:		
Pool: Bravo Dome	Formation: Tubb		Unit: BDCDGU
Completion Date: 11-28-83	Total Depth: 2627'	Plug Back TD: 2505'	Elevation: 4470'
Farm or Lease Name:			
Csg. Size: 7.0 / Wt.: 20 / d: 6.331 / Set At: 2627	Perforations: From 2073 To 2136		Well No.: 1935-251G
Tbg. Size: 3.5 / Wt.: 9.5 / d: 3.00 / Set At: 2014	Perforations: From To		Unit: G / Sec.: 25 / Twp.: 19 / Rge.: 35
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2014		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25
State: New Mexico			

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
			100	0	0		4.0	Flange

NO.	FLOW DATA: Prover Line Size x Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					291		0		24 hrs
1.	4.026 x 1.50	225	26	61	226	61	0		24 hrs
2.	4.026 x 1.50	235	18	62	236	62	0		24 hrs
3.	4.026 x 1.50	241	13	63	241	63	0		24 hrs
4.	4.026 x 1.50	264	1	61	265	61	0		24 hrs
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							743
3.							645
4.							523
5.							236

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

P_c 303.25 P_c^2 91,960

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		238.25	56,763	35,197
2		248.25	61,628	30,332
3		253.25	64,135	27,825
4		277.25	76,867	15,093
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.6127$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.605$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1936$

Absolute Open Flow 1936 Mcfd @ 15.025 Angle of Slope θ 44.91 Slope, n .9972

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	