NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date:

Company: Amoco Production Company — Connection:

Pool: Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area — Formation:

Unit: BDCDGU

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
11-6-85	2708	2655	4972	

Csg. Size	Wt.	d	Set At	Perforations	Well No.
7	20		2708	From 2402 To 2604	2134 311G
Tbg. Size	Wt.	d	Set At	Perforations	Unit / Sec. / Twp. / Rge.
3-1/2	9.3		2596	From To	G / 31 / 21 / 34

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
Singe	2380	Union

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
Tubing	90 @ 2503	50	12.25	New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2503	2503	1.529	100	0	0		4.0	Flange

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							297				
1.	4.026	x	3.000	183.5	18	48	195.75	48			1.5
2.	4.026	x	3.000	155.7	26.5	49	167.95	49			1.5
3.	4.026	x	3.000	129.3	38.5	47	141.55	47			1.5
4.	4.026	x	3.000	103.4	56	46	115.65	46			1.5
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							2557
3.							2847
4.							3101
5.							3310

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.

A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.

Specific Gravity Separator Gas 1.529 XXXXXXXXX

Specific Gravity Flowing Fluid XXXXX

Critical Pressure 1072 P.S.I.A. _____ P.S.I.A.

Critical Temperature 496 R _____ R

P_c 309.2 P_c^2 95.605

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		196		57.189
2		168		67.381
3		142		75.441
4		116		82.149
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.16$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.11$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3686$

Absolute Open Flow 3686 Mcfd @ 15.025 — Angle of Slope θ _____ — Slope, n .71

Remarks:

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
		Don Kimble	