

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date	
Company Amoco Production Company				Connection			
Pool Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area				Formation		Unit BDCDGU	
Completion Date 1-10-86		Total Depth 2533		Plug Back TD 2570~		Elevation 4771	
Csg. Size 7	Wt. 20	d	Set At 2530	Perforations: From 2302 To 2408		Well No. 2034 021K	
Tbg. Size 3-1/2	Wt. 9.3	d	Set At 2413	Perforations: From To		Unit Sec. Twp. Rge. K 2 20 34	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2284		County Union	
Producing Thru Tubing		Reservoir Temp. °F 90 @ 2355		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.25	
L 2355		H 2355	G _g 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover Meter Run 4.0
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
Si							299			
1.	4.026 x 3.000			185.5	20.5	43	197.75	43		
2.	4.026 x 3.000			157.4	28	45	169.65	45		
3.	4.026 x 3.000			130.7	38	43	142.95	43		
4.	4.026 x 3.000			101.9	54	43	114.15	43		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.							2400
2.							2641
3.							2900
4.							3246
5.							

NO.	P _t	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					0	
2.						
3.						
4.						
5.						

A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas 1.529 Specific Gravity Flowing Fluid X X X X X Critical Pressure 1072 P.S.I.A. Critical Temperature 496 R			
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P _c 311.2 P _c ² 96.845	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.16$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.123$																														
<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>NO.</th> <th>P_t²</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> </thead> <tbody> <tr> <td>1.</td> <td></td> <td>198</td> <td></td> <td>57.641</td> </tr> <tr> <td>2.</td> <td></td> <td>170</td> <td></td> <td>67.945</td> </tr> <tr> <td>3.</td> <td></td> <td>143</td> <td></td> <td>76.396</td> </tr> <tr> <td>4.</td> <td></td> <td>114</td> <td></td> <td>83.849</td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table>	NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	1.		198		57.641	2.		170		67.945	3.		143		76.396	4.		114		83.849	5.					AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3645$	
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5.																																

Absolute Open Flow 3645 Mcfd @ 15.025	Angle of Slope θ	Slope, n .81
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Remarks:			

Approved By Commission:	Conducted By:	Calculated By: Dor Kimble	Checked By:
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