

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date				
Company Amoco Production Company				Connection					
Pool Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area				Formation				Unit BDCDGU	
Completion Date 1-10-86		Total Depth 2380		Plug Back TD 2350		Elevation 4620		Farm or Lease Name	
Csg. Size 7	Wt. 20	d	Set At 2380	Perforations: From 2099 To 2282		Well No. 1935 091 K			
Thq. Size 3-1/2	Wt. 9.3	d	Set At 1935	Perforations: From To		Unit Sec. Twp. Rge. K 9 19 35			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 1905		County Union		
Producing Thru Tubing		Reservoir Temp. °F 90 • 2191		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.25		State New Mexico	
L 2191	H 2191	G _g 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover	Meter Run 4.0	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							305			
1.	4.026 x	3.000		188.5	18.5	45	200.75	45		
2.	4.026 x	3.000		158.7	24.5	46	170.95	46		
3.	4.026 x	3.000		132.2	34	46	144.45	46		
4.	4.026 x	3.000		101.7	46	43	113.95	43		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							2310
2							2540
3							2720
4							2992
5							

NO.	P _t	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.			
					A.P.I. Gravity of Liquid Hydrocarbons Deq.			
					Specific Gravity Separator Gas 1.529 X X X X X X X X			
					Specific Gravity Flowing Fluid X X X X X			
					Critical Pressure 1072 P.S.I.A. P.S.I.A.			
					Critical Temperature 496 R R			

P _c 317.2	P _c ² 100,616	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.15$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	
1		201		60.215	
2		171		71.375	
3		144		79.880	
4		114		87.620	
5					

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3296$

Absolute Open Flow 3296 Mcfd @ 15.025

Angle of Slope θ

Slope, n .70

Remarks:

Approved by Commission:	Conducted By:	Calculated By: Don Kimble	Checked By:
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