

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

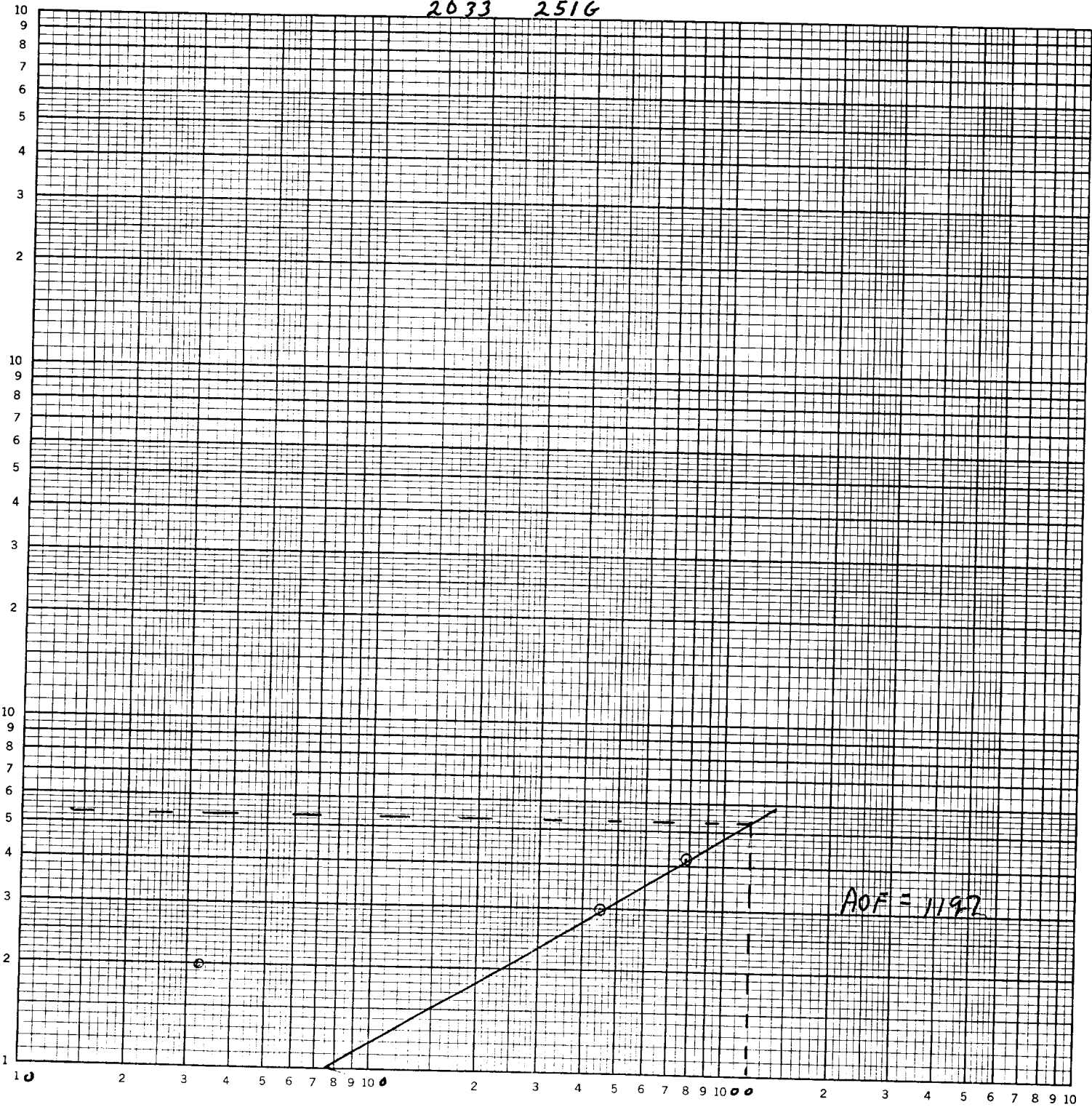
Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 8-20-85									
Company Amoco Production Company		Connection									
Pool Bravo Dome Carbon Dioxide Gas Unit 640 Acre Area		Formation Tubb									
Completion Date 5-9-81		Total Depth 2638	Plug Back TD 2530								
		Elevation 4918									
Csg. Size 5.5	Wt. 14	Set At 2638	Perforations: From 2349 To 2443								
Thq. Size 2-7/8	Wt. 6.5	Set At 2201	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 2152	Well No. 2033 251 G								
Producing Thru Tubing		Reservoir Temp. °F 90 # 2396	Mean Annual Temp. °F 50								
		Baro. Press. - P _a 12.2	Unit Sec. Twp. Rge. G 25 20 33								
L 2396	H 2396	G _g 1.529	% CO ₂ 100								
		% N ₂ 0	% H ₂ S 0								
Prover		Meter Run 4.0	Taps Flange								
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	4.026 x 1.500			192	47	62	278	192	50		24 hr.
2.	"	"	"	219	9	62	219	"	"		"
3.	"	"	"	241	5	60	241	"	"		"
4.	"	"	"	248	1	60	248	"	"		"
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1.							794				
2.							450				
3.							32				
4.							0				
5.											
NO.	R _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ 0			Mcf/bbl.			
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ 0			Deq.			
2.					Specific Gravity Separator Gas _____ 1.529			XXXXXXX			
3.					Specific Gravity Flowing Fluid _____ XXXXX						
4.					Critical Pressure _____ 1072 P.S.I.A.			P.S.I.A.			
5.					Critical Temperature _____ 547 R			R			
P _c 290.2		P _c 84.216									
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.98$						
1.		204.2		42.518	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.51$						
2.		231.2		30.762							
3.		253.2		20.106							
4.		260.2		16.812	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1197$						
5.											
Absolute Open Flow _____ 1197					Mcf/d @ 15.025		Angle of Slope θ _____	Slope, n _____ .60			
Remarks:											
Approved By Commission:		Conducted By:		Calculated By:		Checked By:					
				D. D. Kimble							

2033 2516

46 7400

LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.



$$Q = MCFD$$