

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test:		☒ Initial ☐ Annual ☐ Special		Test Date			
Company				Connection			
Amoco Production Company							
Pool Carbon Dioxide Gas Unit				Formation		Unit	
Bravo Dome 640 acre area				Tubb		BDCDGU	
Completion Date		Total Depth		Plug Back TD		Elevation	
11-9-83		2668		2660		4933	
Csg. Size	Wt.	d	Set At	Perforations:		Well No.	
7"	20		2668	From 2355 To 2534		2033 241G	
Tbg. Size	Wt.	d	Set At	Perforations:		Unit Sec. Twp. Rge.	
3.5	9.3		2343	From To		G 24 20 33	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At		County	
Single				2312		Harding	
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a	
Tubing		90° @ 2445		50		12.2	
L		H		Gg		Prover	
2445		2445		1.529		4.0	
				% CO ₂ 100		% N ₂ 0	
				% H ₂ S 0		Meter Run	
						Taps	
						Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							310				
1.	4.026 x 1.875			240	23	63	252.2	50			24 hr.
2.	4.026 x 1.875			240	22	61	252.2	50			24 hr.
3.	4.026 x 1.875			267	11	60	279.2	50			24 hr.
4.	4.026 x 1.875			301	3	57	313.2	50			24 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1							1037
2							1037
3							765
4							397
5							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio		A.P.I. Gravity of Liquid Hydrocarbons		Specific Gravity Separator Gas		Specific Gravity Flowing Fluid		Critical Pressure		Critical Temperature	
1.					0		0		1.529		X X X X X X X X		1072		547	
2.											X X X X X					
3.																
4.																
5.																

P _c 322.2		P _c ² 103.813	
NO.	P _t ²	P _w	P _w ²
1		252.2	
2		252.2	
3		279.2	
4		315.2	
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.58$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.59$	
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1650$			

Absolute Open Flow 1650		Mcfd @ 15.025		Angle of Slope θ		Slope, n .49	
Remarks:							

Approved By Commission:		Conducted By:		Calculated By:		Checked By:	
				D. D. Kimble			