NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 5-10-85	
Company: Amoco Production Company		Connection:			
Pool: Bravo Dome Carbon Dioxide Gas Unit 640-acre area		Formation: Tubb			Unit: BDCDGU
Completion Date: 11-9-83	Total Depth: 2845'	Plug Back TD: 2790'	Elevation: 4924 GL		Farm or Lease Name:
Csg. Size: 7" / Wt.: 20# / d: / Set At: 2845'		Perforations: From 2523' To 2568'			Well No.: 1933 211G
Tbg. Size: 3-1/2" / Wt.: 9.3# / d: / Set At: 2505'		Perforations: From To			Unit: G / Sec.: 21 / Twp.: 19 / Rge.: 33
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 2473'			County: Harding
Producing Thru: Tubing	Reservoir Temp. °F: 90° @ 2546'	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.2		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2546'	2546'	1.529	100	0	0		4.0"	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					298				
1.	4.026 x 1.75	212	32	62	224.2	50			24 hrs
2.	4.026 x 1.75	234	20	60	246.2	50			24 hrs
3.	4.026 x 1.75	255	12	59	267.2	50			24 hrs
4.	4.026 x 1.75	277	6	60	289.2	50			24 hrs
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1050
2							877
3							715
4							
5							

NO.	P_t	Temp. °R	T_r	Z
1				
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. P.S.I.A.
Critical Temperature 547 R R

P_c 310.2 P_c^2 96.224

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		224.2		45.958
2		246.2		35.610
3		267.2		24.828
4		289.2		12.587
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.09$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.25$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1311$

Absolute Open Flow 1311 Mcfd @ 15.025 Angle of Slope θ Slope, n .30

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		D. D. Kimble	